

# **TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL**

Volume I of II

***Prepared for:***

Basic Remediation Company  
875 W. Warm Springs Road  
Henderson, NV 89015

***Prepared by:***



2270 Corporate Circle, Suite 100  
Henderson, Nevada 89074-6382  
Phone: (702)-263-7275

October 6, 2006  
PBS&J Reference No.: 511693.19



Date Submitted \_\_\_\_\_  
PIN # \_\_\_\_\_



CLARK COUNTY DEPARTMENT OF DEVELOPMENT SERVICES  
CIVIL ENGINEERING DIVISION

HTE # \_\_\_\_\_

**DRAINAGE STUDY SUBMITTAL SHEET**

(Each Drainage Study must have a separate submittal sheet and separate check)

Is this project located within a Major Project? ☐ Yes ☒ No If yes, which Major Project is it? \_\_\_\_\_

**Assessor's Parcel Number (APN)**

1. 178-11-501-006 2. 178-12-201-002 3. 178-12-301-001

This project is within the city limits of: ☐ Henderson ☐ Las Vegas ☐ North Las Vegas ☒ Other Clark County

**Type of Submittal** ☒ Initial of 1st study review ☐ Over 2 study reviews

**Number of Acres**

☐ up to 5 acres ☐ up to 40 acres ☒ up to 320 acres ☐ up to 2,560 acres ☐ over 2,560 acres

**Project Name** Technical Drainage Study for Eastside Landfill

**Street Location**

East/West Eastgate Rd/ 4<sup>th</sup> Street North/South Warm Springs Rd/ Lake Mead Dr

**Land Use Applications**

1. Landfill 2. \_\_\_\_\_ 3. \_\_\_\_\_  
4. \_\_\_\_\_ 5. \_\_\_\_\_ 6. \_\_\_\_\_

**Engineering Firm** PBS&J **Responsible Engineer** Harshal Desai, P.E., CFM

**Address** 2270 Corporate Circle, Suite 100

**City/State/Zip** Henderson, NV 89074 **Phone Number** (702) 263-7275

**Owner/Developer** Basic Remediation Company

**Address** 875 West Warm Springs Rd

**City/State/Zip** Henderson, NV 89015 **Phone Number** (702) 567-0400



## HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## DRAINAGE STUDY INFORMATION FORM

Name of Development: Eastside Landfill Date: 6th Oct 06

Location of Development: a) Descriptive (Cross Streets) Eastgate Rd/ Warm Springs Rd  
b) Sect. 11/12 Twn. 22S Rng. 62E  
178-11-501-006, 178-11-201-002  
Name of Owner: Basic Remediation Company Assessors Parcel No: and 178-12-301-001

Telephone No: (702) 567-0473 Facsimile No: \_\_\_\_\_

Address: 875 West Warm Springs Rd  
Henderson, NV 89015

Contact Person Name: Harshal Desai, P.E., CFM Telephone No: (702) 263-7275

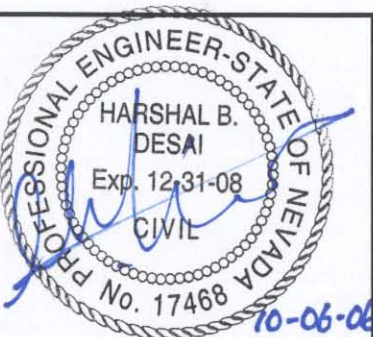
Firm: P B S & J

Address: 2270 Corporate Circle, Suite 100, Henderson, Nevada 89074

Type of Land Development/Land Disturbance Process:

<input type="checkbox"/>	Rezoning	<input type="checkbox"/>	Subdivision Map	<input type="checkbox"/>	Clearing and Grading Only
<input type="checkbox"/>	Parcel Map	<input type="checkbox"/>	Planned Unit Development	<input checked="" type="checkbox"/>	Other (Please specify below)
<input type="checkbox"/>	Large Parcel Map	<input type="checkbox"/>	Building Permit	<input type="checkbox"/>	CCRFCD Facility

1. Total Owned Land Area: At Site: 113 +/- acres Being Developed/Disturbed: 74 +/- acres
2. Is a portion or all of the subject property located in a designated FEMA Flood Hazard Area? YES ☐ NO ☒
3. Is the property bordered or crossed by an existing or proposed Clark County Regional Flood Control District Master Planned Facility? YES ☐ NO ☒
4. Proposed type of development (Residential, Commercial, Etc.)? Landfill
5. Approximate upstream land area which drains to the subject site? 80 +/-acres
6. Has the site drainage been evaluated in the past? ☒ YES\* NO ☐ If yes, please identify documentation:  
Henderson Commerce Center Two (Formerly known as Harsch)
7. If known, please briefly identify the proposed discharge point(s) of runoff from the site:  
Into existing 60" storm drain located on adjacent property and to the undeveloped land to the north
8. Briefly describe your proposed schedule for the subject project: ASAP



Engineer's Seal

Submit this form as part of the required drainage study to the local entity which has jurisdiction over the subject property. This form may provide sufficient information to serve as the Conceptual Drainage Study.

\* Review and concurrence of the Clark County Regional Flood Control District is required.

Local Entity File No. \_\_\_\_\_

Revision	Date

PBS&amp;J Job Number:

511693.19

STANDARD FORM 1



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## DRAINAGE SUBMITTAL CHECKLIST

Project Name:	Eastside Landfill	Map ID:	
Firm Name:	PBS&J	Engineer:	Harshal Desai, P.E., CFM
Address:	2270 Corporate Circle, Suite 100		
City:	Henderson	State:	NV Zip: 89074
Phone Number:	(702) 263-7275	Fax Number:	(702) 263-7200
Property Owner:	Basin Remediation Company		
Address:	875 Warm Springs Rd		
City:	Henderson	State:	NV Zip: 89015
Reviewed By:		Date Received:	
		Date Accepted for Review:	

The following checklist is intended as a guide for the engineer preparing a Technical Drainage Study to submit to the local entity and Clark County Regional Flood Control District (if necessary). The listed items are the minimum information required prior to the entity performing a review. The engineer will remain responsible to ensure the Technical Drainage Study is prepared within the guidelines as set forth in the Clark County Regional Flood Control District (CCRFCDD) Hydrologic Criteria and Drainage Design Manual (MANUAL).

This document is intended as an aid in preparing Technical Drainage Studies. Each study submitted is reviewed for compliance with local and regional criteria. This form is not intended to be all inclusive and does not limit the extent of the information, calculations or exhibits which may be necessary to properly evaluate the intended land use.

If items are not applicable for the subject site, provide N/A.

### I. GENERAL REQUIREMENT

Yes	No	
<u>X</u>	<u>      </u>	Design Manual <b>Standard Form 1</b> with the engineer's seal and signature.
<u>X</u>	<u>      </u>	Design Manual <b>Standard Form 4</b> .
<u>X</u>	<u>      </u>	2 copies of the 24" x 36" Drainage Plan.
<u>N/A</u>	<u>      </u>	A notarized letter from the adjacent property owner(s) allowing off-site grading or discharge.

REFERENCE:

STANDARD FORM 2



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## DRAINAGE SUBMITTAL CHECKLIST

### II. MAPS AND EXHIBITS

Yes	No	
<u>X</u>	<u>      </u>	A copy of a current Flood Insurance Rate Map (FIRM) with the site delineated.
<u>X</u>	<u>      </u>	A copy of the current CCRFCD Master Plan Update Figure, (F-22), for Flood Control Facilities and Environmental areas with the site delineated.
<u>X</u>	<u>      </u>	Off-site drainage basin maps for existing, interim and future conditions showing the existing topography, basin boundaries, concentration points, and flows in cfs.
<u>X</u>	<u>      </u>	On-site drainage basin maps for existing and proposed conditions showing the existing topography, basin boundaries, concentration points, and on-site and off-site flows in cfs.
<u>X</u>	<u>      </u>	Vicinity Map with local and major cross streets identified and a north arrow.

### III. DRAINAGE PLAN

Yes	No	
<u>X</u>	<u>      </u>	Sheet size: 24" x 36" sealed by a registered engineer in the State of Nevada.
<u>X</u>	<u>      </u>	Minimum scale: 1" = 60'.
<u>X</u>	<u>      </u>	Project name.
<u>X</u>	<u>      </u>	Vicinity Map with local and major cross streets.
<u>X</u>	<u>      </u>	Revision box.
<u>X</u>	<u>      </u>	North arrow and bar scale.
<u>X</u>	<u>      </u>	Engineer's/consultant's address and phone number.
<u>X</u>	<u>      </u>	Elevation datum and benchmark.
<u>X</u>	<u>      </u>	Legend for symbols and abbreviations.
<u>X</u>	<u>      </u>	Cut/fill scarps, where applicable.
<u>X</u>	<u>      </u>	Street names, grades, widths.
<u>X</u>	<u>      </u>	Proposed future and existing spot grades for top of curbs and street crowns at lot lines, grade breaks, and along curb returns on both sides of the street.

REFERENCE:

STANDARD FORM 2



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## DRAINAGE SUBMITTAL CHECKLIST

### III. DRAINAGE PLAN (Continued)

Yes	No	
<u>X</u>	<u>      </u>	Existing contours encompassing the site and 100 feet beyond with spot elevations for important locations, where appropriate.
<u>NA</u>	<u>      </u>	Minimum finish floor elevations with top-of-curb elevations at upstream end of lot.
<u>X</u>	<u>      </u>	Proposed typical street sections.
<u>NA</u>	<u>      </u>	Streets with off-set crowns.
<u>X</u>	<u>      </u>	Proposed contours or spot elevations in sufficient detail to exhibit intended drainage patterns and slopes
<u>X</u>	<u>      </u>	Property lines.
<u>X</u>	<u>      </u>	Right-of-way lines and widths, existing and proposed.
<u>X</u>	<u>      </u>	Existing improvements and their elevations.
<u>X</u>	<u>      </u>	Delineation of proposed on-site drainage basins indicating area and 10-year and 100-year storm peak flows at basin concentration points.
<u>NA</u>	<u>      </u>	Concentration points and drainage flow direction with $Q_{100}$ and $V_{100}$ and $D_{100}$ in streets.
<u>X</u>	<u>      </u>	Cumulative flows, velocity, and drainage of flow at upstream and downstream ends of site for the 10-year and 100-year flows.
<u>X</u>	<u>      </u>	Location and cross-section of street capacity calculations.
<u>X</u>	<u>      </u>	Cross-sectional detail for channels, including cutoff wall locations.
<u>X</u>	<u>      </u>	Existing and proposed drainage facilities, appurtenances, and connections, (i.e., Sidewalk, ditches, swales, storm drain systems, unimproved and improved channels, and culverts, etc.) stating size, material, shape, and slope with plan and profile and HGL calculations.
<u>NA</u>	<u>      </u>	Existing and proposed drainage easements and widths shown with sufficient detail. A cross sectional detail must be provided that shows appropriate lining and reinforcement.
<u>NA</u>	<u>      </u>	Location and detail of existing, proposed, and future block wall openings. Minimum size is 16" x 48". Wrought iron gate is required for flows > 10 cfs.
<u>X</u>	<u>      </u>	Location and detail of flood walls illustrating depth of flow, proposed grouting height, etc.

REFERENCE:

STANDARD FORM 2



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## DRAINAGE SUBMITTAL CHECKLIST

### III. DRAINAGE PLAN (Continued)

Yes	No	
<u>NA</u>	<u>      </u>	Perimeter retaining wall locations. All existing and proposed walls (retaining screen and flood) must be shown with adjacent ground elevations. Flood walls with 8-inch concrete masonry unit.
<u>N/A</u>	<u>      </u>	Building and/or lot numbers.
<u>NA</u>	<u>      </u>	Alignment of all existing, proposed, or future Regional Facilities adjacent to the site.
<u>X</u>	<u>      </u>	Limits of existing floodplain based on current FIRM or best available information; limits of proposed floodplains based on best available information.
<u>X</u>	<u>      </u>	For areas in Zone A, AE, AH and AO, base flood elevations(BFEs) must be shown for each lot; BFEs may be listed on each lot, or in a table. Finish floor elevations must be a minimum of 18 inches above BFE.
<u>N/A</u>	<u>      </u>	Appropriately elevated "humps" 6 inches above the 100 year water surface elevation at site accesses where the intent is to protect the site from the Q <sub>100</sub> flows.
<u>N/A</u>	<u>      </u>	Street slopes perimeter and interior streets. The minimum slope is 0.4 percent.

### IV. HYDROLOGIC ANALYSIS

Yes	No	
<u>X</u>	<u>      </u>	Appropriate soil information and Soils Map for existing and future conditions with subbasins and property delineated.
<u>X</u>	<u>      </u>	Input and output information for existing conditions from computer models (HEC-1 and TR-55). The flow routing diagram must be provided with HEC-1 models.
<u>X</u>	<u>      </u>	Input and output information for future conditions from computer models (HEC-1 and TR-55). The flow routing diagram must be provided with HEC-1 models.
<u>X</u>	<u>      </u>	Use of correct precipitation values in and around the McCarran Airport rainfall area.
<u>X</u>	<u>      </u>	A discussion in the text of the hydrologic analysis justifying subbasin boundaries and cutoffs, supporting assumptions, and calculations.
<u>X</u>	<u>      </u>	A summary table of stormwater flows showing basin area, Q <sub>10</sub> and <sub>100</sub> for both individual basins and combined basin flows, where applicable.
<u>X</u>	<u>      </u>	Copies of supporting technical information referenced from a previously approved study and a statement accepting these results.
<u>X</u>	<u>      </u>	On-site facilities must perpetuate flows through or around the site without significantly impacting adjacent property owners in accordance with current Nevada Drainage Law.

REFERENCE:

STANDARD FORM 2



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## DRAINAGE SUBMITTAL CHECKLIST

### V. HYDRAULIC ANALYSIS

Yes	No	
<u>NA</u>	<u>      </u>	Flow split calculations and supporting documentation or reference for the method of flow split calculations used.
<u>NA</u>	<u>      </u>	Normal depth street flow calculations and cross section diagrams for all interior and perimeter streets. Provide "d x v" products for the $Q_{100}$ and $Q_{10}$ flows representing the worst case for interior and all perimeter streets. $Q_{100} d \times v \leq 8$ . $Q_{10} d \times v \leq 6$ and 12 foot dry lane for rights-of-way $\geq 80$ feet. Calculations must be labeled by street name as indicated on the Grading Plan.
<u>NA</u>	<u>      </u>	A summary table of interior and exterior street capacity calculations showing the street name, $Q_{100}$ flow, slope, depth of flow, velocity and depth times velocity product and streets needing to meet 12 foot dry lane criteria.
<u>NA</u>	<u>      </u>	Appropriate hydraulic calculations for block wall openings assuming a 50 percent vertical clogging factor. (Assume the lower half of the opening is plugged.)
<u>NA</u>	<u>      </u>	Appropriate hydraulic calculations at drainage easement entrance and discharge locations to set finish floor elevations. Hydraulic calculations must include submerged weir, superelevation and tee intersection losses, where appropriate.
<u>NA</u>	<u>      </u>	Provide necessary freeboard requirements to set the finish floor elevations of all proposed buildings, 2 x depth of flow or depth of flow plus 18 inches of freeboard, whichever is less. The minimum requirement is 6 inches above adjacent upstream top of curb. Buildings adjacent to drainage easements must always be provided with 18 inches of freeboard above the $Q_{100}$ weir height of flow depth, which ever is greater.
<u>NA</u>	<u>      </u>	A complete water surface profile analysis (HEC-2, HEC-RAS, etc.) for channel flows and FEMA Zone A flood zones. <ul style="list-style-type: none"> <li>→ Field survey data.</li> <li>→ Input and output information.</li> <li>→ Plotted cross-sections based on survey with proper encroachments.</li> <li>→ A map showing the location of the cross-sections.</li> <li>→ Analysis of both sub and super-critical flow segments.</li> <li>→ A summary table and a discussion of the results in the text for drop inlets.</li> </ul>
<u>NA</u>	<u>      </u>	Provide a 50 percent clogging factor in the capacity calculations for drop inlets.
<u>X</u>	<u>      </u>	Hydraulic calculations for culverts and storm drains. D-Load calculations must be provided for storm drain pipes in public rights-of-way, including headwater pool inundation.
<u>X</u>	<u>      </u>	The mitigation of nuisance water, both during construction and in the fully developed condition, must be addressed.

REFERENCE:

STANDARD FORM 2



October 6, 2006

Dave Betley, P.E.  
Clark County Development Services  
500 S. Grand Central Parkway  
PO Box 551842  
Las Vegas, NV 89155-1842

**RE: TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL  
PBS&J PROJECT NO.: 511693.19**

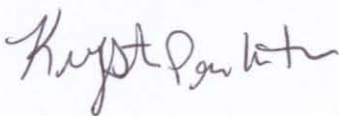
Dear Mr. Betley:

Submitted for your review and approval are two copies of the *Technical Drainage Study for Eastside Landfill*.

If you have any questions regarding this study, please contact our office at (702) 263-7275.

Sincerely,

PBS&J



Krystle Pemberton, E.I  
Hydrologist



Harshal Desai, P.E., CFM  
Project Manager



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<b>Figure 4</b>	Existing Condition Drainage Map
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<b>Figure 7</b>	Cross Section and Drainage Facility Map
<b>Figure B-4</b>	Soil Map



## I. Introduction and Purpose

This report is intended to serve as the Technical Drainage Study (TDS) for Eastside Landfill. The purpose of this study is to establish a technical analysis of peak flow rates affecting the site under existing, interim and developed conditions. It includes an analysis of onsite and offsite drainage patterns and flow rates for use in the design of flood protection facilities. The study shows that the flood protection facilities designed within this study will improve/perpetuate existing drainage patterns.

This study was conducted in accordance with the criteria set forth by Clark County Regional Flood Control District (CCRFGD) *Hydrologic Criteria and Drainage Design Manual* (Criteria Manual), prepared by WRC Engineering and updated by Montgomery Watson, August 1999.

## II. General Information

### A. Location and Description

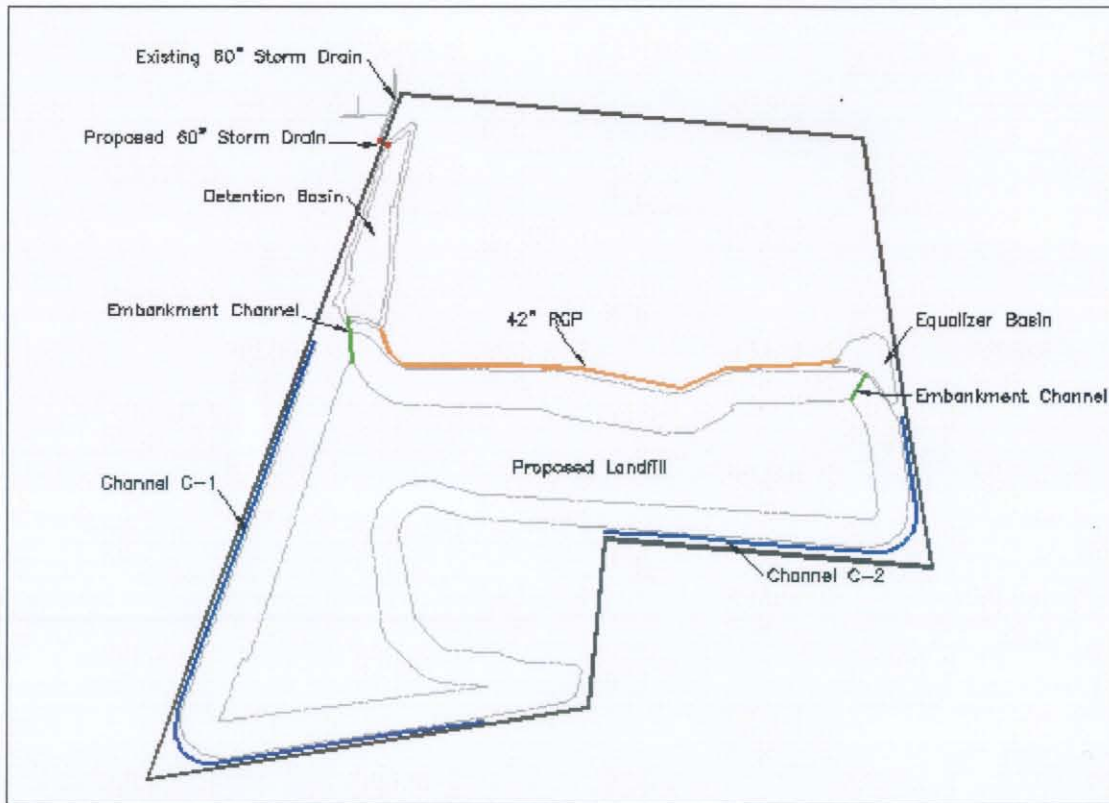
The Eastside Landfill property is located within Sections 11 and 12, Township 22 South, Range 62 East of Clark County, Nevada. The Assessor's Parcel Numbers for the subject site are 178-11-501-006, 178-12-201-002, and 178-12-301-001. The proposed development is located south of Warm Springs Road, west of 4<sup>th</sup> Street and north of the Union Pacific Railroad (UPRR).

The proposed site is bordered to the north by undeveloped land and to the south by Pioneer America LLC (north of the Union Pacific Railroad). American Potash & Chemical Corporation is located east of the project site and undeveloped land is west of the project site. Henderson Commerce Center II (formerly known as Harsch Development) is northwest of the site. Please refer to **Figure 1: Area/Vicinity Map** in **Appendix A**.

The project site area is approximately 113 (+/-) acres. The project entails the construction of a landfill with a total volume of approximately 2.6 million cubic yards of fill. The top of the proposed landfill will be approximately 40 feet above existing grade to reach the desired volume. Channels are proposed around the perimeter of the landfill to collect / convey the offsite and onsite flows. These proposed channels will serve as drainage facilities as wells as access roads for the maintenance of the landfill. The west channel (Channel C-1) drains into a proposed detention basin, with a volume of 16+/- ac-ft, located in the northwest corner of the project site. The purpose of this detention basin is to provide necessary storage to perpetuate the design outflow of the existing 60" storm drain constructed with the Harsch Development. The east channel (Channel C-2) drains into an equalizer basin located just northeast of the proposed landfill. This equalizer basin was designed to split the flow north to perpetuate the existing drainage conditions and west through a proposed storm drain that drains into the detention basin. The top of the landfill was graded such that the runoff would reach the two proposed



embankment channels, one draining into equalizer basin and the other draining into the detention basin. The conceptual layout of the proposed drainage facilities discussed above is shown in the exhibit below. The hydraulic calculations associated with the above mentioned facilities are further discussed in **Section III-D**. The improvement plans for the proposed facilities are provided in **Appendix E**.



**Exhibit 1: Conceptual Layout of Proposed Drainage Facility**

## **B. CCRFCD Master Plan Information**

**Figure 2: CCRFCD Flood Control Facilities Map** (in **Appendix A**) shows the subject property in relation to CCRFCD Master Planned facilities. The exhibits were reproduced from the 2002 CCRFCD Master Plan Update (MPU) of the Las Vegas Valley. The figure shows that the nearest regional facility, Pioneer Detention Basin (PTVW 0185), is located southwest of the proposed site. The detention basin's associated drainage system located west of the site carries the flow north past Warm Springs Road. The drainage from this development will not contribute flow through this facility.

The majority of flow from the project site is conveyed through the existing 60" storm drain which ultimately drains into the existing 10'x5' Reinforced Concrete Box (RCB) located under Warm Springs Road.



### C. FEMA Floodplain Information

**Figure 3: FEMA Map** (in **Appendix A**) is a reproduction of the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map for Clark County, Nevada, Community-Panel Numbers 32003C2595E dated September 27, 2002. **Figure 3** shows that the project site is within a non-shaded Zone X. Zone X is defined by FEMA as areas determined to be outside the 500-year floodplain.

### D. Hydrologic Procedures Used

HEC-1 Flood Hydrograph Package, Version 4.1, developed by the U.S. Army Corps of Engineers Hydrologic Engineering Center, was used to develop runoff data for this study. This is in accordance with the CCRFCD Criteria Manual. The methodology and calculations used to determine the hydrologic parameters are located in **Appendix B-4**. The hydrologic analysis is discussed in further detail under **Section III** of this TDS. HEC-1 runoff models for existing, interim and developed conditions are included in **Appendix B-1, B-2 and B-3** respectively.

### E. Hydraulic Procedures Used

Various hydraulic procedures were used for the analysis and design of different drainage facilities. The procedures used were in accordance with the CCRFCD Criteria Manual.

HEC-RAS, version 3.1.2, was used to model the two channels (Channel C-1 and Channel C-2) bordering the east and west side of the proposed landfill. Please refer to the conceptual layout above for the location of the two channels

WSPG model was used to model the proposed and existing storm drains.

FlowMaster was used for normal depth calculations to estimate the velocity and water depth for other minor channels, top of the landfill and embankment channels.

The hydraulic procedures and associated analyses are discussed in further detail under the hydraulic section (**Section III-D**) of this TDS.

### F. Previous Studies in Project Vicinity

The following studies were reviewed in the preparation of this study. Reference material from each of these studies is included in **Appendix D**.

1. *Addendum #1 to the Technical Drainage Study for Henderson Commerce Center II (Formerly known as Harsch). Prepared by PBS&J., February 2003.*

This reference study performed a hydrologic analysis for the area located west of the proposed site. Offsite basin, OFFD1, from the 2003 referenced TDS is a combination of onsite and offsite basins, ONEX1 and OFFEX1, of this TDS. The hydrologic drainage



patterns derived from the referenced TDS contributed to the design of the existing 60" storm drain located along the east side of the Harsch Development. An inlet is located just southeast of Harsch Development (combination point C18), where 100-year flow of 120 cfs was determined to be collected. At combination point C18B 100-year flow of 127 cfs was calculated to be in the existing 60" storm drain. Please refer to **Appendix D** for the reference material.

**2. Update to the Technical Drainage Study for Henderson Commerce Center (Formerly known as Harsch). Prepared by PBS&J., February 2005.**

This reference study is an update to the previous study and had only minor changes to the storm drain design that runs along the east boundary of the Harsch Development, but does not change the overall hydrology of the site. Refer to **Appendix D** for the latest storm drain alignment and WSPG model.

### **III. Hydrology / Hydraulics**

#### **A. Existing Condition Hydrology**

The 113 (+/-) acre site presently has two existing landfills and the rest of the site is undeveloped. The locations of the existing landfills are delineated on **Figure 4: Existing Condition Drainage Map** included in Appendix B-1. The existing landfills and the undeveloped land are hydrologically characterized as industrial and natural desert landscape respectively.

The onsite subbasins for the existing condition hydrology were delineated using 1 foot aerial topography and field reconnaissance. The onsite subbasins are labeled as ONEX1 through ONEX5. The existing condition hydrology used the offsite hydrology from the above mentioned reference study in **Section II-F**. In addition to the referenced offsite subbasins, PBS&J delineated offsite subbasins (OFFEX1 through OFFEX5) north of the UPRR that contribute flow to the proposed property. The area of the existing chemical ponds located within these offsite basins was deducted from the total area of the basins because these ponds will contain the precipitation and will not contribute to the runoff to the proposed site. **Figure 4** located in **Appendix B-1** shows the onsite and offsite basins for the project site under existing condition. The flow leaving the site is identified on the figures as a combination point or a discharge point.

The offsite basins OFFEX1 and OFFEX2 routes through the project site combining with ONEX1 at Combination point CP-1, with a 10-year and 100-year flow of 33 cfs and 105 cfs respectively. This flow is conveyed to an existing inlet (Combination Point C18) via an existing channel where it combines with the flow from the referenced basins west of the property boundary. The referenced basins are clearly identified on **Figure-4**. The 10-year and 100-year flow at C18 is 57 cfs and 162 cfs respectively. The flow captured by the inlet is conveyed through the existing 60" storm drain which ultimately discharges into the existing 10'x5' RCB under Warm Springs Road.



Subbasin ONEX2 flows northwest to combine with referenced basins HR1 through HR3 and C18 at combination point C18B. The 10-year and 100-year flow at this combination point was determined to be 78 cfs and 212 cfs respectively. Onsite subbasin ONEX3 discharges directly north into existing washes. The 10-year and 100-year flow at that discharge point is 27 cfs and 59 cfs respectively.

The offsite subbasin OFFEX5 flows north through an existing channels within ONEX4 to combine with ONEX4 at combination point CP-3. Combination point CP-3 outlets 10-year and 100-year flows of 27 and 65 cfs respectively into an existing channel north of the property boundary.

Flow produced by offsite subbasin OFFEX4 will be diverted east by an existing culvert under Fourth Street. The flow will reach the culvert through an existing riprap channel or by an existing graded swale along the northern border of this offsite basin. Therefore, the flow from this basin will not impact the project site. The picture below shows the riprap channel and the culvert under Fourth Street.



**Exhibit 2: Picture of the riprap channel and the culvert under Fourth Street (looking west)**

The offsite subbasin OFFEX3 has a shallow ponding area where the runoff is contained, preventing the flow from continuing north and impacting the project site. This low area also captures flow produced by onsite subbasin ONEX5. These two basins were combined at combination point CP-2. The existing shallow ponding area within OFFEX3 was modeled in the existing drainage condition HEC-1 model using a stage-



storage discharge curve. The volume of the shallow area was determined by using 1' aerial topography. A negligible outflow was used to run the model. The existing condition HEC-1 model determined a water surface elevation (WSE) of 1768.34 feet produced by the runoff generated by these two subbasins. This shallow ponding area has containment up to an elevation of 1770 feet, therefore this flow was not assumed to continue north. Below is the summary of the information used in the stage-storage discharge curve.

**Table 1: Summary Table for OFFEX3 Shallow Ponding Area Stage-Storage Discharge Curve**

ELEVATION	AREA (ft <sup>2</sup> )	VOLUME (ft <sup>3</sup> )	VOLUME (ac-ft)	CUMULATIVE VOLUME (ac-ft)	OUTFLOW (cfs)
1766	10475	0	0.00	0.00	0
1767	30499	20487	0.47	0.47	0.01
1768	47931	39215	0.90	1.37	0.02
1769	68570	58250.5	1.34	2.71	0.03
1770	89398	78984	1.81	4.52	0.04

The discussion on the development of the hydrologic parameters is included in **Appendix B-4**. The existing condition HEC-1 model is included in **Appendix B-1**. **Table 2** below shows the summary of the flows in existing condition.

**Table 2: Summary Table for Existing Condition**

BASIN ID	AREA (ac)	Q <sub>100</sub> (cfs)	Q <sub>10</sub> (cfs)
ONEX1	32.76	47	17
ONEX2	28.77	49	21
ONEX3	22.12	59	29
ONEX4	28.27	56	25
ONEX5	1.06	3	2
OFFEX1	42.20	48	14
OFFEX2	9.63	13	4
OFFEX3	16.40	21	8
OFFEX4	7.61	14	6
OFFEX5	5.11	10	4
CP-1	NA	105	33
CP-2	NA	23	8
CP-3	NA	65	27
C18	NA	162	57
C18B	NA	212	78

## B. Interim Condition Hydrology

The interim condition hydrology is analyzed assuming that the onsite basins are developed and the offsite basins have existing condition hydrologic parameters.

The onsite subbasins for the interim drainage condition hydrology were developed using the improvement plans included in **Appendix E**. The onsite subbasins are labeled as OND1 through OND15. **Figure 5: Interim Condition Drainage Map** shows the onsite and offsite basins for the project site under interim drainage condition. This figure is included in **Appendix B-2**.



As previously mentioned, two main channels were designed around the perimeter of the proposed landfill. Channel C-1 collects runoff produced by the west side of the landfill (from onsite basins OND1 through 3 and OND7) and offsite flow (from offsite basins OFFEX1 and OFFEX2) and eventually discharges into the proposed detention basin. The combination point CP-4 represents the total flow collected by Channel C-1. The 10-year and 100-year flow at CP-4 is 26 cfs and 79 cfs respectively.

Subbasin OND8 produces a flow of 16 cfs / 33 cfs (10-year / 100-year) which is conveyed through a graded channel along the perimeter of the proposed landfill. The channel starts at the southern boundary of OND8 and is graded to convey the flow to Channel C-2.

Channel C-2 collects flow from the east side of the landfill (from onsite basins OND8, OND10 and OND12) and offsite flow (from offsite basin OFFEX5). The combination point CP-10A represents the total flow collected by Channel C-2. The 10-year and 100-year flow at CP-4 is 25 cfs and 55 cfs respectively. Channel C-2 discharges into the proposed equalizer basin.

As discussed above, the top of the landfill has been graded to have positive drainage and to convey the flow to the two embankment channels located on either side of the proposed landfill. The top of the landfill was divided into three subbasins: OND4, OND5 and OND11. Subbasins OND4 and OND5 drains to the embankment channel located on west side of the proposed landfill (CP-5) whereas OND11 drains to the embankment channel located on east side of the proposed landfill. The west embankment channel conveys the flow of 19 cfs / 40 cfs (10-year / 100-year) from CP-5 to the proposed detention basin. The east embankment channel conveys the flow of 12 cfs / 24 cfs (10-year / 100-year) from OND11 to the proposed equalizer basin.

Subbasin OND6 has a proposed graded channel proposed along the perimeter of the landfill directing the flow into the detention basin. This subbasin will produce 10-year/100-year flow of 11/23 cfs. Subbasin OND13 also has a proposed graded channel along the perimeter of the landfill proposed directing the 10-year and 100-year flow of 6 cfs and 12 cfs respectively into the equalizer basin.

The purposed of the equalizer basin proposed at the northeast corner of the proposed landfill is to split the flow north and west. The peak flow (10-year/ 100-year) reaching the equalizer basin in interim drainage condition is 42 cfs / 90 cfs (10-year / 100-year) represented by combination point CP-10. This is the combined flow from CP-10A, OND11 and OND13. An elliptical pipe (53"x 34"), equivalent to a 42" RCP, is proposed as the outlet structure for this basin. A 30' spillway is proposed at an elevation of 1747.75 feet on the north side of the basin. The equalizer basin was modeled in HEC-1 using a stage storage discharge curve. The outflow through the 42" elliptical pipe was determined using the inlet control nomograph provided in the CCRFCD manual and flow overtopping the spillway was calculated using the weir equation. The WSE in interim drainage condition in the equalizer basin is 1747.53 feet, preventing any flow



from overtopping the spillway and continuing north. Below is a table containing the flows and areas calculated by the above mentioned procedure. Please refer to **Appendix B-3** for sample calculations of the flow used in the stage-storage discharge curve for the equalizer basin.

**Table 3: Summary Table for Equalizer Basin Stage-Storage Discharge Curve**

ELEVATION	AREA (ft <sup>2</sup> )	AREA (ac-ft)	42" ELLIPTICAL PIPE FLOW (cfs)	SPILLWAY OVERFLOW (cfs)	TOTAL DISCHARGE(cfs)
1744.50	0	0.00	0	0	0
1745.00	3480	0.08	0	0	0
1746.00	30510	0.70	18	0	18
1747.00	34005	0.78	42	0	42
1747.75	36890	0.85	59	0	59
1748.00	37850	0.87	64	10	74
1748.50	42210	0.97	73	53	126

As previously mentioned, a 16+/- ac-ft detention pond is proposed at the northwest side of the property. The peak flow reaching the detention pond, represented by HEC-1 combination point CP-6, is contributed by Channel C-1, the west embankment channel, flow conveyed through the 42" RCP and subbasin OND6. The 10 year and 100 year flows reaching the detention pond are 79 cfs and 190 cfs respectively.

A 60" outlet pipe is proposed from the detention pond which ties into the existing 60" storm drain placed with the Harsch Development. A 25" restrictor plate is designed for the 60" outlet pipe to control the outflow. The peak 100-year outflow from the detention is calculated to be 41 cfs with a peak WSE of 1732.22 feet. The calculated freeboard for the detention basin in the interim condition is 2.78 feet (1735-1732.22). A stage-storage discharge curve was used to model the proposed detention basin in HEC-1. The outflow was calculated using the orifice equation. Please refer to **Appendix B-3** for sample calculations of the calculated outflows. Below is a summary table containing the information used in stage-storage discharge curve.

**Table 4: Summary Table for Detention Basin Stage-Storage Discharge Curve**

ELEVATION	HEIGHT (ft)	AREA (ft <sup>2</sup> )	VOLUME (ft <sup>3</sup> )	VOLUME (acre-ft)	CUMMULATIVE VOLUME (acre/ft)	OUTFLOW (ft <sup>3</sup> /s)
1725.25	0.0	0	0	0.00	0.00	0
1726.00	0.75	9360	3510	0.08	0.08	0
1728.00	2.0	53790	63150	1.45	1.53	22
1729.00	1.0	76290	65040	1.49	3.02	27
1730.00	1.0	82060	79175	1.82	4.84	32
1732.00	2.0	93665	175725	4.03	8.88	40
1734.00	2.0	105690	199355	4.58	13.45	46
1735.00	1.0	112360	109025	2.50	15.95	49

HEC-1 combination point C18 is the combination of the outflow from the detention basin and the referenced subbasins. The 10-year and 100-year flow at combination point



C18 is 62 cfs and 123 cfs. The referenced hydrology from Addendum #1 for the Harsch Development calculated a 100-year discharge of 120 cfs at this combination point. The difference in the flows computed at CP-18 is only 3 cfs (2.5%). The existing 60" storm drain is analyzed for flow greater than 120 cfs and has the capacity for the additional flow. The analysis completed will be discussed in further detail in **Section D**.

The remaining two onsite subbasins, OND14 and OND15, discharge into existing channels to the north. The 10-year and 100-year peak flows at CP-11 are 15 cfs and 31 cfs respectively. It should be noted that the flow reaching the northeast corner of the property after the proposed improvements is lower than the existing condition peak flow (27/65 cfs) at this location.

The discussion on the development of the hydrologic parameters is included in **Appendix B-4**. The interim drainage condition HEC-1 model is included in **Appendix B-2**. **Table 2** below shows the summary of the flows in interim condition.

**Table 5: Summary Table for Interim Condition**

BASIN ID	AREA (ac)	Q <sub>100</sub> (cfs)	Q <sub>10</sub> (cfs)
OND1	0.94	3	1
OND2	3.70	8	4
OND3	1.38	4	2
OND4	11.67	27	13
OND5	5.03	12	6
OND6	9.90	23	11
OND7	5.87	16	8
OND8	14.26	33	16
OND9	1.06	3	2
OND10	4.28	10	5
OND11	9.60	24	12
OND12	2.77	8	4
OND13	4.70	12	6
OND14	11.12	31	15
OND15	21.47	57	28
DETPD	5.14	16	8
OFFEX1	42.20	48	14
OFFEX2	9.63	13	4
OFFEX3	16.40	21	8
OFFEX4	7.61	14	6
OFFEX5	5.11	10	4
CP-1	NA	15	5
CP-2	NA	68	22
CP-3	NA	70	22
CP-4	NA	79	26
CP-5	NA	40	19
CP-6	NA	190	79
CP-7	NA	23	8
CP-9	NA	51	23
CP-10	NA	90	42
CP-10A	NA	55	25
CP-11	NA	31	15
C18	NA	123	62
C18B	NA	133	67



### C. Developed Condition Hydrology

The developed condition hydrology was analyzed assuming that onsite and offsite basins were developed. The developed curve numbers for the offsite basins were assumed to be industrial based on its current land use and the surrounding properties. Please refer to **Appendix B-4** for the development of the hydrologic parameters. It should be noted that developed condition produced higher runoff, and therefore was used in the design of the drainage facilities. **Figure 6 Developed Condition Drainage Map** shows the onsite and offsite basins for the project site under developed drainage condition. This figure is included in **Appendix B-3**.

The drainage patterns of the onsite and offsite basins are consistent with the drainage patterns discussed in the interim drainage condition. Only one modification was made to the drainage patterns in the developed condition hydrology. The shallow ponding area located within subbasin OFFD3 was removed from the HEC-1 model. Therefore, the flow produced by OFFD3 and OND9 will now combine with the flow in Channel C-2 at HEC-1 combination point CP-8. HEC-1 combination point CP-8 is the combination of subbasins OND8, OND9 and OFFD3. The remaining flow contributions to Channel C-2 remain unchanged.

The 10-year and 100-year peak flow reaching the equalizer basin in developed conditions is 60 cfs and 127 cfs respectively. The peak WSE in the equalizer basin was determined by the HEC-1 model to be 1748.19 feet. This WSE is 0.44 feet above the spillway height. It was determined that 67 cfs will be conveyed through the 42" RCP into the detention basin whereas 26 cfs will flow north combining with subbasin OND14 at HEC-1 combination point CP-11. The peak flow (10-year/100-year) at this combination point is 15/39 cfs. The peak flow reaching the northeast corner of the property is less than existing drainage condition peak flows of 27/65 cfs.

The 10-year and 100-year peak flow reaching the detention basin in developed conditions is 119 cfs and 254 cfs respectively. The 100-year WSE in the detention basin determined by the HEC-1 model is 1733.80ft, resulting in a freeboard of 1.2 feet. The outflow through the 25" opening is 45 cfs, resulting in the 100-year peak flow at HEC-1 combination point C18 to be 126 cfs. The proposed development will add an additional 6 cfs (additional 5%) to the existing 60" storm drain. A hydraulic analysis was performed on the additional flow anticipated to be conveyed through the existing 60" storm drain. This will be discussed in further detail in **Section D**.



**Table 6: Summary Table for Developed Condition**

<b>BASIN ID</b>	<b>AREA (ac)</b>	<b>Q<sub>100</sub> (cfs)</b>	<b>Q<sub>10</sub> (cfs)</b>
OND1	0.94	3	1
OND2	3.70	8	4
OND3	1.38	4	2
OND4	11.67	27	13
OND5	5.03	12	6
OND6	9.90	23	11
OND7	5.87	16	8
OND8	14.26	33	16
OND9	1.06	3	2
OND10	4.28	10	5
OND11	9.60	24	12
OND12	2.77	8	4
OND13	4.70	12	6
OND14	11.12	31	15
OND15	21.47	57	28
DETPD	5.14	16	8
OFFD1	42.20	87	39
OFFD2	9.63	23	10
OFFD3	16.40	35	16
OFFD4	7.61	19	9
OFFD5	5.11	13	6
CP-1	NA	25	11
CP-2	NA	120	54
CP-3	NA	121	54
CP-4	NA	131	59
CP-5	NA	40	19
CP-6	NA	254	119
CP-7	NA	37	17
CP-8	NA	70	33
CP-9	NA	89	41
CP-10	NA	127	60
CP-10A	NA	92	43
CP-11	NA	39	15
C18	NA	126	68
C18B	NA	136	74

The discussion on the development of the hydrologic parameters is included in **Appendix B-4**. The developed drainage condition HEC-1 model is included in **Appendix B-3**. Please refer to **Appendix E** for the proposed grading plans.



## D. Hydraulics

### HEC-RAS Model for Channel C-1

HEC-RAS was used to model Channel C-1 (from station 10+00 to 20+00) which begins as an unlined 10 feet wide channel, 3:1 side slopes with a minimum depth of 3 ft. The channel then transitions to a 10 feet wide concrete bottom section, with riprap lined banks with 3:1 side slopes with a minimum depth of 3 feet until the channel discharges into the detention basin. Please refer to proposed grading plans included in **Appendix E** for the cross-section details and locations.

Boundary conditions for Channel C-1 were set to anticipate the effects of the proposed grading. The upstream boundary condition was set to normal depth with the channel slope of 0.40%. The downstream boundary condition was set to normal depth with the channel slope of 6.00% which represents the slope of the access road entering the detention basin. This slope was the most critical condition to ensure the velocities meet CCRFCD criteria at the terminus of the model.

The HEC-RAS model was ended at station 38+74.10 because the runoff in Channel C-1 will spread across the access road and over the grouted riprap into the detention basin. The geometry data used in HEC-RAS model is consistent with the proposed grading plans.

The HEC-RAS model simulated under mixed flow regime using the flows summarized in the table below.

Table 7: Summary of flows used for Channel C-1 HEC-RAS model

STATION	FLOW (cfs)	NOTES
1100	3	flow of OND1
1200	33	sum of CP-1 and OND2
2000	120	flow at CP-2
2200	121	flow at CP-3
2587.70	131	flow at CP-4

The results of the analysis shows that the maximum velocity in the unlined channel and the concrete/riprap channel are less than 5 feet/sec and 10feet/sec respectively. The freeboard calculations for Channel C-1 are located in **Appendix C-4**. Superelevation was calculated from station 20+50 through 23+73.86 because of the channel bend.

Please refer to **Figure7 – Cross Section and Drainage Facility Map** in **Appendix C-1** for channel stationing and **Appendix C-2** for the HEC-RAS model. An electronic copy of the HEC-RAS models is also included in **Appendix F**.



## **HEC-RAS Model for Channel C-2**

HEC-RAS was used to model Channel C-2 (from station 10+00 to 26+69.88) which begins as an unlined 10 feet wide channel, 3:1 side slopes with a minimum depth of 3 ft. The channel then transitions to a 10 feet wide concrete bottom section, with riprap lined banks with 3:1 side slopes with a minimum depth of 3 feet (from station 20+00 to 25+45). The channel then transitions to a 10 feet wide concrete bottom section, with riprap lined banks with 3:1 side slopes with a minimum depth of 4 feet until the channel discharges into the equalizer basin. Please refer to proposed grading plans included in **Appendix E** for the cross-section details and locations.

The upstream boundary condition was set to normal depth with the channel slope of 0.40%. The downstream boundary condition was set to known WSE of 1748.19 which represents the peak WSE in the equalizer basin. The geometry data used in HEC-RAS model is consistent with the proposed grading plans.

The HEC-RAS model simulated under mixed flow regime using the flows summarized in the table below.

**Table 8: Summary of flows used for Channel C-2 HEC-RAS model**

STATION	FLOW (cfs)	NOTES
1000	80	sum of CP-8 and OND10
2000	89	flow at CP-9
2319.91	92	flow at CP-10A

The results of the analysis shows that the maximum velocity in the unlined channel and the concrete/riprap channel are less than 5 feet/s and 10feet/s respectively. The freeboard calculations for Channel C-2 are located in **Appendix C-4**. Superelevation was calculated through the channel bend.

Please refer to **Figure 7 – Cross-Section and Drainage Facility Map** in **Appendix C-1** for channel stationing and **Appendix C-2** for the HEC-RAS model. An electronic copy of the HEC-RAS models is also included in **Appendix F**.

## **FlowMaster Calculations**

FlowMaster was used to calculate normal depth and velocity at the cross-sections shown on **Figure7- Cross-Section and Drainage Facility Map** included in **Appendix C-1**. Freeboard was calculated on the channels along the perimeter of the proposed landfill. The cross-sections on the top of the landfill were analyzed to show the peak flow is contained within the cross-section. The embankment channels were also analyzed using the FlowMaster to the show the containment of flow. The embankment channels are grouted riprap lined with 10' feet wide, 3:1 side slopes and depth of 1 foot. The velocities within these embankment channels are less than 15 feet /sec meeting the CCRFCD criteria.



Please refer to **Appendix C-5** for the FlowMaster calculations and the proposed grading plans included in **Appendix E** for the cross-section details.

#### **42" Storm Drain**

WSPG was used to analyze the 42" storm drain. Under developed condition, 67 cfs was calculated to enter the 42" storm drain based on the stage-storage discharge curve that was previously discussed in **Section III-B**. The upstream boundary condition uses a WSE of 1748.19 feet which was taken from HEC-1 model at the equalizer basin. The downstream boundary condition uses a WSE of 1733.8 feet which was taken from HEC-1 model at the detention basin.

Please refer to **Appendix C-6** for the WSPG model and the proposed grading plans included in **Appendix E** for the storm drain alignment, stationing and inverts.

#### **60" Storm Drain**

WSPG was used to analyze the proposed 60" storm drain that ties into the existing 60" storm drain built with the Harsch Development. The outflow from the detention pond was calculated to be 45 cfs determined from the stage-storage discharge curve. At HEC-1 combination point C18 in the developed conditions, the peak flow is 126 cfs. The referenced WSPG model was revised to show the changes in the existing storm drain due to the addition of 6 cfs. In the model, stations 2899.20 thru 1144.65 were directly referenced from the above mentioned study.

The peak outflow from the detention pond was 45 cfs and the peak flow at combination point C18 is 126 cfs. Therefore, 81 cfs was introduced at station 2899.20 where the existing inlet is located ( $126 - 45 = 81$  cfs). As shown in the chart below, the 60" storm drain has adequate capacity to convey additional 6 cfs with minimal differences in the HGL and EGL between the proposed storm drain flow and the original flow calculated in the referenced study.





**Exhibit 3: 60" Storm Drain Analysis Chart**

### Riprap Calculations

Riprap calculations were performed to show that 12" riprap will withstand the shear stress acting on the side slopes of Channel C-1 and Channel C-2. The shear stress calculations were conducted on stations 20+00 thru 38+74.10 of Channel C-1 and stations 20+00 thru 26+69.88 for Channel C-2.

PBS&J sized the riprap based on critical shear stress calculations. The results of proposed HEC-RAS model were used to calculate the average boundary shear stress on the channel bed ( $\tau_o$ ) using the following equation:

$$\tau_o = \lambda D S_f$$

where  $\lambda$  is the density of water (62.4 lb/ft<sup>3</sup>), D is the flow depth, and  $S_f$  is the frictional slope).

The critical shear stress ( $\tau_{cr}$ ) for the riprap bed was calculated based on the following equation:

$$\tau_{cr} = 0.06 (\lambda_s - \lambda_w) d \tan \Phi$$

where  $\lambda_s$  is the density of the riprap (149.76 lb/ft<sup>3</sup>, specific gravity = 2.4),  $\lambda_w$  is the density of water (62.4 lb/ft<sup>3</sup>), d is the median diameter of the riprap, and  $\Phi$  is the angle



of repose, which is based on Figure 705A of the Clark County Regional Flood Control District (CCRFCD) design manual.

PBS&J computed the shear stress on the banks and side slopes ( $\tau_m$ ) using the following equation:

$$\tau_m = 0.75 \lambda D S f$$
$$\tau_m = 0.75 \tau_o$$

where  $\tau_o$  is average boundary shear stress on the bed as discussed above.

The critical shear stress ( $\tau_s$ ) on the banks and side slopes is calculated based on the following equation:

$$\tau_s = \tau_{cr} \sqrt{1 - \frac{\sin^2 \theta}{\sin^2 \phi}}$$

where  $\tau_{cr}$  is critical shear stress on the bed as discussed above, and  $\theta$  is bank side slope.

PBS&J selected the riprap sizes such that the critical stress for banks is always greater than the shear stress for banks with a factor of safety always higher than 3 (refer to **Appendix C-8** for supporting calculations).

## IV. Conclusions

This study presents the findings of a detailed evaluation of existing, interim, and developed drainage conditions for the proposed landfill.

This study investigated the onsite and offsite drainage conditions and determined that the site will be able to convey the 100-year peak flow rate through the proposed drainage facilities.

The study shows that the flood protection facilities designed within this study will improve/perpetuate existing drainage patterns.

A copy of the grading plans are included **Appendix E**.



## V. References

1. *Clark County Regional Flood Control District Hydrologic Criteria and Drainage Design Manual*. Prepared for: Clark County Regional Flood Control District. Adopted August 12, 1999.
2. FlowMaster Version 6.1, Haestad Methods, Inc. 1999.
3. HEC-1 Flood Hydrograph Package Version 4.1. U.S. Army Corps of Engineers, Hydrologic Engineering Center, September 1990.
4. *CCRFCD Master Plan Update of the Las Vegas Valley 2002*. Prepared for Clark County Regional Flood Control District. Prepared by PBS&J and VTN, 2002.
5. *Soil Survey of Las Vegas Valley Area Nevada 1985*. United States Department of Agriculture, Soil Conservation Service
6. *Addendum #1 to the Technical Drainage Study for Henderson Commerce Center Two (Formerly known as Harsch)*. Prepared by PBS&J, February 2003.
7. *Update to the Technical Drainage Study for Henderson Commerce Center (Formerly known as Harsch Development)*. Prepared by PBS&J, February 2005.



## **Appendix A: General Information Figures**



NOTES

This map is for assessment use only and does NOT represent a survey. No liability is assumed for the accuracy of the data delineated herein. Information on roads and other non-assessed parcels may be obtained from the Road Document Listing in the Assessor's Office.

This map is compiled from official records, including surveys and deeds, but only contains the information required for assessment. See the recorded documents for more detailed legal information.

USE THIS SCALE(FEET) WHEN MAP REDUCED FROM 11X17 ORIGINAL

0

50

100

200

400

600

800

AVERAGE  
QA VALUE  
35

MAP LEGEND

—

PARCEL BOUNDARY

—

SUBD BOUNDARY

---

ROAD EASEMENT

—

PM/LD BOUNDARY

---

NON-PARCEL LOT LINE

—

MATCH LINE / LEADER LINE

---

ROAD ID NUMBER

001  
1.00

PARCEL NUMBER  
ACREAGE

202  
PB 25-45

PARCEL SUB/SEQ NUMBER  
PLAT RECORDING NUMBER

5

BLOCK NUMBER

5

LOT NUMBER

GL5

GOV. LOT NUMBER

ASSESSOR'S PARCELS - CLARK CO., NV.  
M. W. Schofield, Assessor

T22S R62E

R61E R62E R63E

T21S

162 161 160

T22S

177 178 179

T23S

191 190 189

11

6 5 4 3 2 1

7 8 9 10 11 12

18 17 16 15 14 13

19 20 21 22 23 24

30 29 28 27 26 25

31 32 33 34 35 36

N 2 NE 4

8 4 8 4

5 1 5 1

6 2 6 2

7 3 7 3

8 4 8 4

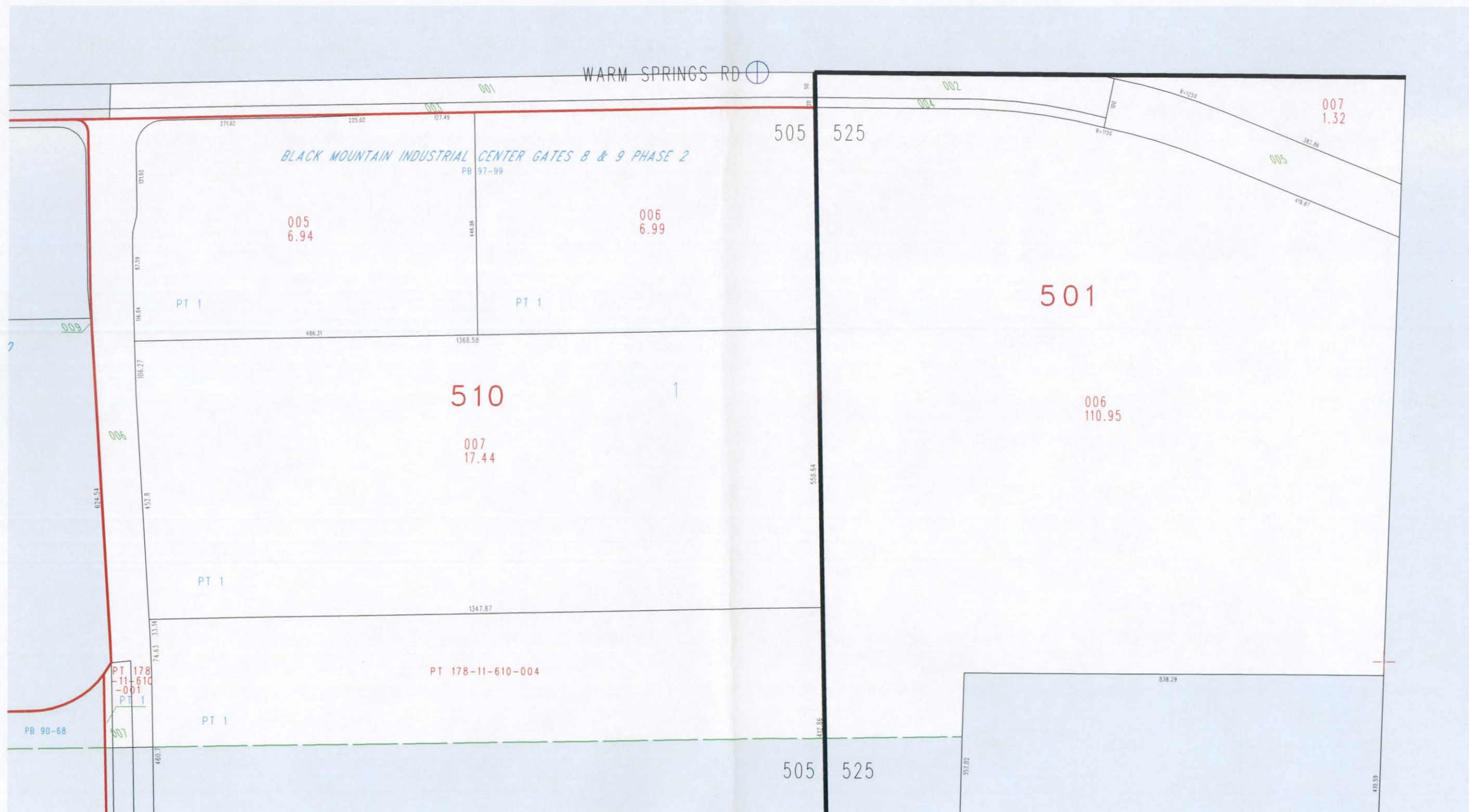
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178-11-5

CLARK COUNTY  
ASSESSOR  
MAPPING DIVISION  
NEVADA

Scale:1"=200'

Rev:02/04/05





NOTES

USE THIS SCALE( FEET ) WHEN MAP REDUCED FROM 11X17 ORIGINAL



AVERAGE  
QA VALUE  
35

ASSESSOR'S PARCELS - CLARK CO., NV.  
M. W. Schofield, Assessor

MAP LEGEND

- \_\_\_\_\_ PARCEL BOUNDARY  
 \_\_\_\_\_ SUBD BOUNDARY  
 - - - - - ROAD EASEMENT  
 \_\_\_\_\_ PM/LD BOUNDARY  
 - - - - - NON-PARCEL LOT LINE  
 \_\_\_\_\_ MATCH LINE / LEADER LINE  
 001 ROAD ID NUMBER

001  
1.00

202

PB 25-45

5

J  
E

GL5

PARCEL NUMBER  
ACREAGE

PARCEL SUB/SEQ. NUMBER

PARCEL SUB/SEQ NUMBER  
PAGE RECORDING NUMBER

PLAT RECORDING NUMBER

BLOCK NUMBER

[illegible]

LOT NUMBER

GOV LOT NUMBER

T22S R62E

11

N 2 SE 4

178-11-7



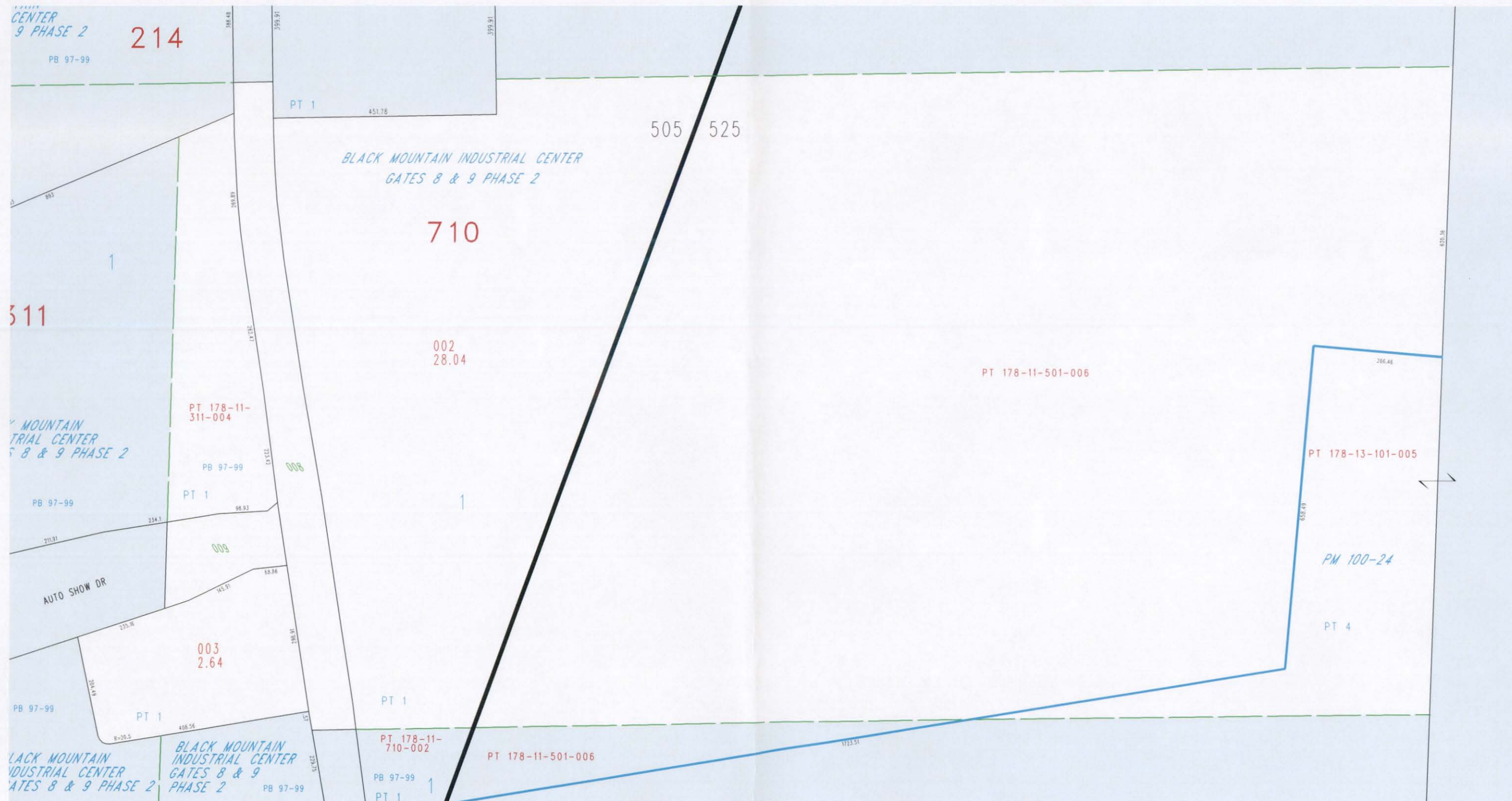
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T21S	162	161	160
T22S	177	178	179
T23S	191	190	189

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7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

8	4	8	4
5	1	5	1
6	2	6	2
7	3	7	3
8	4	8	4

Scale: 1" = 200'

Rev:02/03/06



TAX DIST 505,525



NOTES

This map is for assessment use only and does NOT represent a survey. No liability is assumed for the accuracy of the data delineated herein.

Information on roads and other non-assessed parcels may be obtained from the Road Document Listing in the Assessor's Office.

This map is compiled from official records, including surveys and deeds, but only contains the information required for assessment. See the recorded documents for more detailed legal information.

MAP LEGEND

AVERAGE  
QA VALUE  
45

—

 PARCEL BOUNDARY

—

 SUBD BOUNDARY

---

 ROAD EASEMENT

—

 PM/LD BOUNDARY

---

 NON-PARCEL LOT LINE

—

 MATCH LINE

001

 ROAD ID NUMBER

001  
1.00

 PARCEL NUMBER  
ACREAGE

202  
PB 25-45

 PARCEL SUB/SEQ NUMBER  
PLAT RECORDING NUMBER

5

 BLOCK NUMBER

5

 LOT NUMBER

GL5

 GOV. LOT NUMBER

ASSESSOR'S PARCELS - CLARK CO., NV.

M. W. Schofield, Assessor

BOOK

T22S R62E

SEC

12

MAP

S 2 NW 4

178-12-2

R61E

R62E

R63E

T21S

T22S

T23S

162

177

191

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Scale:1"=200'

Rev:09/17/98

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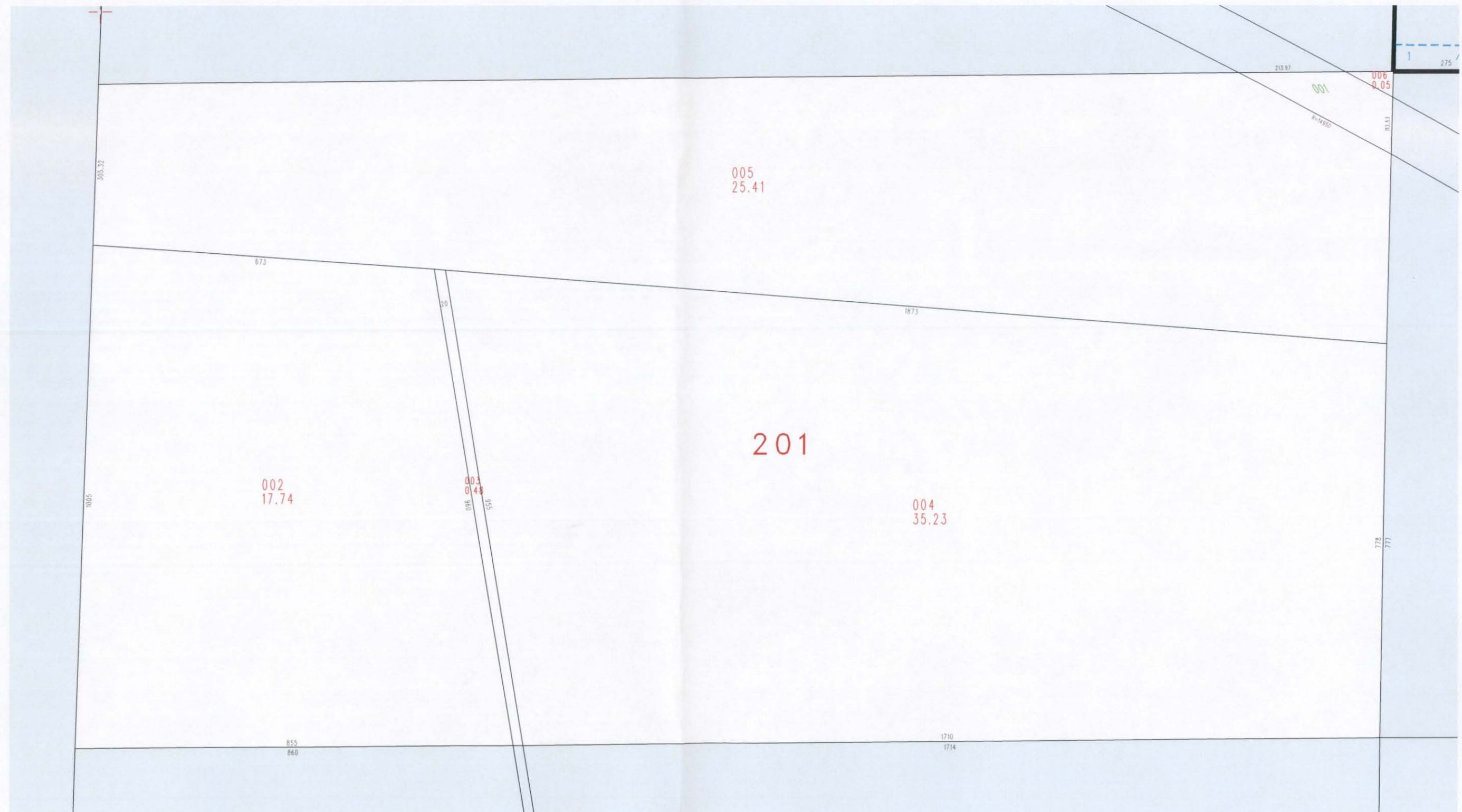
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CLARK COUNTY

ASSESSOR

MAPPING DIVISION

NEVADA





NOTES

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recorded documents for more detailed legal information.

