# TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL

Volume I of II

### Prepared for:

Basic Remediation Company 875 W. Warm Springs Road Henderson, NV 89015

Prepared by:



2270 Corporate Circle, Suite 100 Henderson, Nevada 89074-6382 Phone: (702)-263-7275

October 6, 2006 PBS&J Reference No.: 511693.19

| Date Submitted |  |
|----------------|--|
| PIN #          |  |



# CLARK COUNTY DEPARTMENT OF DEVELOPMENT SERVICES CIVIL ENGINEERING DIVISION

### DRAINAGE STUDY SUBMITTAL SHEET

(Each Drainage Study must have a separate submittal sheet and separate check)

| Is this project located within a Major Project?   Yes   No If yes, which Major Project is it? |                     |                          |                          |
|---|---------------------|--------------------------|--------------------------|
| <b>Assessor's Parcel Number (APN) 1.</b> 178-11-501-006 <b>2.</b>                             | 178-12-201-002      | <b>3.</b> 178-12         | 2-301-001                |
| This project is within the city limits of:  Hend  | erson               | ☐ North Las Vegas ☐ Othe | er Clark County          |
| Type of Submittal   | review O            | ver 2 study reviews      |                          |
| Number of Acres up to 5 acres up to 40 acres  | ☑ up to 320 acres   | up to 2,560 acres over   | er 2,560 acres           |
| Project Name  | r Eastside Landfill |                          |                          |
| Street Location East/West Eastgate Rd/ 4 <sup>th</sup> Street                                 |                     | North/South Warm Springs | s Rd/ Lake Mead Dr       |
| Land Use Applications  1. Landfill  | 2                   | 3.                       |                          |
| 4   | 5                   | 6.                       |                          |
| Engineering Firm PBS&J  |                     | Responsible Engineer     | Harshal Desai, P.E., CFM |
| Address 2270 Corporate Circle, Suite 100  |                     |                          |                          |
| City/State/Zip Henderson, NV 89074  |                     | Phone Number             | (702) 263-7275           |
| Owner/Developer Basic Remediation Comp  | any                 |                          |                          |
| Address 875 West Warm Springs Rd  |                     |                          |                          |
| City/State/Zip Henderson, NV 89015  |                     | Phone Number             | (702) 567-0400           |

#### HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

## **DRAINAGE STUDY INFORMATION FORM**

| Name  | e of Development: Eastsi   | de Landfill                                    |                              |             |                        |           | Date:                 | 6th Oct 06        |      |
|-------|--|--|------------------------------|-------------|------------------------|-----------|-----------------------|-------------------|------|
| Locat | ion of Douglanments  | a) Descript                                    | ive (Crean Streets)          | -           | atmata Dd/ Marw        | Carlas    | - D4                  |                   |      |
| Local | ion of Development:  | <ul><li>a) Descript</li><li>b) Sect.</li></ul> | ive (Cross Streets)<br>11/12 | Twn.        | stgate Rd/ Warn<br>22S | Rng.      | 62E                   |                   |      |
| N1    |  |  |                              |             |                        |           | 178-11-501-006, 178-1 | 1-201-002         |      |
| Name  | e of Owner: Basic Remedia  | ation Company                                  |                              |             | Assessors Parc         | el No:    | and 178-12-301-001    |                   |      |
| Telep | hone No: (702) 567-0473  |  |                              |             | Facsimile No:          |           |                       |                   |      |
| Addre | ess: 875 West Warm Spring  | ne Rd  |                              |             |                        |           |                       |                   |      |
| Addit | oro weat warm opinio   | go riu   |                              |             |                        |           |                       |                   |      |
|       | Henderson, NV 89015  |  |                              |             |                        |           |                       |                   |      |
| Conta | act Person Name: Harsh   | al Desai, P.E., CFI                            | А                            |             | Telepho                | one No:   | (702) 263-7275        |                   |      |
| Come  | or croon name.   | ui 200ui, 1 .E., 01 i                          |                              |             | Tolopin                | 0110 140. | (102) 200 1210        |                   |      |
| F     | irm: PBS&J   |  |                              |             |                        |           |                       |                   |      |
| Addre | ess: 2270 Corporate Ci   | rcle, Suite 100, He                            | enderson, Nevada 8           | 9074        |                        |           |                       |                   |      |
| Type  | of Land Development/Land Dis   | turbance Process:                              |                              |             |                        |           |                       |                   |      |
| 7,5   | Rezoning   | Subdivis                                       | ion Map                      |             |                        | Clearing  | g and Grading Only    | v                 |      |
|       | Parcel Map   |  | Unit Development             |             | X                      |           | Please specify belo   |                   |      |
|       | Large Parcel Map   | Building                                       | Permit                       |             |                        | CCRFC     | D Facility            |                   |      |
| 1.    | Total Owned Land Area: At  | Site:  | 113 +/- acres                |             | Being Deve             | loped/Dis | sturbed:              | 74 +/- acres      |      |
|       |  |  |                              |             |                        |           |                       |                   |      |
| 2.    | Is a portion or all of the subj  | ect property located                           | d in a designated FE         | MA Flood    | Hazard Area?           |           | YES                   | NO                |      |
| 3.    | Is the property bordered or o  |  |                              | k County    |                        |           |                       |                   |      |
|       | Regional Flood Control Distr   | rict Master Planned                            | Facility?                    |             |                        |           | YES                   | NO                |      |
| 4.    | Proposed type of developme   | ent (Besidential, Co                           | ommercial, Etc.)?            |             | Landfill               |           |                       |                   |      |
|       |  |  |                              |             |                        |           |                       |                   |      |
| 5.    | Approximate upstream land  | area which drains                              | to the subject site?         |             | 80 +/-acres            |           |                       |                   |      |
| 6.    | Has the site drainage been   | evaluated in the pa                            | st?                          | YES*        | NO                     |           | If yes, please ider   | ntify documentati | on:  |
|       | Henderson Commerce Cer   | nter Two (Formerl                              | y known as Harsch            | )           |                        |           |                       |                   |      |
|       |  |  |                              |             |                        |           |                       |                   |      |
| 7.    | If known, please briefly iden  | tify the proposed di                           | scharge point(s) of re       | unoff from  | the site:              |           |                       |                   |      |
|       | Into existing 60" storm dra  | in located on adj                              | acent property and           | to the und  | developed land t       | to the no | orth                  |                   |      |
|       |  |  |                              |             |                        |           |                       |                   |      |
| 8.    | Briefly describe your propos   | ed schedule for the                            | subject project:             | AS          | AP                     |           |                       |                   |      |
|       | - ren  |  |                              |             |                        |           |                       |                   |      |
|       | GINEFO   | Sub  | mit this form as part        | of the requ | ired drainage stu      | dy to the |                       |                   |      |
| 3     | N. V. Coccoccoccia   |  | l entity which has jur       |             |                        | 3         |                       |                   |      |
| SSION | HARSHAL B.   |  | form may provide su          |             | ormation to serve      | as the    |                       |                   |      |
| 80    | DESAI SO   | Con  | ceptual Drainage Stu         | udy.        |                        |           |                       |                   |      |
| 888   | Exp. 12,31-08  | * D  | eview and concurren          | ce of the   | Clark County Roa       | ional     |                       |                   |      |
| 14    | 8 m  | 7  | ood Control District i       |             |                        | onai      |                       |                   |      |
| WC    | The state of the s |  |                              |             |                        |           |                       | Revision          | Date |
| 10    | No. 17468  |  |                              |             |                        |           |                       |                   |      |
|       | 17400-00   | 5-06   |                              |             |                        |           |                       |                   |      |
|       | Engineer's Seal  |  | Local                        | Entity File | No.                    |           |                       |                   |      |
|       | Engineer 3 Ocar  |  |                              |             |                        |           |                       |                   |      |

STANDARD FORM 1

PBS&J Job Number:

511693.19

## HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

| DRAINAGE SUBMITTAL CHECKLIST   |   |  |   |  |
|--|---|--|---|--|
| Project Name: I  | Eastside Landfill   | Map ID:  |   |  |
|  | PBS&J   | Engineer: Harshal Desai, P.E.  | ., CFM  |  |
|  | 270 Corporate Circle, Suite 100   |  |   |  |
| City: F  | Henderson   | State: NV  | Zip: 89074  |  |
| Phone Number:  | (702) 263-7275  | Fax Number: (702) 263-720  | 00  |  |
| Property Owner:  | Basin Remediation Company   |  |   |  |
| Address:   | 875 Warm Springs Rd   |  |   |  |
|  |   |  |   |  |
| City:  | Henderson   | State: NV  | Zip: 89015  |  |
| Reviewed By:   |   | Date Received:   | Date Accepted for Review:   |  |
|  |   |  |   |  |
| information re Technical Dra District (CCR  This document for compliance extent of the i use.  If items are not approximately ap | equired prior to the entity performinage Study is prepared within the FCD) Hydrologic Criteria and Extra tis intended as an aid in preparity with local and regional criteria | ming a review. The engineer will he guidelines as set forth in the Orainage Design Manual (MANU) and Technical Drainage Studies.  This form is not intended to be botts which may be necessary to provide the second of the second | y). The listed items are the minim ll remain responsible to ensure the Clark County Regional Flood Con JAL).  Each study submitted is reviewed e all inclusive and does not limit t properly evaluate the intended lane |  |
| Yes No   | Design Manual Standard Fo   | rm 1 with the engineer's seal and  | d signature.  |  |
| X  | Design Manual Standard Fo   | rm 4.  |   |  |
| X  | 2 copies of the 24" x 36" Dra   | inage Plan.  |   |  |
| N/A  | A notarized letter from the ad  | jacent property owner(s) allowing  | ng off-site grading or discharge.   |  |
| DEFEDEN  | CE.   |  | STANDADD FORM 2   |  |
| REFEREN  | LE:   |  | STANDARD FORM 2   |  |

# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL DRAINAGE SUBMITTAL CHECKLIST

| II. MA   | PS AND | EXHIBITS   |  |
|----------|--------|--|--|
| Yes<br>X | No     | A copy of a current Flood Insurance Rate Map (FIRM) with the site delineated.  |  |
| <u>X</u> |        | A copy of the current CCRFCD Master Plan Update Figure, (F-22), for Flood Control Facilities and Environmental areas with the site delineated.                                   |  |
| X        | _      | Off-site drainage basin maps for existing, interim and future conditions showing the existing topography, basin boundaries, concentration points, and flows in cfs.              |  |
| <u>X</u> | _      | On-site drainage basin maps for existing and proposed conditions showing the existing topography, basin boundaries, concentration points, and on-site and off-site flows in cfs. |  |
| X        |        | Vicinity Map with local and major cross streets identified and a north arrow.  |  |
| III. DR  | AINAG  | E PLAN   |  |
| Yes      | No     |  |  |
| X        |        | Sheet size: 24" x 36" sealed by a registered engineer in the State of Nevada.  |  |
| X        |        | Minimum scale: $1'' = 60'$ .   |  |
| X        |        | Project name.  |  |
| X        |        | Vicinity Map with local and major cross streets.   |  |
| X        |        | Revision box.  |  |
| X        |        | North arrow and bar scale.   |  |
| X        |        | Engineer's/consultant's address and phone number.  |  |
| X        |        | Elevation datum and benchmark.   |  |
| X        |        | Legend for symbols and abbreviations.  |  |
| X        |        | Cut/fill scarps, where applicable.   |  |
| X        |        | Street names, grades, widths.  |  |
| X        | _      | Proposed future and existing spot grades for top of curbs and street crowns at lot lines, grade breaks, and along curb returns on both sides of the street.                      |  |
|          |        |  |  |
| REI      | FERENC | CE: STANDARD FORM 2  |  |

# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL DRAINAGE SUBMITTAL CHECKLIST

| DRAINA                       | AGE SUBMITTAL CHECKLIST |
|------------------------------|-------------------------|
| III. DRAINAGE PLAN (Continue | ed)                     |
|                              |                         |

| Yes No | Existing contours encompassing the site and 100 feet beyond with spot elevations for important locations, where appropriate.   |  |  |  |
|--------|--|--|--|--|
| NA     | Minimum finish floor elevations with top-of-curb elevations at upstream end of lot.  |  |  |  |
| X      | Proposed typical street sections.  |  |  |  |
| NA     | Streets with off-set crowns.   |  |  |  |
| X      | Proposed contours or spot elevations in sufficient detail to exhibit intended drainage patterns and slopes   |  |  |  |
| X      | Property lines.  |  |  |  |
| X      | Right-of-way lines and widths, existing and proposed.  |  |  |  |
| X      | Existing improvements and their elevations.  |  |  |  |
| X      | Delineation of proposed on-site drainage basins indicating area and 10-year ad 100-year storm peak flows at basin concentration points.  |  |  |  |
| NA     | Concentration points and drainage flow direction with $Q_{100}$ and $V_{100}$ and $D_{100}$ in streets.  |  |  |  |
| X      | Cumulative flows, velocity, and drainage of flow at upstream and downstream ends of site for the 10-year and 100-year flows.   |  |  |  |
| X      | Location and cross-section of street capacity calculations.  |  |  |  |
| X      | Cross-sectional detail for channels, including cutoff wall locations.  |  |  |  |
| X      | Existing and proposed drainage facilities, appurtenances, and connections, (i.e., Sidewalk, ditches, swales, storm drain systems, unimproved and improved channels, and culverts, etc.) stating size, material, shape, and slope with plan and profile and HGL calculations. |  |  |  |
| NA     | Existing and proposed drainage easements and widths shown with sufficient detail. A cross sectional detail must be provided that shows appropriate lining and reinforcement.   |  |  |  |
| NA     | Location and detail of existing, proposed, and future block wall openings. Minimum size is 16" x 48". Wrought iron gate is required for flows > 10 cfs.  |  |  |  |
| X      | Location and detail of flood walls illustrating depth of flow, proposed grouting height, etc.  |  |  |  |

# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL DRAINAGE SUBMITTAL CHECKLIST

| III. DRAINAG | GE PLAN (Continued)  |                                 |
|--------------|--|---------------------------------|
| Yes No NA    | Perimeter retaining wall locations. All existing and proposed flood) must be shown with adjacent ground elevations. Flood masonry unit.              |                                 |
| N/A          | Building and/or lot numbers.   |                                 |
| NA           | Alignment of all existing, proposed, or future Regional Faciliti   | es adjacent to the site.        |
| X            | Limits of existing floodplain based on current FIRM or best available information.   | vailable information; limits of |
| X            | For areas in Zone A, AE, AH and AO, base flood elevations(B lot; BFEs may be listed on each lot, or in a table. Finish floor of 18 inches above BFE. |                                 |
| N/A          | Appropriately elevated "humps" 6 inches above the 100 year vaccesses where the intent is to protect the site from the $Q_{100}$ flo                  |                                 |
| N/A          | Street slopes perimeter and interior streets. The minimum slop   | pe is 0.4 percent.              |
| Yes No       | OGIC ANALYSIS  Appropriate soil information and Soils Map for existing and fur and property delineated.  | ture conditions with subbasins  |
| X            | Input and output information for existing conditions from com-<br>TR-55). The flow routing diagram must be provided with HEG                         |                                 |
| X            | Input and output information for future conditions from compuTR-55). The flow routing diagram must be provided with HEC                              |                                 |
| X            | Use of correct precipitation values in and around the McCarran   | n Airport rainfall area.        |
| X            | A discussion in the text of the hydrologic analysis justifying su<br>supporting assumptions, and calculations.                                       | bbasin boundaries and cutoffs,  |
| X            | A summary table of stormwater flows showing basin area, $Q_{10}$ basins and combined basin flows, where applicable.                                  | and 100 for both individual     |
| <u>X</u>     | Copies of supporting technical information referenced from a pastatement accepting these results.  | previously approved study and   |
| X            | On-site facilities must perpetuate flows through or around the simpacting adjacent property owners in accordance with current                        |                                 |
| REFEREN      | CE:  | STANDARD FORM 2                 |

# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL DRAINAGE SUBMITTAL CHECKLIST

| V. HYDI   | RAULIC ANALYSIS  |  |
|-----------|--|--|
| Yes<br>NA | No  Flow split calculations and supporting documentation or refere split calculations used.  | ence for the method of flow  |
| NA _      | Normal depth street flow calculations and cross section diagraperimeter streets. Provide "d x v" products for the $Q_{100}$ and $Q_{100}$ case for interior and all perimeter streets. $Q_{100}$ d x $v \le 8$ . $Q_{100}$ for rights-of-way $\ge 80$ feet. Calculations must be labeled by s the Grading Plan.                                      | $t_{10}$ flows representing the worst $t_{10}$ d x v $\leq$ 6 and 12 foot dry lane |
| NA        | A summary table of interior and exterior street capacity calcul $Q_{100}$ flow, slope, depth of flow, velocity and depth times velocity meet 12 foot dry lane criteria.  |  |
| <u>NA</u> | Appropriate hydraulic calculations for block wall openings ass<br>clogging factor. (Assume the lower half of the opening is plug   |  |
| NA        | Appropriate hydraulic calculations at drainage easement entra<br>set finish floor elevations. Hydraulic calculations must includ<br>superelevation and tee intersection losses, where appropriate.   |  |
| NA        | Provide necessary freeboard requirements to set the finish flood buildings, 2 x depth of flow or depth of flow plus 18 inches of The minimum requirement is 6 inches above adjacent upstrear adjacent to drainage easements must always be provided with the Q <sub>100</sub> weir height of flow depth, which ever is greater.                      | freeboard, whichever is less.<br>n top of curb. Buildings                          |
| NA        | A complete water surface profile analysis (HEC-2, HEC-RAS FEMA Zone A flood zones.   | , etc.) for channel flows and  |
|           | <ul> <li>→ Field survey data.</li> <li>→ Input and output information.</li> <li>→ Plotted cross-sections based on survey with proper encroaded A map showing the location of the cross-sections.</li> <li>→ Analysis of both sub and super-critical flow segments.</li> <li>→ A summary table and a discussion of the results in the text</li> </ul> |  |
| NA _      | Provide a 50 percent clogging factor in the capacity calculation   | ns for drop inlets.  |
| X         | Hydraulic calculations for culverts and storm drains. D-Load for storm drain pipes in public rights-of-way, including headw  |  |
| <u>X</u>  | The mitigation of nuisance water, both during construction and condition, must be addressed.   | d in the fully developed   |
| REFE      | ERENCE:  | STANDARD FORM 2  |