USE THIS SCALE(Feet) WHEN MAP REDUCED FROM 11X17 ORIGINAL



MAP LEGEND

AVERAGE  
QA VALUE  
45

- PARCEL BOUNDARY
- SUBD BOUNDARY
- ROAD EASEMENT
- PM/LD BOUNDARY
- NON-PARCEL LOT LINE
- MATCH LINE / LEADER LINE
- ROAD ID NUMBER

ASSESSOR'S PARCELS - CLARK CO., NV.  
M. W. Schofield, Assessor

001  
1.00  
202  
PB 25-45  
5  
5  
GL5

PARCEL NUMBER  
ACREAGE  
PARCEL SUB/SEQ NUMBER  
PLAT RECORDING NUMBER  
BLOCK NUMBER  
LOT NUMBER  
GOV. LOT NUMBER

T22S R62E

	R61E	R62E	R63E
T21S	162	161	160
T22S	177	178	179
T23S	191	190	189

Scale:1"=200'

12

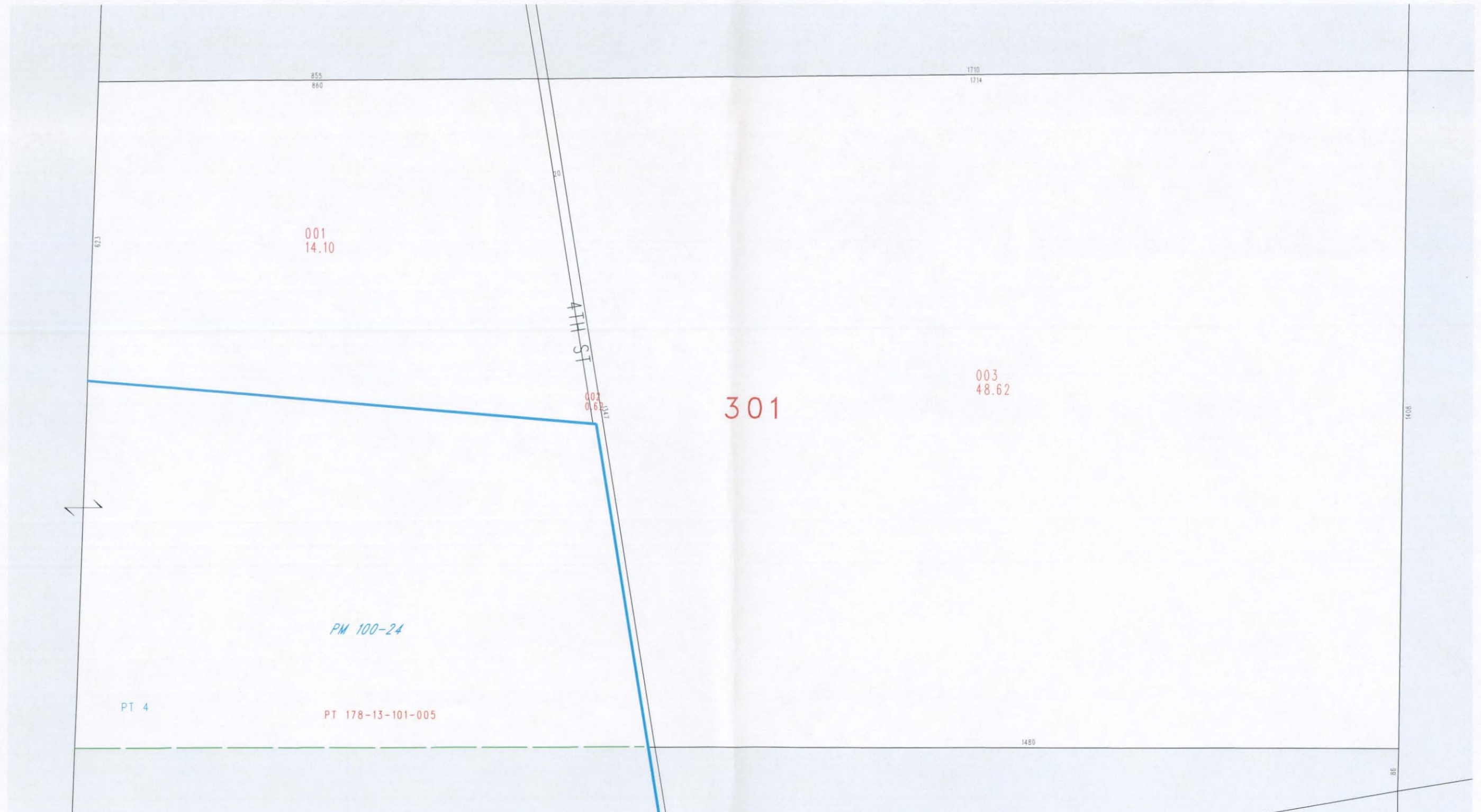
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Rev:05/15/01

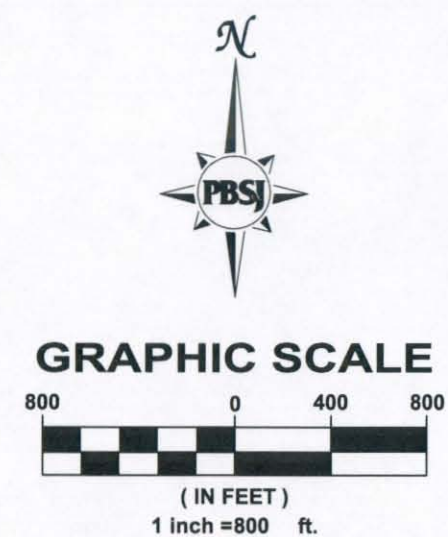
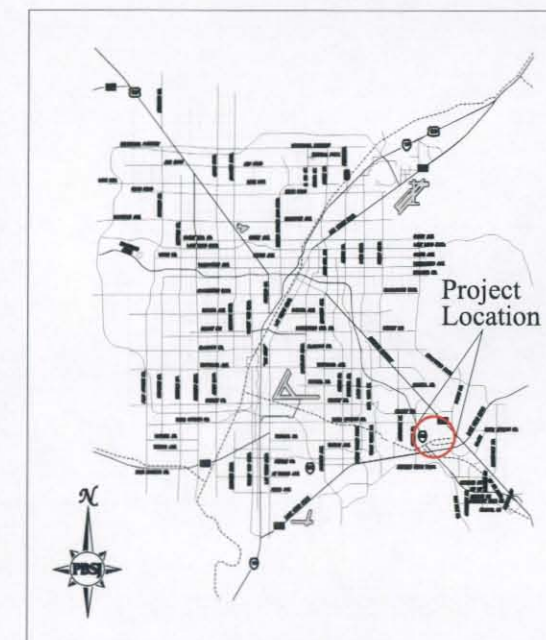
N 2 SW 4

8	4	8	4
5	1	5	1
6	2	6	2
7	3	7	3
8	4	8	4
5	1	5	1

178-12-3







511693.19

SEPTEMBER 2006

**FIGURE 1  
AREA/ VICINITY MAP**

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



2270 Corporate Circle  
Suite 100  
Henderson, Nevada 89074-6382  
Telephone: 702/263-7275  
Fax: 702/263-7200

ENGINEERING • PLANNING • SURVEYING • CONSTRUCTION SERVICES





FIGURE 2: CCRFCD FLOOD CONTROL FACILITIES MAP

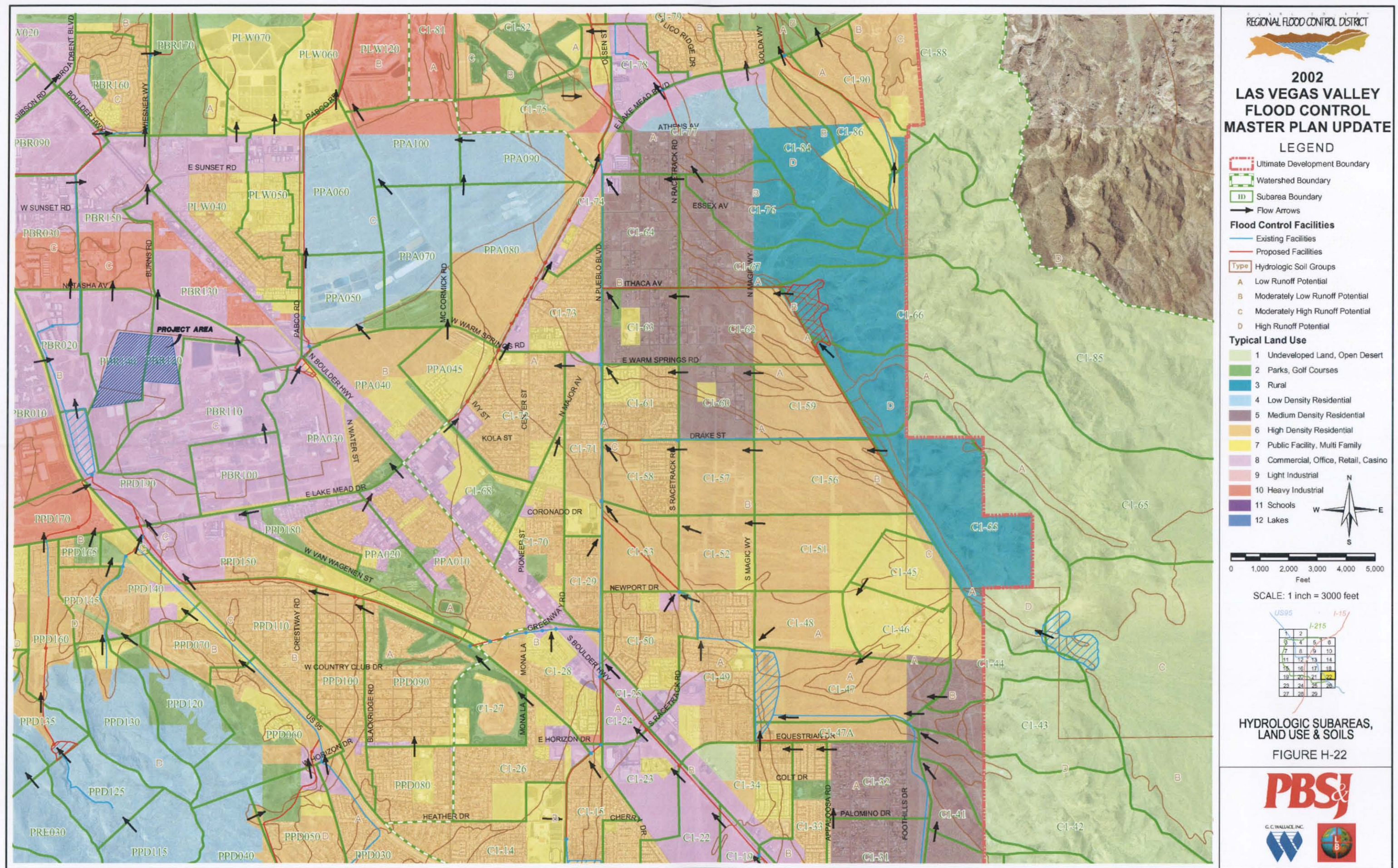


ID / River Mile	Status	Facility Description	Length (ft.)	Flow (cfs)	HEC-1 Node	HEC-1 Model	Tributary Area (sq.mi.)	Channel Slope (%) **
C1BH		C-1 CHANNEL - BOULDER HWY						
0000	P1	Conc Chnl 30'W 6'D 2:1 SS	2140	3224	CP22	C1SDN3	3.19	1.00
0040	P1	3: 15' X 6' RCBC @ Horizon Dr	100	3194	CP21	C1SDN3	3.11	1.00
0042	P1	Conc Chnl 30'W 6'D 2:1 SS	1525	3194	CP21	C1SDN3	3.11	1.00
0071	E	10' X 4' RCBC @ Equestrian Dr	100	2842	CP20	C1SDN3	2.77	1.00
0071	P1	3: 14' X 6' RCBC @ Equestrian Dr	100	2842	CP20	C1SDN3	2.77	1.00
0073	P1	Conc Chnl 30'W 6'D 2:1 SS	2000	2842	CP20	C1SDN3	2.77	0.80
0111	P1	Conc Chnl 20'W 6'D 2:1 SS	1960	1937	CP17	C1SDN3	1.53	0.80
0148	E	5: 8' X 4' RCBC @ Robert Way	120	1832	CP16	C1SDN3	1.42	1.00
0150	E	Earth Chnl 80'-90'W 5'D 2:1 SS with Drop Structures	1745	1832	CP16	C1SDN3	1.42	1.30
0150	P0	Conc Chnl 40'W 4'D 2:1 SS	1745	1832	CP16	C1SDN3	1.42	1.30
C1CH		C-1 CHANNEL						
0040	P2	Conc Chnl 40'W 10'D 0:1 SS	4200	7324	CP61*	C1SDN4	11.92	1.00
0125	P2	Conc Chnl 40'W 10'D 0:1 SS	2100	7324	CP61*	C1SDN4	11.92	1.00
0159	E	Energy Dissipator	7324	7324	CP61*	C1SDN4	11.92	
0161	E	Earth Chnl 30'-60'W 7'-20'D with Gabion 2:1 SS	2750	7324	CP61*	C1SDN4	11.92	2.00
0161	P0	Conc Chnl 40'W 8'D 0:1 SS	2750	7325	CP61*	C1SDN4	11.92	2.00
0213	E	Energy Dissipator	7324	7324	CP61*	C1SDN4	11.92	
0215	E	2: 12' X 9' RCBC @ Lake Mead Dr	270	7324	CP61*	C1SDN4	11.92	3.20
0220	E	Conc Chnl 15'W 9'D 1:1 SS: West Floodwall	2560	7324	CP61*	C1SDN4	11.92	2.30
0269	E	Conc Chnl 15'W 7'D 2:1 SS: West Floodwall	1740	7324	CP61*	C1SDN4	11.92	2.30
0284	E	Conc Chnl 15'W 9'D 1:1 SS: West Floodwall	1760	7324	CP61*	C1SDN4	11.92	1.70
0335	E	Conc Chnl 40'W 12'D 0:1 SS	280	7324	CP61*	C1SDN4	11.92	1.20
0340	E	Conc Chnl 40'-50'W 12'D 0:1 SS	300	7324	CP61*	C1SDN4	11.92	1.20
0346	E	Conc Chnl 40'W 6'D 2:1 SS: West Floodwall	290	7324	CP61*	C1SDN4	11.92	1.20
0351	E	4: 12' X 7' RCBC @ Warm Springs Rd	100	7175	CP59	C1SDN4	11.25	1.00
0353	E	Conc Chnl 14.5'W 8'D 2:1 SS: West Floodwall	1245	6961	CPC1D	C1SDN4	10.44	0.84
0377	E	Conc Chnl 15'W 10'D 2:1 SS: West Floodwall	815	6961	CPC1D	C1SDN4	10.44	0.84
0392	E	Conc Chnl 50'W 14'D 0:1 SS	325	6961	CPC1D	C1SDN4	10.44	0.70
0398	E	Junction Structure	70	6961	CPC1D	C1SDN4	10.44	
0400	E	Conc Chnl 39.5'W 9'-14'D 0:1 SS	450	5919	CP51	C1SDN4	8.52	2.70
0408	E	Conc Chnl 25'W 9'D 2:1 SS	1650	5919	CP51	C1SDN4	8.52	2.00
0439	E	Single Span Bridge @ Burkholder Blvd	100	5919	CP51	C1SDN4	8.52	2.00
0441	E	Conc Chnl 25'W 9'D 2:1 SS	500	5666	CP27	C1SDN3	6.48	2.00
0455	E	Conc Chnl 25'W 7.5'D 2:1 SS	2895	5666	CP27	C1SDN3	6.48	2.60
0502	E	Conc Chnl 25'W 7'D 2:1 SS	1100	5666	CP27	C1SDN3	6.48	2.50
0523	E	Conc Chnl 39'W 8'D 0:1 SS with Junction Structure	310	5630	CP26	C1SDN3	6.33	2.00
0528	E	Conc Chnl 25'W 7'D 2:1 SS	1340	4876	CP23	C1SDN3	5.33	2.00
0554	E	2: 20' X 7' RCBC @ Boulder Hwy	350	4828	CPC1BH	C1SDN3	5.26	2.40
0561	P3	Conc Chnl 20'W 6'D 0:1 SS	1801	1765	CP14	C1SDN3	2.08	2.00
0600	E	3: 10' X 7' RCBC @ Horizon Dr	436	1765	CP14	C1SDN3	2.08	1.20
0603	P3	Conc Chnl 30'W 6'D 0:1 SS	520	1765	CP14	C1SDN3	2.08	5.34
0604	E	Bridge 36'W 8.5'D @ UPRR	50	1765	CP14	C1SDN3	2.08	1.00
0613	P3	Conc Chnl 12.5'W 6'D 2:1 SS	1470	1765	CP14	C1SDN3	2.08	2.40
0641	P3	Conc Chnl 12.5'W 5'D 2:1 SS	1645	1641	CP13	C1SDN3	1.84	2.70
0672	E	4: 10' X 5' RCBC @ Vermillion Dr	115	1641	CP13	C1SDN3	1.84	0.50
0674	E	Conc Chnl 25'W 6'D 2:1 SS	630	1641	CP13	C1SDN3	1.84	0.70
0686	E	NDOT Sediment Basin	1239		CP12	C1SDN3	1.43	
C1DC		C-1 CHANNEL - DRAKE CHANNEL						
0000	E	Conc Chnl 25'W 5'-14'D 0:1 SS	700	1778	CP55	C1SDN3	1.92	2.70
0013	E	Earth Chnl 10'W 5'D with Conc 2:1 SS	650	1778	CP55	C1SDN3	1.92	2.70
0013	P1	Conc Chnl 16'W 5'D 2:1 SS	650	1778	CP55	C1SDN3	1.92	2.70
0026	E	Conc Chnl 20.5'W 5'D 0:1 SS South Wall, 2:1 SS North Wall	300	1778	CP55	C1SDN3	1.92	2.70
0031	E	Conc Chnl 26'W 5'D 0:1 SS South Wall, 2:1 SS North Wall	750	1778	CP55	C1SDN3	1.92	2.70
0045	E	Junction Structure	200	1778	CP55	C1SDN3	1.92	
0049	E	2: 12' X 6' RCBC @ Racetrack Rd	92	1628	CP54	C1SDN3	1.69	0.50
0051	E	Earth Chnl 20'-50'W 20'-10'D 2:1 SS with 9'-12' Gabion Drop Structures	2640	1628	CP54	C1SDN3	1.69	0.50
0101	E	Earth Chnl 20'-50'W 20'-10'D 2:1 SS with 9'-12' Gabion Drop Structures	3660	1486	CP53	C1SDN3	1.44	0.50
0170	P1	Soil Cement Levee 7.5'	2950	1132	CP52	C1SDN3B	6.39	2.90
0226	E	Soil Cement Levee 5'	3800	1132	CP52	C1SDN3B	6.39	2.90
0298	E	48" RCPC Outlet	226	90	DB6	C1SDN3B	5.41	0.50
0302	E	20,789 cfs PMF Spillway		20789	C1-54	C1SDN3B	5.41	
0303	E	880 ac-ft East C-1 Detention Basin		3397	C1-54	C1SDN3B	5.41	

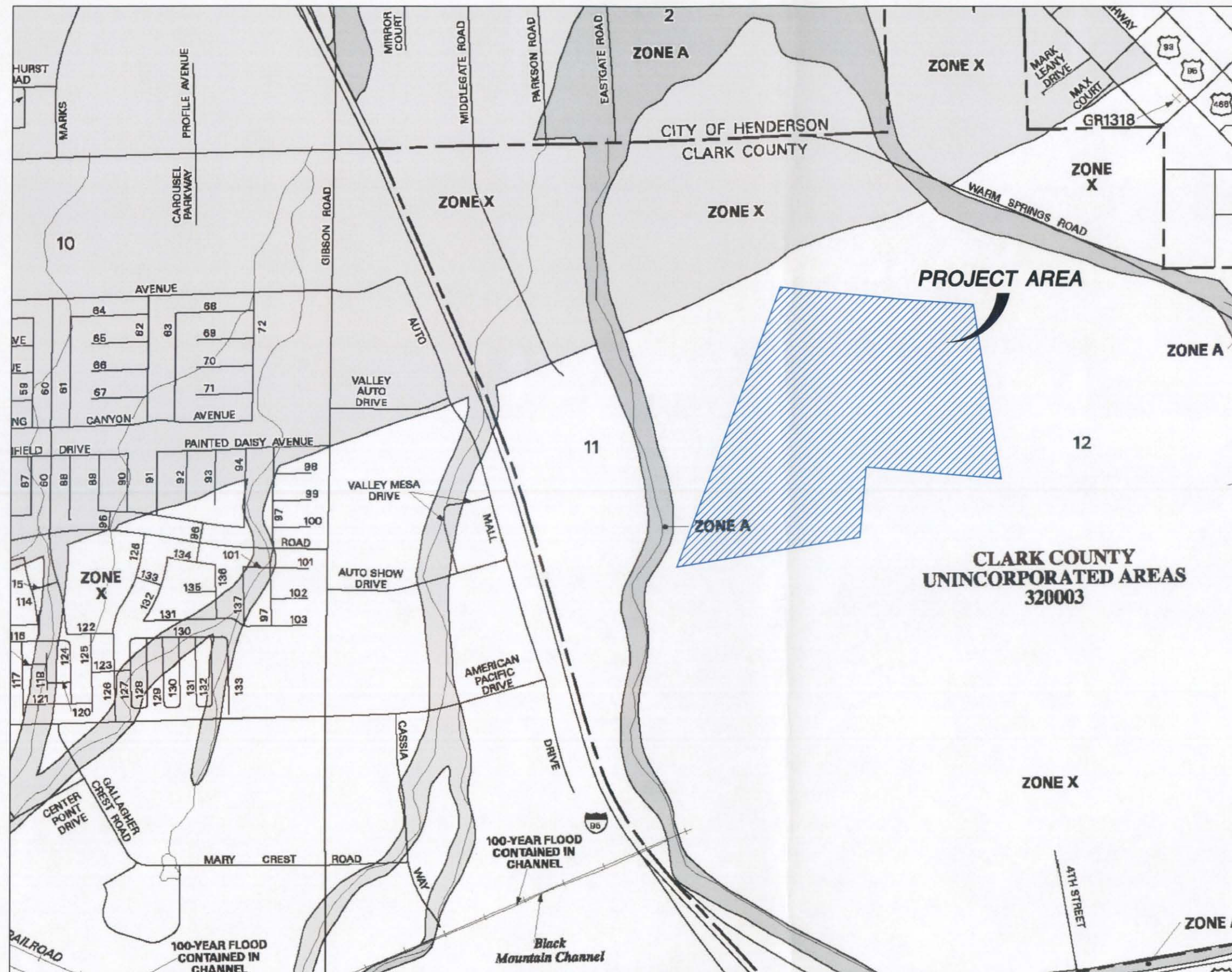
ID / River Mile	Status	Facility Description	Length (ft.)	Flow (cfs)	HEC-1 Node	HEC-1 Model	Tributary Area (sq.mi.)	Channel Slope (%) **
C1E1		C-1 CHANNEL - EQUESTRIAN TRIBUTARY 1						
0000	P1	Energy Dissipator		688	CP30	C1SDN3B	1.21	
0002	P1	Conc Chnl 10'W 4.5'D 2:1 SS	2200	688	CP30	C1SDN3B	1.21	1.40
C1EQ		C-1 CHANNEL - EQUESTRIAN D.B. OUTFALL						
0000	P1	Conc Chnl 10'W 5.5'D 2:1 SS	3920	1097	CP48	C1SDN3	1.38	1.40
0074	E	9: 45' X 29' HERCP	220	679	CP46	C1SDN3B	7.82	0.50
0078	E	Grass Chnl 40'W 4.5'D 5:1 SS	1760	679	CP46	C1SDN3B	7.82	1.50
0112	E	Earth Chnl 45'-60'W 4'D 2:1 SS with Drop Structures	1445	679	CP46	C1SDN3B	7.82	1.40
0139	E	5' X 4' RCBC	585	224	DB4	C1SDN3B	7.06	1.90
0151	E	Energy Dissipator		224	DB4	C1SDN3B	7.06	
0152	E	48" RCPC Outlet	325	224	DB4	C1SDN3B	7.06	0.40
0158	E	39,100 cfs PMF Spillway		39100	CP44	C1SDN3B	7.06	
0159	E	409 ac-ft Equestrian Detention Basin		5196	CP44	C1SDN3B	7.06	
0202	E	Conc Chnl 20'W 8.0'D 2:1 SS	5000	3115	CP38	C1SDN3B	4.35	2.40
0297	E	Rip Rap Levee 10'	9000	3115	CP38	C1SDN3B	4.35	2.00
C1FK		C-1 CHANNEL - FOUR KIDS						
0000	P2	10' X 5' RCB	770	935	CP72B	C1SDN3	1.00	2.50
0014	E	Earth Chnl 21'W 4'-5'D with Rock 0:1 SS	1280	935	CP72B	C1SDN3	1.00	1.80
0039	E	12' X 4' RCBC @ Eagle Rock Rd	70	935	CP72B	C1SDN3	1.00	2.70
0040	P1	Conc Chnl 10'W 4.5'D 2:1 SS	1760	935	CP72B	C1SDN3	1.00	2.70
0073	E	4: 6' X 3' RCBC @ Lake Mead Dr	160	721	CP72A	C1SDN3	0.78	2.00
0076	P1	Conc Chnl 10'W 5'D 0:1 SS	1400	721	CP72A	C1SDN3	0.78	3.00
C1GW		C-1 CHANNEL - GREENWAY						
0000	E	16' X 6' RCBC @ Pueblo Blvd	114	920	CP25	C1SDN3	1.01	1.00
0002	E	Conc Chnl 6'W 9.5'D 1:1 SS	1170	920	CP25	C1SDN3	1.01	0.40
0024	E	2: 12' X 4' RCBC @ Boulder Hwy	200	920	CP25	C1SDN3	1.01	0.40
0028	E	Conc Chnl 15'W 4'D 1:1 SS	490	920	CP25	C1SDN3	1.01	0.40
0037	E	2: 12' X 4' RCBC	40	920	CP25	C1SDN3	1.01	0.90
0038	E	Conc Chnl 15.3'W 4.8'D 1:1 SS	450	920	CP25	C1SDN3	1.01	0.70
0047	E	2: 12' X 4' RCBC @ Mona Ln	70	568	CP24	C1SDN3	0.63	0.60
0048	E	Conc Chnl 17'W 4'D 1:1 SS	685	568	CP24	C1SDN3	0.63	1.50
0051	E	2: 12' X 4' RCBC @ Greenway Rd	190	568	CP24	C1SDN3	0.63	1.00
0064	E	Earth Chnl 16'-20'W 6'-9'D 0:1 SS	300	568	CP24	C1SDN3	0.63	1.20
0064	P0	Conc Chnl 15'W 4'D 0:1 SS	300	568	CP24	C1SDN3	0.63	1.20
0070	E	2: 12' X 4' RCBC @ Van Wagon Ave	85	568	CP24	C1SDN3	0.63	0.80
0072	E	Earth Chnl 28'W 3'-8'D 2:1 SS	470	568	CP24	C1SDN3	0.63	0.80
0072	P0	Conc Chnl 15'W 4.5'D 0:1 SS	470	568	CP24	C1SDN3	0.63	0.80
0081	E	3: 9.5' X 6.5' CMAP @ UPRR	50	568	CP24	C1SDN3	0.63	0.80
C1IT		C-1 CHANNEL - ITHACA						
0000	P1	72" RCP Outlet	6200	424	DB6	C1SDN3B	3.42	2.20
0117	P1	16,830 cfs PMF Spillway		16830	CP64	C1SDN3B	3.42	
0118	P1	310 ac-ft N.E. Detention Basin		1683	CP64	C1SDN3B	3.42	
0155	P1	Soil Cement Levee 11'	4000	1514	C1-65	C1SDN3B	2.54	3.00
0273	P1	Soil Cement Levee 11'	400	1514	C1-65	C1SDN3B	2.54	3.00
C1LM		C-1 CHANNEL - LAKE MEAD						
0000	P1	Conc Chnl 10'W 6'D 2:1 SS	2525	1385	CP71	C1SDN3	1.96	0.90
0048	P1	2: 11' X 6' RCBC @ Mohawk Dr	60	1385	CP71	C1SDN3	1.96	0.90
0049	P1	Conc Chnl 10'W 6'D 2:1 SS	1560	1385	CP71	C1SDN3	1.96	0.90
0079	P1	2: 11' X 6' RCBC @ Pawnee Ln	60	1385	CP71	C1SDN3	1.96	0.90
0083	P1	Conc Chnl 10'W 6'D 2:1 SS	570	1385	CP70	C1SDN3	1.77	0.90
0090	P1	2: 11' X 6' RCBC @ Navajo Dr	60	1305	CP70	C1SDN3	1.77	0.90
0092	P1	Conc Chnl 10'W 6'D 2:1 SS	325	1305	CP70	C1SDN3	1.77	0.90
0096	P1	2: 11' X 6' RCBC @ Shoshone Dr	60	1305	CP70	C1SDN3	1.77	0.90
0099	P1	Conc Chnl 10'W 6'D 2:1 SS	345	1305	CP70	C1SDN3	1.77	0.90
0105	P1	2: 11' X 6' RCBC @ Center St	100	1305	CP70	C1SDN3	1.77	0.90
0107	P1	Conc Chnl 10'W 6'D 2:1 SS	555	1305	CP70	C1SDN3	1.77	0.90
0118	P1	2: 11' X 6' RCBC @ Entrance	50	1305	CP70	C1SDN3	1.77	0.90
0119	P1	Conc Chnl 10'W 6'D 2:1 SS	295	1305	CP70	C1SDN3	1.77	0.90
0124	P1	2: 11' X 6' RCBC @ Entrance	50	1305	CP70	C1SDN3	1.77	0.90
0125	P1	Conc Chnl 10'W 6'D 2:1 SS	870	1305	CP70	C1SDN3	1.77	0.90
0142	P1	15' X 6' RCBC @ Warm Springs Rd	125	1054	CP69	C1SDN3	1.44	0.90
0144	P1	Conc Chnl 10'W 4.5'D 2:1 SS	655	682	CP67	C1SDN3	0.81	0.90
0156	P1	11' X 6' RCBC @ Ash St	60	682	CP67	C1SDN3	0.81	0.90
0158	P1	Conc Chnl 10'W 4.5'D 2:1 SS	1305	682	CP67	C1SDN3	0.81	0.90
0182	P1	11' X 6' RCBC @ Ivy St	60	682	CP67	C1SDN3	0.81	0.90
0184	P1	Conc Chnl 10'W 4.5'D 2:1 SS	900	682	CP67	C1SDN3	0.81	0.90

ID / River Mile	Status	Facility Description	Length (ft.)	Flow (cfs)	HEC-1 Node	HEC-1 Model	Tributary Area (sq.mi.)	Channel Slope (%) **
LLMW		LAKE LAS VEGAS - MAGIC WAY						
0003	P0	Conc Chnl 10'W 6'D 2:1 SS	6670	1932	CP60	C1SDN3	3.52	3.50
0129	E	6: 8' X 3' RCBC	160	1842	CP79	C1SDN3	3.04	1.00
0132	P0	Conc Chnl 15'W 5'D 2:1 SS	3720	1564	CP77	C1SDN3	2.30	3.10
0203	E	Conc Chnl 35'W 5'-6'D 0.5:1 SS	3000	1515	C1-85	C1SDN3	2.06	3.10
PTBR		PITTMAN WASH - BURNS						
0029	E	Rip Rap Chnl 35'W 9'D 2:1 SS	2850	5448	CPBR160	PIT3SC	5.85	0.68
0029	P1	Rip Rap Chnl 60'W 9'D 3:1 SS	2850	5448	CPBR160	PIT3SC	5.85	0.68
0090	E	2: 24' X 8.5' RCAC @ Weisner Way	190	5448	CPBR160	PIT3SC	5.85	0.90
0091	E	Conc Chnl 25'W 9'D 2:1 SS	2570	5448	CPBR160	PIT3SC	5.85	1.10
0140	E	Conc Chnl 25'W 9'D 2:1 SS	1110	5254	CPBR150	PIT3SC	5.54	0.50
0180	E	Conc Chnl 10'W 8'D 2:1 SS	210	2881	CPBR090	PIT3SC	3.19	1.00
0163	E	Conc Chnl 20'W 8'D 0:1 SS	250	2881	CPBR090	PIT3SC	3.19	1.00
0164	P1	Add 4: 16' X 4' RCBC @ Boulder Hwy	330	2881	CPBR090	PIT3SC	3.19	1.50
0165	E	2: 6' X 4' RCBC @ Boulder Hwy	330	2881	CPBR090	PIT3SC	3.19	1.50
PTGB		PITTMAN WASH - GIBSON						
0058	P1	Conc Chnl 15'W 5.5'D 2:1 SS	1560	1532	CPBR080	PIT3SC	1.76	1.50
0087	P3	2: 10' X 6' RCB	660	1532	CPBR080	PIT3SC	1.76	0.50
0093	E	Earth/Conc Chnl 8'W 5'D 2:1 SS	550	1532	CPBR080	PIT3SC	1.76	1.50
0093	P1	Conc Chnl 30'W 5'D 0:1 SS	550	1532	CPBR080	PIT3SC	1.76	1.50
PTGL		PITTMAN GAS LINE						
0000	E	72" RCP	1675	678	CPPD030	PIT3SC	0.69	3.40
PTHR		PITTMAN HORIZON RIDGE						
0000	P1	Conc Chnl 15'W 5'D 2:1 SS	2300	1652	CPPD170	PIT3SC	1.49	3.00
0043	P1	2: 12' X 6' RCBC @ UPRR	100	1371	CPPD165	PIT3SC	1.25	2.00
0044	P1	Conc Chnl 15'W 5.5'D 2:1 SS	1250	1371	CPPD165	PIT3SC	1.25	1.20
0049	E	12' X 5' RCBC @ Lake Mead Dr	150	1345	CPPD160	PIT3SC	1.20	1.20
0067	E	8' X 5' RCB	1800	1345	CPPD160	PIT3SC	1.20	2.60
0104	P1	Conc Chnl 15'W 4.5'D 2:1 SS	1825	1345	CPPD160	PIT3SC	1.20	4.90
0139	E	36" RCP @ Horizon Ridge Pkwy	100	1065	CPPD135	PIT3SC	0.89	7.00
0139	P1	12' X 6' RCBC @ Horizon Ridge Pkwy	100	1065	CPPD135	PIT3SC	0.89	7.00
0140	P1	Conc Chnl 15'W 4'D 2:1 SS	3425	1065	CPPD135	PIT3SC	0.89	4.00
0203	P1	84" RCP Outlet	200	882	CPPD125	PIT3SC	0.72	4.00
0204	P1	882 cfs Spillway		882	CPPD125	PIT3SC	0.72	
0205	P1	2.5 ac-ft Pittman Horizon Ridge Debris Basin		882	CPPD125	PIT3SC	0.72	
0210	E	Natural Wash	2950	882	CPPD125	PIT3SC	0.72	7.00
PTIS		PITTMAN WASH - INTERSTATE						
0000	P1	Conc Chnl 30'W 6'D 2:1 SS	2100	4530	CPPD150	PIT3SC	5.90	3.00
0007	P1	4: 14' X 6' RCBC @ I-15	200	4530	CPPD150	PIT3SC	5.90	1.40
0008	P1	Conc Chnl 30'W 6.5'D 2:1 SS	150	4530	CPPD150	PIT3SC	5.90	1.40
0014	P1	4: 14' X 6' RCBC @ I-15	150	4530	CPPD150	PIT3SC	5.90	1.40
0015	P1	Conc Chnl 30'W 6.5'D 2:1 SS	250	4261	CPPD150	PIT3SC	5.24	1.40
0023	E	Conc Chnl 40'W 7'D 2:1 SS	110	3497	CPPD140	PIT3SC	3.68	3.00
0026	E	4: 8' X 8' RCBC @ I-15	350	3497	CPPD140	PIT3	3.68	2.80
0029	E	Conc Chnl 30'W 5'D 2:1 SS	1100	2520	CPPD070	PIT3	2.57	3.00
0050	E	Conc Chnl 30'W 5'D 2:1 SS	380	2520	CPPD070	PIT3SC	2.57	3.00
0055	E	2: 7' X 7' RCBC @ UPRR	1000	2520	CPPD070	PIT3SC	2.57	3.00
0056	E	Conc Chnl 30'W 5'D 2:1 SS	650	2520	CPPD070	PIT3SC	2.57	3.80
0066	E	Rip Rap Chnl 35'W 6'D 2:1 SS	1000	2520	CPPD070	PIT3SC	2.57	1.10
0087	E	Conc Chnl 35'W 6'D 2:1 SS	800	2380	CPPD060	PIT3SC	2.36	2.50
0102	E	Rip Rap Chnl 35'W 6'D 2:1 SS	3390	2380	CPPD060	PIT3SC	2.36	1.10
0166	E	2: 6' X 6' RCB	950	1365	CPPD045	PIT3SC	1.17	3.50
0184	E	Conc Chnl 9'W 4'D 3:1 SS	750	1962	CPPD050	PIT3SC	1.86	5.00
0197	E	3: 60" RCP @ Horizon Ridge Pkwy	150	681	CPPD030	PIT3SC	0.69	3.00
0198	E	Conc Chnl 10'W 4'D 2:1 SS	3150	681	CPPD030	PIT3SC	0.69	1.30









**FIRM**  
FLOOD INSURANCE RATE MAP  
CLARK COUNTY,  
NEVADA AND  
INCORPORATED AREAS

PANEL 2595 OF 4090

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:	COMMUNITY:	NUMBER:	PANEL:	SUFFIX:
HENDERSON CITY OF CLARK COUNTY, UNINCORPORATED AREAS	320003	2595	E	
	320003	2595	E	

Notes to Users: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.



MAP NUMBER  
32003C2595 E

MAP REVISED:  
SEPTEMBER 27, 2002

Federal Emergency Management Agency



**GRAPHIC SCALE**



(IN FEET)  
1 inch = 1000 ft.

511693.19

SEPTEMBER 2006

**FIGURE 3  
FEMA MAP**

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



2270 Corporate Circle  
Suite 100  
Henderson, Nevada 89074-6382  
Telephone: 702/263-7275  
Fax: 702/263-7200

ENGINEERING • PLANNING • SURVEYING • CONSTRUCTION SERVICES



## **Appendix B: Hydrologic Calculations**



## **Appendix B-1: Existing Condition Hydrology**



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

PBS&J

File: TDS-Standard Form 4.xls

EASTSIDE LANDFILL

Existing Condition Hydrology

BY:

DATE:

KP

10/5/06

SUB-BASIN DATA						INITIAL / OVERLAND TIME (Ti)			TRAVEL TIME (Tt)					Tc	Tc Check	Tlag	REMARKS
DESIG:	DEV/JUN. (D or U)	CN	K	AREA Ac	AREA Mi^2	INITIAL LENGTH Feet	SLOPE %	Ti Min	TRAVEL LENGTH Feet	SLOPE %	V1 VELOCITY FPS	V2 VELOCITY FPS	Tt Min	Min (13)	Min (14)	Tlag= 0.6Tc/60 Hours	
(1)			(2)	(3)		(4)	(5)	(6)	(7)	(8)	(9a)	(9b)	(10)				
ONEX1	U	81.9	0.6911	32.76	0.0512	252	4.0	7.4	2082	1.4	1.78	3.5	12.2	19.5	N/A	0.20	
ONEX2	U	86.7	0.7544	28.77	0.0450	300	5.0	6.3	2415	0.8	1.35	2.7	18.1	24.4	N/A	0.24	
ONEX3	U	91.0	0.8112	22.12	0.0346	200	2.5	5.4	711	3.0	2.56	5.1	3.9	9.4	N/A	0.09	
ONEX4	U	87.3	0.7624	28.27	0.0442	300	4.8	6.2	1751	1.5	1.82	3.6	10.4	16.6	N/A	0.17	
ONEX5	U	91.0	0.8112	1.06	0.0017	50	1.3	3.4	453	1.9	2.05	4.1	3.7	7.0	N/A	0.07	
OFFEX1	U	77.6	0.6343	42.20	0.0659	278	2.5	10.3	2213	2.0	2.09	4.1	10.9	21.1	N/A	0.21	
OFFEX2	U	78.5	0.6462	9.63	0.0150	195	3.6	7.4	942	1.8	1.99	3.9	6.1	13.5	N/A	0.14	
OFFEX3	U	82.0	0.6924	16.40	0.0256	300	0.3	18.3	1245	1.7	1.92	3.8	7.6	25.9	N/A	0.26	
OFFEX4	U	85.0	0.7320	7.61	0.0119	300	1.0	11.5	750	1.9	2.02	4.0	5.2	16.6	N/A	0.17	
OFFEX5	U	85.0	0.7320	5.11	0.0080	300	1.3	10.4	625	1.6	1.87	3.7	5.0	15.4	N/A	0.15	
Tc = Ti + Tt Ti = 1.8 (1.1 - K) L^1/2 / S^1/3 K = 0.0132 (CN) - 0.39 Tc Check = L/180+10 Tlag = 0.6 Tc Tt = 500/V1+ (Travel Length-500)/V2						Eqn. 601 Eqn. 602 Eqn. 603 Eqn. 604 Eqn. 612			For the travel time (Tt) calculations (Sec. 602.1), V1 applies to the first 500 feet of travel distance; V2 applies to the remaining travel distance.  Min Tc = 10 mins for undeveloped basins Min Tc = 5 mins for developed basins			Undeveloped V1 = 14.8*(S/100)^1/2  Undeveloped V2 = 29.4*(S/100)^1/2		Developed V1 = 20.2*(S/100)^1/2  Developed V2 = 30.6*(S/100)^1/2			
REFERENCE :														STANDARD FORM 4			



```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 05OCT06 TIME 19:48:16
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS-WRITE STAGE FREQUENCY,

DSS-READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*** FREE ***
*DIAGRAM
1 ID EASTSIDE LANDFILL IMPROVEMENTS
2 ID EXISTING CONDITION MODEL
3 ID INPUT FILE = EXISTING_SDN3.DAT
4 ID SEPTEMBER 2006
5 ID DESIGN STORM = 100-YEAR 6-HR STORM
6 ID STORM DISTRIBUTION = SDN #3
7 ID MODELED BY PBS&J
8 ID
9 IT 5 0 0 300
10 IN 5 0 0
11 IO 5
12 JR PREC 1.00 0.60 0.58
*
13 KK ONEX1
14 KM EXISTING ONSITE BASIN
15 BA 0.0512
16 PB 2.79
17 PC .000 .020 .057 .070 .087 .108 .124 .130 .130 .130
18 PC .130 .130 .130 .133 .140 .142 .148 .158 .172 .181
19 PC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
20 PC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
21 PC .499 .590 .710 .744 .781 .812 .819 .835 .851 .856
22 PC .860 .868 .876 .888 .910 .926 .937 .950 .970 .976
23 PC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
24 PC .998 .999 1.00
25 LS 0 81.9
26 UD 0.20
*
27 KK OFFEX1
28 KM EXISTING OFFSITE BASIN
29 BA 0.0659
30 LS 0 77.6
31 UD 0.21
*
32 KKROFF1-ON1
33 KM ROUTE OFFEX1 FLOW TO CP-1
34 RK 2250 0.016 0.030 0 TRAP 15 3
*
35 KK OFFEX2
36 KM EXISTING OFFSITE BASIN
37 BA .0150
38 LS 0 78.5
39 UD 0.14
*

```

1 HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 KKROFF2-CP1
41 KM ROUTE OFFEX2 FLOW TO CP-1
42 RK 2070 0.020 0.030 0 TRAP 15 3
*
43 KK CP-1
44 KM COMBINE ONEX1 AND OFFEX1
45 HC 3
*
46 KKRCPI-C18
47 KM ROUTE CP-1 FLOW TO C18
48 RK 705 0.008 0.030 0 TRAP 20 3
*
*****
* Referenced from PBSJ
* "Addendum #1 to the Technical Drainage Study for Henderson Commerce
* Center Two (Formerly known as HARSCH)" (February 2003)
*
*****
49 KK OFFD-14
50 KM OFSITE DEVELOPED BASIN OFFD-14
51 KM REFERENCED FROM EG02
52 BA 0.0028
53 PB 2.79
54 LS 0 88

```



1

HEC-1 INPUT

PAGE 3

69	KK	RT-14							
70	KM	ROUTE C15 THROUGH BMIC-2							
71	RK	450	0.018	0.013	0	TRAP	15	10	
	*								
72	KK	BMIC-2							
73	KM	ONSITE DEVELOPED BASIN BMIC-2							
74	KM	REFERENCED FROM EG02							
75	BA	0.0118							
76	PB	2.79							
77	LS	0	92						
78	UD	0.073							

79	KK	C16					
80	KM	COMBINE RT-14 AND EMIC-2					
81	HC	2					
	*						
82	KK	RT-15					
83	KM	ROUTE C16 THROUGH SCH-2					
84	RK	400 0.019 0.013	0	TRAP	15	10	
	*						
85	KK	SCH-2					
86	KM	ONSITE DEVELOPED BASIN SCH-2					
87	KM	REFERENCED FROM EG02					
88	BA	0.0065					
89	PB	2.79					
90	LS	0	92				
91	UD	0.060					

92	KK	C17							
93	KM	COMBINE RT-15 AND SCH-2							
94	HC	2							
	*								
95	KK	RT-16							
96	KM	ROUTE C17 THROUGH BMIC-3							
97	RK	750 0.013 0.013	0	TRAP	15	10			

98	KK	EMIC-3	
99	KM	ONSITE DEVELOPED BASIN EMIC-3	
100	KM	REFERENCED FROM EG02	
101	BA	0.0106	
102	PB	2.79	
103	LS	0	92
104	UD	0.062	

1

HEC-1 INPUT

PAGE 4

105	KK	MGDEV-2	
106	KM	MILGARD MANUFACTURING ONSITE BASIN	
107	KM	REFERENCED FROM EG02	
108	BA	0.0093	
109	PE	2.79	
110	LS	0	92
111	UD	0.075	

112 KK C18  
113 KM COMBINE RT-16, BMIC-3, MGDEV-2 AND CP-1  
114 HC 4

115	KK	ONEX2	
116	KM	EXISTING	ONSITE BASIN
117	BA	.0450	
118	PB	2.79	
119	LS	0	86.7
120	UD	0.24	

\*\*\*\*\*  
 \* Referenced from PBSJ  
 \* "Addendum #1 to the Technical Drainage Study for Henderson Commerce  
 \* Center Two (Formerly known as HARSH)" (February 2003)  
 \* \*\*\*\*\*

121	KK	HR3	
122	KM	HARSCH	ONSITE BASIN
123	BA	0.0014	
124	PE	2.79	
125	LS	0	92
126	UD	0.049	



127 KK HR2  
128 KM HARSHCH ONSITE BASIN  
129 BA 0.0016  
130 PB 2.79  
131 LS 0 98  
132 UD 0.037  
\*

133 KK HR1  
134 KM HARSHCH ONSITE BASIN  
135 BA 0.0015  
136 PB 2.79  
137 LS 0 92  
138 UD 0.05  
\*

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

139 KK CHR1  
140 KM COMBINE HR3, HR2, HR1  
141 KM THESE FLOWS ARE DISCHARGED INTO THE ONSITE  
142 KM STORM DRAIN SYSTEM LABELED ALIGNMENT "H1"  
143 KM ON FIGURE 7  
144 HC 3  
\*  
\*\*\*\*\*  
\*

145 KK C18B  
146 KM COMBINE C18, CHR1 AND ONEX2  
147 HC 3  
\*

148 KK ONEX4  
149 KM EXISTING ONSITE BASIN  
150 BA .0442  
151 PB 2.79  
152 LS 0 87.3  
153 UD 0.17  
\*

154 KK OFFEX5  
155 KM EXISTING OFFSITE BASIN  
156 BA .0080  
157 LS 0 85.0  
158 UD 0.15  
\*

159 KKROFF5-CP3  
160 KM ROUTE OFFEX5 FLOW TO CP-3  
161 RK 1692 0.019 0.030 0 TRAP 10 3  
\*

162 KK CP-3  
163 KM COMBINE ONEX4 AND OFFEX5  
164 HC 2  
\*

165 KK ONEX3  
166 KM EXISTING ONSITE BASIN  
167 BA .0346  
168 PB 2.79  
169 LS 0 91.0  
170 UD 0.09  
\*

171 KK OFFEX4  
172 KM EXISTING OFFSITE BASIN  
173 BA .0119  
174 LS 0 85.0  
175 UD 0.17  
\*

1

HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

176 KK OFFEX3  
177 KM EXISTING OFFSITE BASIN  
178 BA .0256  
179 PB 2.79  
180 LS 0 82.0  
181 UD 0.26  
\*

182 KK ONEX5  
183 KM EXISTING ONSITE BASIN  
184 BA .0017  
185 LS 0 91.0  
186 UD 0.07  
\*

187 KK CP-2  
188 KM COMBINE OFFEX3 AND ONEX5  
189 HC 2  
\*

190 KKROFFEX3POND  
191 KM COLLECTS FLOW FROM OFFEX3 AND ONEX5  
192 RS 1 STOR -1  
193 SV 0 0.47 1.37 2.71 4.52  
194 SE 1766 1767 1768 1769 1770  
195 SQ 0 0.01 0.02 0.03 0.04  
\*

196 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
13 ONEX1  
.  
.  
27 OFFEX1  
.  
V  
V



```

32      .      ROFF1-ON
35      .      .      OFFEX2
36      .      .      V
40      .      .      ROFF2-CP
41      .      .      V
43      CP-1.....
44      .      V
45      .      V
46      RCP1-C18
47      .      .
49      .      OFFD-14
50      .      .      V
51      .      .      V
56      .      RT-B14
57      .      .
58      .      .
59      .      .      EMIC-1
60      .      .      V
61      .      .      V
66      .      C15.....
67      .      .      V
68      .      .      V
69      .      RT-14
70      .      .
71      .      .
72      .      .      EMIC-2
73      .      .      V
74      .      .      V
79      .      C16.....
80      .      .      V
81      .      .      V
82      .      RT-15
83      .      .
84      .      .
85      .      .      SCH-2
86      .      .      V
87      .      .      V
92      .      C17.....
93      .      .      V
94      .      .      V
95      .      RT-16
96      .      .
97      .      .
98      .      .      EMIC-3
99      .      .      V
100     .      .      V
105     .      .      MGDEV-2
106     .      .      V
107     .      .      V
112     C18.....
113     .      .
115     .      ONEX2
116     .      .
121     .      .      HR3
122     .      .      V
123     .      .      V
127     .      .      HR2
128     .      .      V
129     .      .      V
133     .      .      HR1
134     .      .      V
135     .      .      V
139     .      .      CHR1.....
140     .      .      V
141     .      .      V
145     C18B.....
146     .      .
148     .      ONEX4
149     .      .
150     .      .
154     .      .      OFFEX5
155     .      .      V
156     .      .      V
159     .      .      ROFF5-CP
160     .      .      V
161     .      .      V
162     .      CP-3.....
163     .      .
164     .      .
165     .      .      ONEX3
166     .      .      V
167     .      .      V
171     .      .      OFFEX4
172     .      .      V
173     .      .      V
176     .      .      OFFEX3
177     .      .      V
178     .      .      V
182     .      .      ONEX5
183     .      .      V
184     .      .      V
187     .      .      CP-2.....
188     .      .      V
189     .      .      V
190     .      .      OFFEX3PO

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
* RUN DATE 05OCT06 TIME 19:48:16
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*****

```



EXISTING CONDITION MODEL  
INPUT FILE = EXISTING\_SDN3.DAT  
SEPTEMBER 2006  
DESIGN STORM = 100-YEAR 6-HR STORM  
STORM DISTRIBUTION = SDN #3  
MODELED BY PBS&J

11 IO      OUTPUT CONTROL VARIABLES  
            IPRNT            5    PRINT CONTROL  
            IPLOT            0    PLOT CONTROL  
            QSCAL            0.    HYDROGRAPH PLOT SCALE

IT          HYDROGRAPH TIME DATA  
            NMIN            5    MINUTES IN COMPUTATION INTERVAL  
            IDATE            1    0    STARTING DATE  
            ITIME            0000    STARTING TIME  
            NQ                300    NUMBER OF HYDROGRAPH ORDINATES  
            NDDATE           2    0    ENDING DATE  
            NDTIME           0055    ENDING TIME  
            ICENT            19    CENTURY MARK

            COMPUTATION INTERVAL    .08 HOURS  
            TOTAL TIME BASE        24.92 HOURS

ENGLISH UNITS  
DRAINAGE AREA            SQUARE MILES  
PRECIPITATION DEPTH      INCHES  
LENGTH, ELEVATION        FEET  
FLOW                      CUBIC FEET PER SECOND  
STORAGE VOLUME            ACRE-Feet  
SURFACE AREA              ACRES  
TEMPERATURE               DEGREES FAHRENHEIT

JP          MULTI-PLAN OPTION  
            NPLAN            1    NUMBER OF PLANS

JR          MULTI-RATIO OPTION  
            RATIOS OF PRECIPITATION  
            1.00            .60            .58

\*\*\* FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION		
					RATIO 1 1.00	RATIO 2 .60	RATIO 3 .58
HYDROGRAPH AT	ONEX1	.05	1	FLOW	47.	17.	16.
+				TIME	3.67	3.67	3.67
HYDROGRAPH AT	OFFEX1	.07	1	FLOW	48.	14.	13.
+				TIME	3.67	3.67	3.67
ROUTED TO	ROFF1-ON	.07	1	FLOW	47.	14.	12.
+				TIME	3.75	3.83	3.83
HYDROGRAPH AT	OFFEX2	.01	1	FLOW	13.	4.	4.
+				TIME	3.58	3.58	3.58
ROUTED TO	ROFF2-CP	.01	1	FLOW	13.	4.	4.
+				TIME	3.67	3.75	3.75
3 COMBINED AT	CP-1	.13	1	FLOW	105.	33.	30.
+				TIME	3.67	3.75	3.75
ROUTED TO	RCPI-C18	.13	1	FLOW	101.	32.	29.
+				TIME	3.67	3.75	3.83
HYDROGRAPH AT	OFFD-14	.00	1	FLOW	3.	2.	1.
+				TIME	3.58	3.67	3.67
ROUTED TO	RT-B14	.00	1	FLOW	3.	1.	1.
+				TIME	3.67	3.67	3.67
HYDROGRAPH AT	BMIC-1	.01	1	FLOW	26.	13.	12.
+				TIME	3.50	3.50	3.50
2 COMBINED AT	C15	.02	1	FLOW	28.	14.	13.
+				TIME	3.50	3.50	3.50
ROUTED TO	RT-14	.02	1	FLOW	27.	13.	13.
+				TIME	3.50	3.50	3.50
HYDROGRAPH AT	BMIC-2	.01	1	FLOW	22.	11.	11.
+				TIME	3.50	3.50	3.50
2 COMBINED AT	C16	.03	1	FLOW	50.	25.	24.
+				TIME	3.50	3.50	3.50
ROUTED TO	RT-15	.03	1	FLOW	49.	24.	23.
+				TIME	3.50	3.50	3.50
HYDROGRAPH AT	SCH-2	.01	1	FLOW	13.	7.	6.
+				TIME	3.50	3.50	3.50



2 COMBINED AT	C17	.04	1	FLOW	61.	31.	29.
+				TIME	3.50	3.50	3.50
ROUTED TO	RT-16	.04	1	FLOW	59.	29.	27.
+				TIME	3.50	3.50	3.50
HYDROGRAPH AT	EMIC-3	.01	1	FLOW	21.	11.	10.
+				TIME	3.50	3.50	3.50
HYDROGRAPH AT	MSDEV-2	.01	1	FLOW	17.	9.	8.
+				TIME	3.50	3.50	3.50
4 COMBINED AT	C18	.19	1	FLOW	162.	57.	53.
+				TIME	3.58	3.58	3.50
HYDROGRAPH AT	ONEX2	.05	1	FLOW	49.	21.	20.
+				TIME	3.67	3.67	3.67
HYDROGRAPH AT	HR3	.00	1	FLOW	3.	1.	1.
+				TIME	3.50	3.50	3.50
HYDROGRAPH AT	HR2	.00	1	FLOW	4.	2.	2.
+				TIME	3.50	3.50	3.50
HYDROGRAPH AT	HR1	.00	1	FLOW	3.	2.	2.
+				TIME	3.50	3.50	3.50
3 COMBINED AT	CHR1	.00	1	FLOW	10.	5.	5.
+				TIME	3.50	3.50	3.50
3 COMBINED AT	C18B	.24	1	FLOW	212.	78.	73.
+				TIME	3.58	3.67	3.58
HYDROGRAPH AT	ONEX4	.04	1	FLOW	56.	25.	23.
+				TIME	3.58	3.58	3.58
HYDROGRAPH AT	OFFEX5	.01	1	FLOW	10.	4.	4.
+				TIME	3.58	3.58	3.58
ROUTED TO	ROFF5-CP	.01	1	FLOW	9.	4.	3.
+				TIME	3.67	3.67	3.67
2 COMBINED AT	CP-3	.05	1	FLOW	65.	27.	26.
+				TIME	3.58	3.58	3.58
HYDROGRAPH AT	ONEX3	.03	1	FLOW	59.	29.	28.
+				TIME	3.50	3.50	3.50
HYDROGRAPH AT	OFFEX4	.01	1	FLOW	14.	6.	5.
+				TIME	3.58	3.58	3.58
HYDROGRAPH AT	OFFEX3	.03	1	FLOW	21.	8.	7.
+				TIME	3.67	3.75	3.75
HYDROGRAPH AT	ONEX5	.00	1	FLOW	3.	2.	1.
+				TIME	3.50	3.50	3.50
2 COMBINED AT	CP-2	.03	1	FLOW	23.	8.	8.
+				TIME	3.67	3.75	3.75
ROUTED TO	OFFEX3PO	.03	1	FLOW	0.	0.	0.
+				TIME	5.92	5.33	5.42

\*\* PEAK STAGES IN FEET \*\*

1	STAGE	1768.34	1767.24	1767.18
	TIME	6.67	6.58	6.67

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR PLAN = 1 RATIO= 1.00									
ROFF1-ON	MANE	2.18	46.96	222.91	.96	5.00	46.94	225.00	.96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3375E+01 EXCESS= .0000E+00 OUTFLOW= .3380E+01 BASIN STORAGE= .3651E-05 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .60
ROFF1-ON MANE 3.08 13.76 228.58 .30 5.00 13.59 230.00 .30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1061E+01 EXCESS= .0000E+00 OUTFLOW= .1065E+01 BASIN STORAGE= .3304E-05 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .58
ROFF1-ON MANE 3.12 12.50 227.50 .28 5.00 12.40 230.00 .28

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9696E+00 EXCESS= .0000E+00 OUTFLOW= .9733E+00 BASIN STORAGE= .3663E-05 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= 1.00
ROFF2-CP MANE 2.57 13.17 219.45 1.01 5.00 13.07 220.00 1.01



CONTINUITY SUMMARY (AC-FT) - INFLOW= .8075E+00 EXCESS= .0000E+00 OUTFLOW= .8108E+00 BASIN STORAGE= .2611E-05 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .60  
ROFF2-CP MANE 3.75 3.97 225.11 .33 5.00 3.97 225.00 .33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2625E+00 EXCESS= .0000E+00 OUTFLOW= .2649E+00 BASIN STORAGE= .1921E-05 PERCENT ERROR= -.9

FOR PLAN = 1 RATIO= .58  
ROFF2-CP MANE 3.93 3.71 222.59 .30 5.00 3.61 225.00 .30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2406E+00 EXCESS= .0000E+00 OUTFLOW= .2435E+00 BASIN STORAGE= .2215E-05 PERCENT ERROR= -1.2

FOR PLAN = 1 RATIO= 1.00  
RCP1-C18 MANE .77 104.64 221.47 1.06 5.00 101.21 220.00 1.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7492E+01 EXCESS= .0000E+00 OUTFLOW= .7497E+01 BASIN STORAGE= .6376E-05 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .60  
RCP1-C18 MANE 1.09 32.76 226.76 .36 5.00 31.80 225.00 .36

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2533E+01 EXCESS= .0000E+00 OUTFLOW= .2534E+01 BASIN STORAGE= .6774E-05 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .58  
RCP1-C18 MANE 1.10 29.80 226.94 .33 5.00 28.60 230.00 .33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2330E+01 EXCESS= .0000E+00 OUTFLOW= .2331E+01 BASIN STORAGE= .6358E-05 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= 1.00  
RT-B14 MANE 1.36 3.39 218.69 1.64 5.00 3.37 220.00 1.63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2438E+00 EXCESS= .0000E+00 OUTFLOW= .2442E+00 BASIN STORAGE= .7570E-08 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .60  
RT-B14 MANE 1.71 1.51 223.43 .71 5.00 1.50 220.00 .71

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1061E+00 EXCESS= .0000E+00 OUTFLOW= .1063E+00 BASIN STORAGE= .7638E-08 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .58  
RT-B14 MANE 1.76 1.42 222.80 .67 5.00 1.41 220.00 .67

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9979E-01 EXCESS= .0000E+00 OUTFLOW= .9993E-01 BASIN STORAGE= .5886E-08 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= 1.00  
RT-14 MANE .37 27.93 210.77 1.91 5.00 27.32 210.00 1.91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1720E+01 EXCESS= .0000E+00 OUTFLOW= .1721E+01 BASIN STORAGE= .7751E-08 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .60  
RT-14 MANE .42 13.81 211.01 .91 5.00 13.40 210.00 .91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8203E+00 EXCESS= .0000E+00 OUTFLOW= .8205E+00 BASIN STORAGE= .6549E-08 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .58  
RT-14 MANE .41 13.17 210.75 .86 5.00 12.73 210.00 .86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7778E+00 EXCESS= .0000E+00 OUTFLOW= .7780E+00 BASIN STORAGE= .6560E-08 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= 1.00  
RT-15 MANE .36 49.16 210.62 1.93 5.00 48.56 210.00 1.94

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2959E+01 EXCESS= .0000E+00 OUTFLOW= .2959E+01 BASIN STORAGE= .9128E-08 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .60  
RT-15 MANE .35 24.51 210.82 .93 5.00 24.04 210.00 .93

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1419E+01 EXCESS= .0000E+00 OUTFLOW= .1420E+01 BASIN STORAGE= .8611E-08 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .58  
RT-15 MANE .35 23.31 210.84 .88 5.00 22.85 210.00 .88

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1347E+01 EXCESS= .0000E+00 OUTFLOW= .1347E+01 BASIN STORAGE= .8421E-08 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= 1.00  
RT-16 MANE .53 60.94 211.13 1.94 5.00 58.94 210.00 1.95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3645E+01 EXCESS= .0000E+00 OUTFLOW= .3647E+01 BASIN STORAGE= .3120E-07 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .60  
RT-16 MANE .65 30.36 211.36 .93 5.00 28.90 210.00 .93

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1751E+01 EXCESS= .0000E+00 OUTFLOW= .1752E+01 BASIN STORAGE= .3374E-07 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .58  
RT-16 MANE .62 28.82 211.06 .89 5.00 27.44 210.00 .89



CONTINUITY SUMMARY (AC-FT) - INFLOW= .1661E+01 EXCESS= .0000E+00 OUTFLOW= .1663E+01 BASIN STORAGE= .3305E-07 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO= 1.00							
ROFF5-CP	MANE	2.26	9.49	218.94	1.42	5.00	9.35	220.00
								1.42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6031E+00 EXCESS= .0000E+00 OUTFLOW= .6052E+00 BASIN STORAGE= .4046E-06 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO= .60							
ROFF5-CP	MANE	2.88	3.85	221.66	.57	5.00	3.73	220.00
								.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2413E+00 EXCESS= .0000E+00 OUTFLOW= .2419E+00 BASIN STORAGE= .4920E-06 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO= .58							
ROFF5-CP	MANE	2.92	3.61	221.61	.53	5.00	3.45	220.00
								.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2254E+00 EXCESS= .0000E+00 OUTFLOW= .2260E+00 BASIN STORAGE= .3400E-06 PERCENT ERROR= -.2

\*\*\* NORMAL END OF HEC-1 \*\*\*



### OFFEX3 Shallow Pondind Area

ELEVATION	AREA (ft2)	VOLUME (ft3)	VOLUME (ac-ft)	CUMULATIVE VOLUME (ac-ft)	OUTFLOW (cfs)
1766	10475	0	0.00	0.00	0
1767	30499	20487	0.47	0.47	0.01
1768	47931	39215	0.90	1.37	0.02
1769	68570	58250.5	1.34	2.71	0.03
1770	89398	78984	1.81	4.52	0.04

**Note:** Area was determined from 1' topography using AutoCAD



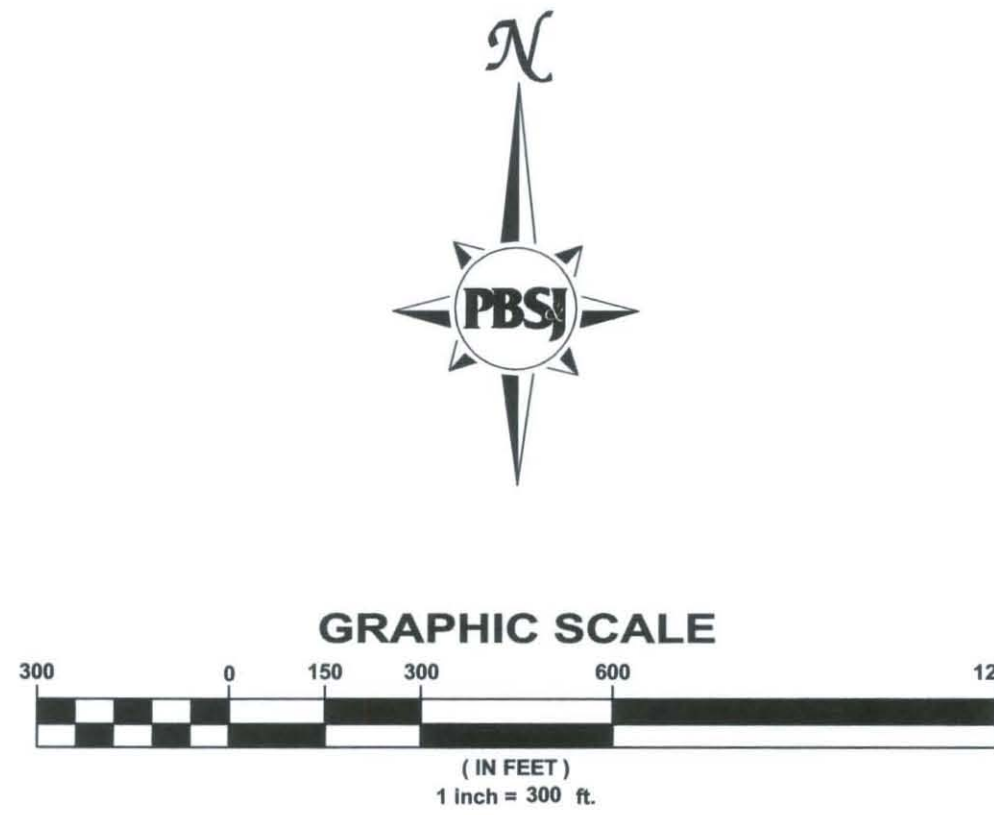


LEGEND	
	ONSITE BASIN BOUNDARY
	OFFSITE BASIN BOUNDARY
	REFERENCED BASIN BOUNDARY
<b>ONEX1</b>	ONSITE BASIN LABEL
<b>OFFEX1</b>	OFFSITE BASIN LABEL
<b>HR1</b>	REFERENCED BASIN LABEL
	HEC-1 COMBINATION POINT
	DISCHARGE POINT
	FLOW DIRECTION
	TOPOGRAPHY BOUNDARY
	EXISTING LANDFILL BOUNDARY

NOTES

\*ADDENDUM #1 TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMERCE CENTER TWO (FORMERLY KNOWN AS HARSCH)\* PREPARED BY PBS&J (FEBRUARY 2003) WAS USED FOR REFERENCED BASINS

BASIN ID	AREA (ac)	Q <sub>100</sub> (cfs)	Q <sub>10</sub> (cfs)
ONEX1	32.76	47	17
ONEX2	28.77	49	21
ONEX3	22.12	59	29
ONEX4	28.27	56	25
ONEX5	1.06	3	2
OFFEX1	42.20	48	14
OFFEX2	9.63	13	4
OFFEX3	16.40	21	8
OFFEX4	7.61	14	6
OFFEX5	5.11	10	4
CP-1	NA	105	33
CP-2	NA	23	8
CP-3	NA	65	27
C18	NA	162	57
C18B	NA	212	78



511963.19 OCTOBER 2006

**FIGURE 4  
EXISTING CONDITION  
DRAINAGE MAP**

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL

2270 Corporate Circle  
Suite 100  
Henderson, Nevada 89074-6382  
Telephone: 702/263-7275  
Fax: 702/263-7200

ENGINEERING PLANNING SURVEYING CONSTRUCTION SERVICES



## **Appendix B-2: Interim Condition Hydrology**

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# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

PBS&J  
File: TDS-Standard Form 4.xls

## EASTSIDE LANDFILL

Interim Condition Hydrology

BY:  
DATE:

KP  
10/5/06

SUB-BASIN DATA						INITIAL / OVERLAND TIME (Ti)			TRAVEL TIME (Tt)					Tc	Tc Check	Tag	REMARKS
DESIG:	DEV./UN. (D or U)	CN	K	AREA Ac (3)	AREA MI² (2)	INITIAL LENGTH Feet (4)	SLOPE % (5)	Ti Min (6)	TRAVEL LENGTH Feet (7)	SLOPE % (8)	V1 VELOCITY FPS (9a)	V2 VELOCITY FPS (9b)	Tt Min (10)	Min (13)	Min (14)	Tag= 0.6Tc/60 Hours	
(1)			(2)	(3)	(2)	(4)	(5)	(6)	(7)	(8)	(9a)	(9b)	(10)	(13)	(14)		
OND1	D	87.7	0.7676	0.94	0.0015	130	33.0	2.1	247	0.4	1.28	1.9	3.2	5.3	12.1	0.05	
OND2	D	87.7	0.7676	3.70	0.0058	137	33.0	2.2	910	0.4	1.28	1.9	10.1	12.2	15.8	0.12	
OND3	D	88.6	0.7795	1.38	0.0022	156	33.0	2.2	360	1.0	2.02	3.1	3.0	5.2	12.9	0.05	
OND4	D	89.7	0.7940	11.67	0.0182	240	2.0	6.8	1276	2.6	3.26	4.9	5.2	12.0	18.4	0.12	
OND5	D	91.0	0.8112	5.03	0.0079	300	1.7	7.6	573	1.1	2.07	3.1	4.4	12.0	14.9	0.12	
OND6	D	91.0	0.8112	9.90	0.0155	70	1.4	3.9	1407	0.6	1.56	2.4	11.7	15.6	18.2	0.16	
OND7	D	90.8	0.8086	5.87	0.0092	158	33.0	2.1	1345	1.8	2.67	4.0	6.6	8.7	18.4	0.09	
OND8	D	90.3	0.8020	14.26	0.0223	128	33.0	1.9	2382	0.4	1.28	1.9	22.7	24.6	23.9	0.24	Use Tag = 0.15 See Note
OND9	U	91.0	0.8112	1.06	0.0017	50	1.3	3.4	453	1.9	2.05	4.1	3.7	7.0	N/A	0.07	
OND10	D	91.0	0.8112	4.28	0.0067	119	33.0	1.8	1190	0.4	1.28	1.9	12.5	14.2	17.3	0.14	
OND11	D	91.0	0.8112	9.60	0.0150	220	1.6	6.6	1050	1.1	2.12	3.2	6.8	13.4	17.1	0.13	
OND12	D	91.4	0.8165	2.77	0.0043	138	33.0	1.9	610	1.5	2.47	3.7	3.9	5.7	14.2	0.06	
OND13	D	91.0	0.8112	4.70	0.0073	95	33.0	1.6	714	0.4	1.28	1.9	8.4	9.9	14.5	0.10	
OND14	U	91.0	0.8112	11.12	0.0174	122	1.0	5.7	559	5.0	3.31	6.6	2.7	8.4	N/A	0.08	
OND15	U	91.0	0.8112	21.47	0.0335	200	2.5	5.4	711	3.0	2.56	5.1	3.9	9.4	N/A	0.09	
DETPD	D	91.4	0.8165	5.14	0.0080	60	8.3	2.0	35	34.0	11.78	17.8	0.0	2.0	10.5	0.02	
OFFEX1	U	77.6	0.6343	42.20	0.0659	278	2.5	10.3	2213	2.0	2.09	4.1	10.9	21.1	N/A	0.21	
OFFEX2	U	78.5	0.6462	9.63	0.0150	195	3.6	7.4	942	1.8	1.99	3.9	6.1	13.5	N/A	0.14	
OFFEX3	U	82.0	0.6924	16.40	0.0256	300	0.3	18.3	1245	1.7	1.92	3.8	7.6	25.9	N/A	0.26	
OFFEX4	U	85.0	0.7320	7.61	0.0119	300	1.0	11.5	750	1.9	2.02	4.0	5.2	16.6	N/A	0.17	
OFFEX5	U	85.0	0.7320	5.11	0.0080	300	1.3	10.4	625	1.6	1.87	3.7	5.0	15.4	N/A	0.15	
<div> <div> <math>T_c = T_i + T_t</math>  <math>T_i = 1.8 (1.1 - K) L^{1/2} / S^{1/3}</math>  <math>K = 0.0132 (CN) - 0.39</math>  <math>T_c \text{ Check} = L/190 + 10</math>  <math>\text{Tag} = 0.6 T_c</math>  <math>T_t = 500/V1 + (\text{Travel Length} - 500)/V2</math> </div> <div> <b>Eqn. 601</b>  <b>Eqn. 602</b>  <b>Eqn. 603</b>  <b>Eqn. 604</b>  <b>Eqn. 612</b> </div> <div> For the travel time (Tt) calculations (Sec. 602.1),  V1 applies to the first 500 feet of travel distance;  V2 applies to the remaining travel distance.    Min Tc = 10 mins for undeveloped basins  Min Tc = 5 mins for developed basins </div> <div> Undeveloped <math>V1 = 14.8 \sqrt{(S/100)^{1/2}}</math>  Undeveloped <math>V2 = 29.4 \sqrt{(S/100)^{1/2}}</math> </div> <div> Developed <math>V1 = 20.2 \sqrt{(S/100)^{1/2}}</math>  Developed <math>V2 = 30.6 \sqrt{(S/100)^{1/2}}</math> </div> </div>																	

**Note:** The lag time or basin OND8 was changed to 0.15 hrs because the velocities were not accurate for the cross section. Please refer to the FlowMaster cross section located in Appendix B-3 for the time calculations.

REFERENCE :

STANDARD FORM 4



```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 27SEP06 TIME 19:18:46
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X X XXXXXXX XXXXX X
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XXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*** FREE ***
*DIAGRAM
1 ID EASTSIDE LANDFILL IMPROVEMENTS
2 ID INTERIM CONDITION MODEL
3 ID INPUT FILE = INT_SDN3.DAT
4 ID SEPTEMBER 2006
5 ID DESIGN STORM = 100-YEAR 6-HR STORM
6 ID STORM DISTRIBUTION = SDN #3
7 ID MODELED BY PBS&J
8 ID
9 ID
10 IT 5 0 0 300
11 IN 5 0 0
12 IO 5
13 JR PREC 1.00 0.60 0.58
14 *
15 KK OND9
16 KM EXISTING ONSITE BASIN
17 BA 0.0017
18 PE 2.79
19 FC .000 .020 .057 .070 .087 .108 .124 .130 .130 .130
20 PC .130 .130 .130 .133 .140 .142 .148 .158 .172 .181
21 PC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
22 PC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
23 PC .499 .590 .710 .744 .781 .812 .819 .835 .851 .856
24 PC .860 .868 .876 .888 .910 .926 .937 .950 .970 .976
25 PC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
26 PC .998 .999 1.00
27 LS 0 91.0
28 UD 0.07
29 *
30 KK OFFEX3
31 KM EXISTING OFFSITE BASIN
32 BA 0.0256
33 LS 0 82.0
34 UD 0.26
35 *
36 KK CP-7
37 KM COMBINE OND9 AND OFFD3
38 HC 2
39 *
40 KK OND6
41 KM DEVELOPED ONSITE BASIN
42 BA 0.0223
43 LS 0 90.3
44 UD 0.15
45 *

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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 KKROND8-CP-9
41 KM ROUTE OND8 TO CP-9
42 RK 1190 0.004 0.025 0 TRAP 10 3
43 *
44 KK OND10
45 KM DEVELOPED ONSITE BASIN
46 BA 0.0067
47 LS 0 91.0
48 UD 0.14
49 *
50 KK OFFEX5
51 KM EXISTING OFFSITE BASIN
52 BA 0.0080
53 LS 0 85.0
54 UD 0.15
55 *
56 KK CP-9
57 KM COMBINE RCP8-CP9, OFFD5 AND OND10
58 HC 3
59 *
60 KK RCP9-CP-10
61 KM ROUTE CP-9 TO CP-10
62 RK 725 0.015 0.015 0 TRAP 10 3

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*
59 KK OND12
60 KM DEVELOPED ONSITE BASIN
61 BA 0.0043
62 LS 0 91.4
63 UD 0.06
*

64 KK CP-10A
65 KM COMBINE CP-9 AND OND12
66 HC 2
*

67 KK OND11
68 KM DEVELOPED ONSITE BASIN
69 BA 0.0150
70 LS 0 91.0
71 UD 0.13
*

72 KK OND13
73 KM DEVELOPED ONSITE BASIN
74 BA 0.0073
75 LS 0 91.0
76 UD 0.10
*

1 HEC-1 INPUT PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

77 KK CP-10
78 KM COMBINE CP-10A, OND11 AND OND13
79 HC 3
*

80 KK EQBASIN
81 KM EQUALIZER BASIN TO SPLIT FLOW NORTH AND
82 TO THE DETENTION POND
83 RS 1 STOR -1
84 SA C 0.08 0.70 0.78 0.85 0.87 0.97
85 SE 1744.5 1745 1746 1747 1747.75 1748 1748.5
86 SQ 0 0 18 42 59 74 126
*

87 KK DIVWEIR
88 KM DIVERT FLOW FROM EQ BASIN
89 DT DVPIPE
90 DI 0 59 74 126
91 DQ 0 59 64 73
*

92 KK OND14
93 KM DEVELOPED ONSITE BASIN
94 BA 0.0174
95 LS 0 91.0
96 UD 0.08
*

97 KK CP-11
98 KM COMBINE WEIR FLOW AND OND14
99 HC 2
*

100 KK OND1
101 KM DEVELOPED ONSITE BASIN
102 BA 0.0015
103 LS 0 87.7
104 UD 0.05
*

105 KK OFFEX2
106 KM EXISTING OFFSITE BASIN
107 BA 0.0150
108 LS 0 78.5
109 UD 0.14
*

110 KK CP-1
111 KM COMBINE OND1 AND OFFD2
112 HC 2
*

1 HEC-1 INPUT PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

113 KKRCPI-CP2
114 KM ROUTE CP-1 TO CP-2
115 RK 910 0.004 0.025 0 TRAP 10 3
*

116 KK OND2
117 KM DEVELOPED ONSITE BASIN
118 BA 0.0058
119 LS 0 87.7
120 UD 0.12
*

121 KK OFFEX1
122 KM EXISTING OFFSITE BASIN
123 BA 0.0659
124 LS 0 77.6
125 UD 0.21
*

126 KK CP-2
127 KM COMBINE CP-1, OFFD1 AND OND2
128 HC 3
*

129 KKRCP2-CP-3
130 KM ROUTE
131 RK 360 0.010 0.015 0 TRAP 10 3
*

132 KK OND3
133 KM DEVELOPED ONSITE BASIN
134 BA 0.0022

```



135 LS 0 88.6  
 136 UD 0.05  
 \*  
 137 KK CP-3  
 138 KM COMBINE CP-2 AND OND3  
 139 HC 2  
 \*  
 140 KKRC3-CP4  
 141 KM ROUTE CP-3 TO CP-4  
 142 RK 1345 0.018 0.015 0 TRAP 10 3  
 \*  
 143 KK OND7  
 144 KM DEVELOPED ONSITE BASIN  
 145 BA 0.0092  
 146 LS 0 90.8  
 147 UD 0.09  
 \*

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

148 KK CP-4  
 149 KM COMBINE CP-3 AND OND7  
 150 HC 2  
 \*  
 151 KK OND4  
 152 KM DEVELOPED ONSITE BASIN  
 153 BA 0.0182  
 154 LS 0 89.7  
 155 UD 0.12  
 \*  
 156 KK OND5  
 157 KM DEVELOPED ONSITE BASIN  
 158 BA 0.0079  
 159 LS 0 91.0  
 160 UD 0.12  
 \*  
 161 KK CP-5  
 162 KM COMBINE OND4 AND OND5  
 163 HC 2  
 \*  
 164 KK OND6  
 165 KM DEVELOPED ONSITE BASIN  
 166 BA 0.0155  
 167 LS 0 91.0  
 168 UD 0.16  
 \*  
 169 KK DVPIPE  
 170 KM RETURN FLOW FROM EQ BASIN PIPE  
 171 DR DVPIPE  
 \*  
 172 KK RDVPIPE  
 173 KM ROUTE FLOW THROUGH 42" RCP  
 174 RK 1880 0.005 0.013 0 CIRC 3.5 0  
 \*  
 175 KK DETPD  
 176 KM DETENTION POND BASIN  
 177 BA 0.0080  
 178 LS 0 91.4  
 179 UD 0.05  
 \*  
 180 KK CP-6  
 181 KM COMBINE CP-4, CP-5, OND6, DVPIPE AND DETPD  
 182 HC 5  
 \*

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HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

183 KK DETPOND  
 184 KM  
 185 RS 1 STOR -1  
 186 SV 0 0.08 1.53 3.02 4.84 8.88 13.45 15.95  
 187 SE 1725.25 1726 1728 1729 1730 1732 1734 1735  
 188 SQ 0 0 22 27 32 40 46 49  
 189 KO 1  
 \*

\*\*\*\*\*  
 \* Referenced from PBSJ  
 \* "Addendum #1 to the Technical Drainage Study for Henderson Commerce  
 \* Center Two (Formerly known as HARSCH)" (February 2003)  
 \* \*\*\*\*\*

190 KK OFFD-14  
 191 KM OFSITE DEVELOPED BASIN OFFD-14  
 192 KM REFERENCED FROM EG02  
 193 BA 0.0028  
 194 PB 2.79  
 195 LS 0 88  
 196 UD 0.200  
 \*  
 197 KK RT-B14  
 198 KM ROUTE OFFD-14 THROUGH BMIC-1  
 199 RK 1050 0.014 0.013 0 TRAP 15 10  
 \*  
 200 KK BMIC-1  
 201 KM ONSITE DEVELOPED BASIN BMIC-1  
 202 KM REFERENCED FROM EG02  
 203 BA 0.0141  
 204 PB 2.79  
 205 LS 0 92  
 206 UD 0.081  
 \*



1 207 KK C15  
208 KM COMBINE RT-B14 AND BMIC-1  
209 HC 2  
\*  
210 KK RT-14  
211 KM ROUTE C15 THROUGH BMIC-2  
212 RK 450 0.018 0.013 0 TRAP 15 10  
\*  
213 KK BMIC-2  
214 KM ONSITE DEVELOPED BASIN BMIC-2  
215 KM REFERENCED FROM EG02  
216 BA 0.0118  
217 PB 2.79  
218 LS 0 92  
HEC-1 INPUT PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

219 UD 0.073  
\*

220 KK C16  
221 KM COMBINE RT-14 AND BMIC-2  
222 HC 2  
\*

223 KK RT-15  
224 KM ROUTE C16 THROUGH SCH-2  
225 RK 400 0.019 0.013 0 TRAP 15 10  
\*

226 KK SCH-2  
227 KM ONSITE DEVELOPED BASIN SCH-2  
228 KM REFERENCED FROM EG02  
229 BA 0.0065  
230 PB 2.79  
231 LS 0 92  
232 UD 0.060  
\*

233 KK C17  
234 KM COMBINE RT-15 AND SCH-2  
235 HC 2  
\*

236 KK RT-16  
237 KM ROUTE C17 THROUGH BMIC-3  
238 RK 750 0.013 0.013 0 TRAP 15 10  
\*

239 KK BMIC-3  
240 KM ONSITE DEVELOPED BASIN BMIC-3  
241 KM REFERENCED FROM EG02  
242 BA 0.0106  
243 PB 2.79  
244 LS 0 92  
245 UD 0.062  
\*

246 KK MGDEV-2  
247 KM MILGARD MANUFACTURING ONSITE BASIN  
248 KM REFERENCED FROM EG02  
249 BA 0.0093  
250 PB 2.79  
251 LS 0 92  
252 UD 0.075  
\*

1 \*\*\*\*\*  
HEC-1 INPUT PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

253 KK C18  
254 KM COMBINE RT-16, BMIC-3, BGDEV-2 AND OUTFLOW FROM DETENTION POND  
255 HC 4  
\*

\*  
\* Referenced from PBSJ  
\* "Addendum #1 to the Technical Drainage Study for Henderson Commerce  
\* Center Two (Formerly known as HARSCH)" (February 2003)  
\*  
\*\*\*\*\*

256 KK HR3  
257 KM HARSCH ONSITE BASIN  
258 BA 0.0014  
259 PB 2.79  
260 LS 0 92  
261 UD 0.049  
\*

262 KK HR2  
263 KM HARSCH ONSITE BASIN  
264 BA 0.0016  
265 PB 2.79  
266 LS 0 98  
267 UD 0.037  
\*

268 KK HR1  
269 KM HARSCH ONSITE BASIN  
270 BA 0.0015  
271 PB 2.79  
272 LS 0 92  
273 UD 0.05  
\*

274 KK CHR1  
275 KM COMBINE HR3, HR2, HR1  
276 KM THESE FLOWS ARE DISCHARGED INTO THE ONSITE  
277 KM STORM DRAIN SYSTEM LABELED ALIGNMENT "H1"  
278 KM ON FIGURE 7  
279 HC 3  
\*  
\*\*\*\*\*



280 KK C18B  
281 KM COMBINE C18 AND CHR1  
282 HC 2  
\*

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HEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

283 KK OND15  
284 KM DEVELOPED ONSITE BASIN  
285 BA 0.0335  
286 LS 0 91.0  
287 UD 0.09  
\*

288 KK OFFEX4  
289 KM EXISTING OFFSITE BASIN  
290 BA 0.0119  
291 LS 0 85.0  
292 UD 0.17  
\*

293 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

13 OND9  
.  
27 OFFEX3  
.  
32 CP-7.....  
.  
35 OND8  
V  
V  
40 ROND8-CP  
.  
43 OND10  
.  
48 OFFEX5  
.  
53 CP-9.....  
V  
V  
56 RCP9-CP-  
.  
59 OND12  
.  
64 CP-10A.....  
.  
67 OND11  
.  
72 OND13  
.  
77 CP-10.....  
V  
V  
80 EQBASIN  
.  
89 DIVWEIR -----> DVPIPE  
87  
.  
92 OND14  
.  
97 CP-11.....  
.  
100 OND1  
.  
105 OFFEX2  
.  
110 CP-1.....  
V  
V  
113 RCP1-CP2  
.  
116 OND2  
.  
121 OFFEX1  
.  
126 CP-2.....  
V  
V  
129 RCP2-CP-  
.  
132 OND3  
.  
137 CP-3.....  
V  
V  
140 RCP3-CP4  
.  
143 OND7



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148      .      .      .      .      .      .      .      .      .      .
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288      .      .      .      .      .      .      .      .      .      .

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CP-4.....

OND4

OND5

CP-5.....

OND6

DVPIPE<----- DVPIPE

DVPIPE

V

V

RDVPIPE

DETPD

CP-6.....

V

DETPOND

OFFD-14

V

RT-B14

EMIC-1

C15.....

V

RT-14

EMIC-2

C16.....

V

RT-15

SCH-2

C17.....

V

RT-16

EMIC-3

MGDEV-2

C18.....

HR3

HR2

HR1

CHR1.....

C18B.....

OND15

OFFEX4

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*      *      *
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
* VERSION 4.1
* RUN DATE 27SEP06 TIME 19:18:46
*      *      *

```

```

*      *      *
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*      *      *

```

EASTSIDE LANDFILL IMPROVEMENTS  
INTERIM CONDITION MODEL  
INPUT FILE = INT\_SDN3.DAT  
SEPTEMBER 2006  
DESIGN STORM = 100-YEAR 6-HR STORM  
STORM DISTRIBUTION = SDN #3  
MODELED BY PBS&J



```

      IPRNT      5 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

IT      HYDROGRAPH TIME DATA
      NMIN      5 MINUTES IN COMPUTATION INTERVAL
      IDATE      1 0 STARTING DATE
      ITIME      0000 STARTING TIME
      NQ      300 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE      2 0 ENDING DATE
      NDTIME      0055 ENDING TIME
      ICENT      19 CENTURY MARK

      COMPUTATION INTERVAL .08 HOURS
      TOTAL TIME BASE 24.92 HOURS

      ENGLISH UNITS
      DRAINAGE AREA      SQUARE MILES
      PRECIPITATION DEPTH INCHES
      LENGTH, ELEVATION FEET
      FLOW      CUBIC FEET PER SECOND
      STORAGE VOLUME ACRE-Feet
      SURFACE AREA ACRES
      TEMPERATURE DEGREES FAHRENHEIT

JP      MULTI-PLAN OPTION
      NPLAN      1 NUMBER OF PLANS

JR      MULTI-RATIO OPTION
      RATIOS OF PRECIPITATION
      1.00 .60 .58

*****

183 KK      *****
      * DETPOND *
      *****

189 KO      OUTPUT CONTROL VARIABLES
      IPRNT      1 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

      HYDROGRAPH ROUTING DATA

185 RS      STORAGE ROUTING
      NSTPS      1 NUMBER OF SUBREACHES
      ITYP      STOR TYPE OF INITIAL CONDITION
      RSVRIC      -1.00 INITIAL CONDITION
      X      .00 WORKING R AND D COEFFICIENT

186 SV      STORAGE      .0      .1      1.5      3.0      4.8      8.9      13.4      15.9

187 SE      ELEVATION      1725.25      1726.00      1728.00      1729.00      1730.00      1732.00      1734.00      1735.00

188 SQ      DISCHARGE      0.      0.      22.      27.      32.      40.      46.      49.

      ***

*****

HYDROGRAPH AT STATION DETPOND
PLAN 1, RATIO = 1.00

*****

DA MON HRMN ORD      OUTFLOW      STORAGE      STAGE      * DA MON HRMN ORD      OUTFLOW      STORAGE      STAGE      * DA MON HRMN ORD      OUTFLOW      STORAGE      STAGE
1      0000      1      0.      .1      1726.0 * 1      0820      101      23.      1.9      1728.2 * 1      1640      201      0.      .1      1726.0
1      0005      2      0.      .1      1726.0 * 1      0825      102      23.      1.7      1728.1 * 1      1645      202      0.      .1      1726.0
1      0010      3      0.      .1      1726.0 * 1      0830      103      22.      1.6      1728.0 * 1      1650      203      0.      .1      1726.0
1      0015      4      0.      .1      1726.0 * 1      0835      104      20.      1.4      1727.8 * 1      1655      204      0.      .1      1726.0
1      0020      5      0.      .1      1726.0 * 1      0840      105      18.      1.3      1727.7 * 1      1700      205      0.      .1      1726.0
1      0025      6      0.      .1      1726.0 * 1      0845      106      16.      1.2      1727.5 * 1      1705      206      0.      .1      1726.0
1      0030      7      0.      .1      1726.0 * 1      0850      107      15.      1.1      1727.3 * 1      1710      207      0.      .1      1726.0
1      0035      8      0.      .1      1726.0 * 1      0855      108      13.      1.0      1727.2 * 1      1715      208      0.      .1      1726.0
1      0040      9      1.      .1      1726.1 * 1      0900      109      12.      .9      1727.1 * 1      1720      209      0.      .1      1726.0
1      0045      10      1.      .1      1726.1 * 1      0905      110      11.      .8      1727.0 * 1      1725      210      0.      .1      1726.0
1      0050      11      1.      .1      1726.1 * 1      0910      111      10.      .7      1726.9 * 1      1730      211      0.      .1      1726.0
1      0055      12      1.      .1      1726.1 * 1      0915      112      9.      .6      1726.8 * 1      1735      212      0.      .1      1726.0
1      0100      13      1.      .1      1726.1 * 1      0920      113      8.      .5      1726.7 * 1      1740      213      0.      .1      1726.0
1      0105      14      1.      .1      1726.1 * 1      0925      114      7.      .4      1726.6 * 1      1745      214      0.      .1      1726.0
1      0110      15      1.      .1      1726.1 * 1      0930      115      6.      .3      1726.5 * 1      1750      215      0.      .1      1726.0
1      0115      16      1.      .2      1726.1 * 1      0935      116      6.      .2      1726.4 * 1      1755      216      0.      .1      1726.0
1      0120      17      1.      .2      1726.1 * 1      0940      117      5.      .1      1726.3 * 1      1800      217      0.      .1      1726.0
1      0125      18      1.      .2      1726.1 * 1      0945      118      5.      .1      1726.2 * 1      1805      218      0.      .1      1726.0
1      0130      19      2.      .2      1726.1 * 1      0950      119      4.      .1      1726.1 * 1      1810      219      0.      .1      1726.0
1      0135      20      2.      .2      1726.2 * 1      0955      120      4.      .1      1726.0 * 1      1815      220      0.      .1      1726.0
1      0140      21      2.      .2      1726.2 * 1      1000      121      3.      .1      1726.0 * 1      1820      221      0.      .1      1726.0
1      0145      22      3.      .3      1726.3 * 1      1005      122      3.      .1      1726.0 * 1      1825      222      0.      .1      1726.0
1      0150      23      3.      .3      1726.3 * 1      1010      123      3.      .1      1726.0 * 1      1830      223      0.      .1      1726.0
1      0155      24      4.      .3      1726.3 * 1      1015      124      2.      .1      1726.0 * 1      1835      224      0.      .1      1726.0
1      0200      25      4.      .3      1726.3 * 1      1020      125      2.      .1      1726.0 * 1      1840      225      0.      .1      1726.0
1      0205      26      4.      .3      1726.4 * 1      1025      126      2.      .1      1726.0 * 1      1845      226      0.      .1      1726.0
1      0210      27      4.      .3      1726.4 * 1      1030      127      2.      .1      1726.0 * 1      1850      227      0.      .1      1726.0
1      0215      28      4.      .4      1726.4 * 1      1035      128      2.      .1      1726.0 * 1      1855      228      0.      .1      1726.0
1      0220      29      5.      .4      1726.4 * 1      1040      129      1.      .1      1726.0 * 1      1900      229      0.      .1      1726.0
1      0225      30      5.      .4      1726.5 * 1      1045      130      1.      .1      1726.0 * 1      1905      230      0.      .1      1726.0
1      0230      31      6.      .5      1726.5 * 1      1050      131      1.      .1      1726.0 * 1      1910      231      0.      .1      1726.0
1      0235      32      6.      .5      1726.6 * 1      1055      132      1.      .1      1726.0 * 1      1915      232      0.      .1      1726.0
1      0240      33      7.      .5      1726.6 * 1      1100      133      1.      .1      1726.0 * 1      1920      233      0.      .1      1726.0
1      0245      34      7.      .6      1726.7 * 1      1105      134      1.      .1      1726.0 * 1      1925      234      0.      .1      1726.0
1      0250      35      8.      .6      1726.7 * 1      1110      135      1.      .1      1726.0 * 1      1930      235      0.      .1      1726.0
1      0255      36      8.      .6      1726.7 * 1      1115      136      1.      .1      1726.0 * 1      1935      236      0.      .1      1726.0
1      0300      37      8.      .6      1726.8 * 1      1120      137      1.      .1      1726.0 * 1      1940      237      0.      .1      1726.0
1      0305      38      9.      .7      1726.8 * 1      1125      138      1.      .1      1726.0 * 1      1945      238      0.      .1      1726.0
1      0310      39      10.      .8      1726.9 * 1      1130      139      1.      .1      1726.0 * 1      1950      239      0.      .1      1726.0
1      0315      40      13.      .9      1727.2 * 1      1135      140      0.      .1      1726.0 * 1      1955      240      0.      .1      1726.0
1      0320      41      17.      1.2      1727.6 * 1      1140      141      0.      .1      1726.0 * 1      2000      241      0.      .1      1726.0
1      0325      42      23.      1.8      1728.2 * 1      1145      142      0.      .1      1726.0 * 1      2005      242      0.      .1      1726.0
1      0330      43      25.      2.6      1728.7 * 1      1150      143      0.      .1      1726.0 * 1      2010      243      0.      .1      1726.0
1      0335      44      29.      3.6      1729.3 * 1      1155      144      0.      .1      1726.0 * 1      2015      244      0.      .1      1726.0
1      0340      45      32.      4.7      1729.9 * 1      1200      145      0.      .1      1726.0 * 1      2020      245      0.      .1      1726.0
1      0345      46      34.      5.7      1730.4 * 1      1205      146      0.      .1      1726.0 * 1      2025      246      0.      .1      1726.0
1      0350      47      35.      6.5      1730.8 * 1      1210      147      0.      .1      1726.0 * 1      2030      247      0.      .1      1726.0

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1	0355	48	37.	7.1	1731.1	*	1	1215	148	0.	.1	1726.0	*	1	2035	248	0.	.1	1726.0
1	0400	49	38.	7.7	1731.4	*	1	1220	149	0.	.1	1726.0	*	1	2040	249	0.	.1	1726.0
1	0405	50	38.	8.1	1731.6	*	1	1225	150	0.	.1	1726.0	*	1	2045	250	0.	.1	1726.0
1	0410	51	39.	8.3	1731.7	*	1	1230	151	0.	.1	1726.0	*	1	2050	251	0.	.1	1726.0
1	0415	52	39.	8.5	1731.8	*	1	1235	152	0.	.1	1726.0	*	1	2055	252	0.	.1	1726.0
1	0420	53	40.	8.7	1731.9	*	1	1240	153	0.	.1	1726.0	*	1	2100	253	0.	.1	1726.0
1	0425	54	40.	8.7	1731.9	*	1	1245	154	0.	.1	1726.0	*	1	2105	254	0.	.1	1726.0
1	0430	55	40.	8.8	1732.0	*	1	1250	155	0.	.1	1726.0	*	1	2110	255	0.	.1	1726.0
1	0435	56	40.	8.9	1732.0	*	1	1255	156	0.	.1	1726.0	*	1	2115	256	0.	.1	1726.0
1	0440	57	40.	9.0	1732.0	*	1	1300	157	0.	.1	1726.0	*	1	2120	257	0.	.1	1726.0
1	0445	58	40.	9.1	1732.1	*	1	1305	158	0.	.1	1726.0	*	1	2125	258	0.	.1	1726.0
1	0450	59	40.	9.2	1732.1	*	1	1310	159	0.	.1	1726.0	*	1	2130	259	0.	.1	1726.0
1	0455	60	41.	9.3	1732.2	*	1	1315	160	0.	.1	1726.0	*	1	2135	260	0.	.1	1726.0
1	0500	61	41.	9.4	1732.2	*	1	1320	161	0.	.1	1726.0	*	1	2140	261	0.	.1	1726.0
1	0505	62	41.	9.4	1732.2	*	1	1325	162	0.	.1	1726.0	*	1	2145	262	0.	.1	1726.0
1	0510	63	41.	9.4	1732.2	*	1	1330	163	0.	.1	1726.0	*	1	2150	263	0.	.1	1726.0
1	0515	64	41.	9.3	1732.2	*	1	1335	164	0.	.1	1726.0	*	1	2155	264	0.	.1	1726.0
1	0520	65	40.	9.2	1732.1	*	1	1340	165	0.	.1	1726.0	*	1	2200	265	0.	.1	1726.0
1	0525	66	40.	9.0	1732.1	*	1	1345	166	0.	.1	1726.0	*	1	2205	266	0.	.1	1726.0
1	0530	67	40.	8.9	1732.0	*	1	1350	167	0.	.1	1726.0	*	1	2210	267	0.	.1	1726.0
1	0535	68	40.	8.7	1731.9	*	1	1355	168	0.	.1	1726.0	*	1	2215	268	0.	.1	1726.0
1	0540	69	39.	8.5	1731.8	*	1	1400	169	0.	.1	1726.0	*	1	2220	269	0.	.1	1726.0
1	0545	70	39.	8.3	1731.7	*	1	1405	170	0.	.1	1726.0	*	1	2225	270	0.	.1	1726.0
1	0550	71	38.	8.1	1731.6	*	1	1410	171	0.	.1	1726.0	*	1	2230	271	0.	.1	1726.0
1	0555	72	38.	7.8	1731.5	*	1	1415	172	0.	.1	1726.0	*	1	2235	272	0.	.1	1726.0
1	0600	73	38.	7.6	1731.4	*	1	1420	173	0.	.1	1726.0	*	1	2240	273	0.	.1	1726.0
1	0605	74	37.	7.4	1731.3	*	1	1425	174	0.	.1	1726.0	*	1	2245	274	0.	.1	1726.0
1	0610	75	37.	7.2	1731.2	*	1	1430	175	0.	.1	1726.0	*	1	2250	275	0.	.1	1726.0
1	0615	76	36.	7.0	1731.0	*	1	1435	176	0.	.1	1726.0	*	1	2255	276	0.	.1	1726.0
1	0620	77	36.	6.7	1730.9	*	1	1440	177	0.	.1	1726.0	*	1	2300	277	0.	.1	1726.0
1	0625	78	35.	6.5	1730.8	*	1	1445	178	0.	.1	1726.0	*	1	2305	278	0.	.1	1726.0
1	0630	79	35.	6.3	1730.7	*	1	1450	179	0.	.1	1726.0	*	1	2310	279	0.	.1	1726.0
1	0635	80	34.	6.0	1730.6	*	1	1455	180	0.	.1	1726.0	*	1	2315	280	0.	.1	1726.0
1	0640	81	34.	5.8	1730.5	*	1	1500	181	0.	.1	1726.0	*	1	2320	281	0.	.1	1726.0
1	0645	82	33.	5.6	1730.4	*	1	1505	182	0.	.1	1726.0	*	1	2325	282	0.	.1	1726.0
1	0650	83	33.	5.3	1730.3	*	1	1510	183	0.	.1	1726.0	*	1	2330	283	0.	.1	1726.0
1	0655	84	33.	5.1	1730.1	*	1	1515	184	0.	.1	1726.0	*	1	2335	284	0.	.1	1726.0
1	0700	85	32.	4.9	1730.0	*	1	1520	185	0.	.1	1726.0	*	1	2340	285	0.	.1	1726.0
1	0705	86	32.	4.7	1729.9	*	1	1525	186	0.	.1	1726.0	*	1	2345	286	0.	.1	1726.0
1	0710	87	31.	4.5	1729.8	*	1	1530	187	0.	.1	1726.0	*	1	2350	287	0.	.1	1726.0
1	0715	88	30.	4.3	1729.7	*	1	1535	188	0.	.1	1726.0	*	1	2355	288	0.	.1	1726.0
1	0720	89	30.	4.1	1729.6	*	1	1540	189	0.	.1	1726.0	*	2	0000	289	0.	.1	1726.0
1	0725	90	29.	3.9	1729.5	*	1	1545	190	0.	.1	1726.0	*	2	0005	290	0.	.1	1726.0
1	0730	91	29.	3.7	1729.3	*	1	1550	191	0.	.1	1726.0	*	2	0010	291	0.	.1	1726.0
1	0735	92	28.	3.5	1729.2	*	1	1555	192	0.	.1	1726.0	*	2	0015	292	0.	.1	1726.0
1	0740	93	28.	3.3	1729.1	*	1	1600	193	0.	.1	1726.0	*	2	0020	293	0.	.1	1726.0
1	0745	94	27.	3.1	1729.0	*	1	1605	194	0.	.1	1726.0	*	2	0025	294	0.	.1	1726.0
1	0750	95	27.	2.9	1728.9	*	1	1610	195	0.	.1	1726.0	*	2	0030	295	0.	.1	1726.0
1	0755	96	26.	2.7	1728.8	*	1	1615	196	0.	.1	1726.0	*	2	0035	296	0.	.1	1726.0
1	0800	97	25.	2.5	1728.7	*	1	1620	197	0.	.1	1726.0	*	2	0040	297	0.	.1	1726.0
1	0805	98	25.	2.4	1728.6	*	1	1625	198	0.	.1	1726.0	*	2	0045	298	0.	.1	1726.0
1	0810	99	24.	2.2	1728.4	*	1	1630	199	0.	.1	1726.0	*	2	0050	299	0.	.1	1726.0
1	0815	100	24.	2.0	1728.3	*	1	1635	200	0.	.1	1726.0	*	2	0055	300	0.	.1	1726.0

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)		24-HR	72-HR		24.92-HR
+	41.	5.08	(CFS)	31.	9.	8.	8.
			(INCHES)	1.944	2.126	2.126	2.126
			(AC-FT)	15.	17.	17.	17.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE			
+	(AC-FT)	(HR)		24-HR	72-HR		24.92-HR
+	9.	5.08	5.	1.	1.		1.
PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE			
+	(FEET)	(HR)		24-HR	72-HR		24.92-HR
+	1732.22	5.08	1730.12	1727.10	1727.06		1727.06
CUMULATIVE AREA =				.15 SQ MI			

HYDROGRAPH AT STATION DETPOND  
PLAN 1, RATIO = .60

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
1	0000	1	0.	.1	1726.0	*	1	0820	101	1.	.2	1726.1	*	1	1640	201	0.	.1	1726.0			
1	0005	2	0.	.1	1726.0	*	1	0825	102	1.	.2	1726.1	*	1	1645	202	0.	.1	1726.0			
1	0010	3	0.	.1	1726.0	*	1	0830	103	1.	.2	1726.1	*	1	1650	203	0.	.1	1726.0			
1	0015	4	0.	.1	1726.0	*	1	0835	104	1.	.1	1726.1	*	1	1655	204	0.	.1	1726.0			
1	0020	5	0.	.1	1726.0	*	1	0840	105	1.	.1	1726.1	*	1	1700	205	0.	.1	1726.0			
1	0025	6	0.	.1	1726.0	*	1	0845	106	1.	.1	1726.1	*	1	1705	206	0.	.1	1726.0			
1	0030	7	0.	.1	1726.0	*	1	0850	107	1.	.1	1726.1	*	1	1710	207	0.	.1	1726.0			
1	0035	8	0.	.1	1726.0	*	1	0855	108	1.	.1	1726.1	*	1	1715	208	0.	.1	1726.0			
1	0040	9	0.	.1	1726.0	*	1	0900	109	1.	.1	1726.1	*	1	1720	209	0.	.1	1726.0			
1	0045	10	0.	.1	1726.0	*	1	0905	110	1.	.1	1726.0	*	1	1725	210	0.	.1	1726.0			
1	0050	11	0.	.1	1726.0	*	1	0910	111	0.	.1	1726.0	*	1	1730	211	0.	.1	1726.0			
1	0055	12	0.	.1	1726.0	*	1	0915	112	0.	.1	1726.0	*	1	1735	212	0.	.1	1726.0			
1	0100	13	0.	.1	1726.0	*	1	0920	113	0.	.1	1726.0	*	1	1740	213	0.	.1	1726.0			
1	0105	14	0.	.1	1726.0	*	1	0925	114	0.	.1	1726.0	*	1	1745	214	0.	.1	1726.0			
1	0110	15	0.	.1	1726.0	*	1	0930	115	0.	.1	1726.0	*	1	1750	215	0.	.1	1726.0			
1	0115	16	0.	.1	1726.0	*	1	0935	116	0.	.1	1726.0	*	1	1755	216	0.	.1	1726.0			
1	0120	17	0.	.1	1726.0	*	1	0940	117	0.	.1	1726.0	*	1	1800	217	0.	.1	1726.0			
1	0125	18	0.	.1	1726.0	*	1	0945	118	0.	.1	1726.0	*	1	1805	218	0.	.1	1726.0			
1	0130	19	0.	.1	1726.0	*	1	0950	119	0.	.1	1726.0	*	1	1810	219	0.	.1	1726.0			
1	0135	20	0.	.1	1726.0	*	1	0955	120	0.	.1	1726.0	*	1	1815	220	0.	.1	1726.0			
1	0140	21	0.	.1	1726.0	*	1	1000	121	0.	.1	1726.0	*	1	1820	221	0.	.1	1726.0			
1	0145	22	0.	.1	1726.0	*	1	1005	122	0.	.1	1726.0	*	1	1825	222	0.	.1	1726.0			
1	0150	23	0.	.1	1726.0	*	1	1010	123	0.	.1	1726.0	*	1	1830	223	0.	.1	1726.0			
1	0155	24	1.	.1	1726.1	*	1	1015	124	0.	.1	1726.0	*	1	1835	224	0.	.1	1726.0			
1	0200	25	1.	.1	1726.1	*	1	1020	125	0.	.1	1726.0	*	1	1840	225	0.	.1	1726.0			
1	0205	26	1.	.1	1726.1	*	1	1025	126	0.	.1	1726.0	*	1	1845	226	0.	.1	1726.0			
1	0210	27	1.	.1	1726.1	*	1	1030	127	0.	.1	1726.0	*	1	1850	227	0.	.1	1726.0			
1	0215	28	1.	.1	1726.1	*	1	1035	128	0.	.1	1726.0	*	1	1855	228	0.	.1	1726.0			
1	0220	29	1.	.1	1726.1	*	1	1040	129	0.	.1	1726.0	*	1	1900	229	0.	.1	1726.0			
1	0225	30	1.	.2	1726.1	*	1	1045	130	0.	.1	1726.0	*	1	1905	230	0.	.1	1726.0			
1	0230	31	1.	.2	1726.1	*	1	1050	131	0.	.1	1726.0	*	1	1910	231	0.	.1	1726.0			
1	0235	32	2.	.2	1726.1	*	1	1055	132	0.	.1	1726.0	*	1	1915	232	0.	.1	1726.0			
1	0240	33	2.	.2	1726.2	*	1	1100	133	0.	.1	1726.0	*	1	1920	233	0.	.1	1726.0			
1	0245	34	2.	.2	1726.2	*	1	1105	134	0.	.1	1726.0	*	1	1925	234	0.	.1	1726.0			



1	0000	1	0.0	0.0	1.1726.0	1	0000	1	0.0	0.0	1.1726.0
1	0005	2	0.0	0.0	1.1726.0	1	0005	2	0.0	0.0	1.1726.0
1	0010	3	0.0	0.0	1.1726.0	1	0010	3	0.0	0.0	1.1726.0
1	0015	4	0.0	0.0	1.1726.0	1	0015	4	0.0	0.0	1.1726.0
1	0020	5	0.0	0.0	1.1726.0	1	0020	5	0.0	0.0	1.1726.0
1	0025	6	0.0	0.0	1.1726.0	1	0025	6	0.0	0.0	1.1726.0
1	0030	7	0.0	0.0	1.1726.0	1	0030	7	0.0	0.0	1.1726.0
1	0035	8	0.0	0.0	1.1726.0	1	0035	8	0.0	0.0	1.1726.0
1	0040	9	0.0	0.0	1.1726.0	1	0040	9	0.0	0.0	1.1726.0
1	0045	10	0.0	0.0	1.1726.0	1	0045	10	0.0	0.0	1.1726.0
1	0050	11	0.0	0.0	1.1726.0	1	0050	11	0.0	0.0	1.1726.0
1	0055	12	0.0	0.0	1.1726.0	1	0055	12	0.0	0.0	1.1726.0
1	0100	13	0.0	0.0	1.1726.0	1	0100	13	0.0	0.0	1.1726.0
1	0105	14	0.0	0.0	1.1726.0	1	0105	14	0.0	0.0	1.1726.0
1	0110	15	0.0	0.0	1.1726.0	1	0110	15	0.0	0.0	1.1726.0
1	0115	16	0.0	0.0	1.1726.0	1	0115	16	0.0	0.0	1.1726.0
1	0120	17	0.0	0.0	1.1726.0	1	0120	17	0.0	0.0	1.1726.0
1	0125	18	0.0	0.0	1.1726.0	1	0125	18	0.0	0.0	1.1726.0
1	0130	19	0.0	0.0	1.1726.0	1	0130	19	0.0	0.0	1.1726.0
1	0135	20	0.0	0.0	1.1726.0	1	0135	20	0.0	0.0	1.1726.0
1	0140	21	0.0	0.0	1.1726.0	1	0140	21	0.0	0.0	1.1726.0
1	0000	1	0.0	0.0	1.1726.0	1	0000	1	0.0	0.0	1.1726.0
1	0005	2	0.0	0.0	1.1726.0	1	0005	2	0.0	0.0	1.1726.0
1	0010	3	0.0	0.0	1.1726.0	1	0010	3	0.0	0.0	1.1726.0
1	0015	4	0.0	0.0	1.1726.0	1	0015	4	0.0	0.0	1.1726.0
1	0020	5	0.0	0.0	1.1726.0	1	0020	5	0.0	0.0	1.1726.0
1	0025	6	0.0	0.0	1.1726.0	1	0025	6	0.0	0.0	1.1726.0
1	0030	7	0.0	0.0	1.1726.0	1	0030	7	0.0	0.0	1.1726.0
1	0035	8	0.0	0.0	1.1726.0	1	0035	8	0.0	0.0	1.1726.0
1	0040	9	0.0	0.0	1.1726.0	1	0040	9	0.0	0.0	1.1726.0
1	0045	10	0.0	0.0	1.1726.0	1	0045	10	0.0	0.0	1.1726.0
1	0050	11	0.0	0.0	1.1726.0	1	0050	11	0.0	0.0	1.1726.0
1	0055	12	0.0	0.0	1.1726.0	1	0055	12	0.0	0.0	1.1726.0
1	0100	13	0.0	0.0	1.1726.0	1	0100	13	0.0	0.0	1.1726.0
1	0105	14	0.0	0.0	1.1726.0	1	0105	14	0.0	0.0	1.1726.0
1	0110	15	0.0	0.0	1.1726.0	1	0110	15	0.0	0.0	1.1726.0
1	0115	16	0.0	0.0	1.1726.0	1	0115	16	0.0	0.0	1.1726.0
1	0120	17	0.0	0.0	1.1726.0	1	0120	17	0.0	0.0	1.1726.0
1	0125	18	0.0	0.0	1.1726.0	1	0125	18	0.0	0.0	1.1726.0
1	0130	19	0.0	0.0	1.1726.0	1	0130	19	0.0	0.0	1.1726.0
1	0135	20	0.0	0.0	1.1726.0	1	0135	20	0.0	0.0	1.1726.0
1	0140	21	0.0	0.0	1.1726.0	1	0140	21	0.0	0.0	1.1726.0
1	0000	1	0.0	0.0	1.1726.0	1	0000	1	0.0	0.0	1.1726.0
1	0005	2	0.0	0.0	1.1726.0	1	0005	2	0.0	0.0	1.1726.0
1	0010	3	0.0	0.0	1.1726.0	1	0010	3	0.0	0.0	1.1726.0
1	0015	4	0.0	0.0	1.1726.0	1	0015	4	0.0	0.0	1.1726.0
1	0020	5	0.0	0.0	1.1726.0	1	0020	5	0.0	0.0	1.1726.0
1	0025	6	0.0	0.0	1.1726.0	1	0025	6	0.0	0.0	1.1726.0
1	0030	7	0.0	0.0	1.1726.0	1	0030	7	0.0	0.0	1.1726.0
1	0035	8	0.0	0.0	1.1726.0	1	0035	8	0.0	0.0	1.1726.0
1	0040	9	0.0	0.0	1.1726.0	1	0040	9	0.0	0.0	1.1726.0
1	0045	10	0.0	0.0	1.1726.0	1	0045	10	0.0	0.0	1.1726.0
1	0050	11	0.0	0.0	1.1726.0	1	0050	11	0.0	0.0	1.1726.0
1	0055	12	0.0	0.0	1.1726.0	1	0055	12	0.0	0.0	1.1726.0
1	0100	13	0.0	0.0	1.1726.0	1	0100	13	0.0	0.0	1.1726.0
1	0105	14	0.0	0.0	1.1726.0	1	0105	14	0.0	0.0	1.1726.0
1	0110	15	0.0	0.0	1.1726.0	1	0110	15	0.0	0.0	1.1726.0
1	0115	16	0.0	0.0	1.1726.0	1	0115	16	0.0	0.0	1.1726.0
1	0120	17	0.0	0.0	1.1726.0	1	0120	17	0.0	0.0	1.1726.0
1	0125	18	0.0	0.0	1.1726.0	1	0125	18	0.0	0.0	1.1726.0
1	0130	19	0.0	0.0	1.1726.0	1	0130	19	0.0	0.0	1.1726.0
1	0135	20	0.0	0.0	1.1726.0	1	0135	20	0.0	0.0	1.1726.0
1	0140	21	0.0	0.0	1.1726.0	1	0140	21	0.0	0.0	1.1726.0
1	0000	1	0.0	0.0	1.1726.0	1	0000	1	0.0	0.0	1.1726.0
1	0005	2	0.0	0.0	1.1726.0	1	0005	2	0.0	0.0	1.1726.0
1	0010	3	0.0	0.0	1.1726.0	1	0010	3	0.0	0.0	1.1726.0
1	0015	4	0.0	0.0	1.1726.0	1	0015	4	0.0	0.0	1.1726.0
1	0020	5	0.0	0.0	1.1726.0	1	0020	5	0.0	0.0	1.1726.0
1	0025	6	0.0	0.0	1.1726.0	1	0025	6	0.0	0.0	1.1726.0
1	0030	7	0.0	0.0	1.1726.0	1	0030	7	0.0	0.0	1.1726.0
1	0035	8	0.0	0.0	1.1726.0	1	0035	8	0.0	0.0	1.1726.0
1	0040	9	0.0	0.0	1.1726.0	1	0040	9	0.0	0.0	1.1726.0
1	0045	10	0.0	0.0	1.1726.0	1	0045	10	0.0	0.0	1.1726.0
1	0050	11	0.0	0.0	1.1726.0	1	0050	11	0.0	0.0	1.1726.0
1	0055	12	0.0	0.0	1.1726.0	1	0055	12	0.0	0.0	1.1726.0
1	0100	13	0.0	0.0	1.1726.0	1	0100	13	0.0	0.0	1.1726.0
1	0105	14	0.0	0.0	1.1726.0	1	0105	14	0.0	0.0	1.1726.0
1	0110	15	0.0	0.0	1.1726.0	1	0110	15	0.0	0.0	1.1726.0
1	0115	16	0.0	0.0	1.1726.0	1	0115	16	0.0	0.0	1.1726.0
1	0120	17	0.0	0.0	1.1726.0	1	0120	17	0.0	0.0	1.1726.0
1	0125	18	0.0	0.0	1.1726.0	1	0125	18	0.0	0.0	1.1726.0
1	0130	19	0.0	0.0	1.1726.0	1	0130	19	0.0	0.0	1.1726.0
1	0135	20	0.0	0.0	1.1726.0	1	0135	20	0.0	0.0	1.1726.0
1	0140	21	0.0	0.0	1.1726.0	1	0140	21	0.0	0.0	1.1726.0
1	0000	1	0.0	0.0	1.1726.0	1	0000	1	0.0	0.0	1.1726.0
1	0005	2	0.0	0.0	1.1726.0	1	0005	2	0.0	0.0	1.1726.0
1	0010	3	0.0	0.0	1.1726.0	1	0010	3	0.0	0.0	1.1726.0
1	0015	4	0.0	0.0	1.1726.0	1	0015	4	0.0	0.0	1.1726.0
1	0020	5	0.0	0.0	1.1726.0	1	0020	5	0.0	0.0	1.1726.0
1	0025	6	0.0	0.0	1.1726.0	1	0025	6	0.0	0.0	1.1726.0
1	0030	7	0.0	0.0	1.1726.0	1	0030	7	0.0	0.0	1.1726.0
1	0035	8	0.0	0.0	1.1726.0	1	0035	8	0.0	0.0	1.1726.0
1	0040	9	0.0	0.0	1.1726.0	1	0040	9	0.0	0.0	1.1726.0
1	0045	10	0.0	0.0	1.1726.0	1	0045	10	0.0	0.0	1.1726.0
1	0050	11	0.0	0.0	1.1726.0	1	0050	11	0.0	0.0	1.1726.0
1	0055	12	0.0	0.0	1.1726.0	1	0055	12	0.0	0.0	1.1726.0
1	0100	13	0.0	0.0	1.1726.0	1	0100	13	0.0	0.0	1.1726.0
1	0105	14	0.0	0.0	1.1726.0	1	0105	14	0.0	0.0	1.1726.0
1	0110	15	0.0	0.0	1.1726.0	1	0110	15	0.0	0.0	1.1726.0
1	0115	16	0.0	0.0	1.1726.0	1	0115	16	0.0	0.0	1.1726.0
1	0120	17	0.0	0.0	1.1726.0	1	0120	17	0.0	0.0	1.1726.0
1	0125	18	0.0	0.0	1.1726.0	1	0125	18	0.0	0.0	1.1726.0
1	0130	19	0.0	0.0	1.1726.0	1	0130	19	0.0	0.0	1.1726.0
1	0135	20	0.0	0.0	1.1726.0	1	0135	20	0.0	0.0	1.1726.0
1	0140	21	0.0	0.0	1.1726.0	1	0140	21	0.0	0.0	1.1726.0
1	0000	1	0.0	0.0	1.1726.0	1	0000	1	0.0	0.0	1.1726.0
1	0005	2	0.0	0.0	1.1726.0	1	0005	2	0.0	0.0	1.1726.0
1	0010	3	0.0	0.0	1.1726.0	1	0010	3	0.0	0.0	1.1726.0
1	0015	4	0.0	0.0	1.1726.0	1	0015	4	0.0	0.0	1.1726.0
1	0020	5	0.0	0.0	1.1726.0	1	0020	5	0.0	0.0	1.1726.0
1	0025	6	0.0	0.0	1.1726.0	1	0025	6	0.0	0.0	1.1726.0
1	0030	7	0.0	0.0	1.1726.0	1	0030	7	0.0	0.0	1.1726.0
1	0035	8	0.0	0.0	1.1726.0	1	0035	8	0.0	0.0	1.1726.0
1	0040	9	0.0	0.0	1.1726.0	1	0040	9	0.0	0.0	1.1726.0
1	0045	10	0.0	0.0	1.1726.0	1	0045	10	0.0	0.0	1.1726.0
1	0050	11	0.0	0.0	1.1726.0	1	0050	11	0.0	0.0	1.1726.0
1	0055	12	0.0	0.0	1.1726.0	1	0055	12	0.0	0.0	1.1726.0
1	0100	13	0.0	0.0	1.1726.0	1	0100	13	0.0	0.0	



1	0145	22	0.	.1	1726.0	*	1	1005	122	0.	.1	1726.0	*	1	1825	222	0.	.1	1726.0
1	0150	23	0.	.1	1726.0	*	1	1010	123	0.	.1	1726.0	*	1	1830	223	0.	.1	1726.0
1	0155	24	0.	.1	1726.0	*	1	1015	124	0.	.1	1726.0	*	1	1835	224	0.	.1	1726.0
1	0200	25	1.	.1	1726.0	*	1	1020	125	0.	.1	1726.0	*	1	1840	225	0.	.1	1726.0
1	0205	26	1.	.1	1726.0	*	1	1025	126	0.	.1	1726.0	*	1	1845	226	0.	.1	1726.0
1	0210	27	1.	.1	1726.1	*	1	1030	127	0.	.1	1726.0	*	1	1850	227	0.	.1	1726.0
1	0215	28	1.	.1	1726.1	*	1	1035	128	0.	.1	1726.0	*	1	1855	228	0.	.1	1726.0
1	0220	29	1.	.1	1726.1	*	1	1040	129	0.	.1	1726.0	*	1	1900	229	0.	.1	1726.0
1	0225	30	1.	.1	1726.1	*	1	1045	130	0.	.1	1726.0	*	1	1905	230	0.	.1	1726.0
1	0230	31	1.	.2	1726.1	*	1	1050	131	0.	.1	1726.0	*	1	1910	231	0.	.1	1726.0
1	0235	32	1.	.2	1726.1	*	1	1055	132	0.	.1	1726.0	*	1	1915	232	0.	.1	1726.0
1	0240	33	1.	.2	1726.1	*	1	1100	133	0.	.1	1726.0	*	1	1920	233	0.	.1	1726.0
1	0245	34	2.	.2	1726.1	*	1	1105	134	0.	.1	1726.0	*	1	1925	234	0.	.1	1726.0
1	0250	35	2.	.2	1726.2	*	1	1110	135	0.	.1	1726.0	*	1	1930	235	0.	.1	1726.0
1	0255	36	2.	.2	1726.2	*	1	1115	136	0.	.1	1726.0	*	1	1935	236	0.	.1	1726.0
1	0300	37	2.	.2	1726.2	*	1	1120	137	0.	.1	1726.0	*	1	1940	237	0.	.1	1726.0
1	0305	38	2.	.2	1726.2	*	1	1125	138	0.	.1	1726.0	*	1	1945	238	0.	.1	1726.0
1	0310	39	3.	.3	1726.2	*	1	1130	139	0.	.1	1726.0	*	1	1950	239	0.	.1	1726.0
1	0315	40	4.	.3	1726.3	*	1	1135	140	0.	.1	1726.0	*	1	1955	240	0.	.1	1726.0
1	0320	41	5.	.4	1726.5	*	1	1140	141	0.	.1	1726.0	*	1	2000	241	0.	.1	1726.0
1	0325	42	8.	.6	1726.7	*	1	1145	142	0.	.1	1726.0	*	1	2005	242	0.	.1	1726.0
1	0330	43	12.	.9	1727.1	*	1	1150	143	0.	.1	1726.0	*	1	2010	243	0.	.1	1726.0
1	0335	44	18.	1.3	1727.6	*	1	1155	144	0.	.1	1726.0	*	1	2015	244	0.	.1	1726.0
1	0340	45	22.	1.6	1728.1	*	1	1200	145	0.	.1	1726.0	*	1	2020	245	0.	.1	1726.0
1	0345	46	23.	2.0	1728.3	*	1	1205	146	0.	.1	1726.0	*	1	2025	246	0.	.1	1726.0
1	0350	47	24.	2.2	1728.5	*	1	1210	147	0.	.1	1726.0	*	1	2030	247	0.	.1	1726.0
1	0355	48	25.	2.5	1728.6	*	1	1215	148	0.	.1	1726.0	*	1	2035	248	0.	.1	1726.0
1	0400	49	26.	2.6	1728.7	*	1	1220	149	0.	.1	1726.0	*	1	2040	249	0.	.1	1726.0
1	0405	50	26.	2.7	1728.8	*	1	1225	150	0.	.1	1726.0	*	1	2045	250	0.	.1	1726.0
1	0410	51	26.	2.8	1728.9	*	1	1230	151	0.	.1	1726.0	*	1	2050	251	0.	.1	1726.0
1	0415	52	26.	2.8	1728.9	*	1	1235	152	0.	.1	1726.0	*	1	2055	252	0.	.1	1726.0
1	0420	53	26.	2.8	1728.9	*	1	1240	153	0.	.1	1726.0	*	1	2100	253	0.	.1	1726.0
1	0425	54	26.	2.8	1728.9	*	1	1245	154	0.	.1	1726.0	*	1	2105	254	0.	.1	1726.0
1	0430	55	26.	2.8	1728.8	*	1	1250	155	0.	.1	1726.0	*	1	2110	255	0.	.1	1726.0
1	0435	56	26.	2.7	1728.8	*	1	1255	156	0.	.1	1726.0	*	1	2115	256	0.	.1	1726.0
1	0440	57	26.	2.7	1728.8	*	1	1300	157	0.	.1	1726.0	*	1	2120	257	0.	.1	1726.0
1	0445	58	26.	2.7	1728.8	*	1	1305	158	0.	.1	1726.0	*	1	2125	258	0.	.1	1726.0
1	0450	59	26.	2.7	1728.8	*	1	1310	159	0.	.1	1726.0	*	1	2130	259	0.	.1	1726.0
1	0455	60	26.	2.7	1728.8	*	1	1315	160	0.	.1	1726.0	*	1	2135	260	0.	.1	1726.0
1	0500	61	26.	2.7	1728.8	*	1	1320	161	0.	.1	1726.0	*	1	2140	261	0.	.1	1726.0
1	0505	62	26.	2.6	1728.7	*	1	1325	162	0.	.1	1726.0	*	1	2145	262	0.	.1	1726.0
1	0510	63	25.	2.6	1728.7	*	1	1330	163	0.	.1	1726.0	*	1	2150	263	0.	.1	1726.0
1	0515	64	25.	2.5	1728.6	*	1	1335	164	0.	.1	1726.0	*	1	2155	264	0.	.1	1726.0
1	0520	65	25.	2.4	1728.6	*	1	1340	165	0.	.1	1726.0	*	1	2200	265	0.	.1	1726.0
1	0525	66	25.	2.3	1728.5	*	1	1345	166	0.	.1	1726.0	*	1	2205	266	0.	.1	1726.0
1	0530	67	24.	2.2	1728.4	*	1	1350	167	0.	.1	1726.0	*	1	2210	267	0.	.1	1726.0
1	0535	68	24.	2.1	1728.4	*	1	1355	168	0.	.1	1726.0	*	1	2215	268	0.	.1	1726.0
1	0540	69	23.	1.9	1728.3	*	1	1400	169	0.	.1	1726.0	*	1	2220	269	0.	.1	1726.0
1	0545	70	23.	1.8	1728.2	*	1	1405	170	0.	.1	1726.0	*	1	2225	270	0.	.1	1726.0
1	0550	71	22.	1.7	1728.1	*	1	1410	171	0.	.1	1726.0	*	1	2230	271	0.	.1	1726.0
1	0555	72	22.	1.5	1728.0	*	1	1415	172	0.	.1	1726.0	*	1	2235	272	0.	.1	1726.0
1	0600	73	20.	1.4	1727.8	*	1	1420	173	0.	.1	1726.0	*	1	2240	273	0.	.1	1726.0
1	0605	74	18.	1.3	1727.7	*	1	1425	174	0.	.1	1726.0	*	1	2245	274	0.	.1	1726.0
1	0610	75	17.	1.2	1727.5	*	1	1430	175	0.	.1	1726.0	*	1	2250	275	0.	.1	1726.0
1	0615	76	15.	1.1	1727.4	*	1	1435	176	0.	.1	1726.0	*	1	2255	276	0.	.1	1726.0
1	0620	77	14.	1.0	1727.3	*	1	1440	177	0.	.1	1726.0	*	1	2300	277	0.	.1	1726.0
1	0625	78	13.	.9	1727.1	*	1	1445	178	0.	.1	1726.0	*	1	2305	278	0.	.1	1726.0
1	0630	79	11.	.8	1727.0	*	1	1450	179	0.	.1	1726.0	*	1	2310	279	0.	.1	1726.0
1	0635	80	10.	.8	1726.9	*	1	1455	180	0.	.1	1726.0	*	1	2315	280	0.	.1	1726.0
1	0640	81	9.	.7	1726.9	*	1	1500	181	0.	.1	1726.0	*	1	2320	281	0.	.1	1726.0
1	0645	82	9.	.6	1726.8	*	1	1505	182	0.	.1	1726.0	*	1	2325	282	0.	.1	1726.0
1	0650	83	8.	.6	1726.7	*	1	1510	183	0.	.1	1726.0	*	1	2330	283	0.	.1	1726.0
1	0655	84	7.	.5	1726.6	*	1	1515	184	0.	.1	1726.0	*	1	2335	284	0.	.1	1726.0
1	0700	85	6.	.5	1726.6	*	1	1520	185	0.	.1	1726.0	*	1	2340	285	0.	.1	1726.0
1	0705	86	6.	.5	1726.5	*	1	1525	186	0.	.1	1726.0	*	1	2345	286	0.	.1	1726.0
1	0710	87	5.	.4	1726.5	*	1	1530	187	0.	.1	1726.0	*	1	2350	287	0.	.1	1726.0
1	0715	88	5.	.4	1726.4	*	1	1535	188	0.	.1	1726.0	*	1	2355	288	0.	.1	1726.0
1	0720	89	4.	.4	1726.4	*	1	1540	189	0.	.1	1726.0	*	2	0000	289	0.	.1	1726.0
1	0725	90	4.	.3	1726.3	*	1	1545	190	0.	.1	1726.0	*	2	0005	290	0.	.1	1726.0
1	0730	91	3.	.3	1726.3	*	1	1550	191	0.	.1	1726.0	*	2	0010	291	0.	.1	1726.0
1	0735	92	3.	.3	1726.3	*	1	1555	192	0.	.1	1726.0	*	2	0015	292	0.	.1	1726.0
1	0740	93	3.	.3	1726.3	*	1	1600	193	0.	.1	1726.0	*	2	0020	293	0.	.1	1726.0
1	0745	94	2.	.2	1726.2	*	1	1605	194	0.	.1	1726.0	*	2	0025	294	0.	.1	1726.0
1	0750	95	2.	.2	1726.2	*	1	1610	195	0.	.1	1726.0	*	2	0030	295	0.	.1	1726.0
1	0755	96	2.	.2	1726.2	*	1	1615	196	0.	.1	1726.0	*	2	0035	296	0.	.1	1726.0
1	0800	97	2.	.2	1726.2	*	1	1620	197	0.	.1	1726.0	*	2	0040	297	0.	.1	1726.0
1	0805	98	2.	.2	1726.1	*	1	1625	198	0.	.1	1726.0	*	2	0045	298	0.	.1	1726.0
1	0810	99	1.	.2	1726.1	*	1	1630	199	0.	.1	1726.0	*	2	0050	299	0.	.1	1726.0
1	0815	100	1.	.2	1726.1	*	1	1635	200	0.	.1	1726.0	*	2	0055	300	0.	.1	1726.0

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)	(CFS)			
+	26.	4.25	13.	3.	3.
		(INCHES)	.838	.852	.852
		(AC-FT)	7.	7.	7.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)				
+	3.	4.25	1.	0.	0.</



				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	OFFEX3	.03	1	FLOW	21.	8.	7.
				TIME	3.67	3.75	3.75
2 COMBINED AT							
+	CP-7	.03	1	FLOW	23.	8.	8.
				TIME	3.67	3.75	3.75
HYDROGRAPH AT							
+	OND8	.02	1	FLOW	33.	16.	15.
				TIME	3.58	3.58	3.58
ROUTED TO							
+	ROND8-CP	.02	1	FLOW	32.	16.	15.
				TIME	3.67	3.67	3.67
HYDROGRAPH AT							
+	OND10	.01	1	FLOW	10.	5.	5.
				TIME	3.58	3.58	3.58
HYDROGRAPH AT							
+	OFFEX5	.01	1	FLOW	10.	4.	4.
				TIME	3.58	3.58	3.58
3 COMBINED AT							
+	CP-9	.04	1	FLOW	51.	23.	22.
				TIME	3.58	3.67	3.67
ROUTED TO							
+	RCP9-CP-	.04	1	FLOW	50.	23.	22.
				TIME	3.58	3.67	3.67
HYDROGRAPH AT							
+	OND12	.00	1	FLOW	8.	4.	4.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	CP-10A	.04	1	FLOW	55.	25.	24.
				TIME	3.58	3.67	3.67
HYDROGRAPH AT							
+	OND11	.01	1	FLOW	24.	12.	11.
				TIME	3.58	3.58	3.58
HYDROGRAPH AT							
+	OND13	.01	1	FLOW	12.	6.	6.
				TIME	3.50	3.50	3.50
3 COMBINED AT							
+	CP-10	.06	1	FLOW	90.	42.	40.
				TIME	3.58	3.58	3.58
ROUTED TO							
+	EQBASIN	.06	1	FLOW	54.	27.	26.
				TIME	3.83	3.83	3.83
** PEAK STAGES IN FEET **							
1	STAGE				1747.53	1746.40	1746.34
	TIME				3.83	3.83	3.83
DIVERSION TO							
+	DVPIPE	.06	1	FLOW	54.	27.	26.
				TIME	3.83	3.83	3.83
HYDROGRAPH AT							
+	DIVWEIR	.06	1	FLOW	0.	0.	0.
				TIME	.00	.00	.00
HYDROGRAPH AT							
+	OND14	.02	1	FLOW	31.	15.	14.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	CP-11	.08	1	FLOW	31.	15.	14.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	OND1	.00	1	FLOW	3.	1.	1.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	OFFEX2	.01	1	FLOW	13.	4.	4.
				TIME	3.58	3.58	3.58
2 COMBINED AT							
+	CP-1	.02	1	FLOW	15.	5.	4.
				TIME	3.58	3.58	3.58
ROUTED TO							
+	RCP1-CP2	.02	1	FLOW	14.	5.	4.
				TIME	3.58	3.67	3.67
HYDROGRAPH AT							
+	OND2	.01	1	FLOW	8.	4.	3.
				TIME	3.58	3.58	3.58
HYDROGRAPH AT							
+	OFFEX1	.07	1	FLOW	48.	14.	13.
				TIME	3.67	3.67	3.67
3 COMBINED AT							
+	CP-2	.09	1	FLOW	68.	22.	20.
				TIME	3.67	3.67	3.67
ROUTED TO							
+	RCP2-CP-	.09	1	FLOW	68.	21.	19.
				TIME	3.67	3.67	3.67
HYDROGRAPH AT							
+	OND3	.00	1	FLOW	4.	2.	2.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	CP-3	.09	1	FLOW	70.	22.	20.
				TIME	3.67	3.67	3.67
ROUTED TO							
+	RCP3-CP4	.09	1	FLOW	69.	21.	19.



				TIME	3.67	3.67	3.75
HYDROGRAPH AT							
+	OND7	.01	1	FLOW	16.	8.	7.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	CP-4	.10	1	FLOW	79.	26.	24.
				TIME	3.58	3.67	3.67
HYDROGRAPH AT							
+	OND4	.02	1	FLOW	27.	13.	12.
				TIME	3.58	3.58	3.58
HYDROGRAPH AT							
+	OND5	.01	1	FLOW	12.	6.	6.
				TIME	3.58	3.58	3.58
2 COMBINED AT							
+	CP-5	.03	1	FLOW	40.	19.	18.
				TIME	3.58	3.58	3.58
HYDROGRAPH AT							
+	OND6	.02	1	FLOW	23.	11.	11.
				TIME	3.58	3.58	3.58
HYDROGRAPH AT							
+	DVPIPE	.00	1	FLOW	54.	27.	26.
				TIME	3.83	3.83	3.83
ROUTED TO							
+	RDVPIPE	.00	1	FLOW	54.	27.	26.
				TIME	3.83	3.83	3.83
HYDROGRAPH AT							
+	DETPD	.01	1	FLOW	16.	8.	8.
				TIME	3.50	3.50	3.50
5 COMBINED AT							
+	CP-6	.15	1	FLOW	190.	79.	74.
				TIME	3.58	3.58	3.58
ROUTED TO							
+	DETPOND	.15	1	FLOW	41.	27.	26.
				TIME	5.08	4.25	4.25
** PEAK STAGES IN FEET **							
1	STAGE				1732.22	1729.02	1728.88
	TIME				5.08	4.25	4.25
HYDROGRAPH AT							
+	OFFD-14	.00	1	FLOW	3.	2.	1.
				TIME	3.58	3.67	3.67
ROUTED TO							
+	RT-B14	.00	1	FLOW	3.	1.	1.
				TIME	3.67	3.67	3.67
HYDROGRAPH AT							
+	EMIC-1	.01	1	FLOW	26.	13.	12.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	C15	.02	1	FLOW	28.	14.	13.
				TIME	3.50	3.50	3.50
ROUTED TO							
+	RT-14	.02	1	FLOW	27.	13.	13.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	EMIC-2	.01	1	FLOW	22.	11.	11.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	C16	.03	1	FLOW	50.	25.	24.
				TIME	3.50	3.50	3.50
ROUTED TO							
+	RT-15	.03	1	FLOW	49.	24.	23.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	SCH-2	.01	1	FLOW	13.	7.	6.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	C17	.04	1	FLOW	61.	31.	29.
				TIME	3.50	3.50	3.50
ROUTED TO							
+	RT-16	.04	1	FLOW	59.	29.	27.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	EMIC-3	.01	1	FLOW	21.	11.	10.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	MSDEV-2	.01	1	FLOW	17.	9.	8.
				TIME	3.50	3.50	3.50
4 COMBINED AT							
+	C18	.20	1	FLOW	123.	62.	58.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	HR3	.00	1	FLOW	3.	1.	1.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	HR2	.00	1	FLOW	4.	2.	2.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	HR1	.00	1	FLOW	3.	2.	2.
				TIME	3.50	3.50	3.50
3 COMBINED AT							
+	CHR1	.00	1	FLOW	10.	5.	5.



TIME	3.50	3.50	3.50
2 COMBINED AT			
C18B .21 1	FLOW	133.	67.
	TIME	3.50	3.50
HYDROGRAPH AT			
OND15 .03 1	FLOW	57.	28.
	TIME	3.50	3.50
HYDROGRAPH AT			
OFFEX4 .01 1	FLOW	14.	6.
	TIME	3.58	3.58
1			
SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)			
ISTAQ	ELEMENT	DT	PEAK
			TIME TO
			PEAK
			VOLUME
			DT
			COMPUTATION INTERVAL
			PEAK
			TIME TO
			PEAK
			VOLUME
			(IN)
FOR PLAN = 1	RATIO= 1.00		
ROND8-CP	MANE	1.62	32.92
			217.65
			1.82
			5.00
			31.53
			220.00
			1.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2161E+01 EXCESS= .0000E+00 OUTFLOW= .2168E+01 BASIN STORAGE= .6696E-06 PERCENT ERROR= -.3			
FOR PLAN = 1	RATIO= .60		
ROND8-CP	MANE	2.13	15.86
			219.44
			.84
			5.00
			15.62
			220.00
			.84
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9996E+00 EXCESS= .0000E+00 OUTFLOW= .1003E+01 BASIN STORAGE= .5867E-06 PERCENT ERROR= -.3			
FOR PLAN = 1	RATIO= .58		
ROND8-CP	MANE	2.07	14.96
			218.61
			.80
			5.00
			14.69
			220.00
			.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9454E+00 EXCESS= .0000E+00 OUTFLOW= .9483E+00 BASIN STORAGE= .6885E-06 PERCENT ERROR= -.3			
FOR PLAN = 1	RATIO= 1.00		
RCP9-CP-	MANE	.52	50.82
			216.00
			1.74
			5.00
			49.63
			215.00
			1.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3439E+01 EXCESS= .0000E+00 OUTFLOW= .3440E+01 BASIN STORAGE= .3381E-06 PERCENT ERROR= .0			
FOR PLAN = 1	RATIO= .60		
RCP9-CP-	MANE	.50	23.33
			220.56
			.79
			5.00
			23.32
			220.00
			.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1560E+01 EXCESS= .0000E+00 OUTFLOW= .1561E+01 BASIN STORAGE= .3045E-06 PERCENT ERROR= .0			
FOR PLAN = 1	RATIO= .58		
RCP9-CP-	MANE	.57	21.96
			220.31
			.75
			5.00
			21.96
			220.00
			.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1473E+01 EXCESS= .0000E+00 OUTFLOW= .1474E+01 BASIN STORAGE= .3331E-06 PERCENT ERROR= .0			
FOR PLAN = 1	RATIO= 1.00		
RCP1-CP2	MANE	1.72	14.82
			218.34
			1.07
			5.00
			14.37
			215.00
			1.07
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9363E+00 EXCESS= .0000E+00 OUTFLOW= .9386E+00 BASIN STORAGE= .2101E-06 PERCENT ERROR= -.2			
FOR PLAN = 1	RATIO= .60		
RCP1-CP2	MANE	2.17	4.84
			219.55
			.36
			5.00
			4.79
			220.00
			.36
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3181E+00 EXCESS= .0000E+00 OUTFLOW= .3191E+00 BASIN STORAGE= .2143E-06 PERCENT ERROR= -.3			
FOR PLAN = 1	RATIO= .58		
RCP1-CP2	MANE	2.23	4.38
			220.13
			.33
			5.00
			4.37
			220.00
			.33
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2929E+00 EXCESS= .0000E+00 OUTFLOW= .2937E+00 BASIN STORAGE= .1728E-06 PERCENT ERROR= -.3			
FOR PLAN = 1	RATIO= 1.00		
RCP2-CP-	MANE	.31	67.94
			220.07
			1.02
			5.00
			67.93
			220.00
			1.02
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4810E+01 EXCESS= .0000E+00 OUTFLOW= .4810E+01 BASIN STORAGE= .9178E-07 PERCENT ERROR= .0			
FOR PLAN = 1	RATIO= .60		
RCP2-CP-	MANE	.34	21.49
			220.45
			.34
			5.00
			21.35
			220.00
			.34
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1596E+01 EXCESS= .0000E+00 OUTFLOW= .1596E+01 BASIN STORAGE= .8670E-07 PERCENT ERROR= .0			
FOR PLAN = 1	RATIO= .58		
RCP2-CP-	MANE	.29	19.59
			220.58
			.31
			5.00
			19.38
			220.00
			.31
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1466E+01 EXCESS= .0000E+00 OUTFLOW= .1466E+01 BASIN STORAGE= .8727E-07 PERCENT ERROR= .0			
FOR PLAN = 1	RATIO= 1.00		
RCP3-CP4	MANE	.61	69.46
			220.77
			1.04
			5.00
			69.27
			220.00
			1.04
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5012E+01 EXCESS= .0000E+00 OUTFLOW= .5015E+01 BASIN STORAGE= .4675E-06 PERCENT ERROR= -.1			
FOR PLAN = 1	RATIO= .60		
RCP3-CP4	MANE	.90	22.00
			222.28
			.35
			5.00
			21.43
			220.00
			.35
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1685E+01 EXCESS= .0000E+00 OUTFLOW= .1686E+01 BASIN STORAGE= .4645E-06 PERCENT ERROR= -.1			



FOR PLAN = 1	RATIO= .58								
RCP3-CP4	MANE	1.00	20.05	221.90	.32	5.00	19.47	225.00	.32
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1550E+01 EXCESS= .0000E+00 OUTFLOW= .1551E+01 BASIN STORAGE= .4728E-06 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= 1.00								
RDVPIPE	MANE	1.05	54.03	231.40	-1.00	5.00	54.01	230.00	-1.00
FOR PLAN = 1	RATIO= .60								
RDVPIPE	MANE	1.27	27.47	231.34	-1.00	5.00	27.45	230.00	-1.00
FOR PLAN = 1	RATIO= .58								
RDVPIPE	MANE	1.18	26.15	231.54	-1.00	5.00	26.12	230.00	-1.00
FOR PLAN = 1	RATIO= 1.00								
RT-B14	MANE	1.36	3.39	218.69	1.64	5.00	3.37	220.00	1.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2438E+00 EXCESS= .0000E+00 OUTFLOW= .2442E+00 BASIN STORAGE= .7570E-08 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO= .60								
RT-B14	MANE	1.71	1.51	223.43	.71	5.00	1.50	220.00	.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1061E+00 EXCESS= .0000E+00 OUTFLOW= .1063E+00 BASIN STORAGE= .7638E-08 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO= .58								
RT-B14	MANE	1.76	1.42	222.80	.67	5.00	1.41	220.00	.67
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9979E-01 EXCESS= .0000E+00 OUTFLOW= .9993E-01 BASIN STORAGE= .5886E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= 1.00								
RT-14	MANE	.37	27.93	210.77	1.91	5.00	27.32	210.00	1.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1720E+01 EXCESS= .0000E+00 OUTFLOW= .1721E+01 BASIN STORAGE= .7751E-08 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .60								
RT-14	MANE	.42	13.81	211.01	.91	5.00	13.40	210.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8203E+00 EXCESS= .0000E+00 OUTFLOW= .8205E+00 BASIN STORAGE= .6549E-08 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .58								
RT-14	MANE	.41	13.17	210.75	.86	5.00	12.73	210.00	.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7778E+00 EXCESS= .0000E+00 OUTFLOW= .7780E+00 BASIN STORAGE= .6560E-08 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= 1.00								
RT-15	MANE	.36	49.16	210.62	1.93	5.00	48.56	210.00	1.94
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2959E+01 EXCESS= .0000E+00 OUTFLOW= .2959E+01 BASIN STORAGE= .9128E-08 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .60								
RT-15	MANE	.35	24.51	210.82	.93	5.00	24.04	210.00	.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1419E+01 EXCESS= .0000E+00 OUTFLOW= .1420E+01 BASIN STORAGE= .8611E-08 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .58								
RT-15	MANE	.35	23.31	210.84	.88	5.00	22.85	210.00	.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1347E+01 EXCESS= .0000E+00 OUTFLOW= .1347E+01 BASIN STORAGE= .8421E-08 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= 1.00								
RT-16	MANE	.53	60.94	211.13	1.94	5.00	58.94	210.00	1.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3645E+01 EXCESS= .0000E+00 OUTFLOW= .3647E+01 BASIN STORAGE= .3120E-07 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .60								
RT-16	MANE	.65	30.36	211.36	.93	5.00	28.90	210.00	.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1751E+01 EXCESS= .0000E+00 OUTFLOW= .1752E+01 BASIN STORAGE= .3374E-07 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .58								
RT-16	MANE	.62	28.82	211.06	.89	5.00	27.44	210.00	.89
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1661E+01 EXCESS= .0000E+00 OUTFLOW= .1663E+01 BASIN STORAGE= .3305E-07 PERCENT ERROR= -.1									

\*\*\* NORMAL END OF HEC-1 \*\*\*





LEGEND

- ONSITE BASIN BOUNDARY
- OFFSITE BASIN BOUNDARY
- REFERENCED BASIN BOUNDARY
- OND1
- OFFEX1
- HR1
- CP-1
- DISCHARGE POINT
- FLOW DIRECTION
- REFERENCED BASIN BOUNDARY
- EXISTING LANDFILL BOUNDARY

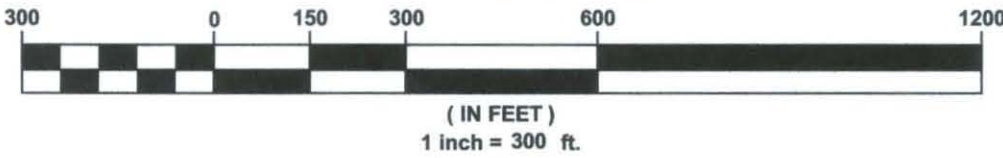
NOTES

"ADDENDUM #1 TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMERCE CENTER TWO (FORMERLY KNOWN AS HARSCH)" PREPARED BY PBS&J (FEBRUARY 2003) WAS USED FOR REFERENCED BASINS

BASIN ID	AREA (ac)	Q <sub>100</sub> (cfs)	Q <sub>10</sub> (cfs)
OND1	0.94	3	1
OND2	3.70	8	4
OND3	1.38	4	2
OND4	11.67	27	13
OND5	5.03	12	6
OND6	9.90	23	11
OND7	5.87	16	8
OND8	14.26	33	16
OND9	1.06	3	2
OND10	4.28	10	5
OND11	9.60	24	12
OND12	2.77	8	4
OND13	4.70	12	6
OND14	11.12	31	15
OND15	21.47	57	28
DETPD	5.14	16	8
OFFEX1	42.20	48	14
OFFEX2	9.63	13	4
OFFEX3	16.40	21	8
OFFEX4	7.61	14	6
OFFEX5	5.11	10	4
CP-1	NA	15	5
CP-2	NA	68	22
CP-3	NA	70	22
CP-4	NA	79	26
CP-5	NA	40	19
CP-6	NA	190	79
CP-7	NA	23	8
CP-9	NA	51	23
CP-10	NA	90	42
CP-10A	NA	55	25
CP-11	NA	31	15
C18	NA	123	62



GRAPHIC SCALE



511963.19 OCTOBER 2006

FIGURE 5  
INTERIM CONDITION  
DRAINAGE MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



2270 Corporate Circle  
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Henderson, Nevada 89074-6382  
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ENGINEERING PLANNING SURVEYING CONSTRUCTION SERVICES



### **Appendix B-3: Developed Condition Hydrology**

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# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

PBS&J  
File: TDS-Standard Form 4.xls

EASTSIDE LANDFILL  
Developed Condition Hydrology

BY:  
DATE:

KP  
10/5/06

SUB-BASIN DATA						INITIAL / OVERLAND TIME (Ti)			TRAVEL TIME (Tt)					Tc	Tc Check	Tag	REMARKS
DESIG:	DEV./JUN. (D or U)	CN	K	AREA Ac	AREA MI^2	INITIAL LENGTH Feet	SLOPE %	Ti Min	TRAVEL LENGTH Feet	SLOPE %	V1 VELOCITY FPS	V2 VELOCITY FPS	Tt Min	Min (13)	Min (14)	Tag= 0.6Tc/60 Hours	
(1)			(2)	(3)		(4)	(5)	(6)	(7)	(8)	(9a)	(9b)	(10)				
OND1	D	87.7	0.7676	0.94	0.0015	130	33.0	2.1	247	0.4	1.28	1.9	3.2	5.3	12.1	0.05	
OND2	D	87.7	0.7676	3.70	0.0058	137	33.0	2.2	910	0.4	1.28	1.9	10.1	12.2	15.8	0.12	
OND3	D	88.6	0.7795	1.38	0.0022	156	33.0	2.2	360	1.0	2.02	3.1	3.0	5.2	12.9	0.05	
OND4	D	89.7	0.7940	11.67	0.0182	240	2.0	6.8	1276	2.6	3.26	4.9	5.2	12.0	18.4	0.12	
OND5	D	91.0	0.8112	5.03	0.0079	300	1.7	7.6	573	1.1	2.07	3.1	4.4	12.0	14.9	0.12	
OND6	D	91.0	0.8112	9.90	0.0155	70	1.4	3.9	1407	0.6	1.56	2.4	11.7	15.6	18.2	0.16	
OND7	D	90.8	0.8086	5.87	0.0092	158	33.0	2.1	1345	1.8	2.67	4.0	6.6	8.7	18.4	0.09	
OND8	D	90.3	0.8020	14.26	0.0223	128	33.0	1.9	2382	0.4	1.28	1.9	22.7	24.6	23.9	0.24	Use Tag = 0.15 See Note
OND9	U	91.0	0.8112	1.06	0.0017	50	1.3	3.4	453	1.9	2.05	4.1	3.7	7.0	N/A	0.07	
OND10	D	91.0	0.8112	4.28	0.0067	119	33.0	1.8	1190	0.4	1.28	1.9	12.5	14.2	17.3	0.14	
OND11	D	91.0	0.8112	9.60	0.0150	220	1.6	6.6	1050	1.1	2.12	3.2	6.8	13.4	17.1	0.13	
OND12	D	91.4	0.8165	2.77	0.0043	138	33.0	1.9	610	1.5	2.47	3.7	3.9	5.7	14.2	0.06	
OND13	D	91.0	0.8112	4.70	0.0073	95	33.0	1.6	714	0.4	1.28	1.9	8.4	9.9	14.5	0.10	
OND14	U	91.0	0.8112	11.12	0.0174	122	1.0	5.7	559	5.0	3.31	6.6	2.7	8.4	N/A	0.08	
OND15	U	91.0	0.8112	21.47	0.0335	200	2.5	5.4	711	3.0	2.56	5.1	3.9	9.4	N/A	0.09	
DETPD	D	91.4	0.8165	5.14	0.0080	60	8.3	2.0	35	34.0	11.78	17.8	0.0	2.0	10.5	0.02	
OFFD1	D	88.2	0.7742	42.20	0.0659	278	2.5	7.2	2213	2.0	2.85	4.3	9.5	16.7	23.8	0.17	
OFFD2	D	88.6	0.7795	9.63	0.0150	195	3.6	5.3	942	1.8	2.71	4.1	4.9	10.1	16.3	0.10	
OFFD3	D	89.9	0.7967	16.40	0.0256	300	0.3	13.6	1245	1.7	2.63	4.0	6.3	19.9	18.6	0.19	
OFFD4	D	91.0	0.8112	7.61	0.0119	300	1.0	9.0	750	1.9	2.76	4.2	4.0	13.0	15.8	0.13	
OFFD5	D	91.0	0.8112	5.11	0.0080	300	1.3	8.2	625	1.6	2.56	3.9	3.8	12.0	15.1	0.12	
Tc = Ti + Tt			Eqn. 601		For the travel time (Tt) calculations (Sec. 602.1),					Undeveloped	V1 = 14.8*(S/100)^1/2			Developed	V1 = 20.2*(S/100)^1/2		
Ti = 1.8 (1.1 - K) L^1/2 / S^1/3			Eqn. 602		V1 applies to the first 500 feet of travel distance;												
K = 0.0132 (CN) - 0.39			Eqn. 603		V2 applies to the remaining travel distance.					Undeveloped	V2 = 29.4*(S/100)^1/2			Developed	V2 = 30.6*(S/100)^1/2		
Tc Check = L/180+10			Eqn. 604														
Tag = 0.6 Tc			Eqn. 612														
Tt = 500/V1+ (Travel Length-500)/V2			Min Tc = 10 mins for undeveloped basins Min Tc = 5 mins for developed basins														

Note: The lag time or basin OND8 was changed to 0.15 hrs because the velocities were not accurate for the cross section. Please refer to the FlowMaster cross section located in Appendix B-3 for the time calculations.

REFERENCE :

STANDARD FORM 4