October 6, 2006

Dave Betley, P.E. Clark County Development Services 500 S. Grand Central Parkway PO Box 551842 Las Vegas, NV 89155-1842

RE: TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL PBS&J PROJECT NO.: 511693.19

Dear Mr. Betley:

Submitted for your review and approval are two copies of the *Technical Drainage Study* for Eastside Landfill.

If you have any questions regarding this study, please contact our office at (702) 263-7275.

Sincerely,

PBS&J

Krystle Pemberton, E.I

Kuyst Par let

Hydrologist

Harshal Desai, P.E., CFM Project Manager

0-06-06



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**Appendix C: Hydraulic Calculations** 

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### I. Introduction and Purpose

This report is intended to serve as the Technical Drainage Study (TDS) for Eastside Landfill. The purpose of this study is to establish a technical analysis of peak flow rates affecting the site under existing, interim and developed conditions. It includes an analysis of onsite and offsite drainage patterns and flow rates for use in the design of flood protection facilities. The study shows that the flood protection facilities designed within this study will improve/perpetuate existing drainage patterns.

This study was conducted in accordance with the criteria set forth by Clark County Regional Flood Control District (CCRFCD) *Hydrologic Criteria and Drainage Design Manual* (Criteria Manual), prepared by WRC Engineering and updated by Montgomery Watson, August 1999.

#### **II. General Information**

#### A. Location and Description

The Eastside Landfill property is located within Sections 11 and 12, Township 22 South, Range 62 East of Clark County, Nevada. The Assessor's Parcel Numbers for the subject site are 178-11-501-006, 178-12-201-002, and 178-12-301-001. The proposed development is located south of Warm Springs Road, west of 4<sup>th</sup> Street and north of the Union Pacific Railroad (UPRR).

The proposed site is bordered to the north by undeveloped land and to the south by Pioneer America LLC (north of the Union Pacific Railroad). American Potash & Chemical Corporation is located east of the project site and undeveloped land is west of the project site. Henderson Commerce Center II (formerly known as Harsch Development) is northwest of the site. Please refer to **Figure 1: Area/Vicinity Map** in **Appendix A**.

The project site area is approximately 113 (+/-) acres. The project entails the construction of a landfill with a total volume of approximately 2.6 million cubic yards of fill. The top of the proposed landfill will be approximately 40 feet above existing grade to reach the desired volume. Channels are proposed around the perimeter of the landfill to collect / convey the offsite and onsite flows. These proposed channels will serve as drainage facilities as wells as access roads for the maintenance of the landfill. The west channel (Channel C-1) drains into a proposed detention basin, with a volume of 16+/-ac-ft, located in the northwest corner of the project site. The purpose of this detention basin is to provide necessary storage to perpetuate the design outflow of the existing 60" storm drain constructed with the Harsch Development. The east channel (Channel C-2) drains into an equalizer basin located just northeast of the proposed landfill. This equalizer basin was designed to split the flow north to perpetuate the existing drainage conditions and west through a proposed storm drain that drains into the detention basin. The top of the landfill was graded such that the runoff would reach the two proposed



embankment channels, one draining into equalizer basin and the other draining into the detention basin. The conceptual layout of the proposed drainage facilities discussed above is shown in the exhibit below. The hydraulic calculations associated with the above mentioned facilities are further discussed in **Section III-D**. The improvement plans for the proposed facilities are provided in **Appendix E**.