```

1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
* RUN DATE 27SEP06 TIME 18:51:46
*****

```

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*****
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*****

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XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*** FREE ***
*DIAGRAM
1 ID EASTSIDE LANDFILL IMPROVEMENTS
2 ID DEVELOPED CONDITION MODEL
3 ID INPUT FILE = DEV_SDN3.DAT
4 ID SEPTEMBER 2006
5 ID DESIGN STORM = 100-YEAR 6-HR STORM
6 ID STORM DISTRIBUTION = SDN #3
7 ID MODELED BY PBS&J
8 ID
9 IT 5 0 0 300
10 IN 5 0 0
11 IO 5
12 JR PREC 1.00 0.60 0.58
*
13 KK OND8
14 KM DEVELOPED ONSITE BASIN
15 BA 0.0223
16 PB 2.79
17 PC .000 .020 .057 .070 .087 .108 .124 .130 .130 .130
18 PC .130 .130 .130 .133 .140 .142 .148 .158 .172 .191
19 PC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
20 PC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
21 PC .499 .590 .710 .744 .781 .812 .819 .835 .851 .856
22 PC .860 .868 .876 .888 .910 .926 .937 .950 .970 .976
23 PC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
24 PC .998 .999 1.00
25 LS 0 90.3
26 UD 0.15
*
27 KK OND9
28 KM DEVELOPED ONSITE BASIN
29 BA 0.0017
30 LS 0 91.0
31 UD 0.07
*
32 KK OFFD3
33 KM DEVELOPED OFFSITE BASIN
34 BA 0.0256
35 LS 0 89.9
36 UD 0.19
*
37 KK CP-7
38 KM COMBINE OND9 AND OFFD3
39 HC 2
*

```

1 HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 KK CP-8
41 KM COMBINE CP-7 AND OND8
42 HC 2
*
43 KK RCP8-CP-9
44 KM ROUTE CP-8 TO CP-9
45 RK 1190 0.004 0.025 0 TRAP 10 3
*
46 KK OND10
47 KM DEVELOPED ONSITE BASIN
48 BA 0.0067
49 LS 0 91.0
50 UD 0.14
*
51 KK OFFD5
52 KM DEVELOPED OFFSITE BASIN
53 BA 0.0080
54 LS 0 91.0
55 UD 0.12
*
56 KK CP-9
57 KM COMBINE RCP8-CP9, OFFD5 AND OND10
58 HC 3

```



\*  
 59 KKRCP9-CP-10  
 60 KM ROUTE CP-9 TO CP-10  
 61 RK 725 0.015 0.015 0 TRAP 10 3  
 \*

62 KK OND12  
 63 KM DEVELOPED ONSITE BASIN  
 64 BA 0.0043  
 65 LS 0 91.4  
 66 UD 0.06  
 \*

67 KK CP-10A  
 68 KM COMBINE CP-9 AND OND12  
 69 HC 2  
 \*

70 KK OND11  
 71 KM DEVELOPED ONSITE BASIN  
 72 BA 0.0150  
 73 LS 0 91.0  
 74 UD 0.13  
 \*

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

75 KK OND13  
 76 KM DEVELOPED ONSITE BASIN  
 77 BA 0.0073  
 78 LS 0 91.0  
 79 UD 0.10  
 \*

80 KK CP-10  
 81 KM COMBINE CP-10A, OND11 AND OND13  
 82 HC 3  
 \*

83 KK EQBASIN  
 84 KM EQUALIZER BASIN TO SPLIT FLOW NORTH AND  
 85 KM TO THE DETENTION POND  
 86 RS 1 STOR -1  
 87 SA 0 0.08 0.70 0.78 0.85 0.87 0.97  
 88 SE 1744.5 1745 1746 1747 1747.75 1748 1748.5  
 89 SQ 0 0 18 42 59 74 126  
 \*

90 KK DIVWEIR  
 91 KM DIVERG FLOW FROM EQ BASIN  
 92 DT DPIPE  
 93 DI 0 59 74 126  
 94 DQ 0 59 64 73  
 \*

95 KK OND14  
 96 KM DEVELOPED ONSITE BASIN  
 97 BA 0.0174  
 98 LS 0 91.0  
 99 UD 0.08  
 \*

100 KK CP-11  
 101 KM COMBINE WEIR FLOW AND OND14  
 102 HC 2  
 \*

103 KK OND1  
 104 KM DEVELOPED ONSITE BASIN  
 105 BA 0.0015  
 106 LS 0 87.7  
 107 UD 0.05  
 \*

108 KK OFFD2  
 109 KM DEVELOPED OFFSITE BASIN  
 110 BA .0150  
 111 LS 0 88.6  
 112 UD 0.10  
 \*

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

113 KK CP-1  
 114 KM COMBINE OND1 AND OFFD2  
 115 HC 2  
 \*

116 KKRCP1-CP2  
 117 KM ROUTE CP-1 TO CP-2  
 118 RK 910 0.004 0.025 0 TRAP 10 3  
 \*

119 KK OND2  
 120 KM DEVELOPED ONSITE BASIN  
 121 BA 0.0058  
 122 LS 0 87.7  
 123 UD 0.12  
 \*

124 KK OFFD1  
 125 KM DEVELOPED OFFSITE BASIN  
 126 BA 0.0659  
 127 LS 0 88.2  
 128 UD 0.17  
 \*

129 KK CP-2  
 130 KM COMBINE CP-1, OFFD1 AND OND2  
 131 HC 3  
 \*

132 KKRCF2-CP-3  
 133 KM ROUTE  
 134 RK 360 0.010 0.015 0 TRAP 10 3



```

*
135 KK OND3
136 KM DEVELOPED ONSITE BASIN
137 BA 0.0022
138 LS 0 88.6
139 UD 0.05
*
140 KK CP-3
141 KM COMBINE CP-2 AND OND3
142 HC 2
*
143 KK RCP3-CP4
144 KM ROUTE CP-3 TO CP-4
145 RK 1345 0.018 0.015 0 TRAP 10 3
*
1 HEC-1 INPUT PAGE 5
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
146 KK OND7
147 KM DEVELOPED ONSITE BASIN
148 BA 0.0092
149 LS 0 90.8
150 UD 0.09
*
151 KK CP-4
152 KM COMBINE CP-3 AND OND7
153 HC 2
*
154 KK OND4
155 KM DEVELOPED ONSITE BASIN
156 BA 0.0182
157 LS 0 89.7
158 UD 0.12
*
159 KK OND5
160 KM DEVELOPED ONSITE BASIN
161 BA 0.0079
162 LS 0 91.0
163 UD 0.12
*
164 KK CP-5
165 KM COMBINE OND4 AND OND5
166 HC 2
*
167 KK OND6
168 KM DEVELOPED ONSITE BASIN
169 BA 0.0155
170 LS 0 91.0
171 UD 0.16
*
172 KK DVPIPE
173 KM RETURN FLOW FROM EQ BASIN PIPE
174 DR DVPIPE
*
175 KK RDVPIPE
176 KM ROUTE FLOW THROUGH 42" RCP
177 RK 1880 0.005 0.013 0 CIRC 3.5 0
*
178 KK DETPD
179 KM DETENTION POND BASIN
180 BA 0.0080
181 LS 0 91.4
182 UD 0.05
*
1 HEC-1 INPUT PAGE 6
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
183 KK CP-6
184 KM COMBINE CP-4, CP-5, OND6, DVPIPE AND DETPD
185 HC 5
*
186 KK DETPOND
187 KM
188 RS 1 STOR -1
189 SV 0 0.08 1.53 3.02 4.84 8.88 13.45 15.95
190 SE 1725.25 1726 1728 1729 1730 1732 1734 1735
191 SQ 0 0 22 27 32 40 46 49
192 KO 1
*
* *****
* Referenced from PBSJ
* "Addendum #1 to the Technical Drainage Study for Henderson Commerce
* Center Two (Formerly known as HARSCH)" (February 2003)
* *****
*
193 KK OFFD-14
194 KM OFSITE DEVELOPED BASIN OFFD-14
195 KM REFERENCED FROM EG02
196 BA 0.0028
197 PB 2.79
198 LS 0 88
199 UD 0.200
*
200 KK RT-B14
201 KM ROUTE OFFD-14 THROUGH BMIC-1
202 RK 1050 0.014 0.013 0 TRAP 15 10
*
203 KK BMIC-1
204 KM ONSITE DEVELOPED BASIN BMIC-1
205 KM REFERENCED FROM EG02
206 BA 0.0141

```



207 PB 2.79  
 208 LS 0 92  
 209 UD 0.081  
 \*  
 210 KK C15  
 211 KM COMBINE RT-B14 AND BMIC-1  
 212 HC 2  
 \*  
 213 KK RT-14  
 214 KM ROUTE C15 THROUGH BMIC-2  
 215 RK 450 0.018 0.013 0 TRAP 15 10  
 \*

1 HEC-1 INPUT PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

216 KK BMIC-2  
 217 KM ONSITE DEVELOPED BASIN BMIC-2  
 218 KM REFERENCED FROM EG02  
 219 BA 0.0118  
 220 PB 2.79  
 221 LS 0 92  
 222 UD 0.073  
 \*  
 223 KK C16  
 224 KM COMBINE RT-14 AND BMIC-2  
 225 HC 2  
 \*  
 226 KK RT-15  
 227 KM ROUTE C16 THROUGH SCH-2  
 228 RK 400 0.019 0.013 0 TRAP 15 10  
 \*  
 229 KK SCH-2  
 230 KM ONSITE DEVELOPED BASIN SCH-2  
 231 KM REFERENCED FROM EG02  
 232 BA 0.0065  
 233 PB 2.79  
 234 LS 0 92  
 235 UD 0.060  
 \*  
 236 KK C17  
 237 KM COMBINE RT-15 AND SCH-2  
 238 HC 2  
 \*  
 239 KK RT-16  
 240 KM ROUTE C17 THROUGH BMIC-3  
 241 RK 750 0.013 0.013 0 TRAP 15 10  
 \*  
 242 KK BMIC-3  
 243 KM ONSITE DEVELOPED BASIN BMIC-3  
 244 KM REFERENCED FROM EG02  
 245 BA 0.0106  
 246 PB 2.79  
 247 LS 0 92  
 248 UD 0.062  
 \*  
 249 KK MGDEV-2  
 250 KM MILGARD MANUFACTURING ONSITE BASIN  
 251 KM REFERENCED FROM EG02  
 252 BA 0.0093  
 253 PB 2.79  
 254 LS 0 92  
 255 UD 0.075  
 \*

1 HEC-1 INPUT PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

256 KK C18  
 257 KM COMBINE RT-16, BMIC-3, BGDEV-2 AND OUTFLOW FROM DETENTION POND  
 258 HC 4  
 \*  
 \* Referenced from PBSJ  
 \* "Addendum #1 to the Technical Drainage Study for Henderson Commerce  
 \* Center Two (Formerly known as HARSCH)" (February 2003)  
 \*  
 259 KK HR3  
 260 KM HARSCH ONSITE BASIN  
 261 BA 0.0014  
 262 PB 2.79  
 263 LS 0 92  
 264 UD 0.049  
 \*  
 265 KK HR2  
 266 KM HARSCH ONSITE BASIN  
 267 BA 0.0016  
 268 PB 2.79  
 269 LS 0 98  
 270 UD 0.037  
 \*  
 271 KK HR1  
 272 KM HARSCH ONSITE BASIN  
 273 BA 0.0015  
 274 PB 2.79  
 275 LS 0 92  
 276 UD 0.05  
 \*  
 277 KK CHR1  
 278 KM COMBINE HR3, HR2, HR1  
 279 KM THESE FLOWS ARE DISCHARGED INTO THE ONSITE  
 280 KM STORM DRAIN SYSTEM LABELED ALIGNMENT "H1"



281 KM ON FIGURE 7  
282 HC 3

\*  
\* \*\*\*\*\*  
\*

283 KK C18B  
284 KM COMBINE C18 AND CHR1  
285 HC 2  
\*

1

HEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

286 KK OND15  
287 KM DEVELOPED ONSITE BASIN  
288 BA 0.0335  
289 LS 0 91.0  
290 UD 0.09  
\*

291 KK OFFD4  
292 KM DEVELOPED OFFSITE BASIN  
293 BA 0.0119  
294 LS 0 91.0  
295 UD 0.13  
\*

296 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

13 OND8  
.  
27 OND9  
.  
32 OFFD3  
.  
37 CP-7  
.  
40 CP-8  
V  
43 RCP8-CP-  
.  
46 OND10  
.  
51 OFFD5  
.  
56 CP-9  
V  
59 RCP9-CP-  
.  
62 OND12  
.  
67 CP-10A  
.  
70 OND11  
.  
75 OND13  
.  
80 CP-10  
V  
83 EQBASIN  
.  
92 DIVWEIR -> DVPIPE  
90  
.  
95 OND14  
.  
100 CP-11  
.  
103 OND1  
.  
108 OFFD2  
.  
113 CP-1  
V  
116 RCP1-CP2  
.  
119 OND2  
.  
124 OFFD1  
.  
129 CP-2  
V  
132 RCP2-CP-  
.  
135 OND3  
.



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(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 27SEP06 TIME 18:51:46 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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INPUT FILE = DEV\_SDN3.DAT  
SEPTEMBER 2006  
DESIGN STORM = 100-YEAR 6-HR STORM  
STORM DISTRIBUTION = SDN #3  
MODELED BY PRS&J

11 IO      OUTPUT CONTROL VARIABLES  
          IPRNT      5      PRINT CONTROL  
          IPILOT      0      PLOT CONTROL  
          QSCAL      0.      HYDROGRAPH PLOT SCALE  
  
IT          HYDROGRAPH TIME DATA  
          NMIN      5      MINUTES IN COMPUTATION INTERVAL  
          IDATE      1      0      STARTING DATE  
          ITIME      0000      STARTING TIME  
          NQ      300      NUMBER OF HYDROGRAPH ORDINATES  
          NDDATE      2      0      ENDING DATE  
          NDTIME      0055      ENDING TIME  
          ICENT      19      CENTURY MARK  
  
          COMPUTATION INTERVAL      .08 HOURS  
          TOTAL TIME BASE      24.92 HOURS  
  
ENGLISH UNITS  
DRAINAGE AREA      SQUARE MILES  
PRECIPITATION DEPTH      INCHES  
LENGTH, ELEVATION      FEET  
FLOW      CUBIC FEET PER SECOND  
STORAGE VOLUME      ACRE-Feet  
SURFACE AREA      ACRES  
TEMPERATURE      DEGREES FAHRENHEIT  
  
JP          MULTI-PLAN OPTION  
          NPLAN      1      NUMBER OF PLANS  
  
JR          MULTI-RATIO OPTION  
          RATIOS OF PRECIPITATION  
          1.00      .60      .58

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186 KK      \* DETPOND \*  
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192 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      1      PRINT CONTROL  
          IPILOT      0      PLOT CONTROL  
          QSCAL      0.      HYDROGRAPH PLOT SCALE  
  
HYDROGRAPH ROUTING DATA  
  
188 RS      STORAGE ROUTING  
          NSTPS      1      NUMBER OF SUBREACHES  
          ITYP      STOR      TYPE OF INITIAL CONDITION  
          RSVRIC      -1.00      INITIAL CONDITION  
          X      .00      WORKING R AND D COEFFICIENT

189 SV	STORAGE	.0	.1	1.5	3.0	4.8	8.9	13.4	15.9
190 SE	ELEVATION	1725.25	1726.00	1728.00	1729.00	1730.00	1732.00	1734.00	1735.00
191 SQ	DISCHARGE	0.	0.	22.	27.	32.	40.	46.	49.

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HYDROGRAPH AT STATION DETPOND  
PLAN 1,      RATIO = 1.00  
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DA	MON	HR	MIN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HR	MIN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HR	MIN	ORD	OUTFLOW	STORAGE	STAGE
1	0000	1	0.	.1	1726.0	*	1	0820	101	30.	4.3	1729.7	*	1	1640	201	0.	.1	1726.0				
1	0005	2	0.	.1	1726.0	*	1	0825	102	30.	4.1	1729.6	*	1	1645	202	0.	.1	1726.0				
1	0010	3	0.	.1	1726.0	*	1	0830	103	29.	3.9	1729.5	*	1	1650	203	0.	.1	1726.0				
1	0015	4	0.	.1	1726.0	*	1	0835	104	29.	3.7	1729.4	*	1	1655	204	0.	.1	1726.0				
1	0020	5	0.	.1	1726.0	*	1	0840	105	28.	3.5	1729.3	*	1	1700	205	0.	.1	1726.0				
1	0025	6	0.	.1	1726.0	*	1	0845	106	28.	3.3	1729.1	*	1	1705	206	0.	.1	1726.0				
1	0030	7	0.	.1	1726.0	*	1	0850	107	27.	3.1	1729.0	*	1	1710	207	0.	.1	1726.0				
1	0035	8	0.	.1	1726.0	*	1	0855	108	27.	2.9	1728.9	*	1	1715	208	0.	.1	1726.0				
1	0040	9	1.	.1	1726.1	*	1	0900	109	26.	2.7	1728.8	*	1	1720	209	0.	.1	1726.0				
1	0045	10	1.	.1	1726.1	*	1	0905	110	25.	2.6	1728.7	*	1	1725	210	0.	.1	1726.0				
1	0050	11	1.	.2	1726.1	*	1	0910	111	25.	2.4	1728.6	*	1	1730	211	0.	.1	1726.0				
1	0055	12	1.	.2	1726.1	*	1	0915	112	24.	2.2	1728.5	*	1	1735	212	0.	.1	1726.0				
1	0100	13	1.	.2	1726.1	*	1	0920	113	24.	2.0	1728.3	*	1	1740	213	0.	.1	1726.0				
1	0105	14	1.	.2	1726.1	*	1	0925	114	23.	1.9	1728.2	*	1	1745	214	0.	.1	1726.0				
1	0110	15	2.	.2	1726.1	*	1	0930	115	23.	1.7	1728.1	*	1	1750	215	0.	.1	1726.0				
1	0115	16	2.	.2	1726.1	*	1	0935	116	22.	1.6	1728.0	*	1	1755	216	0.	.1	1726.0				
1	0120	17	2.	.2	1726.2	*	1	0940	117	20.	1.4	1727.9	*	1	1800	217	0.	.1	1726.0				
1	0125	18	2.	.2	1726.2	*	1	0945	118	18.	1.3	1727.7	*	1	1805	218	0.	.1	1726.0				
1	0130	19	2.	.2	1726.2	*	1	0950	119	17.	1.2	1727.5	*	1	1810	219	0.	.1	1726.0				
1	0135	20	3.	.3	1726.3	*	1	0955	120	15.	1.1	1727.4	*	1	1815	220	0.	.1	1726.0				
1	0140	21	4.	.3	1726.3	*	1	1000	121	13.	1.0	1727.2	*	1	1820	221	0.	.1	1726.0				
1	0145	22	4.	.4	1726.4	*	1	1005	122	12.	.9	1727.1	*	1	1825	222	0.	.1	1726.0				
1	0150	23	5.	.4	1726.5	*	1	1010	123	11.	.8	1727.0	*	1	1830	223	0.	.1	1726.0				
1	0155	24	6.	.5	1726.5	*	1	1015	124	10.	.7	1726.9	*	1	1835	224	0.	.1	1726.0				
1	0200	25	6.	.5	1726.6	*	1	1020	125	9.	.7	1726.8	*	1	1840	225	0.	.1	1726.0				
1	0205	26	7.	.5	1726.6	*	1	1025	126	8.	.6	1726.7	*	1	1845	226	0.	.1	1726.0				
1	0210	27	7.	.5	1726.6	*	1	1030	127	7.	.6	1726.7	*	1	1850	227	0.	.1	1726.0				
1	0215	28	7.	.5	1726.6	*	1	1035	128	6.	.5	1726.6	*	1	1855	228	0.	.1	1726.0				
1	0220	29	8.	.6	1726.7	*	1	1040	129	6.	.5	1726.5	*	1	1900	229	0.	.1	1726.0				
1	0225	30	9.	.7	1726.8	*	1	1045	130	5.	.4	1726.5	*	1	1905	230	0.	.1	1726.0				
1	0230	31	10.	.7	1726.9	*	1	1050	131	5.	.4	1726.4	*	1	1910	231	0.	.1	1726.0				
1	0235	32	10.	.8	1726.9	*	1	1055	132	4.	.4	1726.4	*	1	1915	232	0.	.1	1726.0				
1	0240	33	11.	.8	1727.0	*	1	1100	133	4.	.3	1726.3	*	1	1920	233	0.	.1	1726.0				
1	0245	34	12.	.9	1727.1	*	1	1105	134	3.	.3	1726.3	*	1	1925	234	0.	.1	1726.0				
1	0250	35	13.	.9	1727.2	*	1	1110	135	3.	.3	1726.3	*	1	1930	235	0.	.1	1726.0				
1	0255	36	13.	1.0	1727.2	*	1	1115	136	3.	.3	1726.3	*	1	1935	236	0.	.1	1726.0				
1	0300	37	14.	1.0	1727.3	*	1	1120	137	3.	.2	1726.2	*	1	1940	237	0.	.1	1726.0				
1	0305	38	15.	1.0	1727.3	*	1	1125	138	2.	.2	1726.2	*	1	1945	238	0.	.1	1726.0				
1	0310	39	16.	1.1	1727.5	*	1	1130	139	2.	.2	1726.2	*	1	1950	239	0.	.1	1726.0				







1	0210	27	1.	.1	1726.1	*	1	1030	127	0.	.1	1726.0	*	1	1850	227	0.	.1	1726.0
1	0215	28	1.	.2	1726.1	*	1	1035	128	0.	.1	1726.0	*	1	1855	228	0.	.1	1726.0
1	0220	29	1.	.2	1726.1	*	1	1040	129	0.	.1	1726.0	*	1	1900	229	0.	.1	1726.0
1	0225	30	2.	.2	1726.1	*	1	1045	130	0.	.1	1726.0	*	1	1905	230	0.	.1	1726.0
1	0230	31	2.	.2	1726.2	*	1	1050	131	0.	.1	1726.0	*	1	1910	231	0.	.1	1726.0
1	0235	32	2.	.2	1726.2	*	1	1055	132	0.	.1	1726.0	*	1	1915	232	0.	.1	1726.0
1	0240	33	2.	.2	1726.2	*	1	1100	133	0.	.1	1726.0	*	1	1920	233	0.	.1	1726.0
1	0245	34	3.	.3	1726.3	*	1	1105	134	0.	.1	1726.0	*	1	1925	234	0.	.1	1726.0
1	0250	35	3.	.3	1726.3	*	1	1110	135	0.	.1	1726.0	*	1	1930	235	0.	.1	1726.0
1	0255	36	3.	.3	1726.3	*	1	1115	136	0.	.1	1726.0	*	1	1935	236	0.	.1	1726.0
1	0300	37	4.	.3	1726.3	*	1	1120	137	0.	.1	1726.0	*	1	1940	237	0.	.1	1726.0
1	0305	38	4.	.3	1726.4	*	1	1125	138	0.	.1	1726.0	*	1	1945	238	0.	.1	1726.0
1	0310	39	5.	.4	1726.4	*	1	1130	139	0.	.1	1726.0	*	1	1950	239	0.	.1	1726.0
1	0315	40	6.	.5	1726.5	*	1	1135	140	0.	.1	1726.0	*	1	1955	240	0.	.1	1726.0
1	0320	41	8.	.6	1726.8	*	1	1140	141	0.	.1	1726.0	*	1	2000	241	0.	.1	1726.0
1	0325	42	13.	.9	1727.2	*	1	1145	142	0.	.1	1726.0	*	1	2005	242	0.	.1	1726.0
1	0330	43	20.	1.4	1727.8	*	1	1150	143	0.	.1	1726.0	*	1	2010	243	0.	.1	1726.0
1	0335	44	24.	2.0	1728.3	*	1	1155	144	0.	.1	1726.0	*	1	2015	244	0.	.1	1726.0
1	0340	45	26.	2.6	1728.7	*	1	1200	145	0.	.1	1726.0	*	1	2020	245	0.	.1	1726.0
1	0345	46	28.	3.2	1729.1	*	1	1205	146	0.	.1	1726.0	*	1	2025	246	0.	.1	1726.0
1	0350	47	29.	3.7	1729.4	*	1	1210	147	0.	.1	1726.0	*	1	2030	247	0.	.1	1726.0
1	0355	48	30.	4.1	1729.6	*	1	1215	148	0.	.1	1726.0	*	1	2035	248	0.	.1	1726.0
1	0400	49	31.	4.4	1729.7	*	1	1220	149	0.	.1	1726.0	*	1	2040	249	0.	.1	1726.0
1	0405	50	31.	4.6	1729.9	*	1	1225	150	0.	.1	1726.0	*	1	2045	250	0.	.1	1726.0
1	0410	51	32.	4.7	1729.9	*	1	1230	151	0.	.1	1726.0	*	1	2050	251	0.	.1	1726.0
1	0415	52	32.	4.8	1730.0	*	1	1235	152	0.	.1	1726.0	*	1	2055	252	0.	.1	1726.0
1	0420	53	32.	4.9	1730.0	*	1	1240	153	0.	.1	1726.0	*	1	2100	253	0.	.1	1726.0
1	0425	54	32.	4.9	1730.0	*	1	1245	154	0.	.1	1726.0	*	1	2105	254	0.	.1	1726.0
1	0430	55	32.	4.9	1730.0	*	1	1250	155	0.	.1	1726.0	*	1	2110	255	0.	.1	1726.0
1	0435	56	32.	4.9	1730.0	*	1	1255	156	0.	.1	1726.0	*	1	2115	256	0.	.1	1726.0
1	0440	57	32.	4.9	1730.0	*	1	1300	157	0.	.1	1726.0	*	1	2120	257	0.	.1	1726.0
1	0445	58	32.	4.9	1730.1	*	1	1305	158	0.	.1	1726.0	*	1	2125	258	0.	.1	1726.0
1	0450	59	32.	5.0	1730.1	*	1	1310	159	0.	.1	1726.0	*	1	2130	259	0.	.1	1726.0
1	0455	60	32.	5.0	1730.1	*	1	1315	160	0.	.1	1726.0	*	1	2135	260	0.	.1	1726.0
1	0500	61	32.	5.0	1730.1	*	1	1320	161	0.	.1	1726.0	*	1	2140	261	0.	.1	1726.0
1	0505	62	32.	5.0	1730.1	*	1	1325	162	0.	.1	1726.0	*	1	2145	262	0.	.1	1726.0
1	0510	63	32.	4.9	1730.0	*	1	1330	163	0.	.1	1726.0	*	1	2150	263	0.	.1	1726.0
1	0515	64	32.	4.8	1730.0	*	1	1335	164	0.	.1	1726.0	*	1	2155	264	0.	.1	1726.0
1	0520	65	32.	4.7	1729.9	*	1	1340	165	0.	.1	1726.0	*	1	2200	265	0.	.1	1726.0
1	0525	66	31.	4.6	1729.9	*	1	1345	166	0.	.1	1726.0	*	1	2205	266	0.	.1	1726.0
1	0530	67	31.	4.5	1729.8	*	1	1350	167	0.	.1	1726.0	*	1	2210	267	0.	.1	1726.0
1	0535	68	31.	4.3	1729.7	*	1	1355	168	0.	.1	1726.0	*	1	2215	268	0.	.1	1726.0
1	0540	69	30.	4.2	1729.6	*	1	1400	169	0.	.1	1726.0	*	1	2220	269	0.	.1	1726.0
1	0545	70	30.	4.0	1729.5	*	1	1405	170	0.	.1	1726.0	*	1	2225	270	0.	.1	1726.0
1	0550	71	29.	3.8	1729.4	*	1	1410	171	0.	.1	1726.0	*	1	2230	271	0.	.1	1726.0
1	0555	72	29.	3.7	1729.4	*	1	1415	172	0.	.1	1726.0	*	1	2235	272	0.	.1	1726.0
1	0600	73	28.	3.5	1729.3	*	1	1420	173	0.	.1	1726.0	*	1	2240	273	0.	.1	1726.0
1	0605	74	28.	3.3	1729.2	*	1	1425	174	0.	.1	1726.0	*	1	2245	274	0.	.1	1726.0
1	0610	75	27.	3.2	1729.1	*	1	1430	175	0.	.1	1726.0	*	1	2250	275	0.	.1	1726.0
1	0615	76	27.	3.0	1729.0	*	1	1435	176	0.	.1	1726.0	*	1	2255	276	0.	.1	1726.0
1	0620	77	26.	2.8	1728.9	*	1	1440	177	0.	.1	1726.0	*	1	2300	277	0.	.1	1726.0
1	0625	78	26.	2.7	1728.8	*	1	1445	178	0.	.1	1726.0	*	1	2305	278	0.	.1	1726.0
1	0630	79	25.	2.5	1728.6	*	1	1450	179	0.	.1	1726.0	*	1	2310	279	0.	.1	1726.0
1	0635	80	25.	2.3	1728.5	*	1	1455	180	0.	.1	1726.0	*	1	2315	280	0.	.1	1726.0
1	0640	81	24.	2.2	1728.4	*	1	1500	181	0.	.1	1726.0	*	1	2320	281	0.	.1	1726.0
1	0645	82	24.	2.0	1728.3	*	1	1505	182	0.	.1	1726.0	*	1	2325	282	0.	.1	1726.0
1	0650	83	23.	1.8	1728.2	*	1	1510	183	0.	.1	1726.0	*	1	2330	283	0.	.1	1726.0
1	0655	84	23.	1.7	1728.1	*	1	1515	184	0.	.1	1726.0	*	1	2335	284	0.	.1	1726.0
1	0700	85	22.	1.5	1728.0	*	1	1520	185	0.	.1	1726.0	*	1	2340	285	0.	.1	1726.0
1	0705	86	20.	1.4	1727.8	*	1	1525	186	0.	.1	1726.0	*	1	2345	286	0.	.1	1726.0
1	0710	87	18.	1.3	1727.6	*	1	1530	187	0.	.1	1726.0	*	1	2350	287	0.	.1	1726.0
1	0715	88	16.	1.1	1727.5	*	1	1535	188	0.	.1	1726.0	*	1	2355	288	0.	.1	1726.0
1	0720	89	15.	1.0	1727.3	*	1	1540	189	0.	.1	1726.0	*	2	0000	289	0.	.1	1726.0
1	0725	90	13.	.9	1727.2	*	1	1545	190	0.	.1	1726.0	*	2	0005	290	0.	.1	1726.0
1	0730	91	12.	.9	1727.1	*	1	1550	191	0.	.1	1726.0	*	2	0010	291	0.	.1	1726.0
1	0735	92	11.	.8	1727.0	*	1	1555	192	0.	.1	1726.0	*	2	0015	292	0.	.1	1726.0
1	0740	93	10.	.7	1726.9	*	1	1600	193	0.	.1	1726.0	*	2	0020	293	0.	.1	1726.0
1	0745	94	9.	.7	1726.8	*	1	1605	194	0.	.1	1726.0	*	2	0025	294	0.	.1	1726.0
1	0750	95	8.	.6	1726.7	*	1	1610	195	0.	.1	1726.0	*	2	0030	295	0.	.1	1726.0
1	0755	96	7.	.5	1726.6	*	1	1615	196	0.	.1	1726.0	*	2	0035	296	0.	.1	1726.0
1	0800	97	6.	.5	1726.6	*	1	1620	197	0.	.1	1726.0	*	2	0040	297	0.	.1	1726.0
1	0805	98	6.	.5	1726.5	*	1	1625	198	0.	.1	1726.0	*	2	0045	298	0.	.1	1726.0
1	0810	99	5.	.4	1726.5	*	1	1630	199	0.	.1	1726.0	*	2	0050	299	0.	.1	1726.0
1	0815	100	5.	.4	1726.4	*	1	1635	200	0.	.1	1726.0	*	2	0055	300	0.	.1	1726.0

PEAK FLOW	TIME		6-HR	24-HR	72-HR	24.92-HR
+	(CFS)	(HR)				
+	32.	5.00				
		(CFS)	20.	5.	5.	5.
		(INCHES)	1.266	1.301	1.301	1.301
		(AC-FT)	10.	10.	10.	10.
PEAK STORAGE	TIME		6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)	(HR)				
+	5.	5.00	2.	1.	1.	1.
PEAK STAGE	TIME		6-HR	24-HR	72-HR	24.92-HR
+	(FEET)	(HR)				
+	1730.08	5.00	1728.29	1726.59	1726.56	1726.56
CUMULATIVE AREA =			.15 SQ MI			

HYDROGRAPH AT STATION DETPOND  
PLAN 1, RATIO = .58

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
1	0000	1	0.	.1	1726.0	*	1	0820	101	3.	.3	1726.3	*	1	1640	201	0.	.1	1726.0	*
1	0005	2	0.	.1	1726.0	*	1	0825	102	3.	.3	1726.3	*	1	1645	202	0.	.1	1726.0	*
1	0010	3	0.	.1	1726.0	*	1	0830	103	3.	.3	1726.3	*	1	1650	203	0.	.1	1726.0	*
1	0015	4	0.	.1	1726.0	*	1	0835	104	3.	.2	1726.2	*	1	1655	204	0.	.1	1726.0	*
1	0020	5	0.	.1	1726.0	*	1	0840	105	2.	.2	1726.2	*	1	1700	205	0.	.1	1726.0	*
1	0025	6	0.	.1	1726.0	*	1	0845	106	2.	.2	1726.2	*	1	1705	206	0.	.1	1726.0	*
1	0030	7	0.	.1	1726.0	*	1	0850	107	2.	.2	1726.2	*	1	1710	207	0.	.1	1726.0	*
1	0035	8	0.	.1	1726.0	*	1	0855	108	2.	.2	1726.2	*	1	1715	208	0.	.1	1726.0	*
1	0040	9	0.	.1	1726.0	*	1	0900	109	2.	.2	1726.1	*	1	1720	209	0.	.1	1726.0	*
1	0045	10	0.	.1	1726.0	*	1	0905	110	1.	.1	1726.1	*	1	1725	210	0.	.1	1726.0	*
1	0050	11	0.	.1	1726.0	*	1	0910	111	1.	.2	1726.1	*	1	1730	211	0.	.1	1726.0	*
1	0055	12	0.	.1	1726.0	*	1	0915	112	1.	.2	1726.1	*	1	1735	212	0.	.1	1726.0	*
1	0100	13	0.	.1	1726.0	*	1	0920	113	1.	.1	1726.1	*	1	1740	213	0.	.1	1726.0	*



1	0105	14	0.	.1	1726.0	*	1	0925	114	1.	.1	1726.1	*	1	1745	214	0.	.1	1726.0
1	0110	15	0.	.1	1726.0	*	1	0930	115	1.	.1	1726.1	*	1	1750	215	0.	.1	1726.0
1	0115	16	0.	.1	1726.0	*	1	0935	116	1.	.1	1726.1	*	1	1755	216	0.	.1	1726.0
1	0120	17	0.	.1	1726.0	*	1	0940	117	1.	.1	1726.1	*	1	1800	217	0.	.1	1726.0
1	0125	18	0.	.1	1726.0	*	1	0945	118	1.	.1	1726.1	*	1	1805	218	0.	.1	1726.0
1	0130	19	0.	.1	1726.0	*	1	0950	119	1.	.1	1726.0	*	1	1810	219	0.	.1	1726.0
1	0135	20	0.	.1	1726.0	*	1	0955	120	0.	.1	1726.0	*	1	1815	220	0.	.1	1726.0
1	0140	21	0.	.1	1726.0	*	1	1000	121	0.	.1	1726.0	*	1	1820	221	0.	.1	1726.0
1	0145	22	0.	.1	1726.0	*	1	1005	122	0.	.1	1726.0	*	1	1825	222	0.	.1	1726.0
1	0150	23	0.	.1	1726.0	*	1	1010	123	0.	.1	1726.0	*	1	1830	223	0.	.1	1726.0
1	0155	24	1.	.1	1726.0	*	1	1015	124	0.	.1	1726.0	*	1	1835	224	0.	.1	1726.0
1	0200	25	1.	.1	1726.1	*	1	1020	125	0.	.1	1726.0	*	1	1840	225	0.	.1	1726.0
1	0205	26	1.	.1	1726.1	*	1	1025	126	0.	.1	1726.0	*	1	1845	226	0.	.1	1726.0
1	0210	27	1.	.1	1726.1	*	1	1030	127	0.	.1	1726.0	*	1	1850	227	0.	.1	1726.0
1	0215	28	1.	.1	1726.1	*	1	1035	128	0.	.1	1726.0	*	1	1855	228	0.	.1	1726.0
1	0220	29	1.	.2	1726.1	*	1	1040	129	0.	.1	1726.0	*	1	1900	229	0.	.1	1726.0
1	0225	30	1.	.2	1726.1	*	1	1045	130	0.	.1	1726.0	*	1	1905	230	0.	.1	1726.0
1	0230	31	2.	.2	1726.1	*	1	1050	131	0.	.1	1726.0	*	1	1910	231	0.	.1	1726.0
1	0235	32	2.	.2	1726.2	*	1	1055	132	0.	.1	1726.0	*	1	1915	232	0.	.1	1726.0
1	0240	33	2.	.2	1726.2	*	1	1100	133	0.	.1	1726.0	*	1	1920	233	0.	.1	1726.0
1	0245	34	2.	.2	1726.2	*	1	1105	134	0.	.1	1726.0	*	1	1925	234	0.	.1	1726.0
1	0250	35	3.	.3	1726.3	*	1	1110	135	0.	.1	1726.0	*	1	1930	235	0.	.1	1726.0
1	0255	36	3.	.3	1726.3	*	1	1115	136	0.	.1	1726.0	*	1	1935	236	0.	.1	1726.0
1	0300	37	3.	.3	1726.3	*	1	1120	137	0.	.1	1726.0	*	1	1940	237	0.	.1	1726.0
1	0305	38	4.	.3	1726.3	*	1	1125	138	0.	.1	1726.0	*	1	1945	238	0.	.1	1726.0
1	0310	39	4.	.4	1726.4	*	1	1130	139	0.	.1	1726.0	*	1	1950	239	0.	.1	1726.0
1	0315	40	5.	.4	1726.5	*	1	1135	140	0.	.1	1726.0	*	1	1955	240	0.	.1	1726.0
1	0320	41	8.	.6	1726.7	*	1	1140	141	0.	.1	1726.0	*	1	2000	241	0.	.1	1726.0
1	0325	42	12.	.9	1727.1	*	1	1145	142	0.	.1	1726.0	*	1	2005	242	0.	.1	1726.0
1	0330	43	19.	1.3	1727.7	*	1	1150	143	0.	.1	1726.0	*	1	2010	243	0.	.1	1726.0
1	0335	44	23.	1.9	1728.2	*	1	1155	144	0.	.1	1726.0	*	1	2015	244	0.	.1	1726.0
1	0340	45	25.	2.5	1728.6	*	1	1200	145	0.	.1	1726.0	*	1	2020	245	0.	.1	1726.0
1	0345	46	27.	3.0	1729.0	*	1	1205	146	0.	.1	1726.0	*	1	2025	246	0.	.1	1726.0
1	0350	47	28.	3.5	1729.2	*	1	1210	147	0.	.1	1726.0	*	1	2030	247	0.	.1	1726.0
1	0355	48	29.	3.8	1729.4	*	1	1215	148	0.	.1	1726.0	*	1	2035	248	0.	.1	1726.0
1	0400	49	30.	4.1	1729.6	*	1	1220	149	0.	.1	1726.0	*	1	2040	249	0.	.1	1726.0
1	0405	50	30.	4.3	1729.7	*	1	1225	150	0.	.1	1726.0	*	1	2045	250	0.	.1	1726.0
1	0410	51	31.	4.4	1729.8	*	1	1230	151	0.	.1	1726.0	*	1	2050	251	0.	.1	1726.0
1	0415	52	31.	4.5	1729.8	*	1	1235	152	0.	.1	1726.0	*	1	2055	252	0.	.1	1726.0
1	0420	53	31.	4.5	1729.8	*	1	1240	153	0.	.1	1726.0	*	1	2100	253	0.	.1	1726.0
1	0425	54	31.	4.5	1729.8	*	1	1245	154	0.	.1	1726.0	*	1	2105	254	0.	.1	1726.0
1	0430	55	31.	4.5	1729.8	*	1	1250	155	0.	.1	1726.0	*	1	2110	255	0.	.1	1726.0
1	0435	56	31.	4.6	1729.8	*	1	1255	156	0.	.1	1726.0	*	1	2115	256	0.	.1	1726.0
1	0440	57	31.	4.6	1729.9	*	1	1300	157	0.	.1	1726.0	*	1	2120	257	0.	.1	1726.0
1	0445	58	31.	4.6	1729.9	*	1	1305	158	0.	.1	1726.0	*	1	2125	258	0.	.1	1726.0
1	0450	59	31.	4.6	1729.9	*	1	1310	159	0.	.1	1726.0	*	1	2130	259	0.	.1	1726.0
1	0455	60	31.	4.6	1729.9	*	1	1315	160	0.	.1	1726.0	*	1	2135	260	0.	.1	1726.0
1	0500	61	31.	4.6	1729.9	*	1	1320	161	0.	.1	1726.0	*	1	2140	261	0.	.1	1726.0
1	0505	62	31.	4.6	1729.9	*	1	1325	162	0.	.1	1726.0	*	1	2145	262	0.	.1	1726.0
1	0510	63	31.	4.6	1729.8	*	1	1330	163	0.	.1	1726.0	*	1	2150	263	0.	.1	1726.0
1	0515	64	31.	4.5	1729.8	*	1	1335	164	0.	.1	1726.0	*	1	2155	264	0.	.1	1726.0
1	0520	65	31.	4.4	1729.7	*	1	1340	165	0.	.1	1726.0	*	1	2200	265	0.	.1	1726.0
1	0525	66	30.	4.2	1729.7	*	1	1345	166	0.	.1	1726.0	*	1	2205	266	0.	.1	1726.0
1	0530	67	30.	4.1	1729.6	*	1	1350	167	0.	.1	1726.0	*	1	2210	267	0.	.1	1726.0
1	0535	68	30.	4.0	1729.5	*	1	1355	168	0.	.1	1726.0	*	1	2215	268	0.	.1	1726.0
1	0540	69	29.	3.8	1729.4	*	1	1400	169	0.	.1	1726.0	*	1	2220	269	0.	.1	1726.0
1	0545	70	29.	3.7	1729.3	*	1	1405	170	0.	.1	1726.0	*	1	2225	270	0.	.1	1726.0
1	0550	71	28.	3.5	1729.3	*	1	1410	171	0.	.1	1726.0	*	1	2230	271	0.	.1	1726.0
1	0555	72	28.	3.3	1729.2	*	1	1415	172	0.	.1	1726.0	*	1	2235	272	0.	.1	1726.0
1	0600	73	27.	3.2	1729.1	*	1	1420	173	0.	.1	1726.0	*	1	2240	273	0.	.1	1726.0
1	0605	74	27.	3.0	1729.0	*	1	1425	174	0.	.1	1726.0	*	1	2245	274	0.	.1	1726.0
1	0610	75	26.	2.8	1728.9	*	1	1430	175	0.	.1	1726.0	*	1	2250	275	0.	.1	1726.0
1	0615	76	26.	2.7	1728.8	*	1	1435	176	0.	.1	1726.0	*	1	2255	276	0.	.1	1726.0
1	0620	77	25.	2.5	1728.7	*	1	1440	177	0.	.1	1726.0	*	1	2300	277	0.	.1	1726.0
1	0625	78	25.	2.4	1728.6	*	1	1445	178	0.	.1	1726.0	*	1	2305	278	0.	.1	1726.0
1	0630	79	24.	2.2	1728.4	*	1	1450	179	0.	.1	1726.0	*	1	2310	279	0.	.1	1726.0
1	0635	80	24.	2.0	1728.3	*	1	1455	180	0.	.1	1726.0	*	1	2315	280	0.	.1	1726.0
1	0640	81	23.	1.9	1728.2	*	1	1500	181	0.	.1	1726.0	*	1	2320	281	0.	.1	1726.0
1	0645	82	23.	1.7	1728.1	*	1	1505	182	0.	.1	1726.0	*	1	2325	282	0.	.1	1726.0
1	0650	83	22.	1.6	1728.0	*	1	1510	183	0.	.1	1726.0	*	1	2330	283	0.	.1	1726.0
1	0655	84	20.	1.4	1727.9	*	1	1515	184	0.	.1	1726.0	*	1	2335	284	0.	.1	1726.0
1	0700	85	18.	1.3	1727.7	*	1	1520	185	0.	.1	1726.0	*	1	2340	285	0.	.1	1726.0
1	0705	86	17.	1.2	1727.5	*	1	1525	186	0.	.1	1726.0	*	1	2345	286	0.	.1	1726.0
1	0710	87	15.	1.1	1727.4	*	1	1530	187	0.	.1	1726.0	*	1	2350	287	0.	.1	1726.0
1	0715	88	14.	1.0	1727.2	*	1	1535	188	0.	.1	1726.0	*	1	2355	288	0.	.1	1726.0
1	0720	89	12.	.9	1727.1	*	1	1540	189	0.	.1	1726.0	*	2	0000	289	0.	.1	1726.0
1	0725	90	11.	.8	1727.0	*	1	1545	190	0.	.1	1726.0	*	2	0005	290	0.	.1	1726.0
1	0730	91	10.	.7	1726.9	*	1	1550	191	0.	.1	1726.0	*	2	0010	291	0.	.1	1726.0
1	0735	92	9.	.7	1726.8	*	1	1555	192	0.	.1	1726.0	*	2	0015	292	0.	.1	1726.0
1	0740	93	8.	.6	1726.7	*	1	1600	193	0.	.1	1726.0	*	2	0020	293	0.	.1	1726.0
1	0745	94	7.	.6	1726.6	*	1	1605	194	0.	.1	1726.0	*	2	0025	294	0.	.1	1726.0
1	0750	95	7.	.5	1726.6	*	1	1610											



OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION		
				RATIO 1 1.00	RATIO 2 .60	RATIO 3 .58
HYDROGRAPH AT +	OND8	.02	1 FLOW TIME	33. 3.58	16. 3.58	15. 3.58
HYDROGRAPH AT +	OND9	.00	1 FLOW TIME	3. 3.50	2. 3.50	1. 3.50
HYDROGRAPH AT +	OFFD3	.03	1 FLOW TIME	35. 3.58	16. 3.58	15. 3.58
2 COMBINED AT +	CP-7	.03	1 FLOW TIME	37. 3.58	17. 3.58	16. 3.58
2 COMBINED AT +	CP-8	.05	1 FLOW TIME	70. 3.58	33. 3.58	32. 3.58
ROUTED TO +	RCP8-CP-	.05	1 FLOW TIME	67. 3.67	32. 3.67	31. 3.67
HYDROGRAPH AT +	OND10	.01	1 FLOW TIME	10. 3.58	5. 3.58	5. 3.58
HYDROGRAPH AT +	OFFD5	.01	1 FLOW TIME	13. 3.58	6. 3.58	6. 3.58
3 COMBINED AT +	CP-9	.06	1 FLOW TIME	89. 3.58	41. 3.58	39. 3.67
ROUTED TO +	RCP9-CP-	.06	1 FLOW TIME	87. 3.58	41. 3.67	39. 3.67
HYDROGRAPH AT +	OND12	.00	1 FLOW TIME	8. 3.50	4. 3.50	4. 3.50
2 COMBINED AT +	CP-10A	.07	1 FLOW TIME	92. 3.58	43. 3.67	41. 3.67
HYDROGRAPH AT +	OND11	.01	1 FLOW TIME	24. 3.58	12. 3.58	11. 3.58
HYDROGRAPH AT +	OND13	.01	1 FLOW TIME	12. 3.50	6. 3.50	6. 3.50
3 COMBINED AT +	CP-10	.09	1 FLOW TIME	127. 3.58	60. 3.58	57. 3.58
ROUTED TO +	EQBASIN	.09	1 FLOW TIME	93. 3.75	39. 3.83	37. 3.83
				** PEAK STAGES IN FEET **		
1 STAGE				1748.19	1746.86	1746.78
TIME				3.75	3.83	3.83
DIVERSION TO +	DVPIPE	.09	1 FLOW TIME	67. 3.75	39. 3.83	37. 3.83
HYDROGRAPH AT +	DIVWEIR	.09	1 FLOW TIME	26. 3.75	0. .00	0. .00
HYDROGRAPH AT +	OND14	.02	1 FLOW TIME	31. 3.50	15. 3.50	14. 3.50
2 COMBINED AT +	CP-11	.11	1 FLOW TIME	39. 3.75	15. 3.50	14. 3.50
HYDROGRAPH AT +	OND1	.00	1 FLOW TIME	3. 3.50	1. 3.50	1. 3.50
HYDROGRAPH AT +	OFFD2	.01	1 FLOW TIME	23. 3.50	10. 3.50	10. 3.50
2 COMBINED AT +	CP-1	.02	1 FLOW TIME	25. 3.50	11. 3.50	11. 3.50
ROUTED TO +	RCP1-CP2	.02	1 FLOW TIME	24. 3.58	11. 3.58	11. 3.58
HYDROGRAPH AT +	OND2	.01	1 FLOW TIME	8. 3.58	4. 3.58	3. 3.58
HYDROGRAPH AT +	OFFD1	.07	1 FLOW TIME	87. 3.58	39. 3.58	37. 3.58
3 COMBINED AT +	CP-2	.09	1 FLOW TIME	120. 3.58	54. 3.58	51. 3.58
ROUTED TO +	RCP2-CP-	.09	1 FLOW	119.	53.	50.



					TIME	3.58	3.58	3.58
HYDROGRAPH AT								
+	OND3	.00	1	FLOW	4.	2.	2.	
				TIME	3.50	3.50	3.50	
2 COMBINED AT								
+	CP-3	.09	1	FLOW	121.	54.	51.	
				TIME	3.58	3.58	3.58	
ROUTED TO								
+	RCP3-CP4	.09	1	FLOW	118.	52.	49.	
				TIME	3.58	3.58	3.58	
HYDROGRAPH AT								
+	OND7	.01	1	FLOW	16.	8.	7.	
				TIME	3.50	3.50	3.50	
2 COMBINED AT								
+	CP-4	.10	1	FLOW	131.	59.	55.	
				TIME	3.58	3.58	3.58	
HYDROGRAPH AT								
+	OND4	.02	1	FLOW	27.	13.	12.	
				TIME	3.58	3.58	3.58	
HYDROGRAPH AT								
+	OND5	.01	1	FLOW	12.	6.	6.	
				TIME	3.58	3.58	3.58	
2 COMBINED AT								
+	CP-5	.03	1	FLOW	40.	19.	18.	
				TIME	3.58	3.58	3.58	
HYDROGRAPH AT								
+	OND6	.02	1	FLOW	23.	11.	11.	
				TIME	3.58	3.58	3.58	
HYDROGRAPH AT								
+	DVPIPE	.00	1	FLOW	67.	39.	37.	
				TIME	3.75	3.83	3.83	
ROUTED TO								
+	RDVPIPE	.00	1	FLOW	67.	38.	36.	
				TIME	3.83	3.83	3.83	
HYDROGRAPH AT								
+	DETPD	.01	1	FLOW	16.	8.	8.	
				TIME	3.50	3.50	3.50	
5 COMBINED AT								
+	CP-6	.15	1	FLOW	254.	119.	112.	
				TIME	3.58	3.58	3.58	
ROUTED TO								
+	DETPOND	.15	1	FLOW	45.	32.	31.	
				TIME	5.17	5.00	5.00	
** PEAK STAGES IN FEET **								
1	STAGE	1733.80	1730.08	1729.88				
	TIME	5.17	5.00	5.00				
HYDROGRAPH AT								
+	OFFD-14	.00	1	FLOW	3.	2.	1.	
				TIME	3.58	3.67	3.67	
ROUTED TO								
+	RT-B14	.00	1	FLOW	3.	1.	1.	
				TIME	3.67	3.67	3.67	
HYDROGRAPH AT								
+	EMIC-1	.01	1	FLOW	26.	13.	12.	
				TIME	3.50	3.50	3.50	
2 COMBINED AT								
+	C15	.02	1	FLOW	28.	14.	13.	
				TIME	3.50	3.50	3.50	
ROUTED TO								
+	RT-14	.02	1	FLOW	27.	13.	13.	
				TIME	3.50	3.50	3.50	
HYDROGRAPH AT								
+	EMIC-2	.01	1	FLOW	22.	11.	11.	
				TIME	3.50	3.50	3.50	
2 COMBINED AT								
+	C16	.03	1	FLOW	50.	25.	24.	
				TIME	3.50	3.50	3.50	
ROUTED TO								
+	RT-15	.03	1	FLOW	49.	24.	23.	
				TIME	3.50	3.50	3.50	
HYDROGRAPH AT								
+	SCH-2	.01	1	FLOW	13.	7.	6.	
				TIME	3.50	3.50	3.50	
2 COMBINED AT								
+	C17	.04	1	FLOW	61.	31.	29.	
				TIME	3.50	3.50	3.50	
ROUTED TO								
+	RT-16	.04	1	FLOW	59.	29.	27.	
				TIME	3.50	3.50	3.50	
HYDROGRAPH AT								
+	EMIC-3	.01	1	FLOW	21.	11.	10.	
				TIME	3.50	3.50	3.50	
HYDROGRAPH AT								
+	MGDEV-2	.01	1	FLOW	17.	9.	8.	
				TIME	3.50	3.50	3.50	
4 COMBINED AT								
+	C18	.20	1	FLOW	126.	68.	65.	
				TIME	3.50	3.50	3.50	
HYDROGRAPH AT								
+	HR3	.00	1	FLOW	3.	1.	1.	



				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	HR2	.00	1	FLOW	4.	2.	2.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	HR1	.00	1	FLOW	3.	2.	2.
				TIME	3.50	3.50	3.50
3 COMBINED AT							
+	CHR1	.00	1	FLOW	10.	5.	5.
				TIME	3.50	3.50	3.50
2 COMBINED AT							
+	C18B	.21	1	FLOW	136.	74.	70.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	OND15	.03	1	FLOW	57.	28.	27.
				TIME	3.50	3.50	3.50
HYDROGRAPH AT							
+	OFFD4	.01	1	FLOW	19.	9.	9.
				TIME	3.58	3.58	3.58

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR PLAN = 1	RATIO= 1.00								
RCP8-CP-	MANE	1.36	69.67	217.50	1.81	5.00	66.60	220.00	1.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4767E+01 EXCESS= .0000E+00 OUTFLOW= .4776E+01 BASIN STORAGE= .5556E-06 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO= .60								
RCP8-CP-	MANE	1.75	33.06	218.31	.83	5.00	32.31	220.00	.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2194E+01 EXCESS= .0000E+00 OUTFLOW= .2198E+01 BASIN STORAGE= .5369E-06 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO= .58								
RCP8-CP-	MANE	1.71	31.11	219.15	.79	5.00	30.65	220.00	.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2075E+01 EXCESS= .0000E+00 OUTFLOW= .2079E+01 BASIN STORAGE= .5580E-06 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO= 1.00								
RCP9-CP-	MANE	.43	88.20	215.76	1.82	5.00	86.53	215.00	1.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6239E+01 EXCESS= .0000E+00 OUTFLOW= .6240E+01 BASIN STORAGE= .3111E-06 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .60								
RCP9-CP-	MANE	.49	41.32	216.17	.84	5.00	41.28	220.00	.84
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2889E+01 EXCESS= .0000E+00 OUTFLOW= .2889E+01 BASIN STORAGE= .3050E-06 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .58								
RCP9-CP-	MANE	.50	39.15	220.28	.80	5.00	39.15	220.00	.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2735E+01 EXCESS= .0000E+00 OUTFLOW= .2735E+01 BASIN STORAGE= .3190E-06 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= 1.00								
RCP1-CP2	MANE	1.40	25.01	212.57	1.68	5.00	24.19	215.00	1.68
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1472E+01 EXCESS= .0000E+00 OUTFLOW= .1478E+01 BASIN STORAGE= .1971E-06 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO= .60								
RCP1-CP2	MANE	1.83	11.24	214.86	.74	5.00	11.22	215.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6495E+00 EXCESS= .0000E+00 OUTFLOW= .6514E+00 BASIN STORAGE= .2695E-06 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO= .58								
RCP1-CP2	MANE	1.82	10.72	214.12	.70	5.00	10.59	215.00	.70
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6118E+00 EXCESS= .0000E+00 OUTFLOW= .6142E+00 BASIN STORAGE= .1771E-06 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO= 1.00								
RCP2-CP-	MANE	.25	119.25	215.41	1.65	5.00	118.57	215.00	1.65
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7768E+01 EXCESS= .0000E+00 OUTFLOW= .7768E+01 BASIN STORAGE= .8974E-07 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .60								
RCP2-CP-	MANE	.29	53.80	215.59	.72	5.00	53.11	215.00	.72
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3399E+01 EXCESS= .0000E+00 OUTFLOW= .3399E+01 BASIN STORAGE= .9188E-07 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .58								
RCP2-CP-	MANE	.34	50.63	215.67	.68	5.00	50.01	215.00	.68
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3201E+01 EXCESS= .0000E+00 OUTFLOW= .3201E+01 BASIN STORAGE= .8963E-07 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= 1.00									



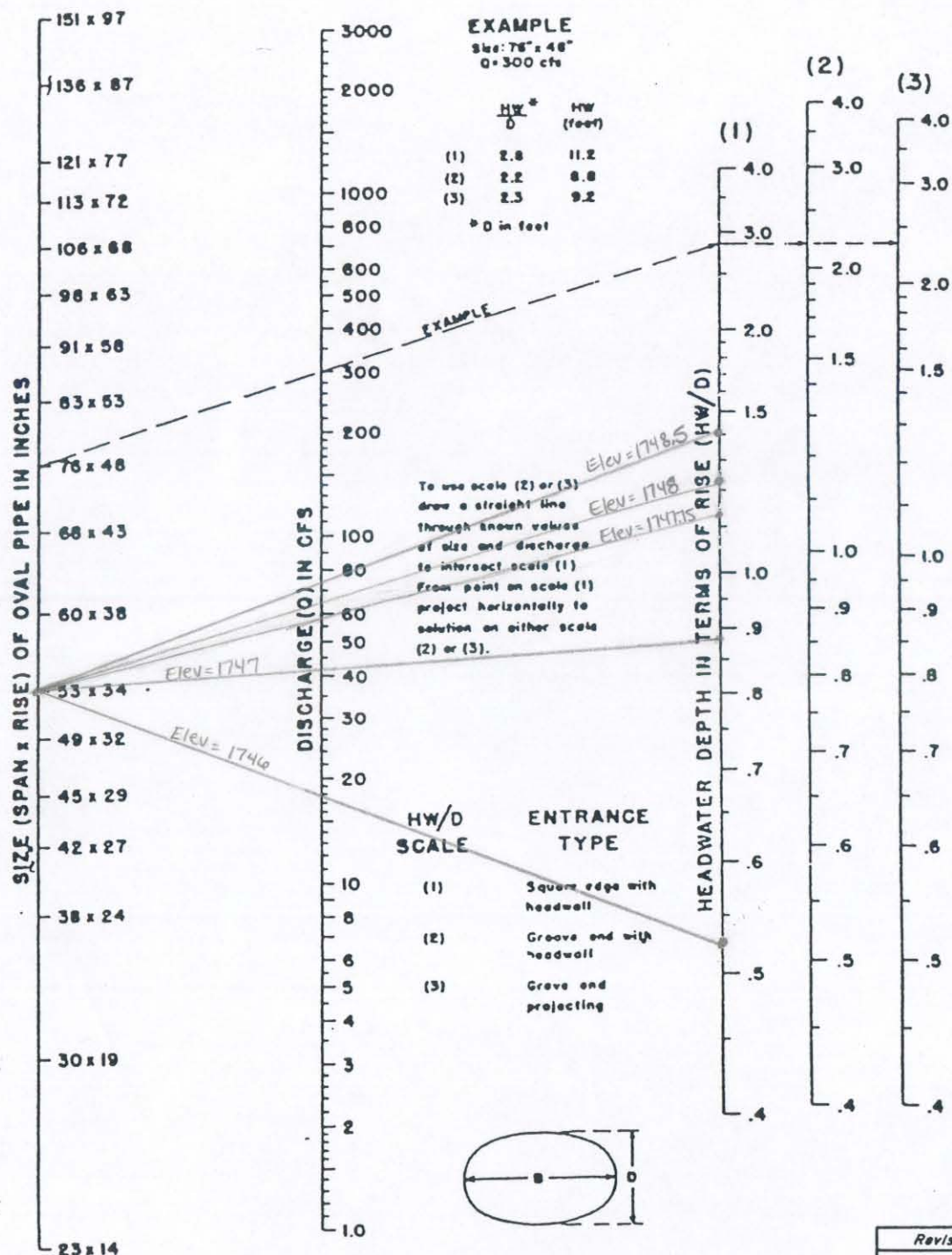
RCP3-CP4	MANE	.56	120.24	215.94	1.65	5.00	117.64	215.00	1.66
CONTINUITY SUMMARY (AC-PT) - INFLOW= .7973E+01 EXCESS= .0000E+00 OUTFLOW= .7976E+01 BASIN STORAGE= .3874E-06 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .60									
RCP3-CP4	MANE	.72	53.97	216.59	.72	5.00	51.67	215.00	.73
CONTINUITY SUMMARY (AC-PT) - INFLOW= .3490E+01 EXCESS= .0000E+00 OUTFLOW= .3493E+01 BASIN STORAGE= .4528E-06 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .58									
RCP3-CP4	MANE	.79	50.57	216.98	.68	5.00	48.54	215.00	.68
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3287E+01 EXCESS= .0000E+00 OUTFLOW= .3290E+01 BASIN STORAGE= .4272E-06 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= 1.00									
RDVPIPE	MANE	1.04	67.24	226.83	-1.00	5.00	66.79	230.00	-1.00
FOR PLAN = 1 RATIO= .60									
RDVPIPE	MANE	1.18	38.60	232.47	-1.00	5.00	38.25	230.00	-1.00
FOR PLAN = 1 RATIO= .58									
RDVPIPE	MANE	1.15	36.67	232.60	-1.00	5.00	36.35	230.00	-1.00
FOR PLAN = 1 RATIO= 1.00									
RT-B14	MANE	1.36	3.39	218.69	1.64	5.00	3.37	220.00	1.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2438E+00 EXCESS= .0000E+00 OUTFLOW= .2442E+00 BASIN STORAGE= .7570E-08 PERCENT ERROR= -.2									
FOR PLAN = 1 RATIO= .60									
RT-B14	MANE	1.71	1.51	223.43	.71	5.00	1.50	220.00	.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1061E+00 EXCESS= .0000E+00 OUTFLOW= .1063E+00 BASIN STORAGE= .7638E-08 PERCENT ERROR= -.2									
FOR PLAN = 1 RATIO= .58									
RT-B14	MANE	1.76	1.42	222.80	.67	5.00	1.41	220.00	.67
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9979E-01 EXCESS= .0000E+00 OUTFLOW= .9993E-01 BASIN STORAGE= .5886E-08 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= 1.00									
RT-14	MANE	.37	27.93	210.77	1.91	5.00	27.32	210.00	1.91
CONTINUITY SUMMARY (AC-PT) - INFLOW= .1720E+01 EXCESS= .0000E+00 OUTFLOW= .1721E+01 BASIN STORAGE= .7751E-08 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .60									
RT-14	MANE	.42	13.81	211.01	.91	5.00	13.40	210.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8203E+00 EXCESS= .0000E+00 OUTFLOW= .8205E+00 BASIN STORAGE= .6549E-08 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .58									
RT-14	MANE	.41	13.17	210.75	.86	5.00	12.73	210.00	.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7778E+00 EXCESS= .0000E+00 OUTFLOW= .7780E+00 BASIN STORAGE= .6560E-08 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= 1.00									
RT-15	MANE	.36	49.16	210.62	1.93	5.00	48.56	210.00	1.94
CONTINUITY SUMMARY (AC-PT) - INFLOW= .2959E+01 EXCESS= .0000E+00 OUTFLOW= .2959E+01 BASIN STORAGE= .9128E-08 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .60									
RT-15	MANE	.35	24.51	210.82	.93	5.00	24.04	210.00	.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1419E+01 EXCESS= .0000E+00 OUTFLOW= .1420E+01 BASIN STORAGE= .8611E-08 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .58									
RT-15	MANE	.35	23.31	210.84	.88	5.00	22.85	210.00	.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1347E+01 EXCESS= .0000E+00 OUTFLOW= .1347E+01 BASIN STORAGE= .8421E-08 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= 1.00									
RT-16	MANE	.53	60.94	211.13	1.94	5.00	58.94	210.00	1.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3645E+01 EXCESS= .0000E+00 OUTFLOW= .3647E+01 BASIN STORAGE= .3120E-07 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .60									
RT-16	MANE	.65	30.36	211.36	.93	5.00	28.90	210.00	.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1751E+01 EXCESS= .0000E+00 OUTFLOW= .1752E+01 BASIN STORAGE= .3374E-07 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .58									
RT-16	MANE	.62	28.82	211.06	.89	5.00	27.44	210.00	.89
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1661E+01 EXCESS= .0000E+00 OUTFLOW= .1663E+01 BASIN STORAGE= .3305E-07 PERCENT ERROR= -.1									



\*\*\* NORMAL END OF HEC-1 \*\*\*



## NOMOGRAPH - INLET CONTROL ELLIPTICAL PIPE



Revision	Date



### Equalizer Basin

ELEVATION	AREA (ft <sup>2</sup> )	AREA (ac-ft)	42" ELLIPTICAL PIPE FLOW (cfs)	SPILLWAY OVERFLOW (cfs)	TOTAL DISCHARGE(cfs)
1744.50	0	0.00	0	0	0
1745.00	3480	0.08	0	0	0
1746.00	30510	0.70	18	0	18
1747.00	34005	0.78	42	0	42
1747.75	36890	0.85	59	0	59
1748.00	37850	0.87	64	10	74
1748.50	42210	0.97	73	53	126

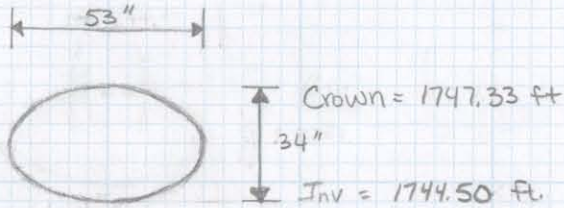
**NOTE:** 1) Areas were determined by using AutoCAD

2) The flow through the 42" elliptical pipe was calculated using the nomograph. See attached nomograph.

3) The flow overtopping the equalizer basin was calculated using the weir equation. See attached calculations.



Subject: 42" Elliptical RCP at Equalizer Basin  
Sample Calculations



42" Elliptical RCP

Sample Calculation @ Elevation 1748.50

$$HW = 1748.5 - 1744.5 = 4 \text{ ft}$$

$$D = \left(\frac{34}{12}\right) = 2.83 \text{ ft}$$

$$\frac{HW}{D} = \frac{4.0 \text{ ft}}{2.83 \text{ ft}} = 1.41$$

Plot 1.41 on nomograph to get flow through elliptical pipe.

∴ Flow through elliptical pipe at elevation 1748.50 is 73 cfs

Wier Equation

$$Q = CLH^{3/2}$$

$$Q = 2.7(30 \text{ ft})(1748.50 - 1747.75)^{3/2} = 53 \text{ cfs}$$

Total flow leaving equalizer basin at elevation 1748.50:

$$Q_{\text{TOTAL}} = 73 \text{ cfs} + 53 \text{ cfs} = 126 \text{ cfs}$$



## Detention Basin

ELEVATION	HEIGHT (ft)	AREA (ft <sup>2</sup> )	VOLUME (ft <sup>3</sup> )	VOLUME (acre-ft)	CUMMULATIVE VOLUME (acre/ft)	OUTFLOW (ft <sup>3</sup> /s)
1725.25	0.0	0	0	0.00	0.00	0
1726.00	0.75	9360	3510	0.08	0.08	0
1728.00	2.0	53790	63150	1.45	1.53	22
1729.00	1.0	76290	65040	1.49	3.02	27
1730.00	1.0	82060	79175	1.82	4.84	32
1732.00	2.0	93665	175725	4.03	8.88	40
1734.00	2.0	105690	199355	4.58	13.45	46
1735.00	1.0	112360	109025	2.50	15.95	49

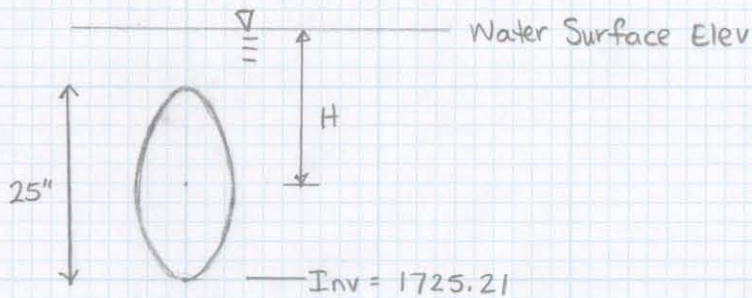
**Note:** 1) Areas were determined by using AutoCAD

2) The outflow was calculated by using the orifice equation. See attached calculations.



Subject: Detention Basin Outlet

$$Q = 0.61 A \sqrt{2gH}$$



Center Elev of 25" orifice =

$$1725.21 + \frac{(25")}{12} = 1726.25$$

Sample Calculation for orifice outlet

Water Surface Elev = 1728

$$Q = 0.61 (\pi (1.042 ft)^2) \sqrt{2 (32.2) (1728 - 1726.25)} = 22.08 \text{ cfs}$$



## Project Description

### Input Data

## Section Definitions

## Results

10/4/2006 3:02:24 PM Bentley Systems, Inc. Haestad Methods Solution Center Bentley FlowMaster [08.01.066.00]  
27 Siemens Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2



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## Worksheet for OND8 channel

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### Results

Flow Type                      Subcritical

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.87	ft
Critical Depth	0.65	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.01133	ft/ft



## Cross Section for OND8 channel

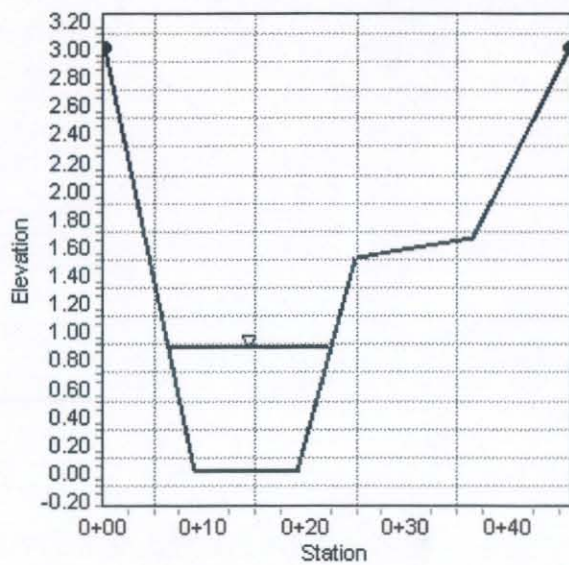
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Channel Slope	0.40000	%
Normal Depth	0.87	ft
Discharge	33.00	ft <sup>3</sup> /s

### Cross Section Image



$$t_{\text{channel}} = \frac{\text{channel path length}}{\text{velocity}} = \frac{2382 \text{ ft}}{2.95 \text{ ft/s}} = \left( \frac{807.5 \text{ sec}}{1} \right) \left( \frac{1 \text{ min}}{60 \text{ sec}} \right) = 13.5 \text{ min}$$

$t_{\text{overland}} = \text{calculated from standard form 4} = 1.9 \text{ min}$

$$t_c = 13.5 + 1.9 = 15.4 \text{ min} \quad \therefore t_{\text{lag}} = 0.15 \text{ hrs}$$





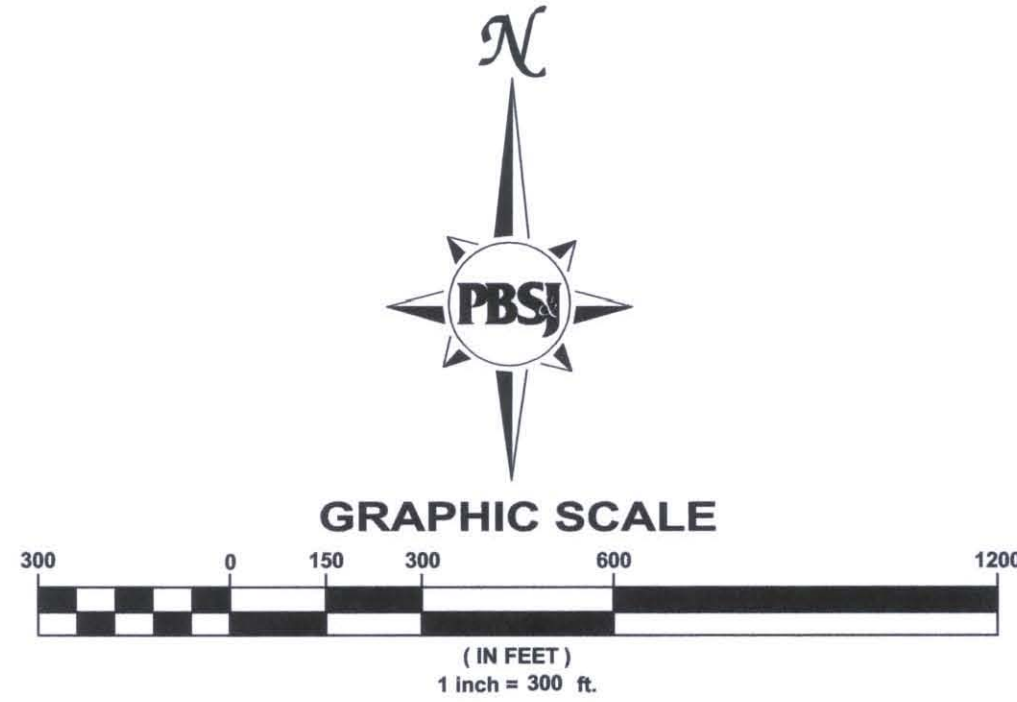
LEGEND

- ON-SITE BASIN BOUNDARY
- OFF-SITE BASIN BOUNDARY
- REFERENCED BASIN BOUNDARY
- OND1 ON-SITE BASIN LABEL
- OFFD1 OFF-SITE BASIN LABEL
- HR1 REFERENCED BASIN LABEL
- CP-1 HEC-1 COMBINATION POINT
- DISCHARGE POINT
- FLOW DIRECTION
- REFERENCED BASIN BOUNDARY
- EXISTING LANDFILL BOUNDARY

NOTES

"ADDENDUM #1 TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMERCE CENTER TWO (FORMERLY KNOWN AS HARSH) PREPARED BY PBS&J (FEBRUARY 2003) WAS USED FOR REFERENCED BASINS

BASIN ID	AREA (ac)	Q <sub>100</sub> (cfs)	Q <sub>10</sub> (cfs)
OND1	0.94	3	1
OND2	3.70	8	4
OND3	1.38	4	2
OND4	11.67	27	13
OND5	5.03	12	6
OND6	9.90	23	11
OND7	5.87	16	8
OND8	14.26	33	16
OND9	1.06	3	2
OND10	4.28	10	5
OND11	9.60	24	12
OND12	2.77	8	4
OND13	4.70	12	6
OND14	11.12	31	15
OND15	21.47	57	28
DETPD	5.14	16	8
OFFD1	42.20	87	39
OFFD2	9.63	23	10
OFFD3	16.40	35	16
OFFD4	7.61	19	9
OFFD5	5.11	13	6
CP-1	NA	25	11
CP-2	NA	120	54
CP-3	NA	121	54
CP-4	NA	131	59
CP-5	NA	40	19
CP-6	NA	254	119
CP-7	NA	37	17
CP-8	NA	70	33
CP-9	NA	89	41
CP-10	NA	127	60
CP-10A	NA	92	43
CP-11	NA	39	15
C18	NA	126	68
C18B	NA	136	74



511963.19 OCTOBER 2006

FIGURE 6  
DEVELOPED CONDITION  
DRAINAGE MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL






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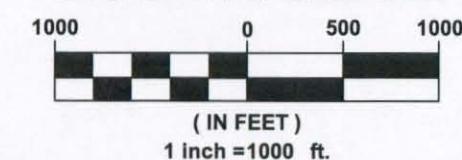


# LEGEND

-  PROPERTY BOUNDARY
-  SOIL BOUNDARY
-  SOIL MAP SYMBOL



## GRAPHIC SCALE



511693.19

SEPTEMBER 2006

### FIGURE B-4 SOIL MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



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## Curve Number Calculations



Existing Condition Hydrology

Basin Name	Soil Type	Hydrologic Group	Land Use	Curve No.	% of Composition				Composite Curve No.
ONEX1	187	0 %A 100 %B 0 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	77.00	46%	46%	35.42	35.42	--
	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	44%	90%	37.40	72.82	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	10%	100%	9.10	81.92	81.9
ONEX2	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	72%	72%	61.20	61.20	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	28%	100%	25.48	86.68	86.7
ONEX3	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	100%	91.00	91.00	91.0
ONEX4	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	61%	61%	51.85	51.85	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	39%	100%	35.49	87.34	87.3
ONEX5	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	100%	91.00	91.00	91.0
OFFEX1	187	0 %A 100 %B 0 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	77.00	92%	92%	70.84	70.84	--
	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	8%	100%	6.80	77.64	77.6
OFFEX2	187	0 %A 100 %B 0 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	77.00	81%	81%	62.37	62.37	--
	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	19%	100%	16.15	78.52	78.5
OFFEX3	187	0 %A 100 %B 0 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	77.00	37%	37%	28.49	28.49	--
	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	63%	100%	53.55	82.04	82.0
OFFEX4	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	100%	100%	85.00	85.00	85.0
OFFEX5	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	100%	100%	85.00	85.00	85.0



## Curve Number Calculations

Insert

Delete

Interim Condition Hydrology

Basin Name	Soil Type	Hydrologic Group	Land Use	Curve No.	% of Composition	Composite Curve No.
OND1	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	85%	--
	187	0 %A 100 %B 0 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	86.00	15%	87.7
OND2	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	87%	--
	187	0 %A 100 %B 0 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	86.00	13%	87.7
OND3	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	94%	--
	187	0 %A 100 %B 0 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	6%	88.6
OND4	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	42%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	58%	89.7
OND5	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND6	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	92%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	8%	91.0
OND7	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	19%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	76%	--
	615	0 %A 0 %B 100 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	6%	90.8
OND8	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	21%	--
	187	0 %A 100 %B 0 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	86.00	1%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	75%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	3%	90.3
OND9	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND10	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	95%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	5%	91.0
OND11	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND12	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	95%	--
	615	0 %A 0 %B 100 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	5%	91.4
OND13	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	96%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	4%	91.0
OND14	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND15	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	97%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	3%	91.0
DETPD	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	31%	--
	615	0 %A 0 %B 100 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	5%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	64%	91.4
OFFEX1	187	0 %A 100 %B 0 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	77.00	92%	--
	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	8%	77.6
OFFEX2	187	0 %A 100 %B 0 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	77.00	81%	--
	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	19%	78.5
OFFEX3	187	0 %A 100 %B 0 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	77.00	37%	--
	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	63%	82.0
OFFEX4	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	100%	85.0
OFFEX5	615	0 %A 0 %B 100 %C 0 %D	Western Desert Urban Area - Natural Desert Landscaping	85.00	100%	85.0



## Curve Number Calculations

Insert

Delete

Developed Condition Hydrology

Basin Name	Soil Type	Hydrologic Group	Land Use	Curve No.	% of Composition	Composite Curve No.
OND1	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	85%	--
	187	0 %A 100 %B 0 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	86.00	15%	87.7
OND2	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	87%	--
	187	0 %A 100 %B 0 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	86.00	13%	87.7
OND3	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	94%	--
	187	0 %A 100 %B 0 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	6%	88.6
OND4	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	42%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	58%	89.7
OND5	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND6	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	92%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	8%	91.0
OND7	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	19%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	76%	--
	615	0 %A 0 %B 100 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	6%	90.8
OND8	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	21%	--
	187	0 %A 100 %B 0 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	86.00	1%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	75%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	3%	90.3
OND9	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND10	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	95%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	5%	91.0
OND11	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND12	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	95%	--
	615	0 %A 0 %B 100 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	5%	91.4
OND13	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	96%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	4%	91.0
OND14	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OND15	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	97%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	3%	91.0
DETPD	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	31%	--
	615	0 %A 0 %B 100 %C 0 %D	Impervious Area- Paved Parking Lots, Roofs, Driveways etc.	98.00	5%	--
	615	0 %A 0 %B 100 %C 0 %D	Newly Graded Areas (Pervious Areas Only, No Vegetation)	91.00	64%	91.4
OFFD1	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	92%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	8%	88.2
OFFD2	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	81%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	19%	88.6
OFFD3	187	0 %A 100 %B 0 %C 0 %D	Industrial (72% Imp)	88.00	37%	--
	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	63%	89.9
OFFD4	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0
OFFD5	615	0 %A 0 %B 100 %C 0 %D	Industrial (72% Imp)	91.00	100%	91.0



## **Rainfall Methodology**

### *A. Point Rainfall*

According to Figure 513 of the Criteria Manual the site is located outside the McCarran Rainfall area. The 100-year, 6-hour rainfall depth duration frequency values for areas located outside the McCarran Airport Rainfall area were obtained from Figure 506 of the Criteria Manual. According to Figure 506, the rainfall depth for the 100-year 6-hour event is 1.95 inches. This value was adjusted according to Table 501 by 1.43, for a 100-year recurrence interval. The adjusted rainfall depth is 2.79 inches and was calculated as follows:  $(1.95)(1.43) = 2.79$  inches. According to Figure 503, the rainfall depth for the 10-year 6-hour event is 1.35 inches. This value was adjusted according to Table 501 by 1.24, for a 10-year recurrence interval. The adjusted rainfall depth is 1.67 inches and is calculated as follows:  $(1.35)(1.24) = 1.67$  inches.

The HEC-1 multi-ratio option (HEC 1990) was used to model the 10-year and 100-year design storms in the HEC-1 input file. The HEC-1 JR card was used to specify the ratio by which to multiply the 100-year precipitation values (point rainfall). The 10-year and 100-year ratios are 0.60 and 1.00, respectively (see calculation for 10-year ratio included in this appendix).

### *B. Storm Distribution*

Table 503 in the Criteria Manual specifies that the 6-hour storm distribution, SDN 3 should be used for drainage areas less than eight square miles.

## **Runoff Methodology**

### *A. Lag Time*

The Criteria Manual's Standard Form 4 was completed to determine the time of concentration for each drainage basin. For all basins which comprise less than 1 square mile, the time of concentration was calculated as follows:

$$T_c = T_i + T_t$$

Where:  $T_c$  = Time of Concentration  
 $T_i$  = Initial, inlet or overland flow time  
 $T_t$  = Travel time in the ditch, gutter, etc.

The time of concentration is the sum of the initial flow time,  $T_i$  and the travel time,  $T_t$ . The minimum  $T_c$  recommended for non-urban watersheds is 10 minutes and 5 minute minimum for urban watersheds.

Initial flow time was calculated as follows:



$$T_i = 1.8(1.1 - K)L_o^{1/2}/S^{1/3}$$

Where:  $T_i$  = Initial overland flow time (in minutes)  
 $K = 0.0132CN - 0.39$   
 $CN$  = Curve Number  
 $L_o$  = Length of overland flow (maximum 500 feet)  
 $S$  = Average basin slope (in percent)

The lag time was calculated as follows:

$$T_{lag} = 0.6T_c \text{ (in hours)}$$

Travel time is calculated as follows:

$$T_t = L_t/(60 V)$$

Where:

$T_t$  = Travel time in the ditch, gutter, etc. (minutes)  
 $L_t$  = Travel Length (feet)  
 $V$  = Average velocity of flow (ft/s)

Now,

$$V = CS^{1/2}$$

$$C = 1.49/nR^{2/3}$$

$$R = A/P$$

Where:

$V$  = Average Velocity (fps)  
 $S$  = Average Slope (ft/ft)  
 $n$  = Manning's Roughness Coefficient  
 $R$  = Hydraulic Radius (ft)  
 $P$  = Wetted perimeter  
 $A$  = Area of Flow (sq ft)