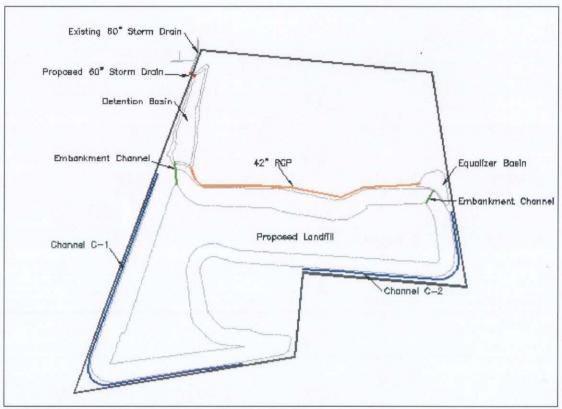


Exhibit 1: Conceptual Layout of Proposed Drainage Facility

#### **B. CCRFCD Master Plan Information**

**Figure 2: CCRFCD Flood Control Facilities Map** (in **Appendix A**) shows the subject property in relation to CCRFCD Master Planned facilities. The exhibits were reproduced from the 2002 CCRFCD Master Plan Update (MPU) of the Las Vegas Valley. The figure shows that the nearest regional facility, Pioneer Detention Basin (PTVW 0185), is located southwest of the proposed site. The detention basin's associated drainage system located west of the site carries the flow north past Warm Springs Road. The drainage from this development will not contribute flow through this facility.

The majority of flow from the project site is conveyed through the existing 60" storm drain which ultimately drains into the existing 10'x5' Reinforced Concrete Box (RCB) located under Warm Springs Road.



#### C. FEMA Floodplain Information

**Figure 3: FEMA Map** (in **Appendix A**) is a reproduction of the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map for Clark County, Nevada, Community-Panel Numbers 32003C2595E dated September 27, 2002. **Figure 3** shows that the project site is within a non-shaded Zone X. Zone X is defined by FEMA as areas determined to be outside the 500-year floodplain.

#### D. Hydrologic Procedures Used

HEC-1 Flood Hydrograph Package, Version 4.1, developed by the U.S. Army Corps of Engineers Hydrologic Engineering Center, was used to develop runoff data for this study. This is in accordance with the CCRFCD Criteria Manual. The methodology and calculations used to determine the hydrologic parameters are located in **Appendix B-4**. The hydrologic analysis is discussed in further detail under **Section III** of this TDS. HEC-1 runoff models for existing, interim and developed conditions are included in **Appendix B-1**, **B-2** and **B-3** respectively.

#### E. Hydraulic Procedures Used

Various hydraulic procedures were used for the analysis and design of different drainage facilities. The procedures used were in accordance with the CCRFCD Criteria Manual.

HEC-RAS, version 3.1.2, was used to model the two channels (Channel C-1 and Channel C-2) bordering the east and west side of the proposed landfill. Please refer to the conceptual layout above for the location of the two channels

WSPG model was used to model the proposed and existing storm drains.

FlowMaster was used for normal depth calculations to estimate the velocity and water depth for other minor channels, top of the landfill and embankment channels.

The hydraulic procedures and associated analyses are discussed in further detail under the hydraulic section (**Section III-D**) of this TDS.

### F. Previous Studies in Project Vicinity

The following studies were reviewed in the preparation of this study. Reference material from each of these studies is included in Appendix D.

1. Addendum #1 to the Technical Drainage Study for Henderson Commerce Center II (Formerly known as Harsch). Prepared by PBS&J., February 2003.

This reference study performed a hydrologic analysis for the area located west of the proposed site. Offsite basin, OFFD1, from the 2003 referenced TDS is a combination of onsite and offsite basins, ONEX1 and OFFEX1, of this TDS. The hydrologic drainage



patterns derived from the referenced TDS contributed to the design of the existing 60" storm drain located along the east side of the Harsch Development. An inlet is located just southeast of Harsch Development (combination point C18), where 100-year flow of 120 cfs was determined to be collected. At combination point C18B 100-year flow of 127 cfs was calculated to be in the existing 60" storm drain. Please refer to **Appendix D** for the reference material.

# 2. Update to the Technical Drainage Study for Henderson Commerce Center (Formerly known as Harsch). Prepared by PBS&J., February 2005.

This reference study is an update to the previous study and had only minor changes to the storm drain design that runs along the east boundary of the Harsch Development, but does not change the overall hydrology of the site. Refer to **Appendix D** for the latest storm drain alignment and WSPG model.

## III. Hydrology / Hydraulics

#### A. Existing Condition Hydrology

The 113 (+/-) acre site presently has two existing landfills and the rest of the site is undeveloped. The locations of the existing landfills are delineated on **Figure 4: Existing Condition Drainage Map** included in Appendix B-1. The existing landfills and the undeveloped land are hydrologically characterized as industrial and natural desert landscape respectively.

The onsite subbasins for the existing condition hydrology were delineated using 1 foot aerial topography and field reconnaissance. The onsite subbasins are labeled as ONEX1 through ONEX5. The existing condition hydrology used the offsite hydrology from the above mentioned reference study in **Section II-F**. In addition to the referenced offsite subbasins, PBS&J delineated offsite subbasins (OFFEX1 through OFFEX5) north of the UPRR that contribute flow to the proposed property. The area of the existing chemical ponds located within these offsite basins was deducted from the total area of the basins because these ponds will contain the precipitation and will not contribute to the runoff to the proposed site. **Figure 4** located in **Appendix B-1** shows the onsite and offsite basins for the project site under existing condition. The flow leaving the site is identified on the figures as a combination point or a discharge point.

The offsite basins OFFEX1 and OFFEX2 routes through the project site combining with ONEX1 at Combination point CP-1, with a 10-year and 100-year flow of 33 cfs and 105 cfs respectively. This flow is conveyed to an existing inlet (Combination Point C18) via an existing channel where it combines with the flow from the referenced basins west of the property boundary. The referenced basins are clearly identified on **Figure-4.** The 10-year and 100-year flow at C18 is 57 cfs and 162 cfs respectively. The flow captured by the inlet is conveyed through the existing 60" storm drain which ultimately discharges into the existing 10'x5' RCB under Warm Springs Road.



Subbasin ONEX2 flows northwest to combine with referenced basins HR1 through HR3 and C18 at combination point C18B. The 10-year and 100-year flow at this combination point was determined to be 78 cfs and 212 cfs respectively. Onsite subbasin ONEX3 discharges directly north into existing washes. The 10-year and 100-year flow at that discharge point is 27 cfs and 59 cfs respectively.

The offsite subbasin OFFEX5 flows north through an existing channels within ONEX4 to combine with ONEX4 at combination point CP-3. Combination point CP-3 outlets 10-year and 100-year flows of 27 and 65 cfs respectively into an existing channel north of the property boundary.

Flow produced by offsite subbasin OFFEX4 will be diverted east by an existing culvert under Fourth Street. The flow will reach the culvert through an existing riprap channel or by an existing graded swale along the northern border of this offsite basin. Therefore, the flow from this basin will not impact the project site. The picture below shows the riprap channel and the culvert under Fourth Street.



Exhibit 2: Picture of the riprap channel and the culvert under Fourth Street (looking west)

The offsite subbasin OFFEX3 has a shallow ponding area where the runoff is contained, preventing the flow from continuing north and impacting the project site. This low area also captures flow produced by onsite subbasin ONEX5. These two basins were combined at combination point CP-2. The existing shallow ponding area within OFFEX3 was modeled in the existing drainage condition HEC-1 model using a stage-



storage discharge curve. The volume of the shallow area was determined by using 1' aerial topography. A negligible outflow was used to run the model. The existing condition HEC-1 model determined a water surface elevation (WSE) of 1768.34 feet produced by the runoff generated by these two subbasins. This shallow ponding area has containment up to an elevation of 1770 feet, therefore this flow was not assumed to continue north. Below is the summary of the information used in the stage-storage discharge curve.

Table 1: Summary Table for OFFEX3 Shallow Ponding Area Stage-Storage Discharge Curve

| ELEVATION | AREA<br>(ft2) | VOLUME<br>(ft3) | VOLUME (ac-<br>ft) | CUMULATIVE VOLUME (ac-ft) | OUTFLOW<br>(cfs) |
|-----------|---------------|-----------------|--------------------|---------------------------|------------------|
| 1766      | 10475         | 0               | 0.00               | 0.00                      | 0                |
| 1767      | 30499         | 20487           | 0.47               | 0.47                      | 0.01             |
| 1768      | 47931         | 39215           | 0.90               | 1.37                      | 0.02             |
| 1769      | 68570         | 58250.5         | 1.34               | 2.71                      | 0.03             |
| 1770      | 89398         | 78984           | 1.81               | 4.52                      | 0.04             |

The discussion on the development of the hydrologic parameters is included in **Appendix B-4**. The existing condition HEC-1 model is included in **Appendix B-1**. **Table 2** below shows the summary of the flows in existing condition.

Table 2: Summary Table for Existing Condition

| BASIN ID | AREA (ac) | Q <sub>100</sub> (cfs) | Q <sub>10</sub> (cfs) |
|----------|-----------|------------------------|-----------------------|
| ONEX1    | 32.76     | 47                     | 17                    |
| ONEX2    | 28.77     | 49                     | 21                    |
| ONEX3    | 22.12     | 59                     | 29                    |
| ONEX4    | 28.27     | 56                     | 25                    |
| ONEX5    | 1.06      | 3                      | 2                     |
| OFFEX1   | 42.20     | 48                     | 14                    |
| OFFEX2   | 9.63      | 13                     | 4                     |
| OFFEX3   | 16.40     | 21                     | 8                     |
| OFFEX4   | 7.61      | 14                     | 6                     |
| OFFEX5   | 5.11      | 10                     | 4                     |
| CP-1     | NA        | 105                    | 33                    |
| CP-2     | NA        | 23                     | 8                     |
| CP-3     | NA        | 65                     | 27                    |
| C18      | NA        | 162                    | 57                    |
| C18B     | NA        | 212                    | 78                    |

#### B. Interim Condition Hydrology

The interim condition hydrology is analyzed assuming that the onsite basins are developed and the offsite basins have existing condition hydrologic parameters.