Two sets of coefficients were determined, one for developed conditions (Urbanized Areas) and the other for undeveloped (Non-Urbanized Areas) conditions. The following coefficients shall be used for developed areas (Urbanized Areas). For the first developed conditions velocity ( $V_1$ ), the appropriate coefficient ( $C = 20.2$ ) represents street flow with  $n = 0.016$  and a depth in the gutter of 0.3 feet. For the second developed conditions velocity ( $V_2$ ), the appropriate coefficient ( $C=30.6$ ) represents curb height street flow. As may be noted,  $V_2$  is approximately equal to 1.5 times  $V_1$ . Typically, drainage areas are delineated such that the channelized flow considered in the calculations of travel times is within streets and other minor water courses and does not include significant lengths of major improved floodway and channels in the travel distance for the time of concentration.



The second set of coefficients shall be used in existing areas (Non-Urbanized Areas). For the first undeveloped conditions velocity ( $V_1$ ), the appropriate coefficient  $C = 14.8$  represents wide channel flow with  $D = 0.25$  feet and  $n = 0.04$ . For the second undeveloped conditions velocity ( $V_2$ ), the appropriate coefficient  $C = 29.4$  represents wide channel flow with  $D = 0.7$  feet and  $n = 0.04$ . The time of concentration for the first design point in an urbanized basin using this procedure should not exceed the time of concentration calculated using below equation, which was developed using rainfall/runoff data collected in urbanized regions.

$$t_c = L / 180 + 10 \quad (604)$$

Where  $t_c$  = Time of Concentration at the First Design Point in an Urban Watershed (min)

$L$  = Watershed Length (ft)

If the above equation results in a lesser time of concentration at the first design point and thus would govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream reaches. The minimum  $t_c$  recommended for urbanized areas is 5 minutes.

Subbasin OND8 time of concentration was adjusted because the velocities calculated by the above mentioned formulas did not accurately represent to channel velocity. A channel cross section for this basin is included in Appendix B-3. The velocity determined by using FlowMaster was 2.95ft/s. The Standard Form 4 channel velocity was calculated to be 1.9 ft/s. By using the velocity calculated by Flowmaster, the time of concentration reduced to 15 minutes. Please refer to Appendix B-3 for the calculations for the time of concentration.

#### *B. Soils – Curve Number Determination*

Soils information, for the onsite and offsite drainage basins, was obtained from the Soil Conservation Service (SCS) Soil Survey of Las Vegas Valley Area, Nevada, 1985. The project site and offsite basin is depicted on a SCS survey map and is included in this appendix, see **Figure B-4: Soil Map**. The soil types were matched to the corresponding SCS Curve Number (CN) for use in the Standard Form 4 and the HEC-1 analysis. The corresponding CN's for these soils are from Table 602 of the Criteria Manual. The onsite and offsite basins are composed of soil types #187 and #615 with a corresponding hydrologic group of B and C respectively.

In developed condition, the proposed landfill was classified as industrial because the landfill is planned to have a type II layer on the top. Since industrial has an imperviousness of 72%, this was assumed to be an appropriate curve number. The curve numbers for industrial are more conservative than curve numbers for gravel which would represent the type II material.



Imperviousness and newly graded curve numbers were also used to appropriately classify the designed drainage facilities around the landfill.

### *C. Routing*

Routing in improved channels or storm drains were performed using the Kinematic method. Kinematic routing requires the following input parameters: roughness coefficient, base width, side slope, slope, and reach length. Kinematic routing was used for subbasins delineated by PBS&J within this TDS.



## PRECIPITATION ADJUSTMENT RATIOS

<u>Recurrence Interval</u>	<u>Ratio to NOAA Atlas 2</u>
2-year	1.00
5-year	1.16
10-year	1.24
25-year	1.33
50-year	1.39
100-year	1.43

- NOTE: 1. Multiply the values obtained from the NOAA Atlas 2 by the above ratios to obtain the adjusted precipitation values.
2. NOAA Atlas 2 values for use with TR-55 shall not be adjusted by the above ratios.
3. Tables 505 and 506 require no adjustments.

<i>Revision</i>	<i>Date</i>



**SIX-HOUR STORM DISTRIBUTIONS**

Percent of Total Storm Depth				Percent of Total Storm Depth			
Storm Time (In Minutes)	SDN3	SDN4	SDN5	Storm Time (In Minutes)	SDN3	SDN4	SDN5
0	0.0	0.0	0.0	185	32.2	37.6	43.0
5	2.0	2.0	2.0	190	35.2	41.5	47.7
10	5.7	5.8	5.9	195	40.9	46.2	51.4
15	7.0	7.5	8.0	200	49.9	53.0	56.1
20	8.7	9.9	11.0	205	59.0	61.0	63.0
25	10.8	12.6	14.4	210	71.0	71.0	71.0
30	12.4	13.7	15.0	215	74.4	73.2	72.0
35	13.0	14.5	16.0	220	78.1	75.6	73.1
40	13.0	14.9	16.8	225	81.2	78.2	75.2
45	13.0	15.1	17.1	230	81.9	79.9	77.9
50	13.0	15.5	18.0	235	83.5	81.3	79.0
55	13.0	15.6	18.2	240	85.1	82.3	79.5
60	13.0	15.9	18.7	245	85.6	83.0	80.4
65	13.3	16.2	19.0	250	86.0	83.5	81.0
70	14.0	16.9	19.7	255	86.8	84.4	82.0
75	14.2	17.2	20.2	260	87.6	85.1	82.6
80	14.8	17.9	21.0	265	88.8	86.4	84.0
85	15.8	18.9	22.0	270	91.0	88.5	85.9
90	17.2	20.1	23.0	275	92.6	90.8	88.9
95	18.1	21.1	24.1	280	93.7	92.4	91.0
100	19.0	22.0	25.0	285	95.0	94.4	93.8
105	19.7	22.8	25.9	290	97.0	96.8	96.6
110	19.9	23.2	26.5	295	97.6	97.3	97.0
115	20.0	24.0	28.0	300	98.2	97.8	97.4
120	20.1	24.6	29.0	305	98.5	98.2	97.9
125	20.4	25.2	30.0	310	98.7	98.4	98.1
130	21.4	26.0	30.5	315	98.9	98.6	98.3
135	22.9	26.9	30.9	320	99.0	98.8	98.5
140	24.1	27.6	31.0	325	99.3	99.1	98.9
145	24.9	28.3	31.7	330	99.3	99.2	99.0
150	25.1	28.6	32.1	335	99.4	99.3	99.2
155	25.6	29.2	32.7	340	99.5	99.4	99.3
160	27.0	30.2	33.3	345	99.8	99.7	99.6
165	27.8	31.2	34.6	350	99.8	99.8	99.7
170	28.1	32.1	36.1	355	99.9	99.9	99.9
175	28.3	33.2	38.1	360	100.0	100.0	100.0
180	29.5	35.2	40.8				

- Notes: 1. For drainage areas less than 8 square miles in size, use SDN 3.  
 2. For drainage areas greater than or equal to 8 square miles and less than 12 square miles in size, use SDN 4.  
 3. For drainage areas greater than or equal to 12 square miles, use SDN 5.  
 4. A graphical representation of these values is presented on **Figure 515**.

Revision	Date

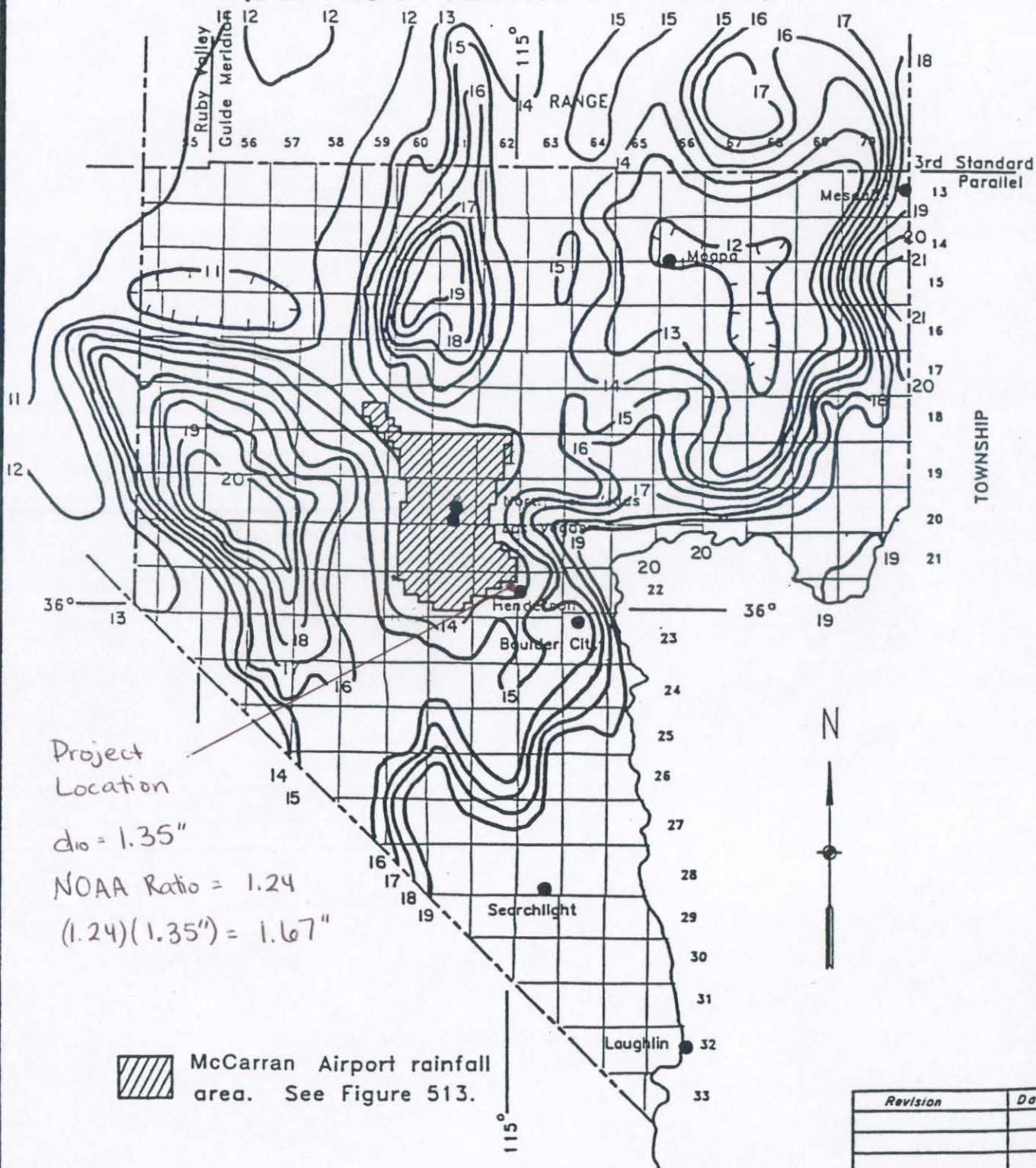
REFERENCE:

TABLE 503



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## RAINFALL DEPTH-DURATION-FREQUENCY 10-YEAR, 6-HOUR (DEPTHS IN TENTHS OF INCHES)

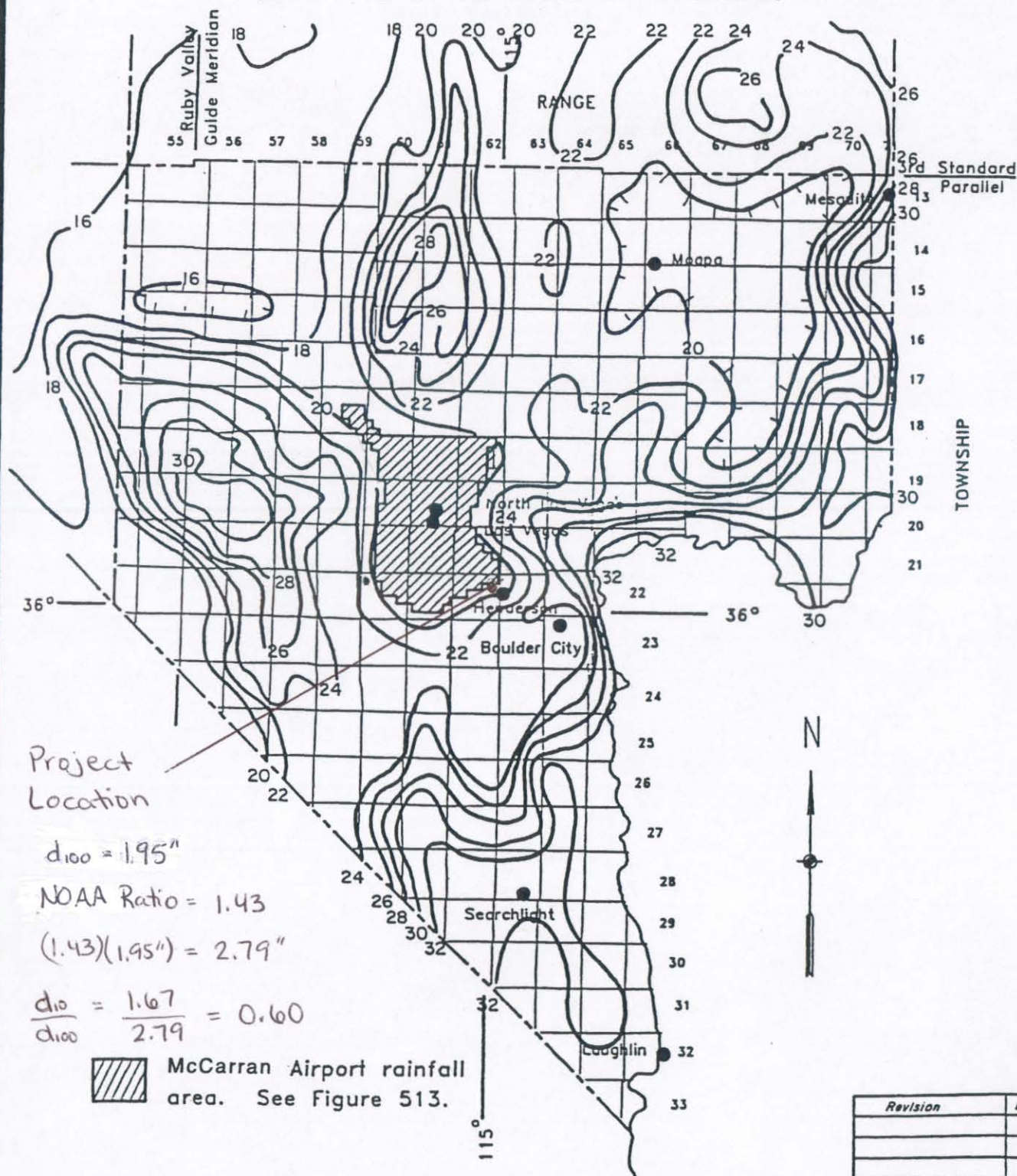




# RAINFALL DEPTH-DURATION-FREQUENCY

## 100-YEAR, 6-HOUR

(DEPTHS IN TENTHS OF INCHES)





This unit is used mainly as habitat for desert wildlife and for recreation. It is also used for urban development.

This unit is well suited to the construction of dwellings.

Unless the density of housing is too high, septic tank absorption fields normally function well on this unit.

Roads can easily be constructed and maintained on this unit.

The main limitations for lawns and landscaping are the cobbles and pebbles throughout the soil. Topsoil is needed for best results when landscaping, particularly in areas used for lawns. Lawn grasses, shrubs, and trees that are not sensitive to lime-induced chlorosis are well suited to use in landscaping. Annual applications of iron chelates reduce the effects of chlorosis.

This map unit is in capability subclass VII<sub>s</sub>, nonirrigated, and in horticultural group 2.

**184—Caliza very gravelly sandy loam, 2 to 8 percent slopes.** This very deep, well drained soil is on erosional fan remnants. It formed in alluvium derived from various kinds of rock.

Typically, the surface layer is light brown very gravelly sandy loam about 3 inches thick. The upper 13 inches of the underlying material is light brown very gravelly sandy loam, and the lower part to a depth of 60 inches or more is light brown, stratified very gravelly coarse sand to very gravelly loamy sand.

Included in this unit is about 5 percent Aztec soils on erosional fan remnants. The percentage varies from one area to another.

Permeability of the Caliza soil is moderately rapid. Available water capacity is very low. Effective rooting depth is 60 inches or more. Runoff is medium, and the hazard of water erosion is slight. The hazard of soil blowing is moderate. This soil is subject to rare periods of flooding during prolonged, high-intensity storms. Channeling and deposition are common along streambanks.

This unit is used mainly as habitat for desert wildlife and for recreation. It is also used for urban development.

The main limitation for construction of dwellings is the hazard of flooding.

Dikes and channels that have outlets for floodwater can be used to protect onsite sewage disposal systems from flooding.

Channeling and deposition can be minimized and maintenance costs reduced by protecting roads from flooding.

The main limitation for lawns and landscaping is the content of pebbles in the soil. Topsoil is needed for best results when landscaping, particularly in areas used for lawns. Lawn grasses, shrubs, and trees that are not sensitive to lime-induced chlorosis are well suited to use in landscaping. Annual applications of iron chelates reduce the effects of chlorosis.

This map unit is in capability subclasses IV<sub>s</sub>, irrigated, and VII<sub>s</sub>, nonirrigated. It is in horticultural group 2.

**187—Caliza extremely cobbly fine sandy loam, 2 to 8 percent slopes.** This very deep, well drained soil is on inset fan remnants. It formed in alluvium derived from various kinds of rock.

Typically, about 85 percent of the surface is covered with a desert pavement of cobbles, stones, and pebbles. The surface layer is a light brown extremely cobbly fine sandy loam about 2 inches thick. The upper 12 inches of the underlying material is light brown and pink very gravelly sandy loam, and the lower part to a depth of 60 inches or more is light brown and pink, stratified material that averages very gravelly loamy coarse sand. In some areas of similar included soils, the surface layer is extremely stony fine sandy loam.

Included in this unit are about 5 percent Arizo soils, flooded, in channels; 5 percent Pittman soils on erosional fan remnants; and 5 percent Aztec soils on erosional fan remnants. Included areas make up about 15 percent of the total acreage. The percentage varies from one area to another.

Permeability of this Caliza soil is moderately rapid. Available water capacity is low. Effective rooting depth is 60 inches or more. Runoff is medium, and the hazard of water erosion is slight. The hazard of soil blowing is moderate if the surface is disturbed.

This unit is used mainly as habitat for desert wildlife and for recreation. It is also used for urban development.

This unit is well suited to the construction of dwellings.

Unless the density of housing is too high, septic tank absorption fields normally function well on this unit.

Roads can easily be constructed and maintained on this unit.

The main limitation for lawns and landscaping is the stones, cobbles, and pebbles on the surface and throughout the soil. Topsoil is needed for best results when landscaping, particularly in areas used for lawns. Lawn grasses, shrubs, and trees that are not sensitive to lime-induced chlorosis are well suited to use in landscaping. Annual applications of iron chelates reduce the effects of chlorosis.

Intermittent streams form the drainageways in this unit. These drainageways are subject to rare or occasional periods of high-velocity flooding. Care should be taken during urbanization to accommodate the runoff from the drainageways. If drains become plugged during a major flood, accelerated erosion and damage to roads, buildings, and other structures can occur.

This map unit is in capability subclass VII<sub>s</sub>, nonirrigated, and in horticultural group 2.

**190—Dalian very gravelly fine sandy loam, 2 to 4 percent slopes.** This very deep, well drained soil is on fan skirts. It formed in alluvium derived dominantly from limestone and dolomite.

Typically, 65 percent of the surface is covered with a weakly developed desert pavement of pebbles. The surface layer is light yellowish brown very gravelly fine



The main limitations for lawns and landscaping are the presence of pebbles throughout the soil and the very low available water capacity of the Weiser soil. Topsoil is needed for best results when landscaping, particularly in areas used for lawns. Frequent irrigation of lawns, gardens, and most other plantings is needed because of the limited available water capacity of the soil. Lawn grasses, shrubs, and trees that are not sensitive to lime-induced chlorosis are well suited to use in landscaping. Annual applications of iron chelates reduce the effects of chlorosis.

Intermittent streams form the drainageways in this unit. These drainageways are subject to rare or occasional periods of high-velocity flooding. Care should be taken during urbanization to accommodate the runoff from the drainageways. If drains become plugged during a major flood, accelerated erosion and damage to roads, buildings, and other structures can occur.

This map unit is in capability subclasses IVs, irrigated, and VIIs, nonirrigated. It is in horticultural group 2.

**545—Weiser-Goodsprings complex, 2 to 4 percent slopes.** This map unit is on erosional fan remnants.

This unit is 60 percent Weiser extremely gravelly fine sandy loam, 2 to 4 percent slopes, and 25 percent Goodsprings very gravelly fine sandy loam, 2 to 4 percent slopes. The Weiser and Goodsprings soils are on summits and shoulders of the fan remnants. The components of this unit are so intricately intermingled that it was not practical to map them separately at the scale used.

Included in this unit are about 5 percent Las Vegas soils and 10 percent Skyhaven soils on relict alluvial flats. Included areas make up about 15 percent of the total acreage. The percentage varies from one area to another.

The Weiser soil is very deep and well drained. It formed in alluvium derived dominantly from limestone and dolomite. Typically, 90 percent of the surface layer is covered with a desert pavement of pebbles. There is a dark desert varnish on the exposed surfaces of the rock fragments. The surface layer is light yellowish brown extremely gravelly fine sandy loam about 1 inch thick. The underlying material to a depth of 63 inches is light brown extremely gravelly fine sandy loam and very gravelly fine sandy loam, averaging extremely gravelly fine sandy loam.

Permeability of the Weiser soil is moderately rapid. Available water capacity is very low. Effective rooting depth is 60 inches or more. Runoff is medium, and the hazard of water erosion is slight. The hazard of soil blowing is moderate if the desert pavement is disturbed.

The Goodsprings soil is shallow and well drained. It formed in alluvium derived from various kinds of rock. Typically, 90 percent of the surface is covered with a desert pavement of pebbles. The surface layer is light brown very gravelly fine sandy loam about 5 inches

thick. The upper 10 inches of the underlying material is pink gravelly fine sandy loam, the next 37 inches is pinkish white, strongly lime-cemented hardpan, and the lower part to a depth of 60 inches or more is pink extremely gravelly loamy fine sand. Depth to the hardpan ranges from 9 to 20 inches.

Permeability of the Goodsprings soil is moderate above the hardpan. Available water capacity is very low. Effective rooting depth is 9 to 20 inches. Runoff is medium, and the hazard of water erosion is slight. The hazard of soil blowing is high if the desert pavement is disturbed.

This unit is used as habitat for desert wildlife and for recreation.

This unit is limited for roads because of the depth to the hardpan in areas of the Goodsprings soil. Roads should be designed to minimize cuts. Heavy equipment is needed for excavation.

This map unit is in capability subclass VIIs, nonirrigated. The Weiser soil is in horticultural group 2, and the Goodsprings soil is in horticultural group 6.

**600—Slickens.** Slickens consists of accumulations of fine-textured material such as that separated in ore-mill operations. It is largely freshly ground rock that commonly has undergone chemical treatment during the milling process. Slickens is commonly confined in specially constructed basins.

This map unit is in capability subclass VIIIs, nonirrigated.

**605—Dumps.** Dumps consists of areas of smoothed or uneven accumulations of waste rock and general refuse.

This map unit is in capability subclass VIIIs, nonirrigated.

**610—Pits, gravel.** Pits, gravel, consists of open excavations from which soil material and gravel have been removed, exposing rock, a hardpan, or other material.

This map unit is in capability subclass VIIIs, nonirrigated.

**615—Urban land.** Urban land consists of areas covered by asphalt, concrete, and buildings or other urban structures.

This map unit is in capability subclass VIIIs, nonirrigated.

**630—Badland.** Badland is moderately steep to very steep barren land dissected by many intermittent drainage channels that have cut into soft geologic material. The areas ordinarily are not stony. Local relief generally ranges from 25 to 100 feet. Potential runoff is very high, and erosion is active. Some small included areas of identifiable soils support vegetation.



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## RUNOFF CURVE NUMBERS (URBAN AREAS<sup>1</sup>)

Cover description		Curve numbers for hydrologic soil group—			
Cover type and hydrologic condition	Average percent impervious area <sup>2</sup>	A	B	C	D
<i>Fully developed urban areas (vegetation established)</i>					
Open space (lawns, parks, golf courses, cemeteries, etc.): <sup>3</sup>					
Poor condition (grass cover < 50%) .....		68	79	86	89
Fair condition (grass cover 50% to 75%) .....		49	69	79	84
Good condition (grass cover > 75%) .....		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc. (excluding right-of-way) .....		98	98	98	98
Streets and roads:					
Paved: curbs and storm sewers (excluding right-of-way) .....		98	98	98	98
Paved: open ditches (including right-of-way) .....		83	89	92	93
Gravel (including right-of-way) .....		76	85	89	91
Dirt (including right-of-way) .....		72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) <sup>4</sup> ...		63	77	85	88
Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders) .....		96	96	96	96
Urban districts:					
Commercial and business .....	85	89	92	94	95
Industrial .....	72	81	88	91	93
Residential districts by average lot size:					

**See Table 602A**

### Developing urban areas

Newly graded areas (pervious areas only, no vegetation) <sup>5</sup> .....	77	86	91	94
--	----	----	----	----

1 Average runoff condition, and  $I_p = 0.25$ .

2 The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system. Impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using Figure 603.

3 CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.

4 Composite CN's for natural desert landscaping should be computed using Figure 603 based on the impervious area percentage (CN #98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.

5 Composite CN's to use for the design of temporary measures during grading and construction should be computed using Figure 603 based on the degree of development impervious area percentage) and the CN's for the newly graded pervious areas.

Revision	Date



# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## RUNOFF CURVE NUMBERS (SEMIARID RANGELANDS<sup>1</sup>)

Cover description		Curve numbers for hydrologic soil group—			
Cover type	Hydrologic condition <sup>2</sup>	A <sup>3</sup>	B	C	D
Herbaceous—mixture of grass, weeds, and low-growing brush, with brush the minor element.	Poor		80	87	93
	Fair		71	81	89
	Good		62	74	85
Oak-aspen—mountain brush mixture of oak brush, aspen, mountain mahogany, bitter brush, maple, and other brush.	Poor		66	74	79
	Fair		48	57	63
	Good		30	41	48
Pinyon-juniper—pinyon, juniper, or both; grass understory.	Poor		75	85	89
	Fair		58	73	80
	Good		41	61	71
Sagebrush with grass understory.	Poor		67	80	85
	Fair		51	63	70
	Good		35	47	55
Desert shrub—major plants include saltbush, greasewood, creosotebush, blackbrush, bursage, palo verde, mesquite, and cactus.	Poor	63	77	85	88
	Fair	55	72	81	86
	Good	49	68	79	84

<sup>1</sup>Average runoff condition, and  $I_a = 0.2S$ .

<sup>2</sup>Poor: <30% ground cover (litter, grass, and brush overstory).

Fair: 30 to 70% ground cover.

Good: >70% ground cover.

<sup>3</sup>Curve numbers for group A have been developed only for desert shrub.

Revision	Date



## **Appendix C: Hydraulic Calculations**



**Appendix C-1: Cross Section and Drainage Facility Map (Figure 7)**





LEGEND

- HEC-RAS CHANNEL (C-1)
- HEC-RAS CHANNEL (C-2)
- 42" RCP STORM DRAIN
- 60" RCP STORM DRAIN
- CROSS SECTION

NOTES

PLEASE REFER TO FIGURE 6 FOR THE DEVELOPED CONDITION BASIN DELINEATION



GRAPHIC SCALE



511963.19 OCTOBER 2006

FIGURE 7  
CROSS-SECTION AND  
DRAINAGE FACILITY MAP

TECHNICAL DRAINAGE STUDY FOR EAST MAP



2270 Corporate Circle  
Suite 100  
Henderson, Nevada 89074-6382  
Telephone: 702/263-7275  
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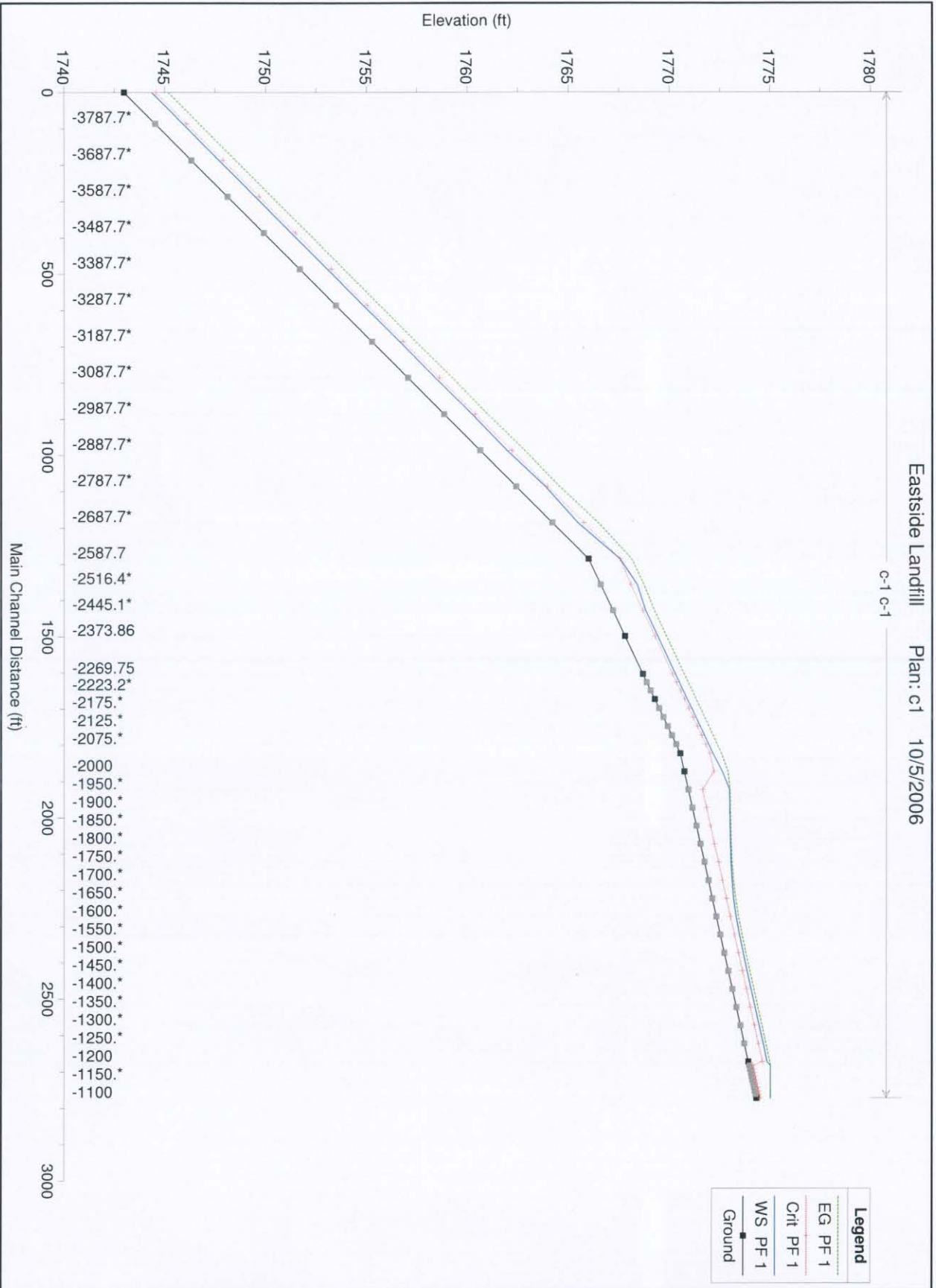
ENGINEERING PLANNING SURVEYING CONSTRUCTION SERVICES



## **Appendix C-2: HEC-RAS Model for Channel C-1**



c-1 c-1





HEC-RAS Plan: c1 River: c-1 Reach: c-1 Profile: PF 1

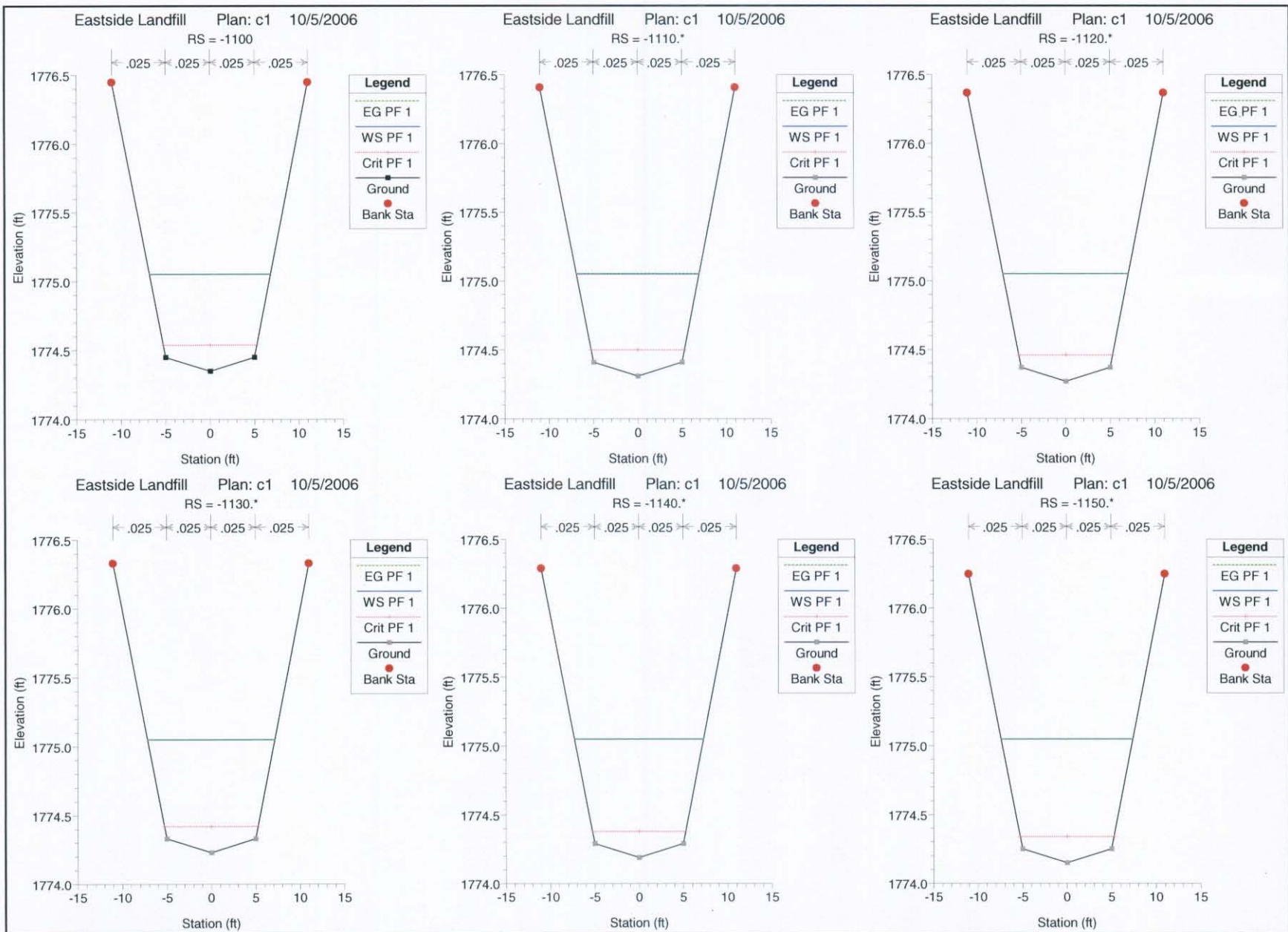
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl	Max Chl Dpth	Frctn Slope
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)		(ft)	(ft/ft)
c-1	-1100	PF 1	3.00	1774.35	1775.05	1774.54	1775.06	0.000097	0.39	7.62	13.62	0.09	0.70	0.000087
c-1	-1110.*	PF 1	3.00	1774.31	1775.05	1774.50	1775.05	0.000079	0.37	8.16	13.85	0.08	0.74	0.000072
c-1	-1120.*	PF 1	3.00	1774.27	1775.05	1774.46	1775.05	0.000065	0.34	8.71	14.09	0.08	0.78	0.000059
c-1	-1130.*	PF 1	3.00	1774.23	1775.05	1774.42	1775.05	0.000054	0.32	9.27	14.33	0.07	0.82	0.000049
c-1	-1140.*	PF 1	3.00	1774.19	1775.05	1774.38	1775.05	0.000045	0.30	9.84	14.56	0.07	0.86	0.000042
c-1	-1150.*	PF 1	3.00	1774.15	1775.05	1774.34	1775.05	0.000038	0.29	10.42	14.80	0.06	0.90	0.000035
c-1	-1160.*	PF 1	3.00	1774.11	1775.05	1774.30	1775.05	0.000033	0.27	11.02	15.04	0.06	0.94	0.000030
c-1	-1170.*	PF 1	3.00	1774.07	1775.05	1774.26	1775.05	0.000028	0.26	11.62	15.28	0.05	0.98	0.000026
c-1	-1180.*	PF 1	3.00	1774.03	1775.05	1774.22	1775.05	0.000024	0.25	12.23	15.52	0.05	1.02	0.000022
c-1	-1190.*	PF 1	3.00	1773.99	1775.05	1774.18	1775.05	0.000021	0.23	12.86	15.76	0.05	1.06	0.0000930
c-1	-1200	PF 1	33.00	1773.95	1774.89	1774.66	1775.03	0.004001	3.01	10.96	15.02	0.62	0.94	0.003997
c-1	-1250.*	PF 1	33.00	1773.75	1774.69	1774.46	1774.83	0.003994	3.01	10.97	15.03	0.62	0.94	0.003997
c-1	-1300.*	PF 1	33.00	1773.55	1774.49	1774.26	1774.63	0.004001	3.01	10.96	15.01	0.62	0.94	0.004001
c-1	-1350.*	PF 1	33.00	1773.35	1774.29	1774.06	1774.43	0.004001	3.01	10.96	15.01	0.62	0.94	0.004001
c-1	-1400.*	PF 1	33.00	1773.15	1774.09	1773.86	1774.23	0.004001	3.01	10.96	15.02	0.62	0.94	0.003999
c-1	-1450.*	PF 1	33.00	1772.95	1773.89	1773.66	1774.03	0.003997	3.01	10.96	15.03	0.62	0.94	0.003991
c-1	-1500.*	PF 1	33.00	1772.75	1773.69	1773.46	1773.83	0.003984	3.01	10.98	15.03	0.62	0.94	0.003964
c-1	-1550.*	PF 1	33.00	1772.55	1773.49	1773.26	1773.63	0.003944	3.00	11.01	15.03	0.62	0.94	0.003872
c-1	-1600.*	PF 1	33.00	1772.35	1773.30	1773.06	1773.44	0.003802	2.96	11.15	15.09	0.61	0.95	0.003603
c-1	-1650.*	PF 1	33.00	1772.15	1773.13	1772.86	1773.25	0.003419	2.85	11.57	15.26	0.58	0.98	0.003045
c-1	-1700.*	PF 1	33.00	1771.95	1772.99	1772.66	1773.10	0.002729	2.64	12.49	15.61	0.52	1.04	0.002262
c-1	-1750.*	PF 1	33.00	1771.75	1772.89	1772.46	1772.98	0.001905	2.33	14.14	16.23	0.44	1.14	0.001510
c-1	-1800.*	PF 1	33.00	1771.55	1772.83	1772.26	1772.89	0.001227	2.00	16.48	17.08	0.36	1.28	0.000962
c-1	-1850.*	PF 1	33.00	1771.35	1772.79	1772.06	1772.84	0.000774	1.70	19.37	18.07	0.29	1.44	0.000611
c-1	-1900.*	PF 1	33.00	1771.15	1772.77	1771.86	1772.81	0.000495	1.46	22.68	19.14	0.24	1.62	0.000396
c-1	-1950.*	PF 1	33.00	1770.95	1772.76	1771.66	1772.78	0.000325	1.25	26.33	20.24	0.19	1.81	0.000318
c-1	-2000	PF 1	33.00	1770.75	1772.75	1771.46	1772.77	0.000311	1.09	30.25	21.38	0.16	2.00	0.002312
c-1	-2050	PF 1	120.00	1770.55	1772.18	1772.03	1772.61	0.008398	5.28	22.72	19.15	0.85	1.62	0.008406
c-1	-2075.*	PF 1	120.00	1770.34	1771.96	1771.82	1772.40	0.008413	5.28	22.71	19.14	0.86	1.62	0.008448
c-1	-2100.*	PF 1	120.00	1770.13	1771.75	1771.61	1772.19	0.008483	5.30	22.63	19.12	0.86	1.62	0.008522
c-1	-2125.*	PF 1	120.00	1769.92	1771.54	1771.40	1771.98	0.008562	5.32	22.55	19.09	0.86	1.62	0.008425
c-1	-2150.*	PF 1	120.00	1769.70	1771.33	1771.18	1771.76	0.008290	5.25	22.84	19.19	0.85	1.63	0.008248
c-1	-2175.*	PF 1	120.00	1769.49	1771.13	1770.97	1771.55	0.008207	5.23	22.93	19.21	0.84	1.64	0.008390
c-1	-2200	PF 1	121.00	1769.28	1770.90	1770.77	1771.35	0.008578	5.33	22.68	19.14	0.86	1.62	0.008570
c-1	-2223.2*	PF 1	121.00	1769.08	1770.70	1770.57	1771.15	0.008562	5.33	22.70	19.14	0.86	1.62	0.008546
c-1	-2246.5*	PF 1	121.00	1768.88	1770.51	1770.37	1770.95	0.008530	5.32	22.73	19.15	0.86	1.63	0.008505
c-1	-2269.75	PF 1	121.00	1768.68	1770.31	1770.17	1770.75	0.008480	5.31	22.79	19.17	0.86	1.63	0.008450
c-1	-2373.86	PF 1	121.00	1767.80	1769.43	1769.29	1769.87	0.008421	5.30	22.85	19.19	0.86	1.63	0.008410
c-1	-2445.1*	PF 1	121.00	1767.20	1768.83	1768.69	1769.27	0.008399	5.29	22.87	19.20	0.85	1.63	0.008934
c-1	-2516.4*	PF 1	121.00	1766.60	1768.42	1768.09	1768.74	0.005821	4.57	26.49	20.29	0.70	1.82	0.008089
c-1	-2587.7	PF 1	131.00	1766.00	1767.56	1767.56	1768.14	0.011604	6.12	21.42	18.73	1.01	1.56	0.011585
c-1	-2687.7*	PF 1	131.00	1764.21	1765.47	1765.77	1766.49	0.023359	8.09	16.19	16.98	1.46	1.26	0.015943
c-1	-2787.7*	PF 1	131.00	1762.42	1763.87	1763.98	1764.57	0.014617	6.71	19.53	18.12	1.14	1.45	0.018227
c-1	-2887.7*	PF 1	131.00	1760.64	1761.97	1762.20	1762.86	0.019865	7.58	17.27	17.36	1.34	1.33	0.016940
c-1	-2987.7*	PF 1	131.00	1758.85	1760.25	1760.41	1761.02	0.016441	7.03	18.63	17.82	1.21	1.40	0.018032



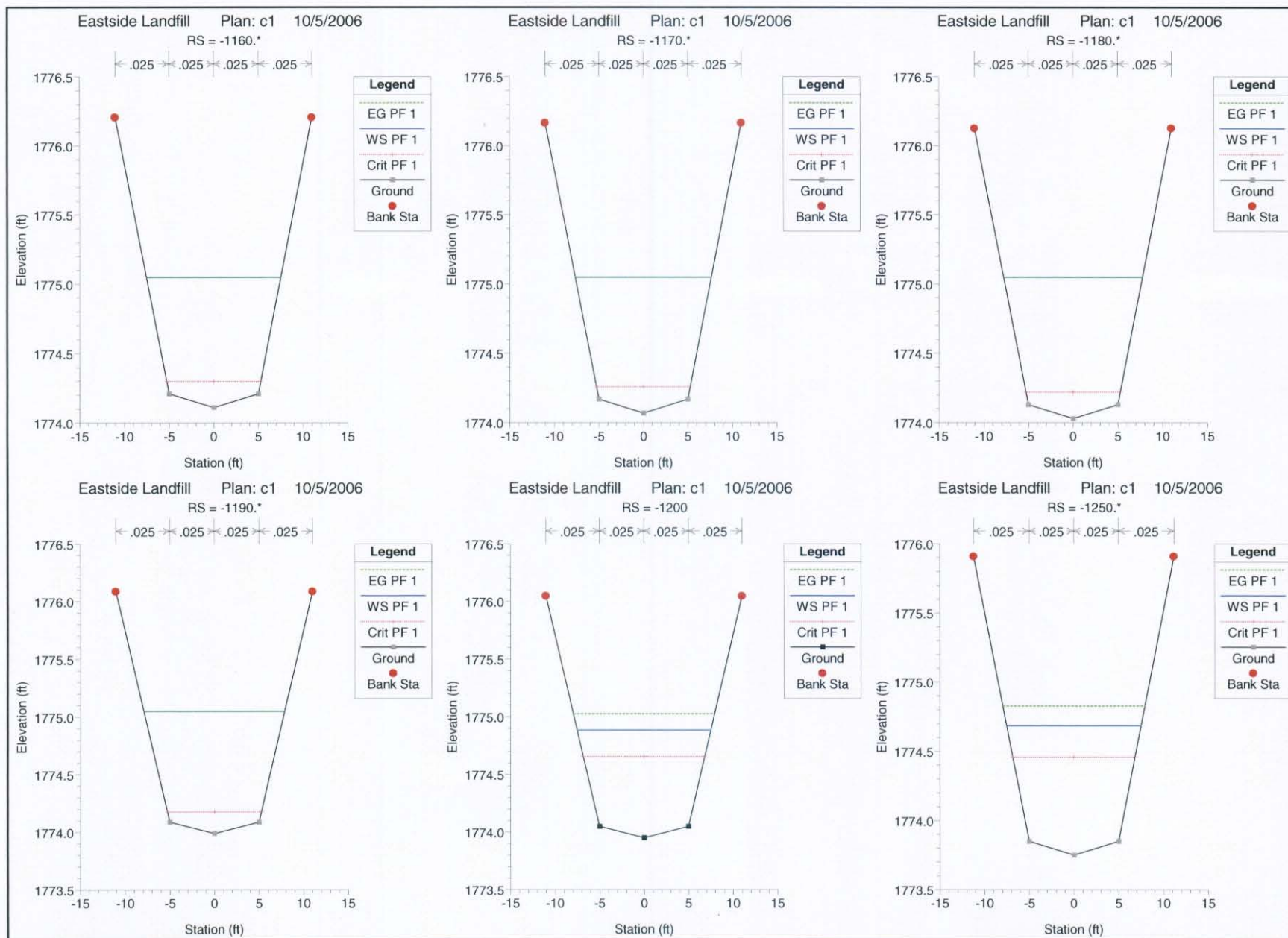
HEC-RAS Plan: c1 River: c-1 Reach: c-1 Profile: PF 1 (Continued)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl	Max Chl Dpth	Frctn Slope
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)		(ft)	(ft/ft)
c-1	-3087.7*	PF 1	131.00	1757.06	1758.41	1758.62	1759.26	0.018674	7.40	17.70	17.51	1.30	1.35	0.017504
c-1	-3187.7*	PF 1	131.00	1755.27	1756.65	1756.83	1757.45	0.017258	7.17	18.27	17.70	1.24	1.38	0.017945
c-1	-3287.7*	PF 1	131.00	1753.48	1754.84	1755.04	1755.67	0.018132	7.31	17.91	17.58	1.28	1.36	0.017687
c-1	-3387.7*	PF 1	131.00	1751.70	1753.07	1753.26	1753.89	0.017639	7.23	18.11	17.65	1.26	1.37	0.017883
c-1	-3487.7*	PF 1	131.00	1749.91	1751.27	1751.47	1752.10	0.018164	7.32	17.90	17.57	1.28	1.36	0.017899
c-1	-3587.7*	PF 1	131.00	1748.12	1749.49	1749.68	1750.31	0.017788	7.26	18.05	17.62	1.26	1.37	0.017975
c-1	-3687.7*	PF 1	131.00	1746.33	1747.70	1747.89	1748.52	0.018000	7.29	17.97	17.60	1.27	1.37	0.017894
c-1	-3787.7*	PF 1	131.00	1744.54	1745.91	1746.10	1746.73	0.017975	7.29	17.98	17.60	1.27	1.37	0.017988
c-1	-3874.10	PF 1	131.00	1743.00	1744.37	1744.56	1745.19	0.017762	7.25	18.06	17.63	1.26	1.37	0.017868

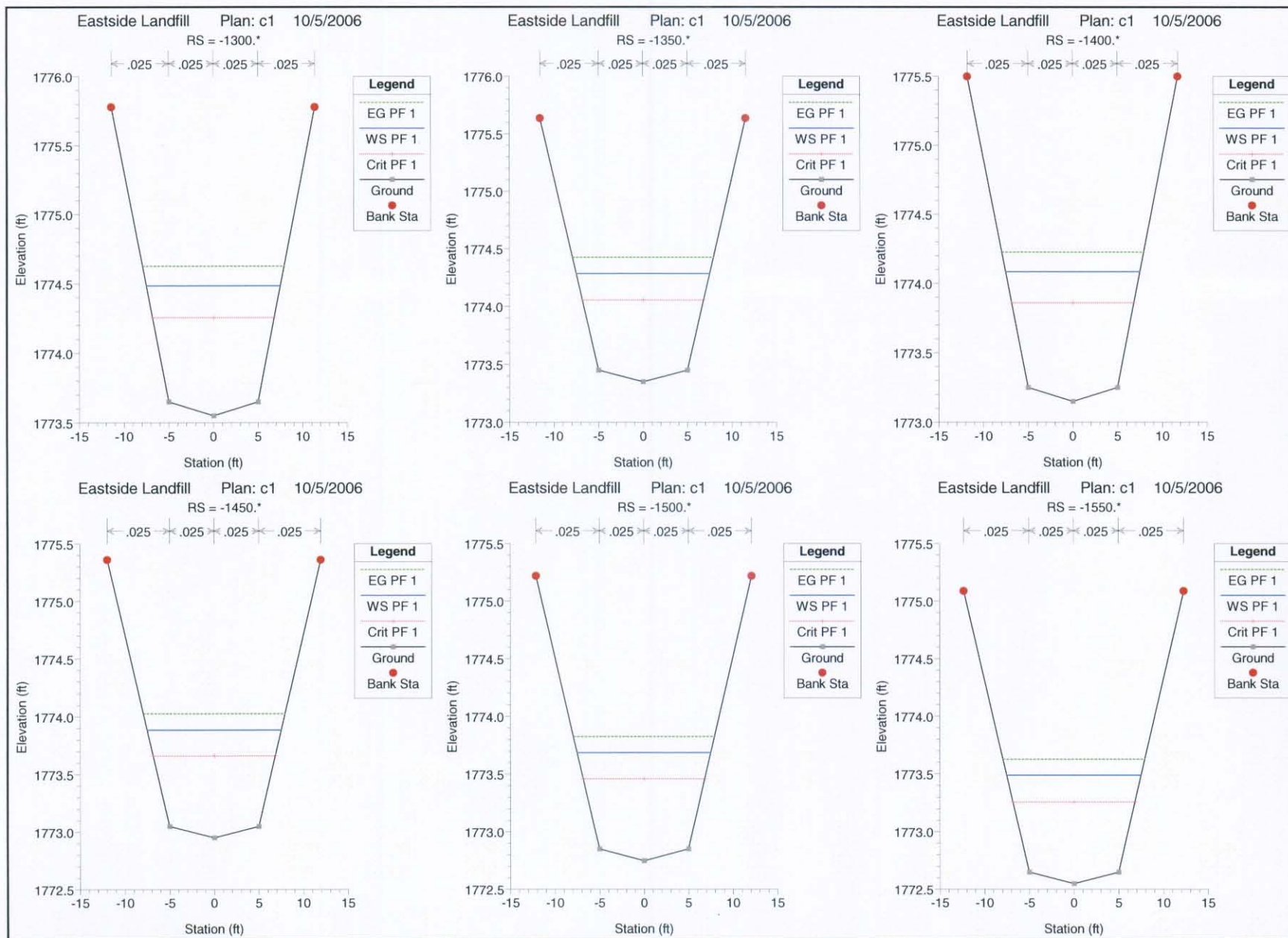




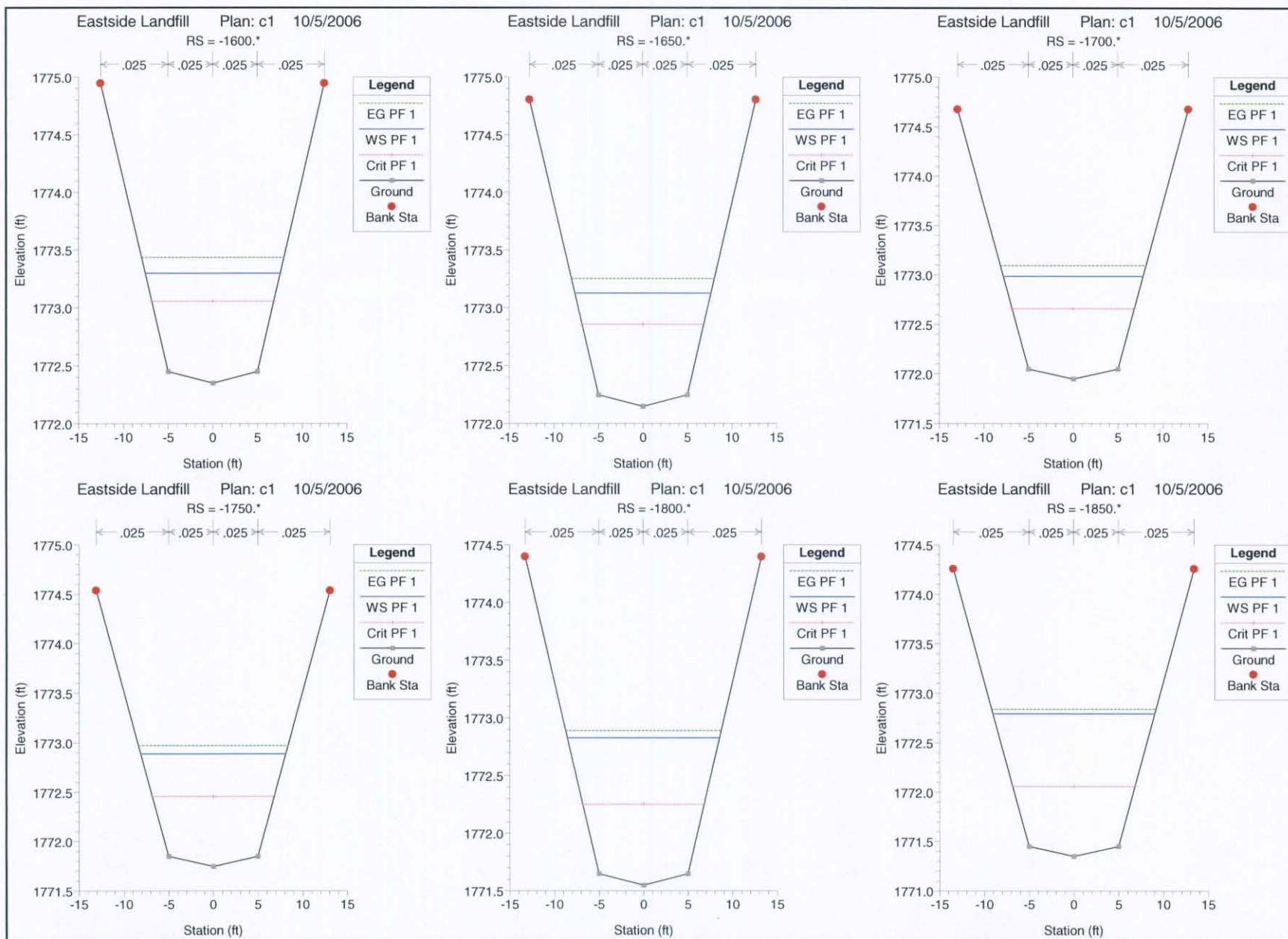




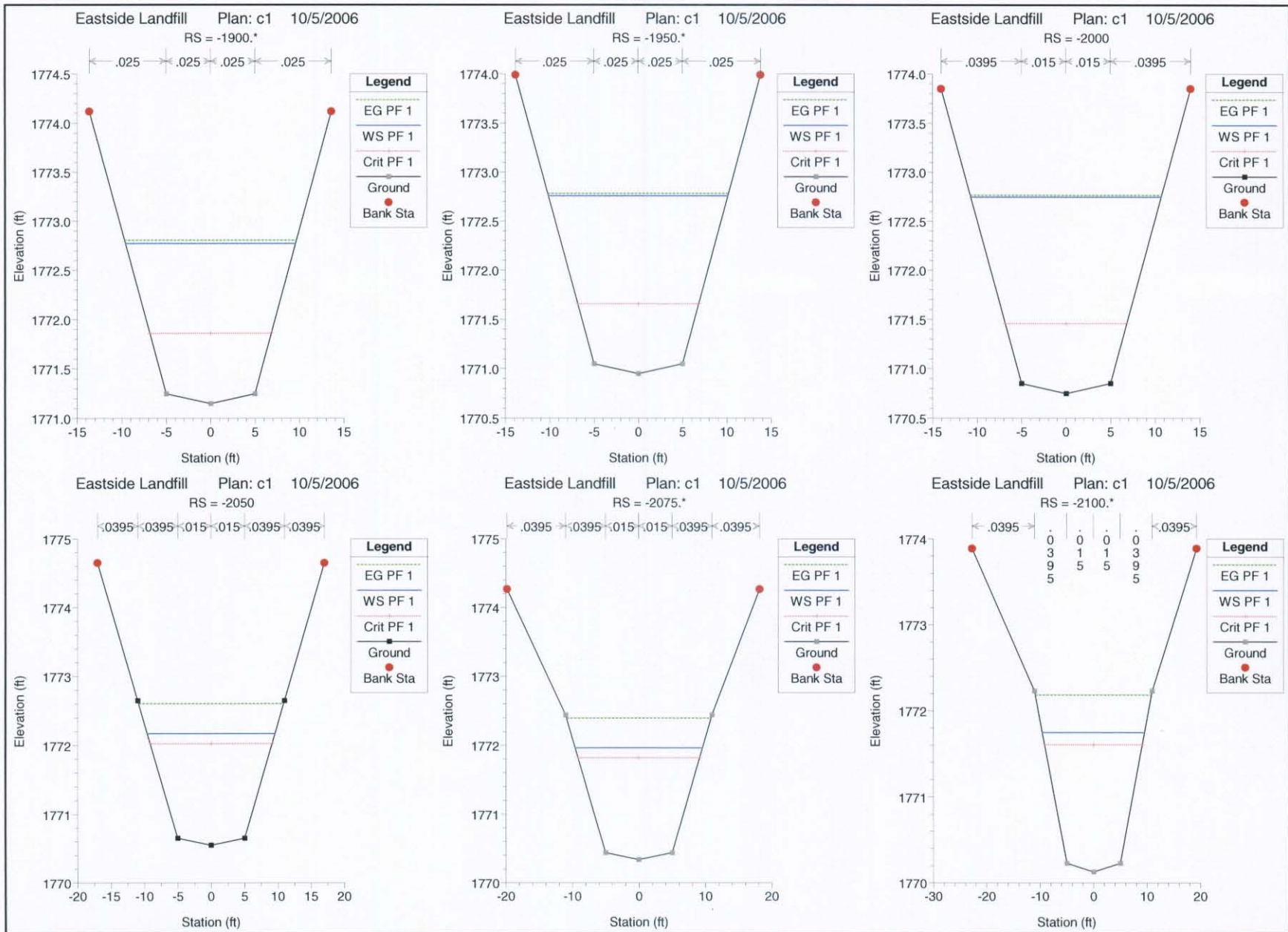




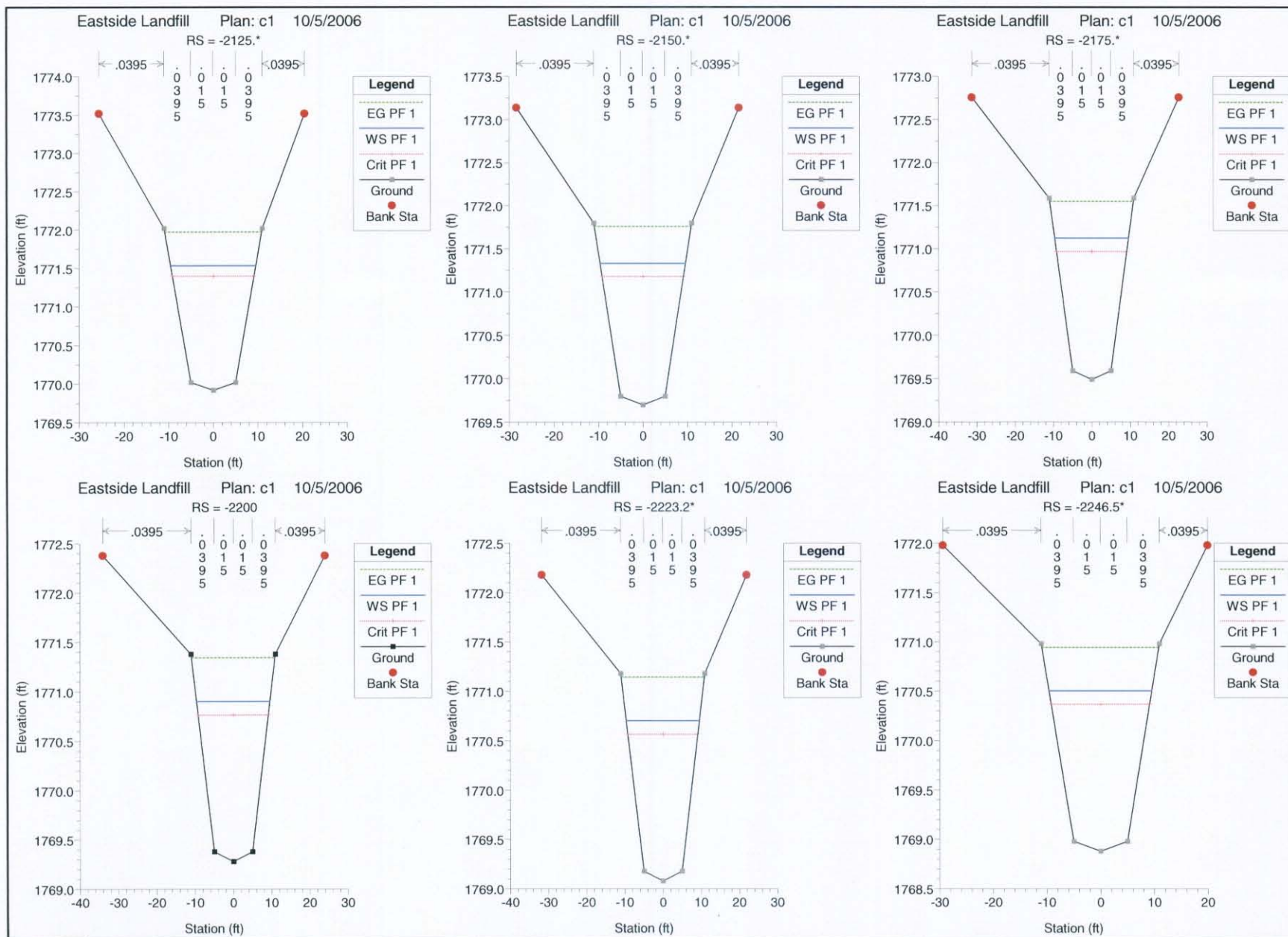




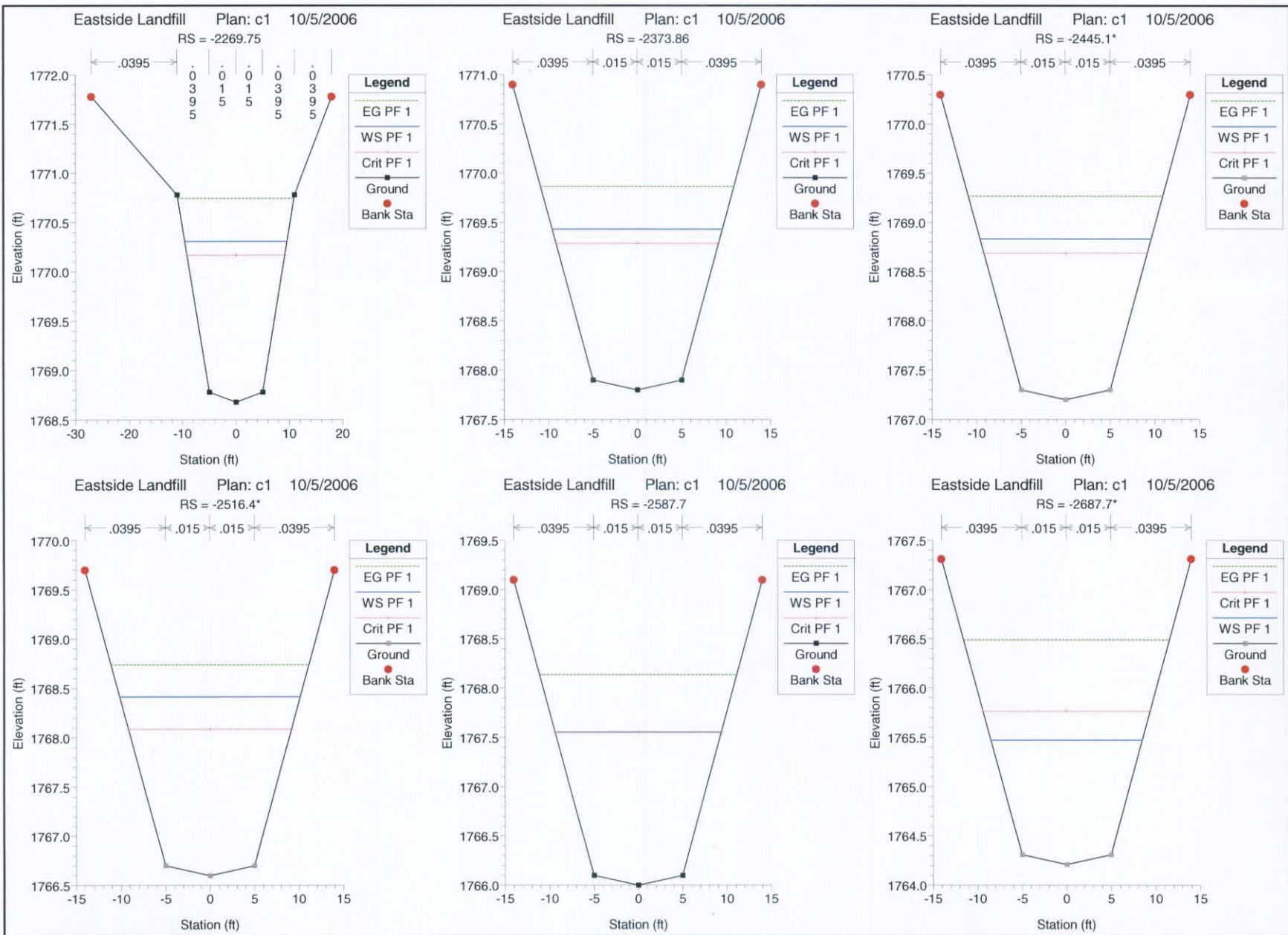




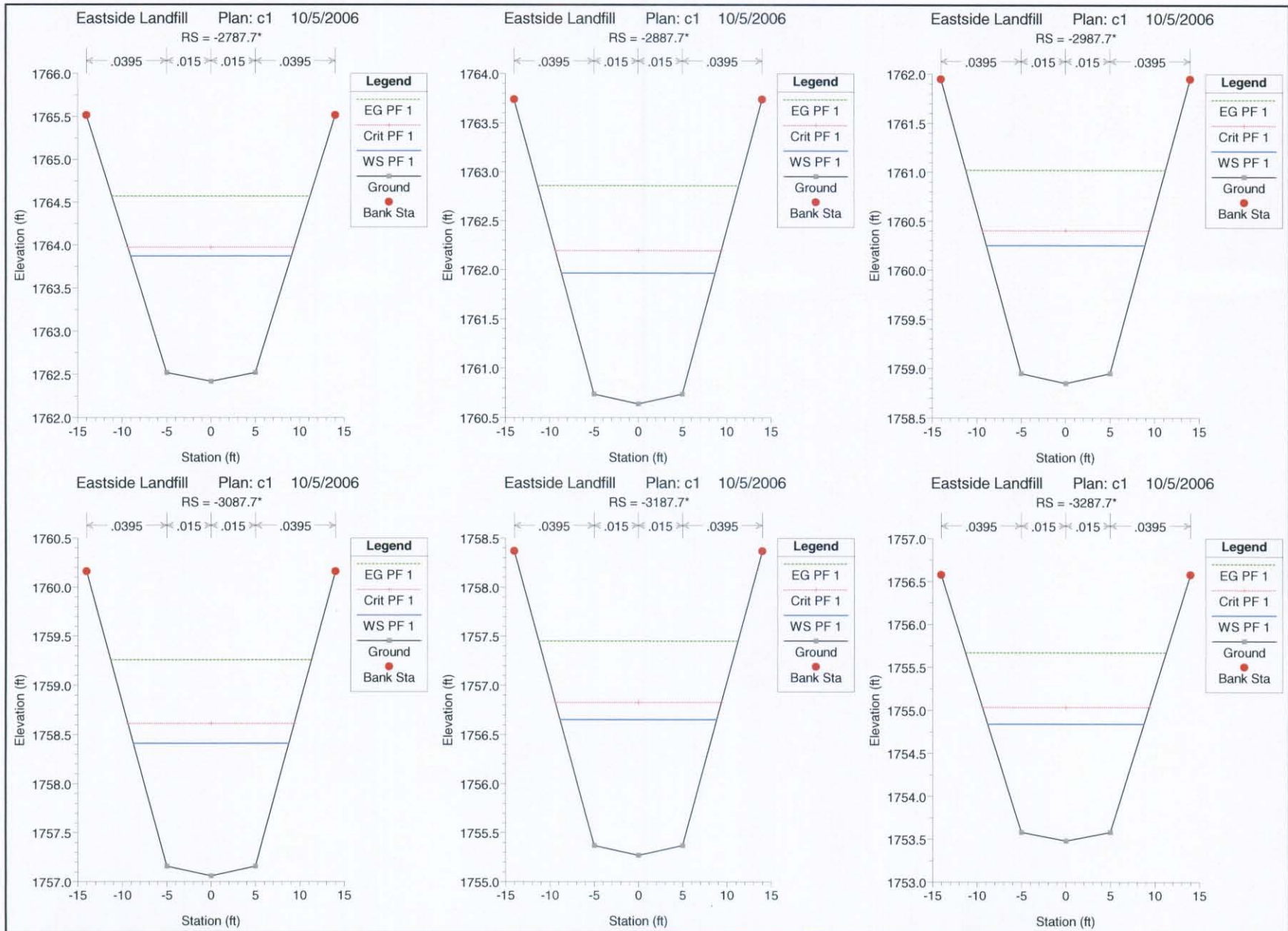




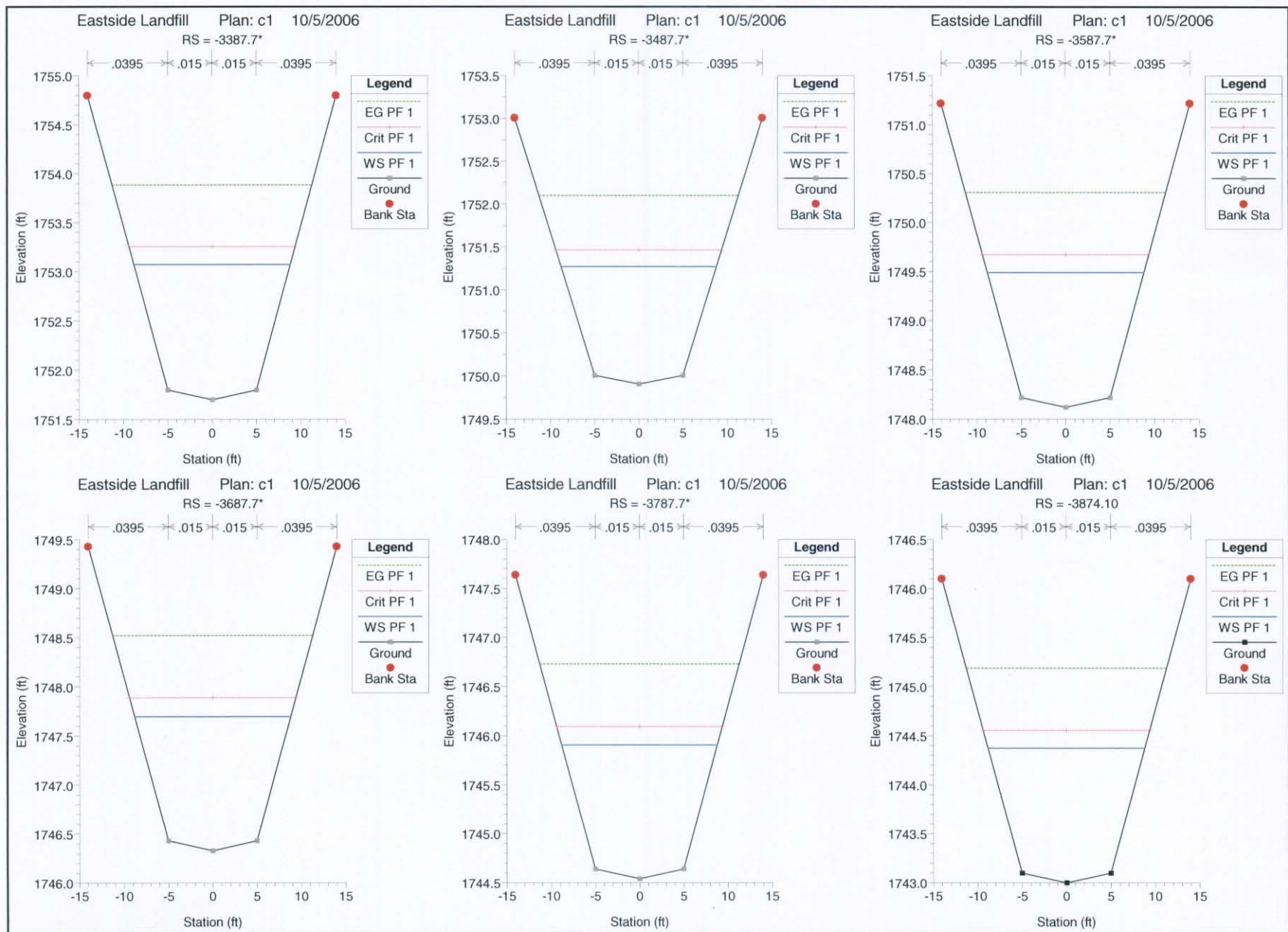














An electronic copy of the HEC-RAS Report is provided in Appendix F.



### **Appendix C-3: HEC-RAS Model for Channel C-2**

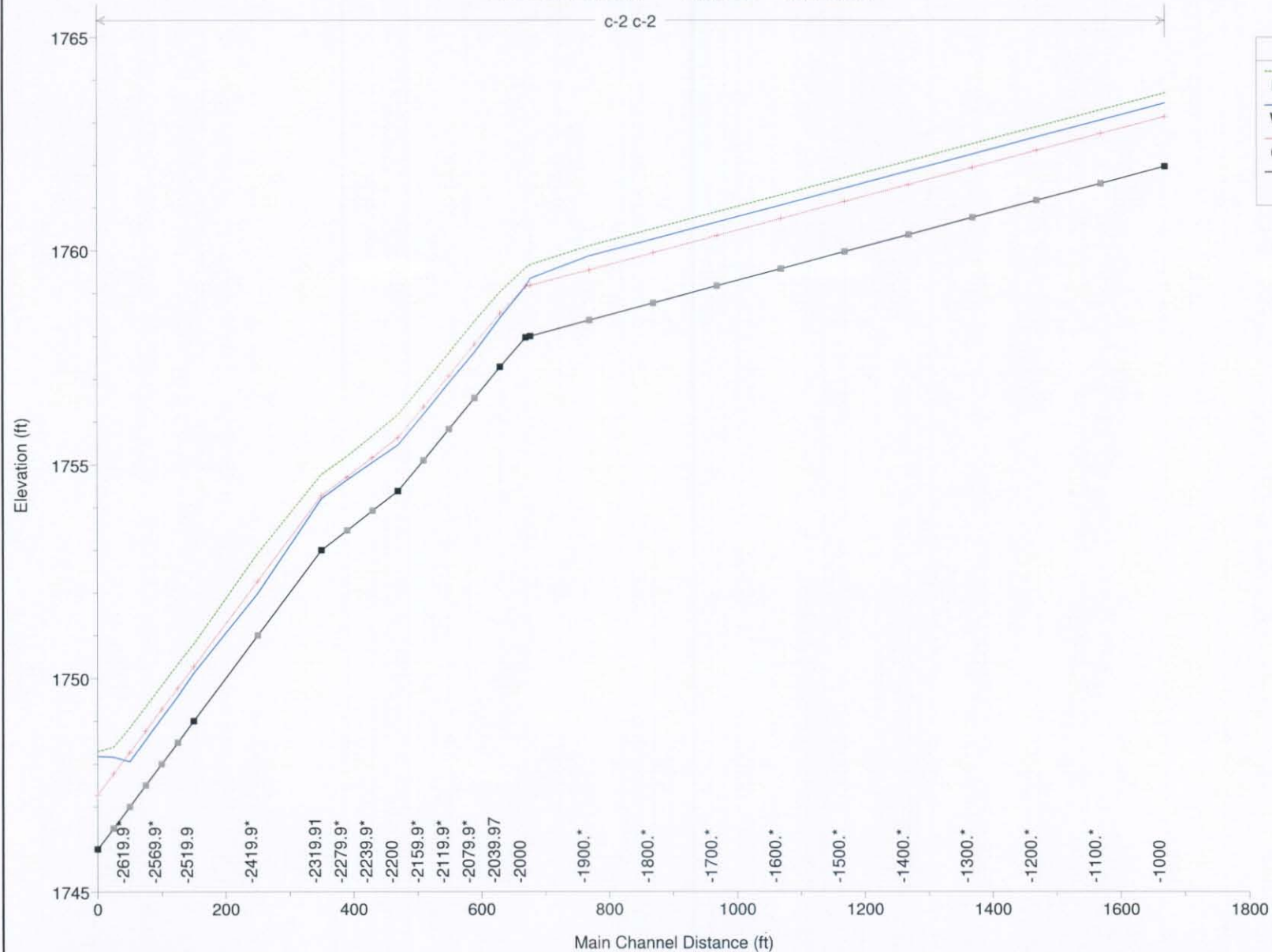


# Eastside Landfill Plan: c2 10/5/2006

c-2 c-2

## Legend

- EG PF 1
- WS PF 1
- Crit PF 1
- Ground





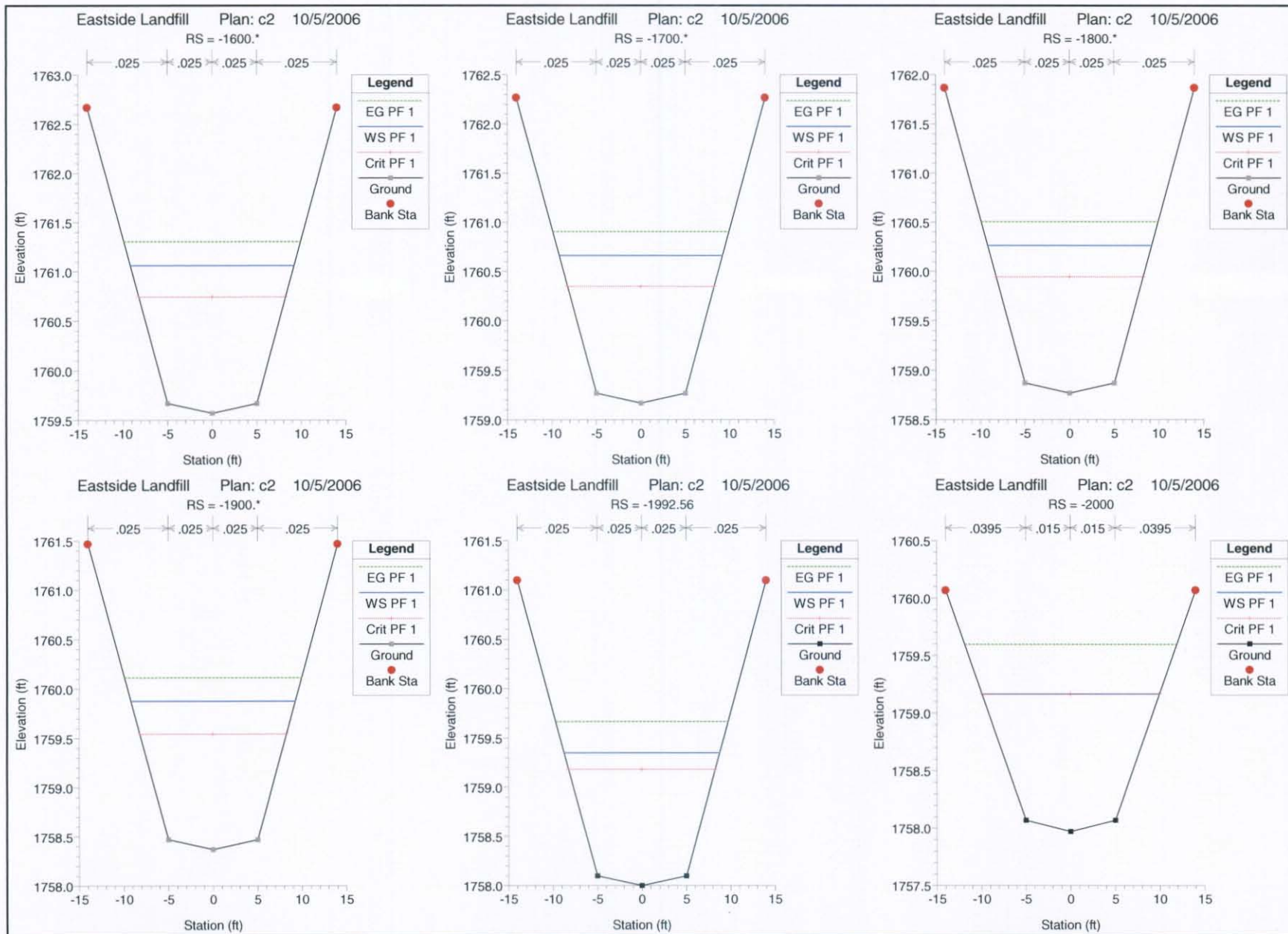
HEC-RAS Plan: c2 River: c-2 Reach: c-2 Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl	Max Chl Dpth (ft)	Frctn Slope (ft/ft)
c-2	-1000	PF 1	80.00	1761.97	1763.46	1763.15	1763.71	0.003999	3.95	20.26	18.36	0.66	1.49	0.004000
c-2	-1100.*	PF 1	80.00	1761.57	1763.06	1762.75	1763.31	0.004000	3.95	20.26	18.36	0.66	1.49	0.004000
c-2	-1200.*	PF 1	80.00	1761.17	1762.66	1762.35	1762.91	0.004001	3.95	20.26	18.36	0.66	1.49	0.004001
c-2	-1300.*	PF 1	80.00	1760.77	1762.26	1761.95	1762.51	0.004001	3.95	20.26	18.36	0.66	1.49	0.004001
c-2	-1400.*	PF 1	80.00	1760.37	1761.86	1761.55	1762.11	0.004001	3.95	20.26	18.36	0.66	1.49	0.004000
c-2	-1500.*	PF 1	80.00	1759.97	1761.46	1761.15	1761.71	0.003999	3.95	20.26	18.36	0.66	1.49	0.004000
c-2	-1600.*	PF 1	80.00	1759.57	1761.06	1760.75	1761.31	0.004000	3.95	20.26	18.36	0.66	1.49	0.004000
c-2	-1700.*	PF 1	80.00	1759.17	1760.66	1760.35	1760.91	0.004001	3.95	20.26	18.36	0.66	1.49	0.003989
c-2	-1800.*	PF 1	80.00	1758.77	1760.27	1759.95	1760.51	0.003977	3.94	20.30	18.37	0.66	1.50	0.003925
c-2	-1900.*	PF 1	80.00	1758.37	1759.88	1759.55	1760.11	0.003874	3.90	20.49	18.44	0.65	1.51	0.004716
c-2	-1992.56	PF 1	80.00	1758.00	1759.35	1759.18	1759.67	0.005867	4.52	17.71	17.51	0.79	1.35	0.008603
c-2	-2000	PF 1	89.00	1757.97	1759.17	1759.17	1759.60	0.013101	5.27	16.88	19.87	1.01	1.20	0.012058
c-2	-2039.97	PF 1	89.00	1757.28	1758.43	1758.53	1759.03	0.014778	6.23	14.28	16.29	1.17	1.15	0.013814
c-2	-2079.9*	PF 1	89.00	1756.56	1757.63	1757.81	1758.36	0.018603	6.83	13.03	15.82	1.33	1.07	0.016526
c-2	-2119.9*	PF 1	89.00	1755.83	1756.92	1757.08	1757.61	0.017629	6.69	13.31	15.93	1.29	1.09	0.018106
c-2	-2159.9*	PF 1	89.00	1755.10	1756.18	1756.35	1756.89	0.018146	6.77	13.16	15.87	1.31	1.08	0.017885
c-2	-2200	PF 1	89.00	1754.38	1755.46	1755.63	1756.17	0.017906	6.73	13.23	15.90	1.30	1.08	0.018026
c-2	-2239.9*	PF 1	89.00	1753.92	1755.06	1755.17	1755.67	0.015100	6.29	14.16	16.25	1.19	1.14	0.013937
c-2	-2279.9*	PF 1	89.00	1753.46	1754.64	1754.72	1755.20	0.013337	5.99	14.87	16.50	1.11	1.18	0.012804
c-2	-2319.91	PF 1	92.00	1753.00	1754.21	1754.28	1754.77	0.013470	6.05	15.21	16.63	1.11	1.20	0.012170
c-2	-2419.9*	PF 1	92.00	1751.00	1751.99	1752.28	1752.93	0.025420	7.79	11.81	15.35	1.56	0.99	0.018045
c-2	-2519.9	PF 1	92.00	1749.00	1750.13	1750.28	1750.81	0.016885	6.62	13.90	16.15	1.26	1.12	0.020503
c-2	-2544.9*	PF 1	92.00	1748.50	1749.58	1749.78	1750.34	0.019368	6.99	13.16	15.87	1.35	1.08	0.018063
c-2	-2569.9*	PF 1	92.00	1748.00	1749.07	1749.28	1749.84	0.019636	7.03	13.09	15.85	1.36	1.07	0.019502
c-2	-2594.9*	PF 1	92.00	1747.50	1748.57	1748.78	1749.34	0.019761	7.05	13.06	15.83	1.37	1.07	0.019698
c-2	-2619.9*	PF 1	92.00	1747.00	1748.06	1748.28	1748.85	0.020254	7.12	12.93	15.78	1.39	1.06	0.020005
c-2	-2644.9*	PF 1	92.00	1746.50	1748.17	1747.78	1748.41	0.004515	3.91	23.55	19.41	0.63	1.67	0.002647
c-2	-2669.88	PF 1	92.00	1746.00	1748.19	1747.28	1748.30	0.001737	2.67	34.50	22.54	0.38	2.19	

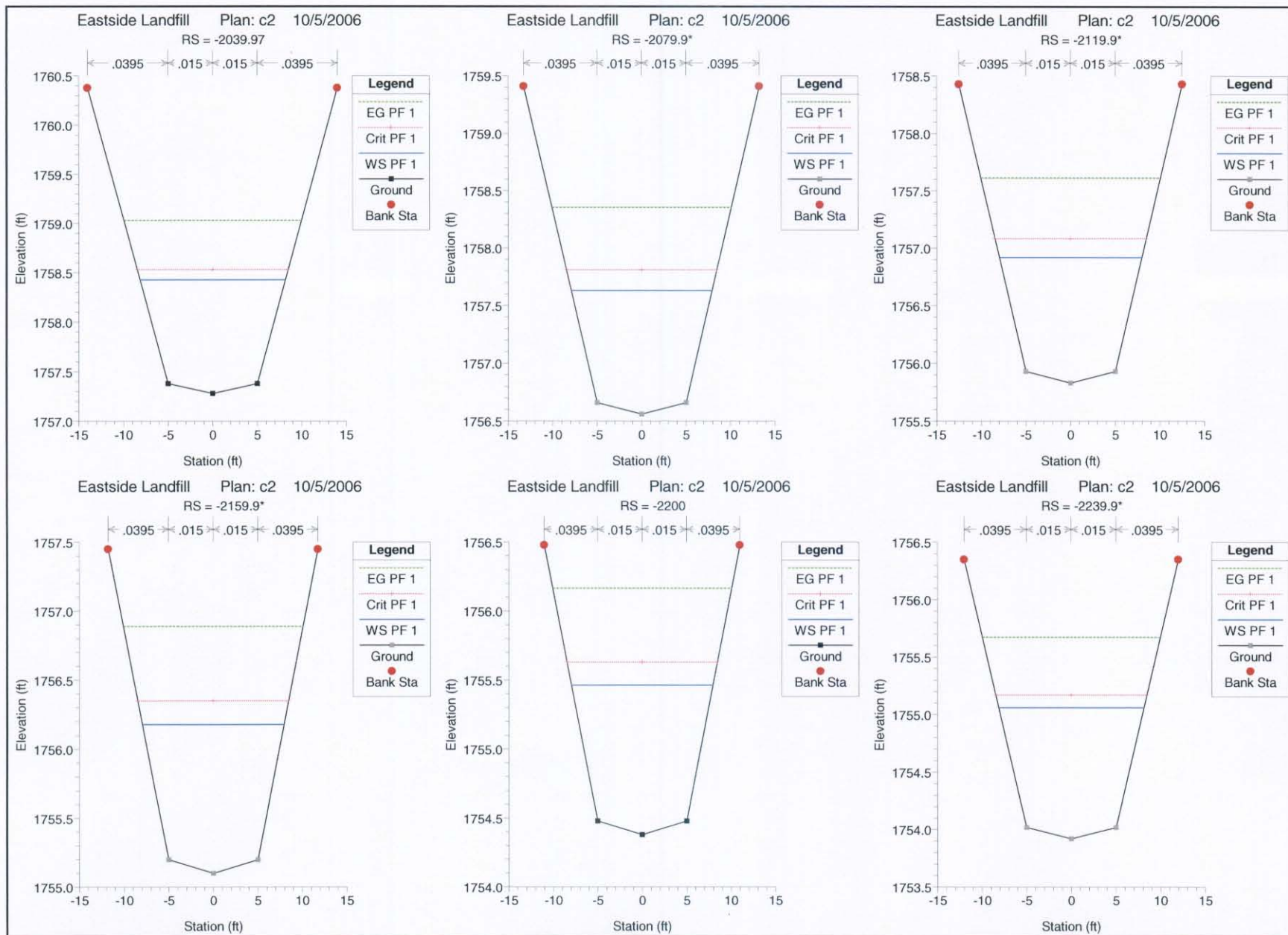




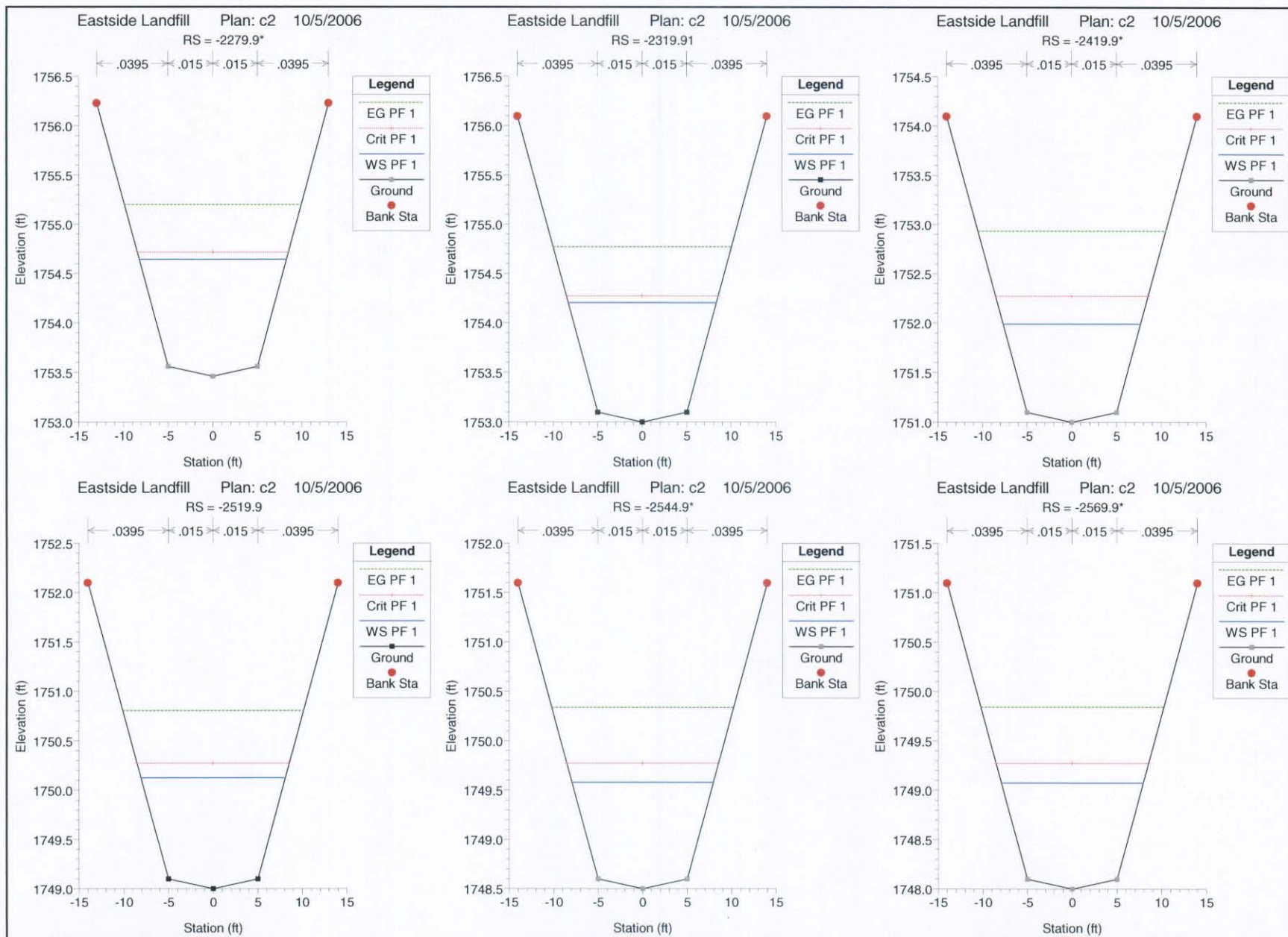




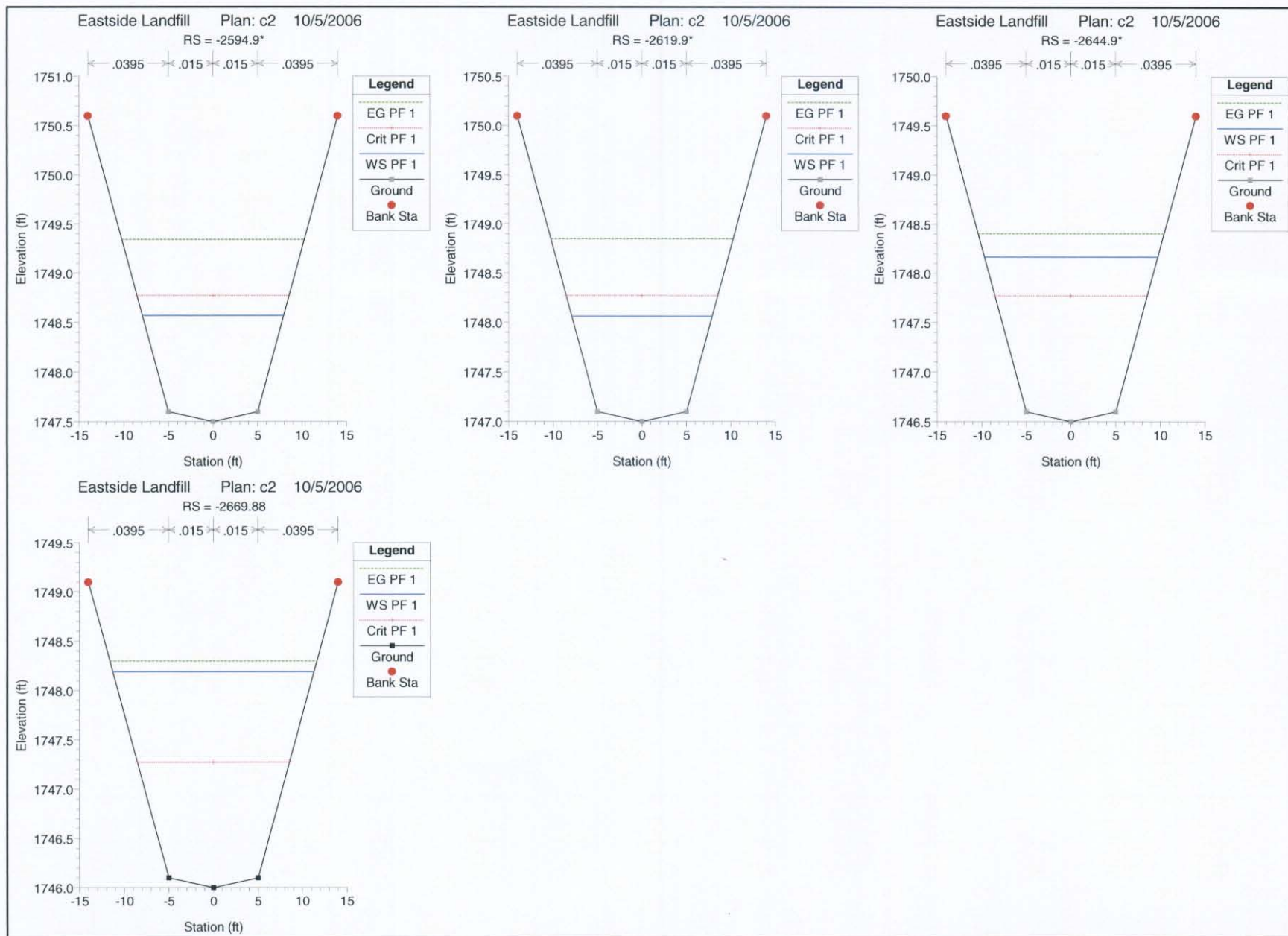














An electronic copy of the HEC-RAS Report is provided in Appendix F.



## **Appendix C-4: Freeboard Calculations for Channel C-1 and C-2**



Channel 1 - (HEC-RAS Channel - C1)

Station	Depth of Water(ft)	Velocity (ft/s)	Channel Top Width (ft)	Froude No.	Subcrit/Supercrit	Freeboard (ft)	Super Elevation (ft)	Required Depth (ft)	Minimum Channel Depth (ft)
+1100	0.70	0.39	13.62	0.09	subcritical	1.0	0.00	1.70	3.00
+1110	0.74	0.37	13.85	0.08	subcritical	1.0	0.00	1.74	3.00
+1120	0.78	0.34	14.09	0.08	subcritical	1.0	0.00	1.78	3.00
+1130	0.82	0.32	14.33	0.07	subcritical	1.0	0.00	1.82	3.00
+1140	0.86	0.30	14.56	0.07	subcritical	1.0	0.00	1.86	3.00
+1150	0.90	0.29	14.80	0.06	subcritical	1.0	0.00	1.90	3.00
+1160	0.94	0.27	15.04	0.06	subcritical	1.0	0.00	1.94	3.00
+1170	0.98	0.26	15.28	0.06	subcritical	1.0	0.00	1.98	3.00
+1180	1.02	0.25	15.52	0.05	subcritical	1.0	0.00	2.02	3.00
+1190	1.06	0.23	15.76	0.05	subcritical	1.0	0.00	2.06	3.00
+1200	0.94	0.31	15.02	0.62	subcritical	1.0	0.00	1.94	3.00
+1250	0.94	0.31	15.03	0.62	subcritical	1.0	0.00	1.94	3.00
+1300	0.94	0.31	15.01	0.62	subcritical	1.0	0.00	1.94	3.00
+1350	0.94	0.31	15.01	0.62	subcritical	1.0	0.00	1.94	3.00
+1400	0.94	0.31	15.02	0.62	subcritical	1.0	0.00	1.94	3.00
+1450	0.94	0.31	15.03	0.62	subcritical	1.0	0.00	1.94	3.00
+1500	0.94	0.31	15.03	0.62	subcritical	1.0	0.00	1.94	3.00
+1550	0.94	0.30	15.03	0.62	subcritical	1.0	0.00	1.94	3.00
+1600	0.95	2.96	15.09	0.61	subcritical	1.0	0.00	1.95	3.00
+1650	0.88	2.85	15.26	0.58	subcritical	1.0	0.00	1.88	3.00
+1700	1.04	2.64	15.61	0.52	subcritical	1.0	0.00	2.04	3.00
+1750	1.14	2.33	16.23	0.44	subcritical	1.0	0.00	2.14	3.00
+1800	1.28	2.00	17.08	0.36	subcritical	1.0	0.00	2.28	3.00
+1850	1.44	1.70	18.07	0.29	subcritical	1.0	0.00	2.44	3.00
+1900	1.62	1.46	19.14	0.24	subcritical	1.0	0.00	2.62	3.00
+1950	1.81	1.25	20.24	0.19	subcritical	1.0	0.00	2.81	3.00
+2000	2.00	1.09	21.38	0.15	subcritical	1.0	0.00	3.00	3.00
+2050	1.62	5.28	19.15	0.85	subcritical	1.0	0.13	3.12	4.00
+2075	1.62	5.28	19.14	0.86	subcritical	1.0	0.13	3.12	4.00
+2100	1.62	5.30	19.12	0.86	subcritical	1.0	0.13	3.12	4.00
+2125	1.62	5.32	19.09	0.86	subcritical	1.0	0.13	3.12	4.00
+2150	1.63	5.25	19.19	0.85	subcritical	1.0	0.13	3.13	4.00
+2175	1.64	5.23	19.21	0.84	subcritical	1.0	0.13	3.14	4.00
+2200	1.62	5.33	19.14	0.86	subcritical	1.0	0.13	3.12	4.00
+2225	1.62	5.33	19.14	0.86	subcritical	1.0	0.13	3.12	4.00
+2245	1.63	5.32	19.15	0.86	subcritical	1.0	0.13	3.13	4.00
+2269.75	1.63	5.31	19.17	0.86	subcritical	1.0	0.13	3.13	4.00
+2273.98	1.63	5.30	19.19	0.86	subcritical	1.0	0.13	3.13	4.00
+2445.1	1.63	5.29	19.20	0.85	subcritical	1.0	0.00	2.63	3.00
+2518.4	1.62	4.97	20.29	0.7	subcritical	1.0	0.00	2.62	3.00
+2587.7	1.66	6.12	18.73	1.01	supercritical	1.2	0.00	2.74	3.00
+2687.7	1.26	8.09	16.98	1.46	supercritical	1.2	0.00	2.48	3.00
+2787.7	1.45	6.71	18.12	1.14	supercritical	1.2	0.00	2.64	3.00
+2887.7	1.33	7.58	17.36	1.34	supercritical	1.2	0.00	2.54	3.00
+2987.7	1.40	7.03	17.82	1.21	supercritical	1.2	0.00	2.60	3.00
+3087.7	1.36	7.40	17.51	1.3	supercritical	1.2	0.00	2.56	3.00
+3187.7	1.38	7.17	17.70	1.34	supercritical	1.2	0.00	2.58	3.00
+3287.7	1.36	7.31	17.58	1.28	supercritical	1.2	0.00	2.56	3.00
+3387.7	1.37	7.23	17.65	1.26	supercritical	1.2	0.00	2.57	3.00
+3487.7	1.36	7.32	17.57	1.29	supercritical	1.2	0.00	2.56	3.00
+3587.7	1.37	7.25	17.62	1.25	supercritical	1.2	0.00	2.57	3.00
+3687.7	1.37	7.29	17.60	1.27	supercritical	1.2	0.00	2.57	3.00
+3787.7	1.37	7.29	17.60	1.27	supercritical	1.2	0.00	2.57	3.00
+3874.1	1.37	7.25	17.63	1.26	supercritical	1.2	0.00	2.57	3.00

Notes: Super Elevation depths were applied from station +2050.00 through +2373.86 around the channel bend. Concrete/Riprap material starts at station +2000.00 and continues through station +3874.10.

Subcritical Freeboard:  $Fb = 0.5 + V^2/2g$

Supercritical Freeboard:  $Fb = 1 + 0.025V^2/d^{1/3}$

Super Elevation:  $Se = CV^2/f_{cr}$  ( $C = 1.0, f_{cr} = 12770$ )

Required Depth = Depth of Flow + Freeboard + Super Elevation

Notes: A minimum of 1R was added for subcritical freeboard if freeboard was less than 1R. If subcritical super elevation was less than 0.5R, 0.5R was to the total channel depth around channel bends.



Channel 2 - (HEC-RAS Channel - C2)

Station	Depth of Water (ft)	Velocity (ft/s)	Channel Top Width (ft)	Froude No.	Subcritical/Supercritical	Freeboard (ft)	Super Elevation (ft)	Required Depth (ft)	Minimum Channel Depth (ft)
+1000	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1100	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1200	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1300	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1400	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1500	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1600	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1700	1.49	3.95	18.36	0.66	subcritical	1.00	0.00	2.49	3.00
+1800	1.50	3.94	18.37	0.66	subcritical	1.00	0.00	2.50	3.00
+1900	1.51	3.90	18.44	0.65	subcritical	1.00	0.00	2.51	3.00
+1992.58	1.25	4.52	17.51	0.79	subcritical	1.00	0.00	2.35	3.00
-2000	1.20	5.27	19.87	1.01	supercritical	1.14	0.00	2.34	3.00
-2039.97	1.15	6.23	15.29	1.17	supercritical	1.16	0.13	2.44	3.00
-2079.9'	1.07	6.53	15.62	1.23	supercritical	1.17	0.15	2.45	3.00
-2119.9'	1.00	6.89	15.93	1.29	supercritical	1.17	0.15	2.41	3.00
-2159.9'	1.08	6.77	15.87	1.31	supercritical	1.17	0.15	2.45	3.00
-2200	1.09	6.73	15.90	1.31	supercritical	1.17	0.15	2.45	3.00
-2239.9'	1.14	6.29	15.25	1.19	supercritical	1.16	0.13	2.44	3.00
-2279.9'	1.18	5.99	15.50	1.11	supercritical	1.16	0.12	2.46	3.00
-2319.91	1.20	6.05	15.63	1.11	supercritical	1.16	0.13	2.49	3.00
-2419.9'	0.99	7.79	15.35	1.56	supercritical	1.19	0.00	2.18	3.00
-2519.9	1.12	6.62	16.15	1.26	supercritical	1.17	0.00	2.29	3.00
-2544.9'	1.08	6.89	15.87	1.35	supercritical	1.18	0.00	2.26	3.00
-2589.9'	1.07	7.03	15.86	1.36	supercritical	1.18	0.00	2.25	4.00
-2594.9'	1.07	7.05	15.83	1.37	supercritical	1.18	0.00	2.25	4.00
-2619.9'	1.06	7.12	15.78	1.38	supercritical	1.18	0.00	2.24	4.00
-2644.9'	1.67	3.91	19.41	0.63	subcritical	1.00	0.00	2.67	4.00
-2669.88	2.19	2.67	22.54	0.38	subcritical	1.00	0.00	3.19	4.00

Notes: Super Elevation depths were applied from station -2039.97 through -2319.91 around the channel bend. Concrete/Riprap material starts at station -2000.00 and continues through station -2269.88.

Subcritical Freeboard:  $Fb = 0.5 + V^2/2g$

Supercritical Freeboard:  $Fb = 1 + 0.033V^2/g^{1/3}$

Super Elevation:  $Se = CV^2/T_{gr}$  ( $C = 1.0$ ,  $r = 1500$ )

Required Depth = Depth of Flow + Freeboard + Super Elevation

Notes: A minimum of 1ft was added for subcritical freeboard if freeboard was less than 1ft. If subcritical super elevation was less than 0.0ft, 0.5ft was to the total channel depth around channel bends.



## **Appendix C-5: Channel and other Hydraulic Cross Sections**

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## Worksheet for Cross Section A

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### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.68	ft
Critical Depth	0.80	ft
Channel Slope	0.02850	ft/ft
Critical Slope	0.01239	ft/ft



## Cross Section A

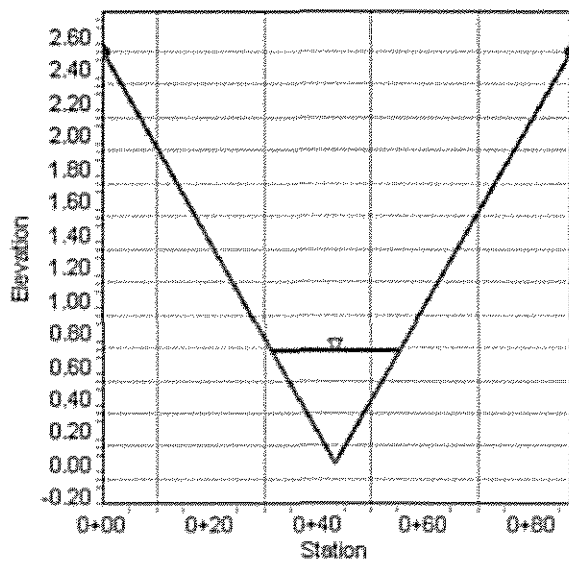
### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

### Input Data

Channel Slope    2.85000    %  
Normal Depth    0.68    ft  
Discharge    40.00    ft<sup>3</sup>/s

### Cross Section Image



$$Q = 40 \text{ cfs} = \text{CP-5}$$



## Project Description

### Input Data

Station (ft)	Elevation (ft)
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### Roughness Segment Definitions

## Results

Bentley Systems, Inc. Haestad Methods Solution Center Bentley FlowMaster [08.01.066.00]  
10/4/2006 3:00:33 PM 27 Siemens Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2



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## Worksheet for Cross Section B

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### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.35	ft
Critical Depth	0.39	ft
Channel Slope	0.02850	ft/ft
Critical Slope	0.01576	ft/ft



## Cross Section B

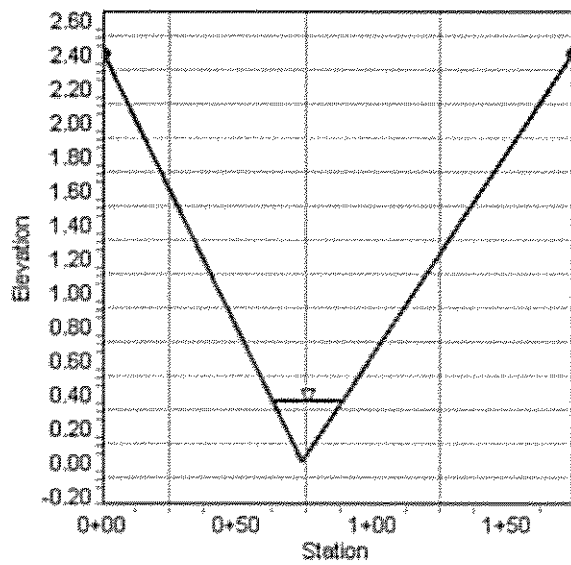
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Channel Slope	2.85000	%
Normal Depth	0.35	ft
Discharge	13.50	ft <sup>3</sup> /s

### Cross Section Image



$$Q = 13.50 \text{ cfs} = \frac{1}{2} \text{ OND } 4$$



## Project Description

## Input Data

## Section Definitions

0+00	2.60
1+10	0.00
1+93	2.60

## Start Station

Ending Station

### Roughness Coefficient

(0+00, 2.60)

(1+93, 2.60)

0.025

## Results

Normal Depth		0.34	ft
Elevation Range	0.00 to 2.60 ft		
Flow Area		4.36	ft²
Wetted Perimeter		25.46	ft
Top Width		25.45	ft
Normal Depth		0.34	ft
Critical Depth		0.38	ft
Critical Slope		0.01581	ft/ft
Velocity		3.10	ft/s
Velocity Head		0.15	ft
Specific Energy		0.49	ft
Froude Number		1.32	
Flow Type	Supercritical		



---

## Worksheet for Cross Section C

---

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.34	ft
Critical Depth	0.38	ft
Channel Slope	0.02850	ft/ft
Critical Slope	0.01581	ft/ft



## Cross Section C

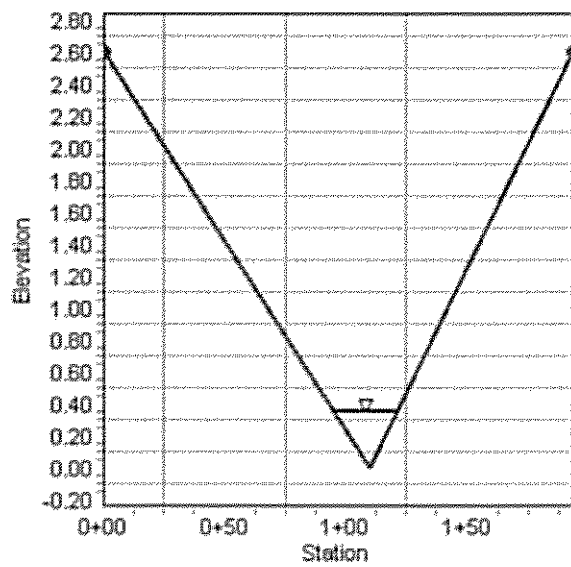
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Channel Slope	2.85000	%
Normal Depth	0.34	ft
Discharge	13.50	ft <sup>3</sup> /s

### Cross Section Image



$$Q = 13.50 \text{ cfs} = \frac{1}{2} \text{ OND4}$$



## Worksheet for Cross Section D

### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

### Input Data

Channel Slope    1.00000    %  
Discharge     12.00    ft<sup>3</sup>/s

### Section Definitions

Station (ft)	Elevation (ft)
--------------	----------------

0+00	1.00
0+35	0.00
0+57	1.00

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 1.00)	(0+57, 1.00)	0.025

### Results

Normal Depth	0.44	ft
Elevation Range	0.00 to 1.00	ft
Flow Area	5.54	ft <sup>2</sup>
Wetted Perimeter	25.15	ft
Top Width	25.13	ft
Normal Depth	0.44	ft
Critical Depth	0.41	ft
Critical Slope	0.01551	ft/ft
Velocity	2.17	ft/s
Velocity Head	0.07	ft
Specific Energy	0.51	ft
Froude Number	0.81	
Flow Type	Subcritical	



---

## Worksheet for Cross Section D

---

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.44	ft
Critical Depth	0.41	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.01551	ft/ft



## Project Description

### Manning Formula

### Normal Depth

12.00 件数

$$Q = 12 \text{ ct} = 0.12 \text{ USD}$$



## Project Description

### Input Data

## Section Definitions

### Roughness Segment Definitions

## Results

10/4/2006 3:00:15 PM Bentley Systems, Inc. Haestad Methods Solution Center Bentley FlowMaster [08.01.066.00]  
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## Worksheet for Cross Section E

---

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.48	ft
Critical Depth	0.45	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.01500	ft/ft



## Cross Section E

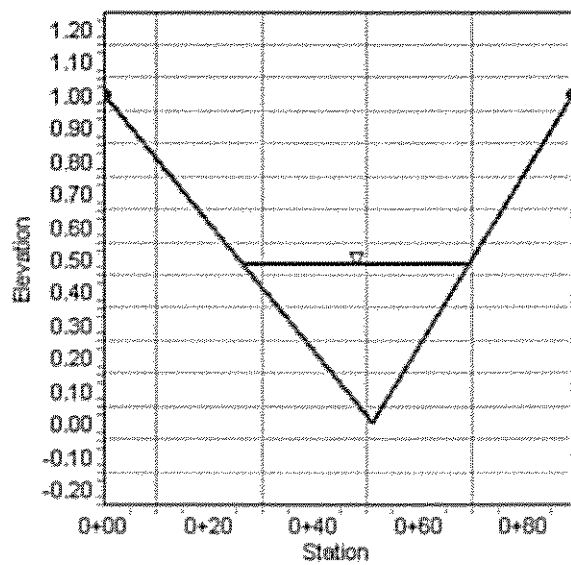
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Channel Slope	1.00000	%
Normal Depth	0.48	ft
Discharge	24.00	ft <sup>3</sup> /s

### Cross Section Image



$$Q = 24 \text{ cfs} = \text{OND11}$$



## Worksheet for Cross Section F

### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

### Input Data

Channel Slope    0.40000    %  
Discharge    12.00    ft<sup>3</sup>/s  
Section Definitions

Station (ft)	Elevation (ft)
0+00	2.30
0+25	0.49
0+48	0.00
0+73	0.00
0+80	2.30

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 2.30)	(0+80, 2.30)	0.025

### Results

Normal Depth    0.27    ft  
Elevation Range    0.00 to 2.30 ft  
Flow Area    8.65    ft<sup>2</sup>  
Wetted Perimeter    38.63    ft  
Top Width    38.58    ft  
Normal Depth    0.27    ft  
Critical Depth    0.18    ft  
Critical Slope    0.01690    ft/ft  
Velocity    1.39    ft/s  
Velocity Head    0.03    ft  
Specific Energy    0.30    ft  
Froude Number    0.52  
Flow Type    Subcritical



## Worksheet for Cross Section F

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.27	ft
Critical Depth	0.18	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.01690	ft/ft



## Cross Section F

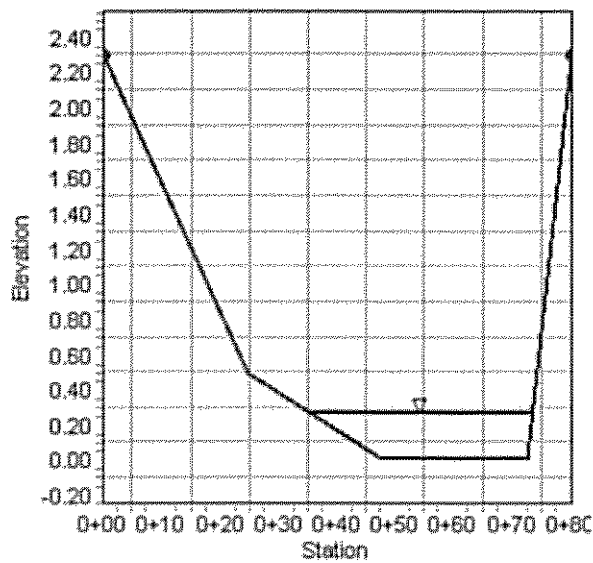
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Channel Slope	0.40000	%
Normal Depth	0.27	ft
Discharge	12.00	ft <sup>3</sup> /s

### Cross Section Image



$$Q = 12 \text{ cfs} = \text{ONDI3}$$

$$F_b = 0.5 + \frac{V^2}{2g} = 0.5 + \frac{(1.39)^2}{2(32.2)} = 0.53 \quad \therefore F_b = 1 \text{ ft}$$

$$\text{Total Depth} = 1 + 0.27 = 1.27 \text{ ft.}$$



## Project Description

## Input Data

## Section Definitions

## Roughness Segment Definitions

## Results

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## Worksheet for Cross Section G

---

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.46	ft
Critical Depth	0.32	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.01359	ft/ft



## Cross Section G

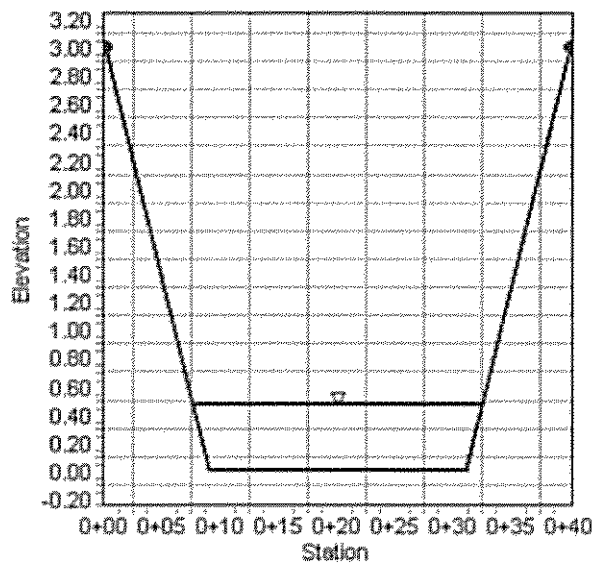
### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

### Input Data

Channel Slope    0.40000    %  
Normal Depth    0.46    ft  
Discharge    23.00    ft<sup>3</sup>/s

### Cross Section Image



$$Q = 23 \text{ cfs} = \text{ONDL}_0$$

$$F_b = 0.5 + \frac{v^2}{2g} = 0.5 + \frac{(2.14)^2}{2(32.2)} = 0.57 \text{ ft} \quad \therefore F_b = 1 \text{ ft}$$

$$\text{Total Depth} = 1 + 0.46 \text{ ft} = 1.46 \text{ ft.}$$



## Worksheet for Cross Section H

### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

### Input Data

Channel Slope    0.40000    %  
Discharge    33.00    ft<sup>3</sup>/s

### Section Definitions

Station (ft)	Elevation (ft)
0+00	3.00
0+09	0.00
0+19	0.00
0+94	0.80
1+06	1.80
1+16	2.80

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 3.00)	(1+16, 2.80)	0.025

### Results

Normal Depth    0.53    ft  
Elevation Range    0.00 to 3.00 ft  
Flow Area    19.16    ft<sup>2</sup>  
Wetted Perimeter    61.80    ft  
Top Width    61.71    ft  
Normal Depth    0.53    ft  
Critical Depth    0.40    ft  
Critical Slope    0.01464    ft/ft  
Velocity    1.72    ft/s  
Velocity Head    0.05    ft  
Specific Energy    0.58    ft  
Froude Number    0.54



## Worksheet for Cross Section H

### Results

Flow Type Subcritical

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.53	ft
Critical Depth	0.40	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.01464	ft/ft



## Cross Section H

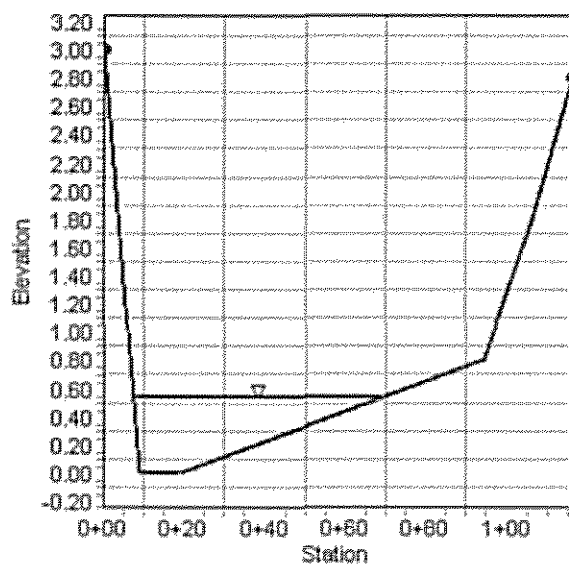
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Channel Slope	0.40000 %
Normal Depth	0.53 ft
Discharge	33.00 ft <sup>3</sup> /s

### Cross Section Image



$$Q = 33 \text{ cfs} = \text{ONDB}$$

$$F_b = 0.5 + \frac{V^2}{2g} = 0.5 + \frac{(1.72)^2}{2(32.2)} = 0.55 \quad \therefore F_b = 1 \text{ ft.}$$

$$S_e = \frac{C V^2 T_w}{g r} = \frac{1.0 (1.72)^2 (61.71)}{32.2 (100)} = 0.06 \text{ ft} \quad \therefore S_e = 0.5 \text{ ft.}$$

Subcritical Supercritical

$$\text{Total Depth} = 1 + 0.5 + 0.53 = 2.03 \text{ ft}$$



## Worksheet for Cross Section I

### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

### Input Data

Channel Slope    0.40000    %  
Discharge     33.00    ft<sup>3</sup>/s

### Section Definitions

Station (ft)	Elevation (ft)
--------------	----------------

0+00	3.00
0+09	0.00
0+19	0.00
0+25	1.52
0+36	1.65
0+46	3.00

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 3.00)	(0+46, 3.00)	0.025

### Results

Normal Depth	0.87    ft
Elevation Range	0.00 to 3.00 ft
Flow Area	11.20    ft <sup>2</sup>
Wetted Perimeter	16.12    ft
Top Width	15.87    ft
Normal Depth	0.87    ft
Critical Depth	0.65    ft
Critical Slope	0.01133    ft/ft
Velocity	2.95    ft/s
Velocity Head	0.14    ft
Specific Energy	1.00    ft
Froude Number	0.62



## Worksheet for Cross Section I

### Results

Flow Type Subcritical

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.87	ft
Critical Depth	0.65	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.01133	ft/ft



## Cross Section I

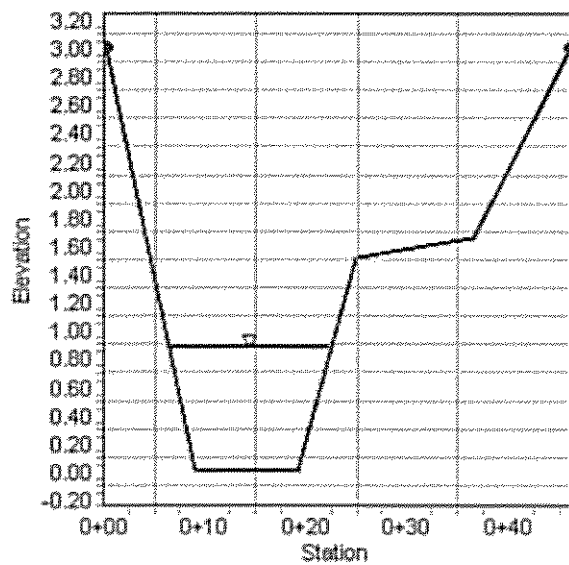
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Channel Slope	0.40000	%
Normal Depth	0.87	ft
Discharge	33.00	ft <sup>3</sup> /s

### Cross Section Image



$$Q = 33 = QND8$$

$$F_0 = 0.5 + \frac{V^2}{2g} = 0.5 + \frac{(2.95)^2}{2(32.2)} = 0.64 \text{ ft.} \quad \therefore F_b = 1 \text{ ft.}$$

$$\text{Total Depth} = 1 + 0.87 = 1.87 \text{ ft.}$$



## Worksheet for Cross Section J

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.025
Channel Slope	1.40000 %
Left Side Slope	3.00 ft/ft (H:V)
Right Side Slope	3.00 ft/ft (H:V)
Bottom Width	24.00 ft
Discharge	33.00 ft <sup>3</sup> /s

### Results

Normal Depth	0.37 ft
Flow Area	9.36 ft <sup>2</sup>
Wetted Perimeter	26.36 ft
Top Width	26.24 ft
Critical Depth	0.38 ft
Critical Slope	0.01281 ft/ft
Velocity	3.53 ft/s
Velocity Head	0.19 ft
Specific Energy	0.57 ft
Froude Number	1.04
Flow Type	Supercritical

### GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

### GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	0.37 ft
Critical Depth	0.38 ft
Channel Slope	0.01400 ft/ft
Critical Slope	0.01281 ft/ft



## Cross Section J

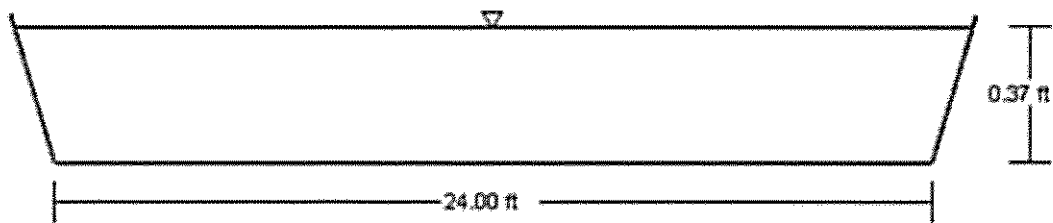
### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.025
Channel Slope	1.40000 %
Normal Depth	0.37 ft
Left Side Slope	3.00 ft/ft (H:V)
Right Side Slope	3.00 ft/ft (H:V)
Bottom Width	24.00 ft
Discharge	33.00 ft <sup>3</sup> /s

### Cross Section Image



$$Q = 33 \text{ cfs} = Q_{ND8}$$

$$F_D = 1.0 + 0.025(V)(d)^{1/3} = 1.0 + 0.025(3.53)(0.37)^{1/3} = 1.06 \text{ ft.}$$

v: 10  
H: 1

$$S_e = \frac{CV^2Tw}{gr} = \frac{1(3.53)^2(26.24)}{(32.2)(55)} = 0.18 \text{ ft.}$$

$$\text{Total Depth} = 1.06 + 0.18 + 0.37 = 1.61 \text{ ft.}$$



## Worksheet for Cross Section K

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.025	
Channel Slope	33.33000	%
Left Side Slope	3.00	ft/ft (H:V)
Right Side Slope	3.00	ft/ft (H:V)
Bottom Width	10.00	ft
Discharge	40.00	ft <sup>3</sup> /s

### Results

Normal Depth	0.27	ft
Flow Area	2.93	ft <sup>2</sup>
Wetted Perimeter	11.72	ft
Top Width	11.63	ft
Critical Depth	0.73	ft
Critical Slope	0.01091	ft/ft
Velocity	13.63	ft/s
Velocity Head	2.89	ft
Specific Energy	3.16	ft
Froude Number	4.78	
Flow Type	Supercritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.27	ft
Critical Depth	0.73	ft
Channel Slope	0.33330	ft/ft
Critical Slope	0.01091	ft/ft



## Cross Section K

### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

### Input Data

Roughness Coefficient	0.025
Channel Slope	33.33000 %
Normal Depth	0.27 ft
Left Side Slope	3.00 ft/ft (H:V)
Right Side Slope	3.00 ft/ft (H:V)
Bottom Width	10.00 ft
Discharge	40.00 ft <sup>3</sup> /s

### Cross Section Image



$$Q = CP - 5 = 40 \text{ cfs}$$

V: 1  
H: 1



## Worksheet for Cross Section L

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.025	
Channel Slope	33.33000	%
Left Side Slope	3.00	ft/ft (H:V)
Right Side Slope	3.00	ft/ft (H:V)
Bottom Width	10.00	ft
Discharge	24.00	ft <sup>3</sup> /s

### Results

Normal Depth	0.20	ft
Flow Area	2.13	ft <sup>2</sup>
Wetted Perimeter	11.27	ft
Top Width	11.20	ft
Critical Depth	0.53	ft
Critical Slope	0.01193	ft/ft
Velocity	11.29	ft/s
Velocity Head	1.98	ft
Specific Energy	2.18	ft
Froude Number	4.57	
Flow Type	Supercritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.20	ft
Critical Depth	0.53	ft
Channel Slope	0.33330	ft/ft
Critical Slope	0.01193	ft/ft



## Cross Section L

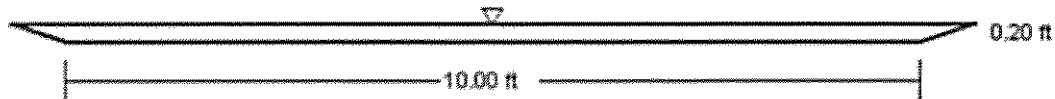
### Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth


### Input Data

Roughness Coefficient	0.025
Channel Slope	33.33000 %
Normal Depth	0.20 ft
Left Side Slope	3.00 ft/ft (H:V)
Right Side Slope	3.00 ft/ft (H:V)
Bottom Width	10.00 ft
Discharge	24.00 ft <sup>3</sup> /s

### Cross Section Image



$$Q = QND11 = 24 \text{ cfs}$$

V: 1   
H: 1



## **Appendix C-6: WSPG model for 42" Storm Drain**

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## STORM DRAIN ANALYSIS PLAN

Original version by Los Angeles County Public Works  
Portions Copyrighted by CIVILSOFT, 1986, 1987, 1989

Version 1.20  
Serial Number 07010318

Oct 5, 2006 21:55:32

Input file : 42rcp.dat  
Output file: 42rcp.out

## INPUT FILE LISTING

```

T1 EASTSIDE LAKEFILL
T2 42" STORM DRAIN
T3 100-YEAR FLOW
NO 1000.001734.00 1 .013 1733.80
WK 1000.001734.00 1 .013
R 1101.201734.50 1 .013
R 1106.201734.70 1 .013
R 1106.201734.70 1 .013
R 1170.161735.00 1 .013
R 1175.161735.20 1 .013
R 1175.161735.20 1 .013
R 1175.161735.20 1 .013
R 1355.391737.00 1 .013
R 1540.591737.20 1 .013
R 1849.771738.40 1 .013
R 1854.771738.80 1 .013
R 2245.011740.70 1 .013
R 2250.011740.90 1 .013
R 2250.011740.90 1 .013
R 2250.011740.90 1 .013
R 2250.011740.90 1 .013
R 2440.121741.92 1 .013
R 2440.121742.12 1 .013
R 2445.121742.12 1 .013
R 2780.601743.70 1 .013
R 2790.601743.90 1 .013
R 2877.941744.50 1 .013
SW 2877.941744.50 1 .013 1740.10
1

```

## WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

CARD	SECT	CHN	NO OF	AVE FIRM	HEIGHT	BASE	EL	2P	INV	V11	V12	V13	V14	V15	V16	V17	V18	V19	V20
NO	NO	TYPE	PIERS	WIDTH	DIAMETER	WIDTH			INCH										

1 1 4 9.50 1733.80

0 OVERLINE LINE NO 1 IS - WATER SURFACE PROFILE - TITLE CARD LISTING

0 OVERLINE LINE NO 2 IS - EASTSIDE LAKEFILL

0 OVERLINE LINE NO 3 IS - 42" STORM DRAIN

0 OVERLINE LINE NO 4 IS - 100-YEAR FLOW

1 1 4 9.50 1733.80

0 ELEMENT NO 1 IS A SYSTEM OUTLET WATER SURFACE PROFILE - ELEMENT CARD LISTING

0 ELEMENT NO 2 IS A WALL EXIT U/S DATA STATION INVERT SECT W S ELEV 1733.80

0 ELEMENT NO 3 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 4 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 5 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 6 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 7 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 8 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 9 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 10 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 11 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 12 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 13 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 14 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 15 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 16 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 17 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 18 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 19 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 20 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 21 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 22 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 23 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 24 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 25 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 26 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 27 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 28 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 29 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 30 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 31 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 32 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 33 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 34 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 35 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 36 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 37 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 38 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 39 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 40 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 41 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 42 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 43 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 44 IS A REACH U/S DATA STATION INVERT SECT

0 ELEMENT NO 45 IS A REACH U/S DATA STATION INVERT SECT







5	1799.80	1738.45	2.73	1741.18	67.0	8.31	1.07	1742.25	.00	2.57		1.30	.00	.00	0	.00
HYDRAULIC JUMP																
0	1799.80	1738.45	2.41	1740.85	67.0	9.30	1.40	1742.25	.00	2.57		1.30	.00	.00	0	.00
0	15.17	.00487					.00684	.07			2.73		.00	.00	0	.00
0	1809.97	1738.50	2.30	1740.85	67.0	9.74	1.47	1742.32	.00	2.57		1.30	.00	.00	0	.00
0	19.45	.00487					.00749	.15			2.73		.00	.00	0	.00
0	1828.61	1738.59	2.36	1740.85	67.0	10.21	1.62	1742.47	.00	2.57		1.30	.00	.00	0	.00
0	20.16	.00487					.00843	.17			2.73		.00	.00	0	.00
0	1849.77	1738.69	2.17	1740.96	67.0	10.71	1.78	1742.64	.00	2.57		1.30	.00	.00	0	.00
0	2.19	.04002					.00945	.02			1.39		.00	.00	0	.00
0	1851.96	1738.78	2.35	1741.03	67.0	10.23	1.63	1742.66	.00	2.57		1.30	.00	.00	0	.00
0	1.56	.04002					.00752	.01			1.39		.00	.00	0	.00
0	1853.59	1738.84	2.35	1741.19	67.0	9.75	1.48	1742.67	.00	2.57		1.30	.00	.00	0	.00
0	.94	.04002					.00669	.01			1.39		.00	.00	0	.00
0	1854.47	1738.88	2.45	1741.33	67.0	9.30	1.34	1742.68	.00	2.57		1.30	.00	.00	0	.00
0	.30	.04002					.00597	.00			1.39		.00	.00	0	.00
0	1854.77	1738.99	2.57	1741.46	67.0	8.86	1.22	1742.68	.00	2.57		1.30	.00	.00	0	.00
0	20.97	.00486					.00534	.11			2.74		.00	.00	0	.00
0	1872.74	1738.99	2.69	1741.60	67.0	8.45	1.11	1742.79	.00	2.57		1.30	.00	.00	0	.00
0	110.84	.00486					.00486	.05			2.74		.00	.00	0	.00
0	1886.19	1739.53	2.74	1742.27	67.0	8.10	1.07	1743.34	.00	2.57		1.30	.00	.00	0	.00
0	210.47	.00486					.00486	1.02			2.74		.00	.00	0	.00

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EASTSIDE LANDFILL  
42" STORM DRAIN  
100-YEAR FLOW

0 STATION	INVERT ELEV FO	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD SF AVE	ENERGY CONC. FO	SUPER ELEV	CRITICAL DEPTH	HWT/ DIA	BASE/ ID NO.	XL IN	NO FEET	AVGFR
*****														
0 2196.66	1740.55	2.74	1743.29	67.0	8.30	1.07	1744.36	.00	2.57		1.30	.00	.00	0 .00
HYDRAULIC JUMP														
0 2196.66	1740.55	2.40	1742.95	67.0	9.31	1.41	1744.36	.00	2.57		1.30	.00	.00	0 .00
0 9.52	.00486					.00685	.07			2.74		.00	.00	0 .00
0 2206.18	1740.60	2.35	1743.95	67.0	9.74	1.47	1744.42	.00	2.57		1.30	.00	.00	0 .00
0 19.55	.00486					.00749	.15			2.74		.00	.00	0 .00
0 2225.73	1740.69	2.36	1743.95	67.0	10.21	1.62	1744.57	.00	2.57		1.30	.00	.00	0 .00
0 20.58	.00486					.00843	.17			2.74		.00	.00	0 .00
0 2240.91	1740.79	2.17	1743.96	67.0	10.71	1.78	1744.74	.00	2.57		1.30	.00	.00	0 .00
0 2.19	.03999					.00945	.02			1.39		.00	.00	0 .00
0 2249.00	1740.88	2.35	1743.13	67.0	10.23	1.63	1744.76	.00	2.57		1.30	.00	.00	0 .00
0 1.57	.03999					.00752	.01			1.39		.00	.00	0 .00
0 2249.37	1740.94	2.35	1743.29	67.0	9.75	1.48	1744.77	.00	2.57		1.30	.00	.00	0 .00
0 .94	.03999					.00669	.01			1.39		.00	.00	0 .00
0 2250.51	1740.98	2.45	1743.43	67.0	9.30	1.34	1744.78	.00	2.57		1.30	.00	.00	0 .00
0 .30	.03999					.00597	.00			1.39		.00	.00	0 .00
0 2250.61	1740.99	2.57	1743.56	67.0	8.86	1.22	1744.78	.00	2.57		1.30	.00	.00	0 .00
0 23.69	.00491					.00534	.13			2.72		.00	.00	0 .00
0 2272.43	1742.11	2.69	1743.79	67.0	8.45	1.11	1744.90	.00	2.57		1.30	.00	.00	0 .00
0 107.88	.00491					.00491	.03			2.72		.00	.00	0 .00
0 2277.30	1741.61	2.73	1744.31	67.0	8.10	1.06	1745.42	.00	2.57		1.30	.00	.00	0 .00
0 10.49	.00491					.00491	.09			2.72		.00	.00	0 .00

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EASTSIDE LANDFILL  
42" STORM DRAIN  
100-YEAR FLOW

SECTION 33-03-00																
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EASTSIDE LANDFILL  
42" STORM DRAIN  
100-YEAR FLOW

SOUTH-TEXAS FLUM																
STATION	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD SF AVE	ENERGY CONC. FO	SUPER ELEV	CRITICAL DEPTH	HWT/ DIA	BASE/ ID NO.	XL IN	NO FEET	AVGFR		
*****																
0 2735.49	1743.54	2.72	1746.27	67.0	8.34	1.08	1747.35	.00	2.57	3.50	.00	.00	0	.00		
HYDRAULIC JUMP																
0 2735.49	1743.54	2.41	1745.96	67.0	9.47	1.39	1747.35	.00	2.57	3.50	.00	.00	0	.00		
0 8.37	.00490					.00674	.06		2.72			.00				
0 2743.86	1743.59	2.37	1745.96	67.0	9.66	1.45	1747.41	.00	2.57	3.50	.00	.00	0	.00		
0 19.31	.00490					.00733	.14		2.72			.00				
0 2763.18	1743.68	2.27	1745.96	67.0	10.13	1.59	1747.55	.00	2.57	3.50	.00	.00	0	.00		
0 20.42	.00490					.00835	.17		2.72			.00				
0 2763.60	1743.78	2.18	1745.96	67.0	10.62	1.75	1747.72	.00	2.57	3.50	.00	.00	0	.00		
0 .00	.00490					.00935	.00		2.72	3.50	.00	.00	0	.00		
0 2783.60	1743.78	2.18	1745.96	67.0	10.62	1.75	1747.72	.00	2.57	3.50	.00	.00	0	.00		
0 1.12	.02856					.00860	.01		1.53			.00				
0 2784.72	1743.81	2.33	1746.02	67.0	10.49	1.71	1747.73	.00	2.57	3.50	.00	.00	0	.00		
0 3.01	.02856					.00798	.02		1.53			.00				
0 2787.74	1743.90	2.30	1746.20	67.0	9.99	1.55	1747.75	.00	2.57	3.50	.00	.00	0	.00		
0 1.95	.02856					.00709	.01		1.53	3.50	.00	.00	0	.00		
0 2789.69	1743.99	2.40	1746.39	67.0	9.53	1.41	1747.81	.00	2.57	3.50	.00	.00	0	.00		
0 1.91	.02856					.00632	.01		1.53			.00				
0 2790.60	1743.98	2.51	1746.49	67.0	9.08	1.28	1747.77	.00	2.57	3.50	.00	.00	0	.00		
0 .00	.02856					.00556	.00		1.53			.00				
0 2790.60	1743.98	2.51	1746.49	67.0	9.08	1.28	1747.77	.00	2.57	3.50	.00	.00	0	.00		
0 75.03	.00855					.00576	.42		2.51	3.50	.00	.00	0	.00		



STATION	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD SF AVE	WATER SURF EL.	SURF ELEV	CRITICAL DEPTH	WATER DEPTH	WET/ DIA	BASE/ ID NO.	SL ELEV	NO FLOW	AVG
0 1/2	1744.43	2.31	1746.91	67.8	9.88	1.28	1748.19	.00	2.37	2.31	3.30	.00	.00	0	.00
0 17.31	.00199					.00199	.10						.00		
0 2877.94	1744.56	2.37	1747.67	67.8	9.88	1.22	1748.29	.00	2.37	2.30	3.30	.00	.00	0	.00



## **Appendix C-7: WSPG model for Detention Basin Outlet**











0	1198.20	1700.43	6.30	1706.73	216.0	11.00	1.00	1708.43	.00	4.18	5.00	.00	0	.00
0	1198.20	1700.43	6.30	1706.84	216.0	11.00	1.00	1708.73	.00	4.18	5.00	.00	0	.00
0	1198.20	1700.43	6.30	1707.03	216.0	11.00	1.00	1708.91	.00	4.18	5.00	.00	0	.00
0	5.00	.01399					.00488	.01			3.09	.00	0	.00
0	1201.20	1700.72	6.34	1707.06	216.0	11.00	1.00	1708.94	.00	4.18	5.00	.00	0	.00
0	175.76	.01447					.00488	.07			3.09	.00	0	.00
0	1228.96	1702.94	5.40	1708.02	216.0	11.00	1.00	1709.90	.00	4.18	5.00	.00	0	.00
0	1229.96	1702.94	5.37	1708.11	216.0	11.00	1.00	1709.99	.00	4.18	5.00	.00	0	.00
0	1229.96	1702.94	5.76	1708.30	216.0	11.00	1.00	1712.38	.00	4.19	5.00	.00	0	.00
0	5.00	.01399					.00488	.01			3.09	.00	0	.00

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EASTSIDE LANDFILL  
OUTLET FROM DETENTION POND WITH 60" HATCHES SD

STATIONS	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD SP AVE	ENERGY GRD. EL. HF	SUPER ELEV	CRITICAL DEPTH	NORM DEPTH	HST/ DIA	BASE/ ID NO.	SL IN	NO PIER	AVRPR
0 1233.96	1702.41	5.73	1708.34	216.0	11.00	1.00	1710.22	.00	4.18	5.00	.00	0	.00	0	.00
0 28.42	.01449					.00488	.27			3.04	.00	0	.00	0	.00
0 1273.45	1703.19	5.42	1708.61	216.0	11.00	1.00	1712.49	.00	4.18	5.00	.00	0	.00	0	.00
0 1100.01	.01001					.00457	.01				.00	0	.00	0	.00
0 1275.45	1703.21	5.75	1708.96	206.0	10.49	1.71	1710.67	.00	4.09	5.00	.00	0	.00	0	.00
0 11.50	.01479					.00626	.07			2.94	.00	0	.00	0	.00
0 1286.95	1703.20	5.74	1709.12	206.0	10.49	1.71	1710.83	.00	4.09	5.00	.00	0	.00	0	.00
0 1286.95	1703.20	5.87	1709.20	206.0	10.49	1.71	1710.91	.00	4.09	5.00	.00	0	.00	0	.00
0 1286.95	1703.20	5.99	1709.37	206.0	10.49	1.71	1711.09	.00	4.09	5.00	.00	0	.00	0	.00
0 5.00	.01399					.00488	.03			2.99	.00	0	.00	0	.00
0 1291.95	1703.20	5.85	1709.40	206.0	10.49	1.71	1711.11	.00	4.09	5.00	.00	0	.00	0	.00
0 86.48	.01447					.00488	.04				.00	0	.00	0	.00
0 1478.43	1704.70	5.36	1709.96	206.0	10.49	1.71	1711.63	.00	4.09	5.00	.00	0	.00	0	.00
0 1478.43	1704.70	5.06	1707.74	206.0	16.36	4.18	1711.93	.00	4.09	5.00	.00	0	.00	0	.00
0 94.47	.01447					.01364	2.19			2.96	.00	0	.00	0	.00
0 1273.30	1705.07	3.13	1709.20	206.0	15.25	3.29	1713.35	.00	4.09	5.00	.00	0	.00	0	.00
0 78.34	.01447					.01335	.90			2.96	.00	0	.00	0	.00
0 1421.34	1707.20	3.26	1710.46	206.0	15.21	3.29	1714.93	.00	4.09	5.00	.00	0	.00	0	.00
0 44.09	.01447					.01028	.49			2.96	.00	0	.00	0	.00
0 1699.23	1707.84	3.40	1711.24	206.0	14.80	3.27	1714.90	.00	4.09	5.00	.00	0	.00	0	.00
0 27.95	.01447					.00913	.25			2.96	.00	0	.00	0	.00

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EASTSIDE LANDFILL  
OUTLET FROM DETENTION POND WITH 60" HATCHES SD

STATION	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD SP AVE	ENERGY GRD. EL. HF	SUPER ELEV	CRITICAL DEPTH	NORM DEPTH	HST/ DIA	BASE/ ID NO.	SL IN	NO PIER	AVRPR
0	1712.88	1708.04	3.55	1711.79	206.0	13.82	3.97	1714.76	.00	4.09	5.00	.00	0	.00	
0	16.95	.01447					.00916	.14			2.96	.00	0	.00	
0	1739.82	1708.48	3.73	1712.19	206.0	13.18	3.70	1714.89	.00	4.09	5.00	.00	0	.00	
0	9.29	.01447					.00722	.07			2.96	.00	0	.00	
0	1749.11	1708.62	3.49	1712.51	206.0	12.37	3.45	1714.96	.00	4.09	5.00	.00	0	.00	
0	2.95	.01447					.00460	.02			2.96	.00	0	.00	
0	1752.06	1709.66	4.09	1712.75	206.0	11.99	3.23	1714.98	.00	4.09	5.00	.00	0	.00	
0	1757.06	1709.74	5.33	1714.07	183.0	8.32	3.73	1719.42	.00	3.87	5.00	.00	0	.00	
0	28.05	.01399					.00488	.14				.00	0	.00	
0	1759.11	1709.31	5.10	1714.21	183.0	9.33	3.35	1719.56	.00	3.87	5.00	.00	0	.00	
0	1759.11	1709.31	2.85	1713.96	183.0	15.82	3.89	1719.84	.00	3.87	5.00	.00	0	.00	
0	144.79	.01302					.01264	3.81			2.84	.00	0	.00	
0	1939.90	1710.99	3.08	1713.87	183.0	15.66	3.81	1717.48	.00	3.87	5.00	.00	0	.00	
0	182.47	.01302					.01176	2.14			2.84	.00	0	.00	
0	2112.32	1713.37	2.39	1716.36	183.0	14.93	3.46	1719.82	.00	3.87	5.00	.00	0	.00	
0	73.39	.01302					.01040	.76			2.84	.00	0	.00	
0	2109.71	1714.32	3.11	1717.43	183.0	14.73	3.10	1720.90	.00	3.87	5.00	.00	0	.00	
0	43.15	.01302					.00922	.32			2.84	.00	0	.00	
0	2224.96	1714.06	3.04	1718.10	183.0	13.37	3.26	1720.96	.00	3.87	5.00	.00	0	.00	
0	23.10	.01302					.00859	.21			2.84	.00	0	.00	
1															END DATA

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EASTSIDE LANDFILL  
OUTLET FROM DETENTION POND WITH 60" HATCHES SD

STATION	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD SP AVE	ENERGY GRD. EL. HF	SUPER ELEV	CRITICAL DEPTH	NORM DEPTH	HST/ DIA	BASE/ ID NO.	SL IN	NO PIER	AVRPR
.....															
0	2251.94	1715.18	3.39	1718.87	183.0	12.94	3.45	1721.17	.00	3.87	5.00	.00	0	.00	
0	15.11	.01302					.00729	.11			2.84	.00	0	.00	
0	2267.07	1715.38	3.23	1718.91	183.0	12.94	3.37	1721.28	.00	3.87	5.00	.00	0	.00	
0	8.30	.01302					.00651	.06			2.84	.00	0	.00	
0	2273.38	1715.49	3.49	1719.10	183.0	11.76	3.10	1721.31	.00	3.87	5.00	.00	0	.00	
0	2.45	.01302					.00583	.01			2.84	.00	0	.00	
0	2277.03	1715.52	3.87	1719.39	183.0	11.21	3.05	1721.35	.00	3.87	5.00	.00	0	.00	
0	2282.03	1715.57	5.76	1721.33	136.0	6.93	3.79	1723.99	.00	3.34	5.00	.00	0	.00	
0	139.65	.00849					.00271	.30				.00	0	.00	
0	2421.68	1716.73	5.00	1721.75	136.0	6.93	3.79	1722.49	.00	3.34	5.00	.00	0	.00	
0	65.30	.00849					.00204	.17			2.89	.00	0	.00	
0	2486.87	1717.35	4.54	1721.84	136.0	7.34	3.82	1723.66	.00	3.34	5.00	.00	0	.00	
0	16.99	.00849					.00142	.04			2.89	.00	0	.00	
0	2503.97	1717.45	4.39	1721.84	136.0	7.44	3.86	1723.70	.00	3.34	5.00	.00	0	.00	
0	2503.97	1717.45	2.50	1719.99	136.0	13.86	3.98	1723.93	.00	3.34	5.00	.00	0	.00	
0	23.23	.00849					.01092	.50			2.89	.00	0	.00	
0	2504.20	1717.45	2.70	1719.99	136.0	13.84	3.98	1723.93	.00	3.34	5.00	.00	0	.00	
0	85.33	.00849					.01466	.76			2.89	.00	0	.00	
0	2509.39	1718.00	2.41	1720.41	136.0	14.93	3.20	1723.69	.00	3.34	5.00	.00	0	.00	
0	90.71	.00849					.01234	.67			2.49	.00	0	.00	

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EASTSIDE LANDFILL  
OUTLET FROM DETENTION POND WITH 60" HATCHES SD

STATION	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD SP AVE	ENERGY GRD. EL. HF	SUPER ELEV	CRITICAL DEPTH	NORM DEPTH	HST/ DIA	BASE/ ID NO.	SL IN	NO PIER	AVRPR
0	2420.04	1718.43	2.33	1720.75	136.0	15.34	3.61	1724.36	.00	3.34	5.00	.00	0	.00	
0	42.30	.00849					.01066	.64			2.89	.00	0	.00	
0	2442.34	1718.79	2.34	1721.03	136.0	15.99	3.97	1725.00	.00	3.34	5.00	.00	0	.00	
0	36.60	.00849					.01714	.62			2.89	.00	0	.00	
0	2499.02	1719.10	2.14	1721.26	136.0	16.77	4.37	1726.63	.00	3.34	5.00	.00	0	.00	
0	32.76	.00849					.01951	.64			2.89	.00	0	.00	
0	2711.78	1719.38	2.50	1721.66	136.0	17.59	4.81	1728.27	.00	3.34	5.00	.00	0	.00	
0	5.00	.00000					.02079	.10			2.10	.00	0	.00	



5	1726.78	1721.48	3.08	1721.36	136.0	17.60	4.81	1726.37	.00	3.24	1.84	5.00	.00	.00	0	.00
5	25.64	.01285					.01961	.55					.00	.00	0	.00
5	1726.42	1720.32	2.10	1722.47	136.0	18.03	4.40	1726.97	.00	3.24	1.84	5.00	.00	.00	0	.00
5	20.64	.01285					.01735	.35					.00	.00	0	.00
5	1723.06	1721.00	2.33	1723.23	136.0	18.04	4.00	1727.23	.00	3.24	1.84	5.00	.00	.00	0	.00
5	15.25	.01280					.01929	.24					.00	.00	0	.00
5	1729.99	1721.52	3.21	1723.93	136.0	19.39	3.64	1727.47	.00	3.24	1.84	5.00	.00	.00	0	.00
5	0.00000	.01281					.01664	.09					.00	.00	0	.00
5	1723.98	1721.48	2.04	1723.72	136.0	18.49	4.33	1728.05	.00	3.21	1.76	5.00	.00	.00	0	.00
5	0.00000	.01281					.01909	.00					.00	.00	0	.00
5	1723.98	1721.48	2.04	1723.72	136.0	18.49	4.33	1728.05	.00	3.21	1.76	5.00	.00	.00	0	.00
5	19.64	.01281					.01798	.35			1.76		.00	.00	0	.00
5	1723.62	1723.32	3.11	1724.44	136.0	19.98	3.97	1728.48	.00	3.21	1.76	5.00	.00	.00	0	.00
5	16.70	.01281					.01388	.27			1.76		.00	.00	0	.00

WATER SURFACE PROFILE LISTING

PAGE 6

EASTSIDE LAKEFILL OUTLET FROM DETENTION POND WITH 60" HATCH SD																
STATION	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD	ENERGY HEAD	SUPER ELEV	CRITICAL DEPTH	WATER DEPTH	WET/ DIA	BASE/ ID NO.	SL NO	NO PIER	AVGPR	
1+00.00	SD					BT AVE	BT									
2840.32	1722.87	2.19	1725.06	126.0	19.24	3.41	1728.67	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	13.10	.01281				.01395	.18						.00	.00	0	.00
2853.41	1723.30	2.27	1725.57	126.0	14.53	3.28	1728.88	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	10.38	.01281				.01227	.13						.00	.00	0	.00
2861.79	1723.64	2.34	1726.00	126.0	13.88	3.29	1729.09	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	9.27	.01281				.01079	.09						.00	.00	0	.00
2872.04	1723.91	2.44	1726.36	126.0	13.21	3.71	1729.27	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	8.58	.01281				.00950	.06						.00	.00	0	.00
2878.64	1724.13	2.54	1726.67	126.0	12.59	3.46	1729.13	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	9.15	.01281				.00837	.04						.00	.00	0	.00
2883.79	1724.30	2.64	1726.93	126.0	12.03	3.24	1729.17	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	3.96	.01281				.00718	.03						.00	.00	0	.00
2887.75	1724.43	2.74	1727.17	126.0	11.45	3.04	1729.20	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	2.93	.01281				.00651	.02						.00	.00	0	.00
2892.66	1724.53	2.85	1727.37	126.0	10.91	3.83	1729.22	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	2.01	.01281				.00575	.01						.00	.00	0	.00
2897.69	1724.59	2.96	1727.59	126.0	10.41	3.68	1729.23	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	1.15	.01281				.00509	.01						.00	.00	0	.00
2893.84	1724.63	3.08	1727.71	126.0	9.93	3.53	1729.24	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	.36	.01281				.00431	.00						.00	.00	0	.00
2894.20	1724.64	3.21	1727.85	126.0	9.46	3.39	1729.24	.00	3.21	1.76	5.00	.00	.00	0	.00	
2	0.00000	.01280				.00227	.01						.00	.00	0	.00

WATER SURFACE PROFILE LISTING

PAGE 7

EASTSIDE LAKEFILL OUTLET FROM DETENTION POND WITH 60" HATCH SD																
STATION	INVERT ELEV	DEPTH OF FLOW	M.S. ELEV	Q	VEL	VEL HEAD	ENERGY HEAD	SUPER ELEV	CRITICAL DEPTH	WATER DEPTH	WET/ DIA	BASE/ ID NO.	SL NO	NO PIER	AVGPR	
1+00.00	SD					BT AVE	BT									
2899.30	1724.75	3.37	1729.92	45.0	2.39	.08	1730.00	.00	1.88	1.23	5.00	.00	.00	0	.00	
2	12.89	.01242				.00010	.00						.00	.00	0	.00
2912.09	1724.91	3.01	1729.92	45.0	2.29	.08	1730.00	.00	1.88	1.09	5.00	.00	.00	0	.00	
2	.46	.01256				.00010	.00						.00	.00	0	.00
2912.35	1724.92	3.00	1729.92	45.0	2.29	.08	1730.00	.00	1.88	1.09	5.00	.00	.00	0	.00	
2	6.54	.01256				.00010	.00						.00	.00	0	.00
2919.09	1725.11	4.81	1729.92	45.0	2.33	.08	1730.01	.00	1.88	1.27	5.00	.00	.00	0	.00	
2	16.15	.00277				.00010	.01						.00	.00	0	.00
2925.34	1725.21	4.72	1729.93	45.0	2.34	.09	1730.02	.00	1.88	1.27	5.00	.00	.00	0	.00	



## **Appendix C-8: Riprap Calculations for C-1 and C-2**



Critical Shear Stress Calculations for Channel 1 (HEC-RAS Channel - C1)

Density of Water	62.4 (lb/ft <sup>3</sup> )	Angle of Repose (12°)	39.5
Specific Gravity of Riprap	2.4	Angle of Repose (18°)	39.8
Density of Riprap	149.76 (lb/ft <sup>3</sup> )	Angle of Repose (24°)	40.2

3

Bank Side Slope (H:V)

18.43

Bank Side Slope (degrees)

HEC-RAS River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Froude # Chl	Frictn Slope (ft/ft)	Rip-Rap Size Used (in)	Shear Stress on banks & side slopes (lb/ft <sup>2</sup> )	Critical Shear Stress on banks & side slopes (lb/ft <sup>2</sup> )	Factor of Safety (Banks & Side Slopes)
-2000	33	1770.75	1772.75	0.00031	1.09	0.16	0.00231	12	0.22	3.75	17.32
-2050	120	1770.55	1772.18	0.00040	5.28	0.85	0.00541	12	0.64	3.75	5.85
-2075	120	1770.34	1771.96	0.00041	5.28	0.86	0.00545	12	0.64	3.75	5.85
-2100	120	1770.13	1771.75	0.00046	5.30	0.86	0.00552	12	0.65	3.75	5.80
-2125	120	1769.92	1771.54	0.00056	5.32	0.86	0.00543	12	0.64	3.75	5.87
-2150	120	1769.70	1771.33	0.00029	5.25	0.85	0.00025	12	0.63	3.75	5.86
-2175	120	1769.49	1771.13	0.00021	5.23	0.84	0.00039	12	0.64	3.75	5.82
-2200	121	1769.28	1770.90	0.00058	5.33	0.86	0.00057	12	0.65	3.75	5.77
-2224.2	121	1769.08	1770.70	0.00056	5.33	0.86	0.00055	12	0.65	3.75	5.79
-2248.5	121	1768.88	1770.51	0.00053	5.32	0.86	0.00051	12	0.65	3.75	5.78
-2269.75	121	1768.68	1770.31	0.00048	5.31	0.86	0.00045	12	0.64	3.75	5.82
-2373.86	121	1767.80	1769.43	0.00042	5.30	0.86	0.00041	12	0.64	3.75	5.84
-2445.1	121	1767.20	1768.83	0.00040	5.29	0.86	0.00033	12	0.53	3.75	7.09
-2516.4	121	1766.60	1768.42	0.00052	4.57	0.70	0.00009	12	0.69	3.75	5.44
-2567.7	131	1766.00	1767.56	0.01160	6.12	1.01	0.01159	12	0.85	3.75	4.43
-2667.7	131	1764.21	1766.47	0.02036	8.09	1.46	0.01594	12	0.94	3.75	3.99
-2767.7	131	1762.42	1763.87	0.01482	6.71	1.14	0.01823	12	1.24	3.75	3.03
-2867.7	131	1760.64	1761.97	0.01987	7.58	1.34	0.01694	12	1.05	3.75	3.56
-2967.7	131	1758.85	1760.25	0.01644	7.03	1.21	0.01803	12	1.18	3.75	3.17
-3067.7	131	1757.06	1758.41	0.01667	7.40	1.30	0.01750	12	1.11	3.75	3.39
-3167.7	131	1755.27	1756.65	0.01726	7.17	1.24	0.01795	12	1.16	3.75	3.23
-3267.7	131	1753.48	1754.84	0.01813	7.31	1.26	0.01769	12	1.13	3.75	3.33
-3367.7	131	1751.70	1753.07	0.01764	7.23	1.26	0.01768	12	1.15	3.75	3.27
-3467.7	131	1749.91	1751.27	0.01816	7.32	1.28	0.01790	12	1.14	3.75	3.29
-3567.7	131	1748.12	1749.49	0.01779	7.26	1.26	0.01798	12	1.15	3.75	3.25
-3667.7	131	1746.33	1747.70	0.01800	7.29	1.27	0.01789	12	1.15	3.75	3.27
-3767.7	131	1744.54	1745.91	0.01798	7.29	1.27	0.01799	12	1.15	3.75	3.25
-3874.1	131	1743.00	1744.37	0.01778	7.25	1.26	0.01787	12	1.15	3.75	3.27

Notes: Riprap design applies to stations -2000 through -3874.10.



**Critical Shear Stress Calculations for Channel 2 (HEC-RAS Channel - C2)**

Density of Water	62.4 (lb/ft <sup>3</sup> )	Angle of Repose (12°)	39.5
Specific Gravity of Riprap	2.4	Angle of Repose (18°)	39.8
Density of Riprap	149.76 (lb/ft <sup>3</sup> )	Angle of Repose (24°)	40.2

Bank Side Slope (H:V) 3  
Bank Side Slope (degrees) 18.43

HEC-RAS River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Froude # Chl	Frctn Slope (ft/ft)	Rip-Rap Size Used (in)	Shear Stress on banks & side slopes (lb/ft <sup>2</sup> )	Critical Shear Stress on banks & side slopes (lb/ft <sup>2</sup> )	Factor of Safety (Banks & Side Slopes)
-2000	89	1757.97	1759.17	0.01310	5.27	1.01	0.01206	12	0.66	3.75	5.54
-2039.97	89	1757.28	1759.43	0.01478	6.23	1.17	0.01381	12	0.74	3.75	5.04
-2079.9	89	1756.56	1757.63	0.01860	6.83	1.33	0.01653	12	0.83	3.75	4.53
-2119.9	89	1755.83	1756.92	0.01783	6.69	1.29	0.01811	12	0.92	3.75	4.06
-2159.9	89	1755.10	1756.18	0.01815	6.77	1.31	0.01789	12	0.90	3.75	4.15
-2200	89	1754.38	1755.46	0.01791	6.73	1.30	0.01803	12	0.91	3.75	4.11
-2239.9	89	1753.62	1755.06	0.01510	6.29	1.19	0.01394	12	0.74	3.75	5.04
-2279.9	89	1753.48	1754.64	0.01334	5.99	1.11	0.01280	12	0.71	3.75	5.30
-2319.91	92	1753.00	1754.21	0.01347	6.05	1.11	0.01217	12	0.69	3.75	5.44
-2419.9	92	1751.00	1751.99	0.02542	7.79	1.56	0.01605	12	0.84	3.75	4.48
-2519.9	92	1749.00	1750.13	0.01689	6.62	1.26	0.00650	12	1.08	3.75	3.48
-2544.9	92	1748.60	1749.58	0.01837	6.99	1.35	0.01606	12	0.91	3.75	4.11
-2569.9	92	1748.00	1749.07	0.01964	7.03	1.36	0.01950	12	0.96	3.75	3.84
-2594.9	92	1747.50	1748.57	0.01976	7.06	1.37	0.01970	12	0.99	3.75	3.80
-2619.9	92	1747.00	1748.06	0.02025	7.12	1.39	0.02001	12	0.99	3.75	3.78
-2644.9	92	1746.50	1748.17	0.02452	3.91	0.83	0.00265	12	0.21	3.75	18.12
-2669.88	92	1746.00	1748.19	0.00174	2.67	0.38					

Notes: Riprap design applies to stations -2000.00 through -2669.88.



## **Appendix D: Reference Material**



“Addendum #1 to the Technical Drainage Study for Henderson Commerce  
Center Two (Formerly known as Harsch)”, Prepared by PBS&J (February 2003)



**ADDENDUM #1 TO THE  
TECHNICAL DRAINAGE STUDY FOR  
HENDERSON COMMMERCE CENTER TWO  
(FORMERLY KNOWN AS HARSCH)**

Prepared for:

**Harsch Investment Properties LLC**  
1121 SW Salmon Street  
Portland, Oregon 97205

Prepared by:

**PBS&J**  
2770 Corporate Circle, Suite 100  
Henderson, Nevada 89074

PBS&J Reference Number: 511434  
February 18, 2003



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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 07JAN83 TIME 16:37:43 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DS, AND HEC1EM.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -ANXXX- ON EN-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81, THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBRKAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION. KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM.

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID TECHNICAL DRAINAGE STUDY FOR HARBOR
2 ID FILE - HADEV_R1.DAT
3 ID HEC-1 FOR HARBOR
4 ID PROJECT NUMBER: 511434
5 ID
6 ID OFFSITE BASINS REFERENCED FROM THE UPDATE TO THE
7 ID TECHNICAL DRAINAGE STUDY FOR EASTGATE ROAD (EG02)
8 ID PREPARED BY FR&J, MAY 2002
9 ID
10 ID
11 ID
*** FREE ***
12 IT 3 0 0 300
13 IO 5 0 0
14 IN 5 0 0
15 JR FREE 0.50 1.00
*
16 EX OFFD-1A
17 EM OFFSITE DEVELOPED BASIN OFFD-1A
18 EM REFERENCED FROM EG02
19 EA 0.0281
20 FB 2.79
21 FC .000 .020 .057 .070 .087 .100 .124 .130 .130 .130
22 FC .130 .130 .130 .133 .140 .142 .148 .158 .172 .181
23 FC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
24 FC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
25 FC .499 .590 .710 .744 .781 .812 .819 .935 .991 .956
26 FC .850 .858 .876 .888 .910 .926 .937 .950 .970 .974
27 FC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
28 FC .998 .999 1.00
29 LS 0 89
30 UD 0.125
*
31 EX OFFD-1B
32 EM OFFSITE DEVELOPED BASIN OFFD-1B
33 EM REFERENCED FROM EG02
34 EA 0.0321
35 FB 2.79
36 LS 0 89
37 UD 0.108
*
38 EX OFFD-M1
39 EM OFFSITE DEVELOPED BASIN OFFD-M1
40 EM REFERENCED FROM EG02
41 EA 0.0064
42 FB 2.79
43 LS 0 88
44 UD 0.084
*

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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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45      KK      RT-1
46      KM      ROUTE OFFD-M1 THROUGH COMMERCIAL WAY
47      KE      420  0.0108  0.015  0  TRAP      15      10
      *

48      KKOFFD-BMIOC
49      KM      OFFSITE DEVELOPED BASIN OFFD-BMIOC
50      KM      REFERENCED FROM EG02
51      BA      0.0032
52      PB      2.79
53      LS      0      88
54      UD      0.105
      *

55      KK      C1
56      KM      COMBINE OFFD-BMIOC, DIV-1 AND RT-1
57      KC      3
      *

58      KK      RT-2
59      KM      ROUTE C1 THROUGH WARM SPRINGS
60      KE      700  0.004  0.015  0  TRAP      15      10
      *

61      KK      OFFD-2
62      KM      OFFSITE DEVELOPED BASIN OFFD-2
63      KM      REFERENCED FROM EG02
64      BA      0.0050
65      PB      2.79
66      LS      0      88
67      UD      0.063
      *

68      KK      C2
69      KM      COMBINE OFFD-2 AND RT-2
70      KC      2
      *

71      KK      RT-3
72      KM      ROUTE C2 THROUGH WARM SPRINGS
73      KE      420  0.004  0.015  0  TRAP      15      10
      *

74      KK      OFFD-3
75      KM      OFFSITE DEVELOPED BASIN OFFD-3
76      KM      REFERENCED FROM EG02
77      BA      0.0040
78      PB      2.79
79      LS      0      88
80      UD      0.052
      *

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1

REC-1 INPUT

PAGE 3

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

81      KK      CWS
82      KM      COMBINE OFFD-3 AND RT-3
83      KC      2
      *

84      KK      DIV-M2
85      KM      FLOWS DIVERTED INTO WARM SPRINGS ROAD
86      KM      STORM DRAIN SYSTEM
87      DIDIV-SDWS
88      DI      0      36      84
89      DO      0      36      75
      *

90      KK      OFFD-12
91      KM      OFFSITE DEVELOPED BASIN OFFD-12
92      KM      REFERENCED FROM EG02
93      BA      0.0129
94      PB      2.79
95      LS      0      97
96      UD      0.113
      *

97      KK      ONDS
98      KM      OFFSITE BASIN 3
99      KM      REFERENCED FROM EG02
100      BA      0.0012
101      PB      2.79
102      LS      0      98
103      UD      0.066
      *

104      KK      CX
105      KM      COMBINE OFFD-12 AND ONDS
106      KC      2
      *

107      KK      DIV-X
108      KM      DIVERT FLOW FROM CX INTO EASTGATE SD

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172      LS      0      92
173      UD      0.084
      *
174      KK      OND-2
175      KM      ONSITE DEVELOPED BASIN OND-2
176      KM      REFERENCED FROM EGG2
177      BA      0.0828
178      PB      2.79
179      LS      0      92
180      UD      0.077
      *
181      KK      C3A
182      KM      COMBINE RT-6, MDEEV-1 AND OND-2
183      KC      3
      *
184      KK      OFFD-OS
185      KM      OFFSITE DEVELOPED BASIN OFFD-OS
186      KM      REFERENCED FROM EGG2
187      BA      0.0253
188      PB      2.79
189      LS      0      92
190      UD      0.061
      *
191      KK      C6
192      KM      COMBINE C3A AND OFFD-OS
193      KC      2
      *
194      KK      DIV-6
195      KM      DIVERT FLOW FROM C6 INTO EASTGATE RD
196      DT      DIV-SD6
197      DI      0      63      120
198      DQ      0      62      88
      *

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1

NBC-1 INPUT

PAGE 6

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
199      KK      RT-7
200      KM      ROUTE DIV-6 THROUGH PART OF OND-1
201      KK      740  0.0146  0.015      0      TRAP      15      10
      *
202      KK      HR7
203      KM      HARSCH ONSITE BASIN
204      BA      0.0825
205      PB      2.79
206      LS      0      92
207      UD      0.086
      *
208      KK      C6A
209      KM      COMBINE RT-7 AND HR7
210      KC      2
      *
211      KK      HR13
212      KM      HARSCH ONSITE BASIN
213      BA      0.0848
214      PB      2.79
215      LS      0      92
216      UD      0.064
      *
217      KK      C6B
218      KM      COMBINE C6A AND HR13 IN EASTGATE ROAD
219      KC      2
      *
220      KK      OFFD-M2
221      KM      OFFSITE DEVELOPED BASIN OFFD-M2
222      KM      REFERENCED FROM EGG2
223      BA      0.0683
224      PB      2.79
225      LS      0      92
226      UD      0.069
      *
227      KK      RT-10
228      KM      ROUTE OFFD-M2 THROUGH OFFD-4
229      KK      520  0.016  0.015      0      TRAP      15      10
      *
230      KK      OFFD-4
231      KM      OFFSITE DEVELOPED BASIN OFFD-4
232      KM      REFERENCED FROM EGG2
233      BA      0.0148
234      PB      2.79
235      LS      0      92
236      UD      0.082

```



LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
237	KK C7
238	KM COMBINE OFFD-M2 AND OFFD-4
239	NC 2
	*
240	KK C11
241	KM COMBINE C7, C18
242	NC 2
	*
243	KK RT-11
244	KM ROUTE C11 THROUGH PART OF OND-1
245	KK 400 0.0145 0.015 0 TRAP 15 10
	*
246	KK OND-1
247	KM ONSITE DEVELOPED BASIN OND-1
248	KM REFERENCED FROM EG02
249	BA 0.0034
250	PB 2.79
251	LS 0 92
252	UD 0.065
	*
253	KK HR16
254	KM HARBORCH ONSITE BASIN
255	BA 0.0034
256	PB 2.79
257	LS 0 92
258	UD 0.065
	*
259	KK C8
260	KM COMBINE OND-1, RT-11 AND HR16
261	NC 3
	*
262	KK DIV-8
263	KM DIVERT FLOW FROM C8 INTO SD
264	DT DIV-8SD
265	DI 0 38 100
266	DQ 0 11 10
	*
267	KK C3
268	KM COMBINE DIV-8 AND DIV-W8
269	NC 2
	*

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
270	KK RT-12
271	KM ROUTE C3 THROUGH WARM SPRINGS
272	KK 700 0.004 0.015 0 TRAP 80 10
	*
273	KK HR18
274	KM HARBORCH ONSITE BASIN
275	BA 0.0047
276	PB 2.79
277	LS 0 92
278	UD 0.090
	*
279	KK C18
280	KM COMBINE RT-12 AND HR18
281	NC 1
	*
282	KK RT-3B
283	KM ROUTE C18 THROUGH WARM SPRINGS
284	KK 800 0.004 0.015 0 TRAP 80 10
	*
285	KK OFFD-14
286	KM OFFSITE DEVELOPED BASIN OFFD-14
287	KM REFERENCED FROM EG02
288	BA 0.0028
289	PB 2.79
290	LS 0 88
291	UD 0.200
	*
292	KK RT-B14
293	KM ROUTE OFFD-14 THROUGH SMIC-1
294	KK 1050 0.014 0.013 0 TRAP 15 10
	*



295 EK BNIC-1  
 296 EM ONSITE DEVELOPED BASIN BNIC-1  
 297 EM REFERENCED FROM EGG2  
 298 BA 0.0141  
 299 PB 2.79  
 300 LS 0 92  
 301 UD 0.081  
 \*

302 EK C15  
 303 EM COMBINE RT-B14, AND BNIC-1  
 304 MC 2  
 \*

1

BEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

305 EK RT-14  
 306 EM ROUTE C15 THROUGH BNIC-2  
 307 EK 450 0.019 0.013 0 TRAP 15 10  
 \*

308 EK BNIC-2  
 309 EM ONSITE DEVELOPED BASIN BNIC-2  
 310 EM REFERENCED FROM EGG2  
 311 BA 0.0118  
 312 PB 2.79  
 313 LS 0 92  
 314 UD 0.073  
 \*

315 EK C16  
 316 EM COMBINE RT-14, AND BNIC-2  
 317 MC 2  
 \*

318 EK RT-15  
 319 EM ROUTE C16 THROUGH SCH-2  
 320 EK 400 0.019 0.013 0 TRAP 15 10  
 \*

321 EK SCH-2  
 322 EM ONSITE DEVELOPED BASIN SCH-2  
 323 EM REFERENCED FROM EGG2  
 324 BA 0.0045  
 325 PB 2.79  
 326 LS 0 92  
 327 UD 0.060  
 \*

328 EK C17  
 329 EM COMBINE RT-15 AND SCH-2  
 330 MC 2  
 \*

331 EK RT-16  
 332 EM ROUTE C17 THROUGH BNIC-3  
 333 EK 750 0.013 0.013 0 TRAP 15 10  
 \*

334 EK BNIC-3  
 335 EM ONSITE DEVELOPED BASIN BNIC-3  
 336 EM REFERENCED FROM EGG2  
 337 BA 0.0106  
 338 PB 2.79  
 339 LS 0 92  
 340 UD 0.082  
 \*

1

BEC-1 INPUT

PAGE 10

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

341 EK MDEEV-2  
 342 EM MILGARD MANUFACTURING ONSITE BASIN  
 343 EM REFERENCED FROM EGG2  
 344 BA 0.0093  
 345 PB 2.79  
 346 LS 0 92  
 347 UD 0.075  
 \*

348 EK OFFD1  
 349 EM OFFSITE BASIN 1  
 350 BA 0.1080  
 351 PB 2.79  
 352 LS 0 77  
 353 UD 0.417  
 \*

354 EK C18  
 355 EM COMBINE RT-16, BNIC-3, MDEEV-2, & OFFD1  
 356 MC 4



```

*
357      KK      HR3
358      EM      HANSEN ONSITE BASIN
359      RA      0.0014
360      PB      2.79
361      LS      0          92
362      UD      0.049
*
363      KK      HR2
364      EM      HANSEN ONSITE BASIN
365      RA      0.0016
366      PB      2.79
367      LS      0          98
368      UD      0.037
*
369      KK      HR1
370      EM      HANSEN ONSITE BASIN
371      RA      0.0018
372      PB      2.79
373      LS      0          92
374      UD      0.05
*
375      KK      CHR1
376      EM      COMBINE HR3, HR2, HR1.
377      EM      THESE FLOWS ARE DISCHARGED INTO THE ONSITE
378      EM      STORM DRAIN SYSTEM LABELED ALIGNMENT "R1"
379      EM      ON FIGURE 7
380      EC      3
*

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1

HRC-1 INPUT

PAGE 11

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

381      KK      C18B
382      EM      COMBINE C18 AND CHR1 IN MAIN STORM DRAIN
383      EM      SYSTEM LABELED H7 ON FIGURE 7
384      EC      2
*
385      KK      HR6
386      EM      HANSEN ONSITE BASIN
387      RA      0.0027
388      PB      2.79
389      LS      0          92
390      UD      0.047
*
391      KK      HR5
392      EM      HANSEN ONSITE BASIN
393      RA      0.0078
394      PB      2.79
395      LS      0          98
396      UD      0.034
*
397      KK      HR4
398      EM      HANSEN ONSITE BASIN
399      RA      0.0078
400      PB      2.79
401      LS      0          98
402      UD      0.034
*
403      KK      CHR2
404      EM      COMBINE HR4, HR5, HR6
405      EM      THESE FLOWS ARE DISCHARGED INTO THE ONSITE
406      EM      STORM DRAIN SYSTEM LABELED ALIGNMENT "R2"
407      EM      ON FIGURE 7
408      EC      3
*
409      KK      C18C
410      EM      COMBINE C18B AND CHR2 IN MAIN STORM DRAIN
411      EM      SYSTEM LABELED H7 ON FIGURE 7
412      EC      2
*
413      KK      HR10
414      EM      HANSEN ONSITE BASIN
415      RA      0.0050
416      PB      2.79
417      LS      0          92
418      UD      0.046
*

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1

HRC-1 INPUT

PAGE 12

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

419      KK      HR9

```



```

420      EM      HANSEN ONSITE BASIN
421      RA      0.0046
422      PB      2.79
423      LS      0          92
424      UD      0.046
      *

425      EK      CHR3
426      EM      COMBINE HR10 AND HR9
427      EM      THESE FLOWS ARE DISCHARGED INTO THE ONSITE
428      EM      STORM DRAIN SYSTEM LABELED ALIGNMENT "HS"
429      EM      ON FIGURE 7
430      NC      2
      *

431      EK      HR8
432      EM      HANSEN ONSITE BASIN
433      RA      0.0031
434      PB      2.79
435      LS      0          92
436      UD      0.061
      *

437      EK      C18D
438      EM      COMBINE C18C, CHR3 AND HR8 IN MAIN STORM DRAIN
439      EM      SYSTEM LABELED N7 ON FIGURE 7
440      NC      1
      *

441      EK      BNIC-4
442      EM      ONSITE DEVELOPED BASIN BNIC-4
443      EM      REFERENCED FROM R002
444      RA      0.0098
445      PB      2.79
446      LS      0          92
447      UD      0.057
      *

448      EK      C18E
449      EM      COMBINE C18D AND BNIC-4 IN MAIN STORM DRAIN
450      EM      SYSTEM LABELED N7 ON FIGURE 7
451      NC      2
      *

452      EK      HR14
453      EM      HANSEN ONSITE BASIN
454      RA      0.0021
455      PB      2.79
456      LS      0          98
457      UD      0.034
      *

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1

HEC-1 INPUT

PAGE 13

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

458      EK      HR11
459      EM      HANSEN ONSITE BASIN
460      RA      0.0046
461      PB      2.79
462      LS      0          98
463      UD      0.034
      *

464      EK      CHR4
465      EM      COMBINE HR14 AND HR11
466      EM      THESE FLOWS ARE DISCHARGED INTO THE ONSITE
467      EM      STORM DRAIN SYSTEM LABELED ALIGNMENT "HS"
468      EM      ON FIGURE 7
469      NC      2
      *

470      EK      HR12
471      EM      HANSEN ONSITE BASIN
472      RA      0.0028
473      PB      2.79
474      LS      0          98
475      UD      0.035
      *

476      EK      HR17
477      EM      HANSEN ONSITE BASIN
478      RA      0.0035
479      PB      2.79
480      LS      0          98
481      UD      0.030
      *

482      EK      HR15
483      EM      HANSEN ONSITE BASIN
484      RA      0.0014
485      PB      2.79
486      LS      0          98
487      UD      0.032
      *

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488      KK      CHR5
489      EM      COMBINE CHR4, HR12, HR17 AND HR15
490      EM      THESE FLOWS ARE DISCHARGED INTO THE ONSITE
491      EM      STORM DRAIN SYSTEM LABELED ALIGNMENT "H3"
492      EM      ON FIGURE 7
493      EC      4
494      *
495      KK      C22
496      EM      COMBINE C18R AND CHR5 AT ENTRANCE TO
497      EM      EXISTING RCB'S UNDER WARM SPRINGS
498      EC      2
499      *

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1

#### HEC-1 INPUT

PAGE 14

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
498      KK      OFFD-13
499      EM      OFFSITE DEVELOPED BASIN OFFD-13
500      EM      REFERENCED FROM RGS2
501      EM      DISCHARGES INTO EASTGATE STORM DRAIN SYSTEM
502      BA      0.0044
503      PE      2.79
504      LE      0          96
505      UD      0.059
506      *
507      KK      SCH-1
508      EM      ONSITE DEVELOPED BASIN SCH-1
509      EM      REFERENCED FROM RGS2
510      BA      0.0073
511      PE      2.79
512      LE      0          92
513      UD      0.062
514      *
515      KK      CULON-1
516      EM      COMMERCIAL WAY CULDESAC ONSITE BASIN 1
517      EM      REFERENCED FROM RGS2
518      BA      0.0013
519      PE      2.79
520      LE      0          98
521      UD      0.043
522      *
523      KK      C23
524      EM      COMBINE SCH-1 AND CULON-1
525      EM      TOTAL FLOW ENTERING CULDESAC DROP INLETS
526      EC      2
527      *
528      KK      *

```

1

#### SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (---) RETURN OF DIVERTED OR PUMPED FLOW

16      OFFD-1A
.
.
31      .      OFFD-1B
.
.
38      .      .      OFFD-M1
.      .      V
.      .      V
45      .      .      RT-1
.      .      .
.      .      .      OFFD-BM1
.      .      .
.      .      .
55      .      C1.....
.      .      V
.      .      V
58      .      RT-2
.      .      .
.      .      .      OFFD-2
.      .      .
.      .      .
68      .      C2.....
.      .      V
.      .      V
71      .      RT-3
.      .      .
.      .      .      OFFD-3
.      .      .
.      .      .
81      .      CWS.....
.      .

```



10



```

237      .      .      .      C7.....
      .      .      .      .
240      .      .      C11.....
      .      .      V
      .      .      V
243      .      .      RT-11
      .      .      .
246      .      .      GND-1
      .      .      .
253      .      .      .      HR16
      .      .      .      .
259      .      .      C8.....
      .      .      .
264      .      .      .-----> DIV-SD8
265      .      .      DIV-8
      .      .      .
267      .      .      C3.....
      .      .      V
      .      .      V
270      .      .      RT-12
      .      .      .
273      .      .      HR18
      .      .      .
279      .      .      C12.....
      .      .      V
      .      .      V
282      .      .      RT-13
      .      .      .
285      .      .      OFFD-14
      .      .      V
      .      .      V
292      .      .      RT-S14
      .      .      .
295      .      .      .      BMIC-1
      .      .      .      .
302      .      .      C15.....
      .      .      V
      .      .      V
305      .      .      RT-14
      .      .      .
308      .      .      .      BMIC-2
      .      .      .      .
315      .      .      C16.....
      .      .      V
      .      .      V
318      .      .      RT-15
      .      .      .
321      .      .      .      SCH-2
      .      .      .      .
328      .      .      C17.....
      .      .      V
      .      .      V
331      .      .      RT-16
      .      .      .
334      .      .      .      BMIC-3
      .      .      .      .
341      .      .      .      .      NGDEV-2
      .      .      .      .      .
348      .      .      .      .      OFFD1
      .      .      .      .      .
354      .      .      C18.....
      .      .      .
357      .      .      .      HR3
      .      .      .      .
363      .      .      .      .      HR2
      .      .      .      .      .
369      .      .      .      .      HR1
      .      .      .      .      .
375      .      .      .      CHR1.....
      .      .      .      .
381      .      .      C18B.....

```







13 IO OUTPUT CONTROL VARIABLES  
 IFENT 5 PRINT CONTROL  
 IFLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 HMIN 3 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 MDATE 1 0 ENDING DATE  
 MTIME 1457 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS  
 TOTAL TIME BASE 14.95 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACER-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANE

JR MULTI-RATIO OPTION  
 RATIO OF PRECIPITATION  
 .55 1.00

\*\*\* FBS&J WARNING TIME STEP CALCULATION FAILED TO CONVERGE. STABILITY PROBLEMS MAY RESULT

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1 .55	RATIO 2 1.00
HYDROGRAPH AT					
* OFFD-1A	.03	1	FLOW TIME	19. 3.55	43. 3.55
HYDROGRAPH AT					
* OFFD-1B	.03	1	FLOW TIME	23. 3.55	52. 3.55
HYDROGRAPH AT					
* OFFD-M1	.01	1	FLOW TIME	4. 3.55	10. 3.55
ROUTED TO					
* RT-1	.01	1	FLOW TIME	4. 3.55	10. 3.55
HYDROGRAPH AT					
* OFFD-BMI	.01	1	FLOW TIME	3. 3.55	8. 3.55
3 COMBINED AT					
* C1	.04	1	FLOW TIME	31. 3.55	79. 3.55
ROUTED TO					
* RT-2	.04	1	FLOW TIME	29. 3.60	68. 3.55
HYDROGRAPH AT					
* OFFD-2	.01	1	FLOW TIME	4. 3.50	10. 3.50
2 COMBINED AT					
* C2	.05	1	FLOW TIME	33. 3.55	77. 3.55
ROUTED TO					
* RT-3	.05	1	FLOW TIME	32. 3.60	76. 3.55
HYDROGRAPH AT					
* OFFD-3	.01	1	FLOW TIME	5. 3.50	11. 3.50



2 COMBINED AT						
+	CMS	.06	1	FLOW	36.	84.
				TIME	3.55	3.55
DIVERSION TO						
+	DIV-SDNS	.06	1	FLOW	26.	75.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	DIV-WB	.06	1	FLOW	0.	9.
				TIME	.00	3.55
HYDROGRAPH AT						
+	OFFD-12	.01	1	FLOW	14.	26.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	OND5	.00	1	FLOW	2.	3.
				TIME	3.50	3.50
2 COMBINED AT						
+	CK	.01	1	FLOW	16.	28.
				TIME	3.55	3.55
DIVERSION TO						
+	DIV-SDX	.01	1	FLOW	15.	21.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	DIV-X	.01	1	FLOW	1.	7.
				TIME	3.55	3.55
ROUTED TO						
+	RT-X	.01	1	FLOW	1.	7.
				TIME	3.60	3.55
HYDROGRAPH AT						
+	OND-4	.00	1	FLOW	2.	3.
				TIME	3.50	3.50
HYDROGRAPH AT						
+	OND-11	.03	1	FLOW	24.	49.
				TIME	3.55	3.55
3 COMBINED AT						
+	C4	.04	1	FLOW	26.	58.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	OND-3	.00	1	FLOW	3.	6.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	CULON-3	.00	1	FLOW	0.	1.
				TIME	2.50	2.50
3 COMBINED AT						
+	C5	.05	1	FLOW	30.	64.
				TIME	3.55	3.55
DIVERSION TO						
+	DIV-SD5	.05	1	FLOW	30.	64.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	DIV-5	.05	1	FLOW	0.	0.
				TIME	.00	.00
HYDROGRAPH AT						
+	OND-10	.03	1	FLOW	24.	48.
				TIME	3.55	3.55
2 COMBINED AT						
+	C14	.07	1	FLOW	24.	48.
				TIME	3.55	3.55
ROUTED TO						
+	RT-6	.07	1	FLOW	23.	48.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	NGDEV-1	.01	1	FLOW	5.	11.
				TIME	3.55	3.50
HYDROGRAPH AT						
+	OND-2	.00	1	FLOW	3.	6.
				TIME	3.50	3.50
3 COMBINED AT						
+	C3A	.08	1	FLOW	32.	65.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	OFFD-09	.03	1	FLOW	33.	57.



				TIME	3.50	3.50
2 COMBINED AT						
+	C6	.11	1	FLOW	63.	129.
				TIME	3.50	3.50
DIVERSION TO						
+	DIV-SD6	.11	1	FLOW	62.	88.
				TIME	3.50	3.50
HYDROGRAPH AT						
+	DIV-6	.11	1	FLOW	1.	32.
				TIME	3.50	3.50
ROUTED TO						
+	RT-7	.11	1	FLOW	1.	30.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	HR7	.00	1	FLOW	2.	5.
				TIME	3.55	3.55
2 COMBINED AT						
+	C6A	.11	1	FLOW	3.	35.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	HR13	.00	1	FLOW	8.	9.
				TIME	3.50	3.50
2 COMBINED AT						
+	C6B	.11	1	FLOW	8.	43.
				TIME	3.50	3.55
HYDROGRAPH AT						
+	OFFD-M2	.01	1	FLOW	10.	18.
				TIME	3.50	3.50
ROUTED TO						
+	RT-10	.01	1	FLOW	10.	18.
				TIME	3.50	3.50
HYDROGRAPH AT						
+	OFFD-4	.01	1	FLOW	13.	27.
				TIME	3.55	3.50
2 COMBINED AT						
+	C7	.02	1	FLOW	23.	48.
				TIME	3.50	3.50
2 COMBINED AT						
+	C11	.14	1	FLOW	31.	88.
				TIME	3.50	3.50
ROUTED TO						
+	RT-11	.14	1	FLOW	30.	87.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	OND-1	.00	1	FLOW	4.	8.
				TIME	3.50	3.50
HYDROGRAPH AT						
+	HR16	.00	1	FLOW	3.	7.
				TIME	3.50	3.50
3 COMBINED AT						
+	C8	.14	1	FLOW	38.	100.
				TIME	3.50	3.55
DIVERSION TO						
+	DIV-SD8	.14	1	FLOW	11.	18.
				TIME	3.50	3.55
HYDROGRAPH AT						
+	DIV-8	.14	1	FLOW	27.	82.
				TIME	3.50	3.55
2 COMBINED AT						
+	C3	.20	1	FLOW	27.	91.
				TIME	3.50	3.55
ROUTED TO						
+	RT-12	.20	1	FLOW	27.	91.
				TIME	3.55	3.55
HYDROGRAPH AT						
+	HR18	.00	1	FLOW	4.	9.
				TIME	3.55	3.55
2 COMBINED AT						
+	C9B	.20	1	FLOW	31.	99.
				TIME	3.55	3.55
ROUTED TO						



+	RT-3B	.20	1	FLOW TIME	30. 3.50	95. 3.55
+	HYDROGRAPH AT OFFD-14	.00	1	FLOW TIME	1. 3.65	4. 3.60
+	ROUTED TO RT-B14	.00	1	FLOW TIME	1. 3.70	3. 3.65
+	HYDROGRAPH AT BMIC-1	.01	1	FLOW TIME	13. 3.55	26. 3.50
+	2 COMBINED AT C15	.02	1	FLOW TIME	14. 3.55	28. 3.55
+	ROUTED TO RT-14	.02	1	FLOW TIME	14. 3.55	28. 3.55
+	HYDROGRAPH AT BMIC-2	.01	1	FLOW TIME	11. 3.50	22. 3.50
+	2 COMBINED AT C16	.03	1	FLOW TIME	24. 3.55	50. 3.50
+	ROUTED TO RT-15	.03	1	FLOW TIME	24. 3.55	50. 3.55
+	HYDROGRAPH AT SCH-2	.01	1	FLOW TIME	6. 3.50	13. 3.50
+	2 COMBINED AT C17	.04	1	FLOW TIME	29. 3.55	62. 3.50
+	ROUTED TO RT-16	.04	1	FLOW TIME	29. 3.55	61. 3.55
+	HYDROGRAPH AT BMIC-3	.01	1	FLOW TIME	10. 3.50	21. 3.50
+	HYDROGRAPH AT HUGHV-2	.01	1	FLOW TIME	8. 3.50	18. 3.50
+	HYDROGRAPH AT OFFD1	.11	1	FLOW TIME	14. 3.95	56. 3.90
+	4 COMBINED AT C18	.16	1	FLOW TIME	50. 3.55	120. 3.55
+	HYDROGRAPH AT HR3	.00	1	FLOW TIME	1. 3.50	3. 3.50
+	HYDROGRAPH AT HR2	.00	1	FLOW TIME	2. 3.50	4. 3.50
+	HYDROGRAPH AT HR1	.00	1	FLOW TIME	2. 3.50	3. 3.50
+	3 COMBINED AT CHR1	.00	1	FLOW TIME	5. 3.50	10. 3.50
+	2 COMBINED AT C18B	.17	1	FLOW TIME	54. 3.55	127. 3.55
+	HYDROGRAPH AT HR6	.00	1	FLOW TIME	3. 3.50	6. 3.50
+	HYDROGRAPH AT HR5	.01	1	FLOW TIME	11. 3.50	19. 3.50
+	HYDROGRAPH AT HR4	.01	1	FLOW TIME	11. 3.50	19. 3.50



3 COMBINED AT	CHR2	.02	1	FLOW	24.	44.
+				TIME	3.50	3.50
2 COMBINED AT	C18C	.19	1	FLOW	79.	169.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR10	.00	1	FLOW	5.	10.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR9	.00	1	FLOW	5.	10.
+				TIME	3.50	3.50
2 COMBINED AT	CHR3	.01	1	FLOW	10.	20.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR8	.00	1	FLOW	3.	6.
+				TIME	3.50	3.50
3 COMBINED AT	C18D	.20	1	FLOW	91.	195.
+				TIME	3.50	3.50
HYDROGRAPH AT	HRIC-4	.01	1	FLOW	10.	20.
+				TIME	3.50	3.50
2 COMBINED AT	C18E	.21	1	FLOW	100.	215.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR14	.00	1	FLOW	3.	5.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR11	.00	1	FLOW	6.	11.
+				TIME	3.50	3.50
2 COMBINED AT	CHR4	.01	1	FLOW	9.	16.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR12	.00	1	FLOW	4.	7.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR17	.00	1	FLOW	5.	9.
+				TIME	3.50	3.50
HYDROGRAPH AT	HR15	.00	1	FLOW	2.	3.
+				TIME	3.50	3.50
4 COMBINED AT	CHR5	.01	1	FLOW	20.	35.
+				TIME	3.50	3.50
2 COMBINED AT	C12	.22	1	FLOW	120.	250.
+				TIME	3.50	3.50
HYDROGRAPH AT	OFFD-13	.00	1	FLOW	5.	10.
+				TIME	3.50	3.50
HYDROGRAPH AT	SCH-1	.01	1	FLOW	7.	14.
+				TIME	3.50	3.50
HYDROGRAPH AT	CULCH-1	.00	1	FLOW	2.	3.
+				TIME	3.50	3.50
2 COMBINED AT	C13	.01	1	FLOW	9.	18.
+				TIME	3.50	3.50

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAG	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		
							PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR PLAN - 1 RATIO*		.58							
RT-1 MAWE		.62	4.44	214.18	.67	3.00	4.38	213.00	.67



CONTINUITY SUMMARY (AC-FT) - INFLOW= .2281E+00 EXCESS= .0000E+00 OUTFLOW= .2284E+00 BASIN STORAGE= .4806E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= 1.00  
RT-1 NAME .61 10.20 213.12 1.63 3.00 10.19 213.00 1.63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2573E+00 EXCESS= .0000E+00 OUTFLOW= .2579E+00 BASIN STORAGE= .4890E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .50  
RT-2 NAME .87 30.66 214.70 .71 3.00 29.28 216.00 .71

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1648E+01 EXCESS= .0000E+00 OUTFLOW= .1651E+01 BASIN STORAGE= .1019E+00 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= 1.00  
RT-2 NAME .85 69.07 213.95 1.69 3.00 67.93 213.00 1.69

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3940E+01 EXCESS= .0000E+00 OUTFLOW= .3945E+01 BASIN STORAGE= .1002E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .50  
RT-3 NAME .61 32.92 214.58 .70 3.00 32.39 216.00 .70

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1864E+01 EXCESS= .0000E+00 OUTFLOW= .1865E+01 BASIN STORAGE= .1875E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= 1.00  
RT-3 NAME .40 77.01 213.87 1.69 3.00 75.58 213.00 1.69

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4467E+01 EXCESS= .0000E+00 OUTFLOW= .4469E+01 BASIN STORAGE= .2059E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .50  
RT-X NAME 1.35 .98 215.44 .02 3.00 .96 216.00 .00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6142E+01 EXCESS= .0000E+00 OUTFLOW= .6159E+01 BASIN STORAGE= .1340E+07 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= 1.00  
RT-X NAME .83 7.02 214.44 .27 3.00 6.88 213.00 .27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2048E+00 EXCESS= .0000E+00 OUTFLOW= .2057E+00 BASIN STORAGE= .1172E+07 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .50  
RT-5 NAME .86 23.42 213.70 .33 3.00 23.30 213.00 .33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1274E+01 EXCESS= .0000E+00 OUTFLOW= .1276E+01 BASIN STORAGE= .4200E+07 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= 1.00  
RT-6 NAME .65 48.13 213.75 .72 3.00 48.09 213.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2775E+01 EXCESS= .0000E+00 OUTFLOW= .2778E+01 BASIN STORAGE= .3022E+07 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .50  
RT-7 NAME 1.49 .98 212.80 .01 3.00 .98 213.00 .01

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5812E+01 EXCESS= .0000E+00 OUTFLOW= .5836E+01 BASIN STORAGE= .2055E+07 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= 1.00  
RT-7 NAME .69 31.47 211.26 .11 3.00 29.95 213.00 .11

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6002E+00 EXCESS= .0000E+00 OUTFLOW= .6035E+00 BASIN STORAGE= .2260E+07 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .50  
RT-10 NAME .57 10.32 210.92 1.40 3.00 9.99 210.00 1.40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6181E+00 EXCESS= .0000E+00 OUTFLOW= .6190E+00 BASIN STORAGE= .5310E+08 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= 1.00  
RT-10 NAME .55 18.20 210.94 2.56 3.00 17.73 210.00 2.56

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1133E+01 EXCESS= .0000E+00 OUTFLOW= .1134E+01 BASIN STORAGE= .6385E+08 PERCENT ERROR= -.1



FOR PLAN = 1	RATIO= .58							
RT-11 NAME	.40	30.70	211.00	.24	3.00	30.47	213.00	.24
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1740E+01 EXCESS= .0000E+00 OUTFLOW= .1740E+01 BASIN STORAGE= .3737E-07 PERCENT ERROR= .0								
FOR PLAN = 1	RATIO= 1.00							
RT-11 NAME	.20	87.73	210.66	.56	3.00	87.15	213.00	.56
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4051E+01 EXCESS= .0000E+00 OUTFLOW= .4051E+01 BASIN STORAGE= .3000E-07 PERCENT ERROR= .0								
FOR PLAN = 1	RATIO= .58							
RT-12 NAME	1.33	26.66	213.92	.15	3.00	26.61	213.00	.15
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1546E+01 EXCESS= .0000E+00 OUTFLOW= .1546E+01 BASIN STORAGE= .7279E-05 PERCENT ERROR= -.4								
FOR PLAN = 1	RATIO= 1.00							
RT-12 NAME	.95	90.85	214.01	.27	3.00	90.61	213.00	.36
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3862E+01 EXCESS= .0000E+00 OUTFLOW= .3878E+01 BASIN STORAGE= .1004E-04 PERCENT ERROR= -.4								
FOR PLAN = 1	RATIO= .58							
RT-3B NAME	1.02	30.32	215.53	.16	3.00	30.03	216.00	.16
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1771E+01 EXCESS= .0000E+00 OUTFLOW= .1774E+01 BASIN STORAGE= .1707E-04 PERCENT ERROR= -.2								
FOR PLAN = 1	RATIO= 1.00							
RT-3B NAME	.64	98.33	214.07	.40	3.00	94.93	213.00	.40
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4366E+01 EXCESS= .0000E+00 OUTFLOW= .4374E+01 BASIN STORAGE= .1547E-04 PERCENT ERROR= -.2								
FOR PLAN = 1	RATIO= .58							
RT-B14 NAME	1.81	1.48	221.29	.67	3.00	1.47	222.00	.67
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9979E+01 EXCESS= .0000E+00 OUTFLOW= .9993E+01 BASIN STORAGE= .6325E-07 PERCENT ERROR= -.1								
FOR PLAN = 1	RATIO= 1.00							
RT-B14 NAME	1.49	3.52	219.64	1.63	3.00	3.50	219.00	1.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2438E+00 EXCESS= .0000E+00 OUTFLOW= .2441E+00 BASIN STORAGE= .6033E-07 PERCENT ERROR= -.1								
FOR PLAN = 1	RATIO= .58							
RT-14 NAME	.51	13.53	213.16	.86	3.00	13.52	213.00	.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7779E+00 EXCESS= .0000E+00 OUTFLOW= .7781E+00 BASIN STORAGE= .5333E-07 PERCENT ERROR= .0								
FOR PLAN = 1	RATIO= 1.00							
RT-14 NAME	.38	28.40	212.96	1.91	3.00	28.40	213.00	1.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1721E+01 EXCESS= .0000E+00 OUTFLOW= .1721E+01 BASIN STORAGE= .5714E-07 PERCENT ERROR= .0								
FOR PLAN = 1	RATIO= .58							
RT-15 NAME	.35	23.91	213.26	.80	3.00	23.90	213.00	.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1346E+01 EXCESS= .0000E+00 OUTFLOW= .1346E+01 BASIN STORAGE= .6782E-07 PERCENT ERROR= .0								
FOR PLAN = 1	RATIO= 1.00							
RT-15 NAME	.38	49.80	211.09	1.93	3.00	49.66	213.00	1.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2958E+01 EXCESS= .0000E+00 OUTFLOW= .2958E+01 BASIN STORAGE= .7279E-07 PERCENT ERROR= .0								
FOR PLAN = 1	RATIO= .58							
RT-16 NAME	.67	29.34	213.15	.80	3.00	29.34	213.00	.80

\*\*\* NORMAL END OF HEC-1 \*\*\*







“Update to the Technical Drainage Study for Henderson Commerce Center  
(Formerly known as Harsch)”, Prepared by PBS&J (February 2005)



**UPDATE TO THE  
TECHNICAL DRAINAGE STUDY  
FOR  
HENDERSON COMMERCE CENTER  
(FORMERLY KNOWN AS HARSCH)  
Permit Number: 2002740088**

**Prepared for:**

**Harsch Investment Properties, LLC  
1121 SW Salmon Street  
Portland, Oregon 97205**

**Prepared by:**

**PBS&J**

**2270 Corporate Circle, Suite 100  
Henderson, Nevada 89074**

**Reference Number 511434.00  
February 22, 2005**



[illegible]

**Verfahren**

Feb 22, 2008 12:44 PM

一、基本理论：1. 马克思主义哲学 2. 辩证唯物主义 3. 历史唯物主义 4. 认识论 5. 方法论 6. 唯物辩证法 7. 唯物史观 8. 唯物论 9. 辩证法 10. 认识论 11. 方法论 12. 唯物辩证法 13. 唯物史观 14. 唯物论 15. 辩证法 16. 认识论 17. 方法论 18. 唯物辩证法 19. 唯物史观 20. 唯物论 21. 辩证法 22. 认识论 23. 方法论 24. 唯物辩证法 25. 唯物史观 26. 唯物论 27. 辩证法 28. 认识论 29. 方法论 30. 唯物辩证法 31. 唯物史观 32. 唯物论 33. 辩证法 34. 认识论 35. 方法论 36. 唯物辩证法 37. 唯物史观 38. 唯物论 39. 辩证法 40. 认识论 41. 方法论 42. 唯物辩证法 43. 唯物史观 44. 唯物论 45. 辩证法 46. 认识论 47. 方法论 48. 唯物辩证法 49. 唯物史观 50. 唯物论 51. 辩证法 52. 认识论 53. 方法论 54. 唯物辩证法 55. 唯物史观 56. 唯物论 57. 辩证法 58. 认识论 59. 方法论 60. 唯物辩证法 61. 唯物史观 62. 唯物论 63. 辩证法 64. 认识论 65. 方法论 66. 唯物辩证法 67. 唯物史观 68. 唯物论 69. 辩证法 70. 认识论 71. 方法论 72. 唯物辩证法 73. 唯物史观 74. 唯物论 75. 辩证法 76. 认识论 77. 方法论 78. 唯物辩证法 79. 唯物史观 80. 唯物论 81. 辩证法 82. 认识论 83. 方法论 84. 唯物辩证法 85. 唯物史观 86. 唯物论 87. 辩证法 88. 认识论 89. 方法论 90. 唯物辩证法 91. 唯物史观 92. 唯物论 93. 辩证法 94. 认识论 95. 方法论 96. 唯物辩证法 97. 唯物史观 98. 唯物论 99. 辩证法 100. 认识论 101. 方法论 102. 唯物辩证法 103. 唯物史观 104. 唯物论 105. 辩证法 106. 认识论 107. 方法论 108. 唯物辩证法 109. 唯物史观 110. 唯物论 111. 辩证法 112. 认识论 113. 方法论 114. 唯物辩证法 115. 唯物史观 116. 唯物论 117. 辩证法 118. 认识论 119. 方法论 120. 唯物辩证法 121. 唯物史观 122. 唯物论 123. 辩证法 124. 认识论 125. 方法论 126. 唯物辩证法 127. 唯物史观 128. 唯物论 129. 辩证法 130. 认识论 131. 方法论 132. 唯物辩证法 133. 唯物史观 134. 唯物论 135. 辩证法 136. 认识论 137. 方法论 138. 唯物辩证法 139. 唯物史观 140. 唯物论 141. 辩证法 142. 认识论 143. 方法论 144. 唯物辩证法 145. 唯物史观 146. 唯物论 147. 辩证法 148. 认识论 149. 方法论 150. 唯物辩证法 151. 唯物史观 152. 唯物论 153. 辩证法 154. 认识论 155. 方法论 156. 唯物辩证法 157. 唯物史观 158. 唯物论 159. 辩证法 160. 认识论 161. 方法论 162. 唯物辩证法 163. 唯物史观 164. 唯物论 165. 辩证法 166. 认识论 167. 方法论 168. 唯物辩证法 169. 唯物史观 170. 唯物论 171. 辩证法 172. 认识论 173. 方法论 174. 唯物辩证法 175. 唯物史观 176. 唯物论 177. 辩证法 178. 认识论 179. 方法论 180. 唯物辩证法 181. 唯物史观 182. 唯物论 183. 辩证法 184. 认识论 185. 方法论 186. 唯物辩证法 187. 唯物史观 188. 唯物论 189. 辩证法 190. 认识论 191. 方法论 192. 唯物辩证法 193. 唯物史观 194. 唯物论 195. 辩证法 196. 认识论 197. 方法论 198. 唯物辩证法 199. 唯物史观 200. 唯物论 201. 辩证法 202. 认识论 203. 方法论 204. 唯物辩证法 205. 唯物史观 206. 唯物论 207. 辩证法 208. 认识论 209. 方法论 210. 唯物辩证法 211. 唯物史观 212. 唯物论 213. 辩证法 214. 认识论 215. 方法论 216. 唯物辩证法 217. 唯物史观 218. 唯物论 219. 辩证法 220. 认识论 221. 方法论 222. 唯物辩证法 223. 唯物史观 224. 唯物论 225. 辩证法 226. 认识论 227. 方法论 228. 唯物辩证法 229. 唯物史观 230. 唯物论 231. 辩证法 232. 认识论 233. 方法论 234. 唯物辩证法 235. 唯物史观 236. 唯物论 237. 辩证法 238. 认识论 239. 方法论 240. 唯物辩证法 241. 唯物史观 242. 唯物论 243. 辩证法 244. 认识论 245. 方法论 246. 唯物辩证法 247. 唯物史观 248. 唯物论 249. 辩证法 250. 认识论 251. 方法论 252. 唯物辩证法 253. 唯物史观 254. 唯物论 255. 辩证法 256. 认识论 257. 方法论 258. 唯物辩证法 259. 唯物史观 260. 唯物论 261. 辩证法 262. 认识论 263. 方法论 264. 唯物辩证法 265. 唯物史观 266. 唯物论 267. 辩证法 268. 认识论 269. 方法论 270. 唯物辩证法 271. 唯物史观 272. 唯物论 273. 辩证法 274. 认识论 275. 方法论 276. 唯物辩证法 277. 唯物史观 278. 唯物论 279. 辩证法 280. 认识论 281. 方法论 282. 唯物辩证法 283. 唯物史观 284. 唯物论 285. 辩证法 286. 认识论 287. 方法论 288. 唯物辩证法 289. 唯物史观 290. 唯物论 291. 辩证法 292. 认识论 293. 方法论 294. 唯物辩证法 295. 唯物史观 296. 唯物论 297. 辩证法 298. 认识论 299. 方法论 300. 唯物辩证法 301. 唯物史观 302. 唯物论 303. 辩证法 304. 认识论 305. 方法论 306. 唯物辩证法 307. 唯物史观 308. 唯物论 309. 辩证法 310. 认识论 311. 方法论 312. 唯物辩证法 313. 唯物史观 314. 唯物论 315. 辩证法 316. 认识论 317. 方法论 318. 唯物辩证法 31

## 22277 7-22-20 15:30

T1 STORM DRAIN ANALYSIS FOR HARSCH H-7  
T2 60" STORM DRAIN - FUTURE CONDITION STORM DRAIN  
T3 Q100-255 CFS

[illegible][illegible]

1992 10 1

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0                                     WATER SURFACE PROFILE - TITLE CARD LISTING
0
0  HEADING LINE NO 1 IS -
0                                     STORM DRAIN ANALYSIS FOR MARCH N-7
0
0  HEADING LINE NO 2 IS -
0                                     40" STORM DRAIN - FUTURE CONDITION STORM DRAIN
0
0  HEADING LINE NO 3 IS -
0                                     Q100=255 CFS

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PAGE NO 3

WATER SURFACE PROFILE - ELEVATION CARD LISTING

0 ELEMENT NO	1 IS A	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99
0 ELEMENT NO	1 IS A	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99
0 ELEMENT NO	1 IS A	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99
0 ELEMENT NO	1 IS A	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99
0 ELEMENT NO	1 IS A	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99
0 ELEMENT NO	1 IS A	2	3	4	5	6	7	8	9																																																																																										



DEV-272.DUT

U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 9 IS A REACH	1194.70	1700.59	1	.013	.00	.00	.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 10 IS A REACH	1198.20	1700.60	1	.013	.00	.00	15.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 11 IS A REACH	1198.20	1700.60	1	.013	.00	.00	15.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 12 IS A REACH	1198.20	1700.60	1	.013	.00	.00	15.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 13 IS A REACH	1203.20	1700.72	1	.013	.00	.00	.00	0

WATER SURFACE PROFILE - ELEMENT CARD LISTING

U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 13 IS A REACH	1328.96	1702.54	1	.013	.00	.00	15.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 14 IS A REACH	1328.96	1702.54	1	.013	.00	.00	15.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 15 IS A REACH	1328.96	1702.54	1	.013	.00	.00	15.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 16 IS A REACH	1333.96	1702.61	1	.013	.00	.00	.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 17 IS A REACH	1373.45	1703.19	1	.013	.00	.00	.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 18 IS A JUNCTION	1375.45	1703.21	1	2	9	0	10.0	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 19 IS A REACH	1386.95	1703.30	1	.013	.00	.00	15.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 20 IS A REACH	1386.95	1703.30	1	.013	.00	.00	15.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 21 IS A REACH	1386.95	1703.30	1	.013	.00	.00	15.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 22 IS A REACH	1391.95	1703.45	1	.013	.00	.00	.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 23 IS A REACH	1752.06	1708.66	1	.013	.00	.00	.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 24 IS A JUNCTION	1757.06	1708.74	1	2	5	0	20.0	0

WATER SURFACE PROFILE - ELEMENT CARD LISTING

U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 25 IS A REACH	2277.83	1719.52	1	.013	.00	.00	.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 26 IS A JUNCTION	2382.83	1719.57	1	7	5	0	44.0	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 27 IS A REACH	2731.78	1719.38	1	.013	.00	.00	15.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 28 IS A REACH	2731.78	1719.38	1	.013	.00	.00	15.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 29 IS A REACH	2736.78	1719.48	1	.013	.00	.00	.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 30 IS A REACH	2798.98	1721.52	1	.013	.00	.00	.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 31 IS A JUNCTION	2803.98	1721.60	1	3	0	0	10.0	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 32 IS A REACH	2894.30	1724.64	1	.013	.00	.00	.00	1
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H
0 ELEMENT NO 33 IS A REACH	2899.20	1724.75	1	.013	.00	.00	.00	0
U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H

NO EDIT ERRORS ENCOUNTERED-COMPUTATION IS NOW BEGINNING

\*\* WARNING NO. 2 \*\* - WATER SURFACE ELEVATION GIVEN IS LESS THAN OR EQUALS INVERT ELEVATION IN ROWS, W.S.ELEV = INV + DC

WATER SURFACE PROFILE LISTING

STORM DRAIN ANALYSIS FOR MARSH H-7

60" STORM DRAIN - FUTURE CONDITION STORM DRAIN

Q100=255 CFS

STATION	INVERT	DEPTH	W.S.	Q	VEL	VEL	ENERGY	SUPER	CRITICAL	HGT/	BASE/	EL	NO	AVBPR
L/ELEM	ELEV	OF FLOW	ELEV		HEAD	HEAD	GRD.EL.	ELEV	DEPTH	DIA	ID NO.	IR	PIER	
					SP AVE	HF								
0 1144.65	1699.87	1.46	1701.33	255.0	17.50	4.76	1706.08	.00	2.72	5.00	19.00	.00	0	.00
0 WALL EXIT														
0 1144.65	1699.87	4.07	1703.94	255.0	14.91	3.46	1707.39	.00	4.45	5.00	.00	.00	0	.00



DEV-272.OUT														
0	13.02	.01427				.00948	.12				3.44		.00	
0	1157.67	1700.06	4.20	1704.26	255.0	14.48	3.26	1707.51	.00	4.45	5.00	.00	.00	.00
0	8.01	.01427				.00885	.07				3.44		.00	
0	1165.68	1700.17	4.45	1704.63	255.0	13.89	2.96	1707.59	.00	4.45	5.00	.00	.00	.00
0	1168.18	1700.20	6.19	1706.39	210.0	10.70	1.78	1708.17	.00	4.13	5.00	.00	.00	.00
0	26.52	.01471				.00650	.17				2.98		.00	
0	1194.70	1700.59	5.97	1706.56	210.0	10.70	1.78	1708.34	.00	4.13	5.00	.00	.00	.00
0	3.50	.01716				.00650	.02				2.84		.00	
0	1198.20	1700.65	6.02	1706.67	210.0	10.70	1.78	1708.45	.00	4.13	5.00	.00	.00	.00
0	1198.20	1700.65	6.11	1706.76	210.0	10.70	1.78	1708.54	.00	4.13	5.00	.00	.00	.00
0	1198.20	1700.65	6.29	1706.94	210.0	10.70	1.78	1708.72	.00	4.13	5.00	.00	.00	.00
0	5.00	.01399				.00650	.01				3.03		.00	
0	1203.20	1700.72	6.25	1706.97	210.0	10.70	1.78	1708.75	.00	4.13	5.00	.00	.00	.00
0	125.76	.01447				.00650	.02				2.99		.00	
0	1328.96	1702.34	5.14	1707.98	210.0	10.70	1.78	1709.65	.00	4.13	5.00	.00	.00	.00
0	1328.96	1702.34	5.42	1708.96	210.0	10.70	1.78	1709.74	.00	4.13	5.00	.00	.00	.00
0	1328.96	1702.34	5.60	1709.14	210.0	10.70	1.78	1709.92	.00	4.13	5.00	.00	.00	.00
0	5.00	.01399				.00650	.03				3.03		.00	

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#### WATER SURFACE PROFILE LISTING

STORM DRAIN ANALYSIS FOR HARSCH N-7  
60" STORM DRAIN - FUTURE CONDITION STORM DRAIN  
Q100=255 CFS

STATION	INVERT ELEV. SG	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD SF AVE	ENERGY GRD. EL. HF	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	EL ZR	NO PIER	AVRPR
0 L/ELEM														
0	1333.96	1702.61	5.56	1708.17	210.0	10.70	1.78	1709.95	.00	4.13	5.00	.00	.00	.00
0	39.49	.01469					.00650	.26			2.98		.00	
0	1373.45	1703.19	5.24	1708.43	210.0	10.70	1.78	1710.21	.00	4.13	5.00	.00	.00	.00
0	1375.45	1703.21	5.56	1708.77	200.0	10.19	1.61	1710.39	.00	4.04	5.00	.00	.00	.00
0	11.50	.01479					.00590	.07			2.88		.00	
0	1386.95	1703.38	5.54	1708.92	200.0	10.19	1.61	1710.53	.00	4.04	5.00	.00	.00	.00
0	1386.95	1703.38	5.62	1709.00	200.0	10.19	1.61	1710.61	.00	4.04	5.00	.00	.00	.00
0	1386.95	1703.38	5.78	1709.16	200.0	10.19	1.61	1710.77	.00	4.04	5.00	.00	.00	.00
0	5.00	.01399					.00590	.03			2.93		.00	
0	1391.95	1703.45	5.74	1709.19	200.0	10.19	1.61	1710.80	.00	4.04	5.00	.00	.00	.00
0	55.71	.01447					.00590	.33			2.98		.00	
0	1447.66	1704.26	5.27	1709.53	200.0	10.19	1.61	1711.14	.00	4.04	5.00	.00	.00	.00
0	1447.66	1704.26	2.97	1707.23	200.0	16.45	4.21	1711.43	.00	4.04	5.00	.00	.00	.00
0	1.32	.01447					.01346	.02			2.90		.00	
0	1448.98	1704.38	2.97	1707.25	200.0	16.44	4.20	1711.45	.00	4.04	5.00	.00	.00	.00
0	144.99	.01447					.01267	1.84			2.90		.00	
0	1593.97	1705.37	3.09	1709.47	200.0	15.68	3.82	1713.28	.00	4.04	5.00	.00	.00	.00
0	66.99	.01447					.01123	.75			2.90		.00	
0	1660.96	1707.34	3.22	1710.57	200.0	14.95	3.47	1714.04	.00	4.04	5.00	.00	.00	.00
0	39.68	.01447					.00997	.40			2.90		.00	

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#### WATER SURFACE PROFILE LISTING

STORM DRAIN ANALYSIS FOR HARSCH N-7  
60" STORM DRAIN - FUTURE CONDITION STORM DRAIN  
Q100=255 CFS

STATION	INVERT ELEV. SG	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD SF AVE	ENERGY GRD. EL. HF	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	EL ZR	NO PIER	AVRPR
0 L/ELEM														
0	1700.64	1707.92	3.36	1711.28	200.0	14.25	3.16	1714.43	.00	4.04	5.00	.00	.00	.00
0	24.80	.01447					.00887	.22			2.90		.00	
0	1725.44	1708.28	3.51	1711.78	200.0	13.59	2.87	1714.65	.00	4.04	5.00	.00	.00	.00
0	15.38	.01447					.00792	.12			2.90		.00	
0	1740.83	1708.50	3.67	1712.17	200.0	12.95	2.61	1714.77	.00	4.04	5.00	.00	.00	.00
0	8.55	.01447					.00709	.06			2.90		.00	
0	1749.38	1708.82	3.84	1712.46	200.0	12.35	2.37	1714.83	.00	4.04	5.00	.00	.00	.00
0	2.68	.01447					.00639	.02			2.90		.00	
0	1752.06	1708.66	4.04	1712.70	200.0	11.77	2.15	1714.85	.00	4.04	5.00	.00	.00	.00
0	1757.06	1708.74	5.27	1714.01	177.0	9.01	1.26	1715.28	.00	3.81	5.00	.00	.00	.00
0	25.83	.01302					.00462	.12			2.78		.00	
0	1782.89	1709.08	5.04	1714.13	177.0	9.01	1.26	1715.40	.00	3.81	5.00	.00	.00	.00
0	1782.89	1709.08	2.79	1711.87	177.0	15.69	3.83	1715.70	.00	3.81	5.00	.00	.00	.00
0	206.14	.01302					.01240	2.57			2.78		.00	
0	1989.03	1711.76	2.84	1714.60	177.0	15.39	3.68	1718.28	.00	3.81	5.00	.00	.00	.00
0	141.95	.01302					.01146	1.63			2.78		.00	
0	2120.98	1713.61	2.95	1716.56	177.0	14.67	3.34	1719.90	.00	3.81	5.00	.00	.00	.00
0	63.49	.01302					.01014	.64			2.78		.00	
0	2194.47	1714.43	3.07	1717.51	177.0	13.99	3.04	1720.95	.00	3.81	5.00	.00	.00	.00
0	36.75	.01302					.00898	.33			2.78		.00	

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#### WATER SURFACE PROFILE LISTING

STORM DRAIN ANALYSIS FOR HARSCH N-7  
60" STORM DRAIN - FUTURE CONDITION STORM DRAIN  
Q100=255 CFS

STATION	INVERT ELEV. SG	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD SF AVE	ENERGY GRD. EL. HF	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	EL ZR	NO PIER	AVRPR
0 L/ELEM														
0	2211.22	1714.91	3.20	1718.11	177.0	13.34	2.76	1720.88	.00	3.81	5.00	.00	.00	.00
0	22.84	.01302					.00797	.18			2.78		.00	
0	2254.06	1715.31	3.34	1718.55	177.0	12.72	2.51	1721.06	.00	3.81	5.00	.00	.00	.00
0	13.90	.01302					.00709	.10			2.78		.00	
0	2267.96	1715.39	3.48	1718.87	177.0	12.12	2.28	1721.16	.00	3.81	5.00	.00	.00	.00
0	7.87	.01302					.00632	.05			2.78		.00	
0	2275.83	1715.49	3.64	1719.13	177.0	11.56	2.08	1721.21	.00	3.81	5.00	.00	.00	.00
0	2.30	.01302					.00566	.01			2.78		.00	
0	2277.83	1715.52	3.81	1719.33	177.0	11.02	1.89	1721.22	.00	3.81	5.00	.00	.00	.00



2022 10-11

姓名	性别	年龄	职业	住址	联系电话
张某某	男	45	教师	北京市朝阳区XX路XX号	138XXXXXX1234
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孙某某	男	60	农民	山东省临沂市XX镇XX村	134XXXXXX7890
周某某	女	40	公务员	北京市西城区XX路XX号	133XXXXXX2345
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郑某某	女	25	学生	浙江省杭州市XX路XX号	131XXXXXX0123
冯某某	男	50	商人	广东省东莞市XX路XX号	130XXXXXX4567
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徐某某	女	48	会计师	湖北省武汉市XX路XX号	127XXXXXX6789
黄某某	男	65	退休	湖南省长沙市XX路XX号	126XXXXXX0123
周某某	女	30	教师	安徽省合肥市XX路XX号	125XXXXXX4567
吴某某	男	52	工程师	福建省厦门市XX路XX号	124XXXXXX8901
郑某某	女	27	学生	江西省南昌市XX路XX号	123XXXXXX2345
冯某某	男	42	商人	广东省广州市XX路XX号	122XXXXXX6789
陈某某	女	33	护士	四川省绵阳市XX路XX号	121XXXXXX0123
林某某	男	20	大学生	河南省洛阳市XX路XX号	120XXXXXX4567
徐某某	女	46	会计师	湖北省武汉市XX路XX号	119XXXXXX8901
黄某某	男	62	退休	湖南省长沙市XX路XX号	118XXXXXX2345
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吴某某	男	54	工程师	福建省厦门市XX路XX号	116XXXXXX0123
郑某某	女	29	学生	江西省南昌市XX路XX号	115XXXXXX4567
冯某某	男	44	商人	广东省广州市XX路XX号	114XXXXXX8901
陈某某	女	34	护士	四川省绵阳市XX路XX号	113XXXXXX2345
林某某	男	21	大学生	河南省洛阳市XX路XX号	112XXXXXX6789
徐某某	女	47	会计师	湖北省武汉市XX路XX号	111XXXXXX0123
黄某某	男	63	退休	湖南省长沙市XX路XX号	110XXXXXX4567
周某某	女	37	教师	安徽省合肥市XX路XX号	109XXXXXX8901
吴某某	男	56	工程师	福建省厦门市XX路XX号	108XXXXXX2345
郑某某	女	31	学生	江西省南昌市XX路XX号	107XXXXXX6789
冯某某	男	45	商人	广东省广州市XX路XX号	106XXXXXX0123
陈某某	女	35	护士	四川省绵阳市XX路XX号	105XXXXXX4567
林某某	男	23	大学生	河南省洛阳市XX路XX号	104XXXXXX8901
徐某某	女	49	会计师	湖北省武汉市XX路XX号	103XXXXXX2345
黄某某	男	64	退休	湖南省长沙市XX路XX号	102XXXXXX6789
周某某	女	39	教师	安徽省合肥市XX路XX号	101XXXXXX0123
吴某某	男	58	工程师	福建省厦门市XX路XX号	100XXXXXX4567
郑某某	女	32	学生	江西省南昌市XX路XX号	099XXXXXX8901
冯某某	男	47	商人	广东省广州市XX路XX号	098XXXXXX2345
陈某某	女	37	护士	四川省绵阳市XX路XX号	097XXXXXX6789
林某某	男	24	大学生	河南省洛阳市XX路XX号	096XXXXXX0123
徐某某	女	51	会计师	湖北省武汉市XX路XX号	095XXXXXX4567
黄某某	男	66	退休	湖南省长沙市XX路XX号	094XXXXXX8901
周某某	女	41	教师	安徽省合肥市XX路XX号	093XXXXXX2345
吴某某	男	60	工程师	福建省厦门市XX路XX号	092XXXXXX6789
郑某某	女	35	学生	江西省南昌市XX路XX号	091XXXXXX0123
冯某某	男	50	商人	广东省广州市XX路XX号	090XXXXXX4567
陈某某	女	40	护士	四川省绵阳市XX路XX号	089XXXXXX8901
林某某	男	26	大学生	河南省洛阳市XX路XX号	088XXXXXX2345
徐某某	女	53	会计师	湖北省武汉市XX路XX号	087XXXXXX6789
黄某某	男	68	退休	湖南省长沙市XX路XX号	086XXXXXX0123
周某某	女	43	教师	安徽省合肥市XX路XX号	085XXXXXX4567
吴某某	男	62	工程师	福建省厦门市XX路XX号	084XXXXXX8901
郑某某	女	38	学生	江西省南昌市XX路XX号	083XXXXXX2345
冯某某	男	53	商人	广东省广州市XX路XX号	082XXXXXX6789
陈某某	女	43	护士	四川省绵阳市XX路XX号	081XXXXXX0123
林某某	男	28	大学生	河南省洛阳市XX路XX号	080XXXXXX4567
徐某某	女	55	会计师	湖北省武汉市XX路XX号	079XXXXXX8901
黄某某	男	70	退休	湖南省长沙市XX路XX号	078XXXXXX2345
周某某	女	45	教师	安徽省合肥市XX路XX号	077XXXXXX6789
吴某某	男	64	工程师	福建省厦门市XX路XX号	076XXXXXX0123
郑某某					

NAME \_\_\_\_\_

THE M. J. O'NEILL CO. INC.

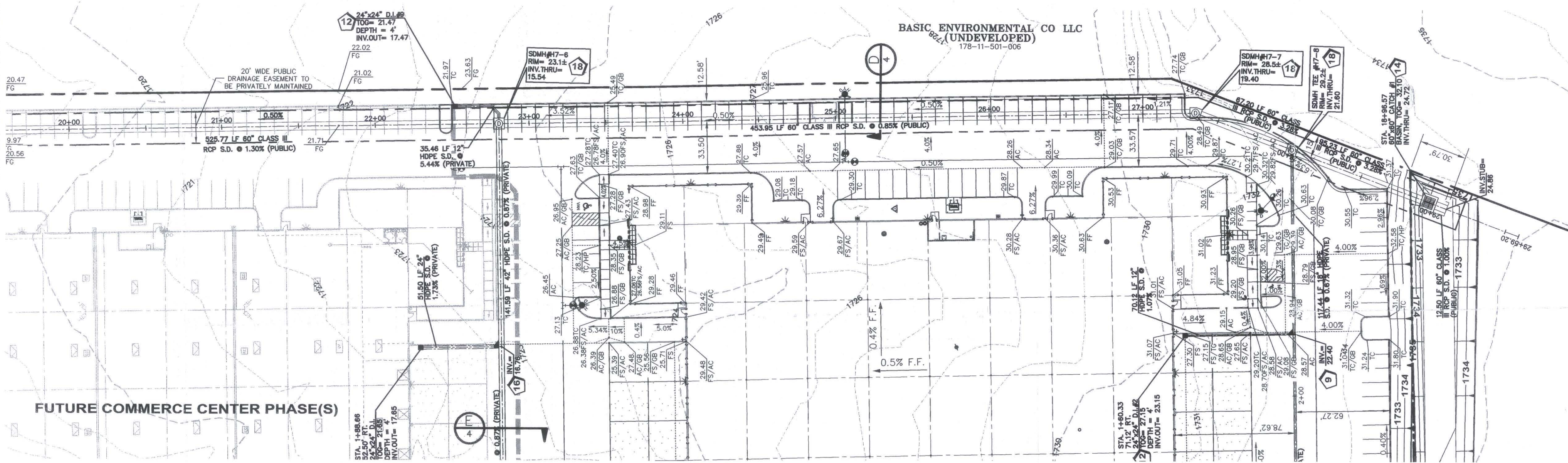
PAGE 3

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20 2323



SEE SHEET 14 FOR STORM DRAIN CONTINUATION



### STORM DRAIN - PLAN VIEW

HORIZONTAL SCALE: 1" = 40'

#### STORM DRAIN CONSTRUCTION NOTES

- 9 INSTALL 12"x18" WYE
- 12 INSTALL 24"x24" DROP INLET PER DETAIL "C" ON SHEET 3.
- 14 INSTALL 60"x60" CATCH BASIN PER DETAIL "U" ON SHEET 4.
- 16 INSTALL 24"x42" WYE
- 18 INSTALL 60" STORM DRAIN TEE RISER PER C.C.A.U.S.D. DWG # 407.
- 20 INSTALL CAP FOR FUTURE EXTENSION. SIZE ACCORDING TO PIPE DIAMETER.
- 21 INSTALL 60" RCP HEADWALL PER NDOT DWG. No. R-2.5.2.

#### BENCHMARK

CITY OF HENDERSON BENCHMARK # 5  
DESCRIPTION: BOLT AND WASHER IN THE  
TOP OF THE CURB ON THE EAST SIDE OF  
HIGHWAY 93, 100 FEET +/- NORTHWEST  
OF THE CENTERLINE OF KING STREET.  
ELEVATION IN FEET = 1702.82 (NAVD '88)  
ELEVATION IN METERS = 519.021 (NAVD '88)

#### BASIS OF BEARINGS

NORTH 89°58'43" EAST - BEING THE NORTH LINE OF THE  
NORTHEAST QUARTER (NE 1/4) OF SECTION 11,  
TOWNSHIP 22 SOUTH,  
RANGE 62 EAST, M.D.M., CLARK COUNTY, NEVADA AS  
SHOWN BY A MAP  
ON FILE IN THE OFFICE OF THE CLARK COUNTY  
RECORDER IN BOOK 97,  
PAGE 99 OF PLATS, OFFICIAL RECORDS.

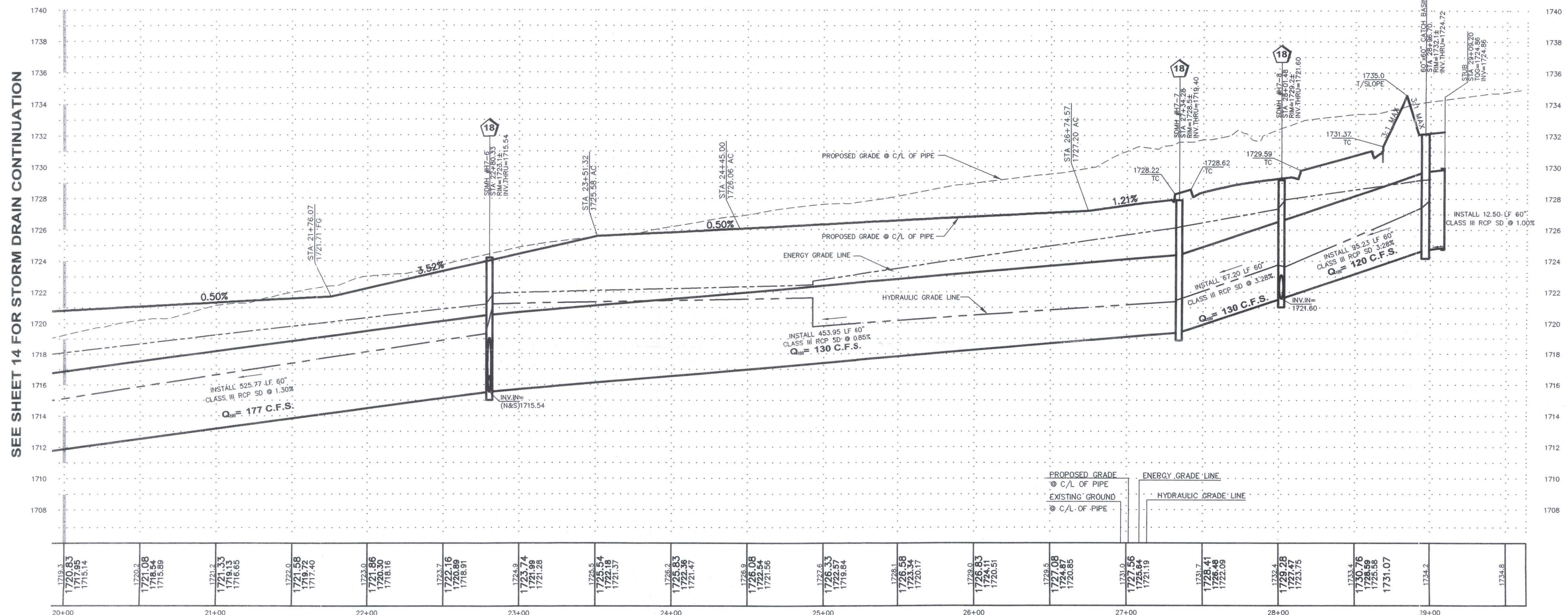
#### APPROVAL

NEW DEVELOPMENT ENGINEER, CITY OF HENDERSON - KEN Y. KOSHIRO, P.E. DATE  
CITY APPROVAL OF THE IMPROVEMENT PLANS IS GRANTED FOR ONE (1) YEAR ONLY. PLANS  
MUST BE RESUBMITTED FOR REVIEW AND APPROVAL TO THE DEPARTMENT OF PUBLIC WORKS,  
CITY OF HENDERSON, IF WORK IS NOT COMPLETED BY 20

Call before you Dig.  
1-800-227-2600  
UNDERGROUND SERVICE ALERT (USA)

Call before you OVERHEAD  
1-702-227-2929  
NEVADA POWER ENVIRONMENT AND  
SAFETY SERVICES DEPARTMENT

Call before you UnderGround  
1-702-455-7511  
CLARK COUNTY DEPT. OF PUBLIC WORKS  
1-702-729-6611  
LAS VEGAS AND CONFIDENTIAL TRAILER TRUCKS

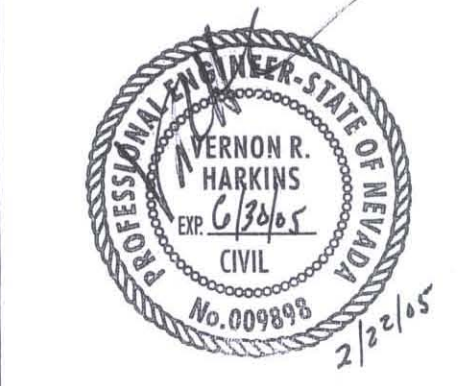


### STORM DRAIN - PROFILE VIEW

HORIZONTAL SCALE: 1" = 40', VERTICAL SCALE: 1" = 4'

WE CERTIFY THAT THIS GRADING PLAN CONFORMS  
TO THE APPROVED DRAINAGE STUDY FOR THIS  
SITE ON FILE AT THE CITY OF HENDERSON  
KIVA# 2002740088  
VERNON R. HARKINS P.E. NO. 9898 DATE

KIVA # 2004870065





- STORM DRAIN CONSTRUCTION NOTES**
- 9 INSTALL 12"x18" WYE
  - 12 INSTALL 24"x24" DROP INLET PER DETAIL "C" ON SHEET 3
  - 14 INSTALL 60"x60" CATCH BASIN PER DETAIL "U" ON SHEET 4.
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  - 18 INSTALL 60" STORM DRAIN TEE RISER PER C.C.A.U.S.D. DWG # 407.
  - 20 INSTALL CAP FOR FUTURE EXTENSION. SIZE ACCORDING TO PIPE DIAMETER.
  - 21 INSTALL 60" RCP HEADWALL PER NDOT DWG. No. R-2.5.2.
  - 22 FUTURE 60" STORM DRAIN TEE RISER BY OTHERS.

**BENCHMARK**

CITY OF HENDERSON BENCHMARK # 5  
DESCRIPTION: BOLT AND WASHER IN THE  
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ELEVATION IN FEET = 1702.82 (NAVD '88)  
ELEVATION IN METERS = 519.021 (NAV '88)

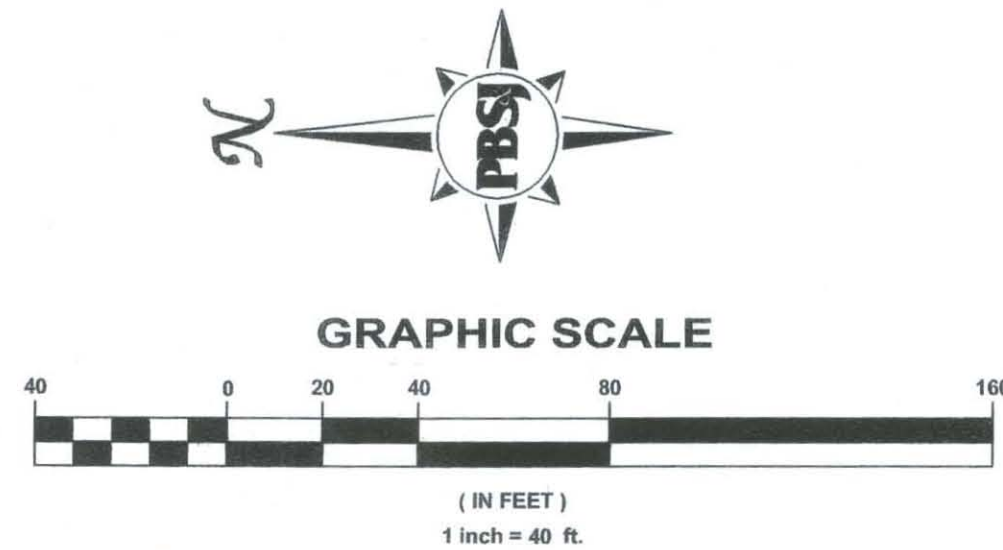
**BASIS OF BEARINGS**

NORTH 89°58'43" EAST - BEING THE NORTH LINE OF  
THE  
NORTHEAST QUARTER (NE 1/4) OF SECTION 11,  
TOWNSHIP 22 SOUTH,  
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**APPROVAL**

NEW DEVELOPMENT ENGINEER, CITY OF HENDERSON - KEN Y. KOSHIRO, P.E. DATE \_\_\_\_\_

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CITY OF HENDERSON, IF WORK IS NOT COMPLETED BY \_\_\_\_\_ 20\_\_\_\_

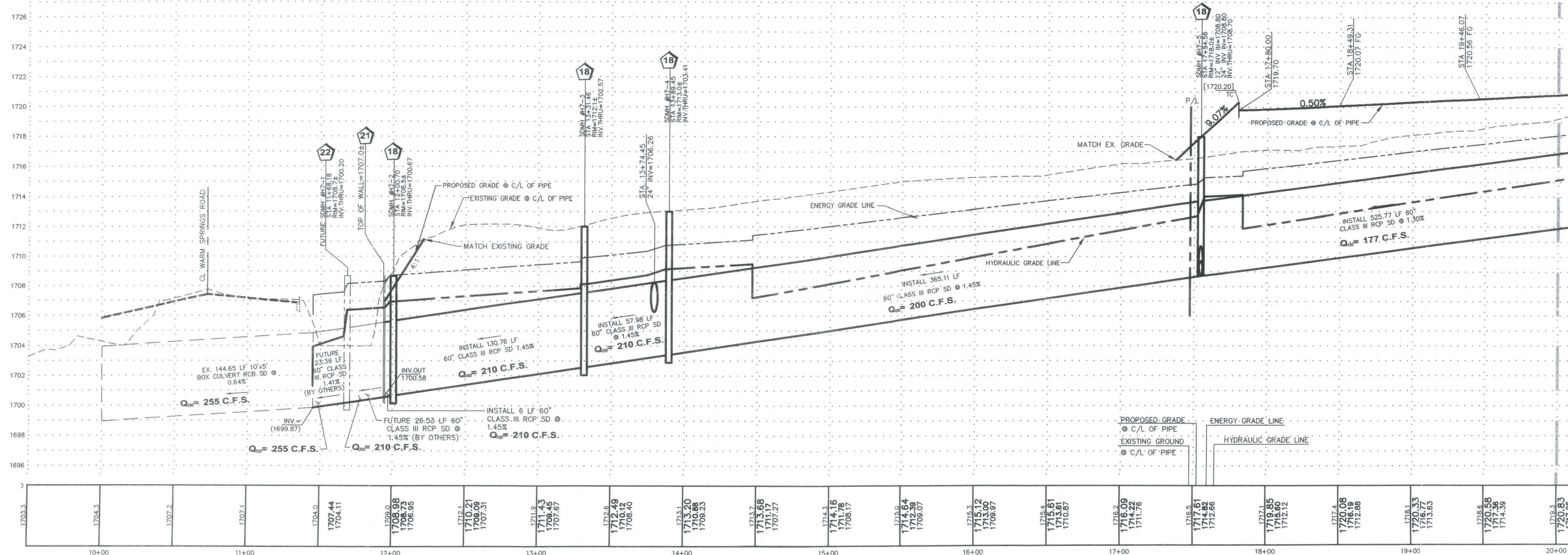


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SAFETY SERVICES DEPARTMENT

**Call before you UNDERGROUND**  
1-702-455-7511  
LAS VEGAS AREA UNIDENTIFIED SERVICE PROVIDERS

SEE SHEET 13 FOR STORM DRAIN CONTINUATION



SEE SHEET 13 FOR STORM DRAIN CONTINUATION

WE CERTIFY THAT THIS GRADING PLAN  
CONFORMS TO THE APPROVED DRAINAGE STUDY  
FOR THIS SITE ON FILE AT THE CITY OF  
HENDERSON  
KIVA# 2002740088

VERNON R. HARKINS P.E. NO. 9898 DATE \_\_\_\_\_

**KIVA # 2004870065**

VERNON R. HARKINS  
P.E. 3045  
CIVIL  
No. 009898  
2/22/05



Please refer to Volume II for Appendix E and Appendix F.



## **Appendix E: Grading Plans**

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## **Appendix F: Electronic CD**