The onsite subbasins for the interim drainage condition hydrology were developed using the improvement plans included in **Appendix E**. The onsite subbasins are labeled as OND1 through OND15. **Figure 5: Interim Condition Drainage Map** shows the onsite and offsite basins for the project site under interim drainage condition. This figure is included in **Appendix B-2**.



As previously mentioned, two main channels were designed around the perimeter of the proposed landfill. Channel C-1 collects runoff produced by the west side of the landfill (from onsite basins OND1 through 3 and OND7) and offsite flow (from offsite basins OFFEX1 and OFFEX2) and eventually discharges into the proposed detention basin. The combination point CP-4 represents the total flow collected by Channel C-1. The 10-year and 100-year flow at CP-4 is 26 cfs and 79 cfs respectively.

Subbasin OND8 produces a flow of 16 cfs / 33 cfs (10-year / 100-year) which is conveyed through a graded channel along the perimeter of the proposed landfill. The channel starts at the southern boundary of OND8 and is graded to convey the flow to Channel C-2.

Channel C-2 collects flow from the east side of the landfill (from onsite basins OND8, OND10 and OND12) and offsite flow (from offsite basin OFFEX5). The combination point CP-10A represents the total flow collected by Channel C-2. The 10-year and 100-year flow at CP-4 is 25 cfs and 55 cfs respectively. Channel C-2 discharges into the proposed equalizer basin.

As discussed above, the top of the landfill has been graded to have positive drainage and to convey the flow to the two embankment channels located on either side of the proposed landfill. The top of the landfill was divided into three subbasins: OND4, OND5 and OND11. Subbasins OND4 and OND5 drains to the embankment channel located on west side of the proposed landfill (CP-5) whereas OND11 drains to the embankment channel located on east side of the proposed landfill. The west embankment channel conveys the flow of 19 cfs / 40 cfs (10-year / 100-year) from CP-5 to the proposed detention basin. The east embankment channel conveys the flow of 12 cfs / 24 cfs (10-year / 100-year) from OND11 to the proposed equalizer basin.

Subbasin OND6 has a proposed graded channel proposed along the perimeter of the landfill directing the flow into the detention basin. This subbasin will produce 10-year/100-year flow of 11/23 cfs. Subbasin OND13 also has a proposed graded channel along the perimeter of the landfill proposed directing the 10-year and 100-year flow of 6 cfs and 12 cfs respectively into the equalizer basin.

The purposed of the equalizer basin proposed at the northeast corner of the proposed landfill is to split the flow north and west. The peak flow (10-year/ 100-year) reaching the equalizer basin in interim drainage condition is 42 cfs / 90 cfs (10-year / 100-year) represented by combination point CP-10. This is the combined flow from CP-10A, OND11 and OND13. An elliptical pipe (53"x 34"), equivalent to a 42" RCP, is proposed as the outlet structure for this basin. A 30' spillway is proposed at an elevation of 1747.75 feet on the north side of the basin. The equalizer basin was modeled in HEC-1 using a stage storage discharge curve. The outflow through the 42" elliptical pipe was determined using the inlet control nomograph provided in the CCRFCD manual and flow overtopping the spillway was calculated using the weir equation. The WSE in interim drainage condition in the equalizer basin is 1747.53 feet, preventing any flow



from overtopping the spillway and continuing north. Below is a table containing the flows and areas calculated by the above mentioned procedure. Please refer to **Appendix B-3** for sample calculations of the flow used in the stage-storage discharge curve for the equalizer basin.

Table 3: Summary Table for Equalizer Basin Stage-Storage Discharge Curve

| ELEVATION | AREA<br>(ft2) | AREA<br>(ac-ft) | 42" ELLIPTICAL PIPE<br>FLOW (cfs) | SPILLWAY<br>OVERFLOW (cfs) | TOTAL<br>DISCHARGE(cfs) |
|-----------|---------------|-----------------|-----------------------------------|----------------------------|-------------------------|
| 1744.50   | 0             | 0.00            | 0                                 | 0                          | 0                       |
| 1745.00   | 3480          | 0.08            | 0                                 | 0                          | 0                       |
| 1746.00   | 30510         | 0.70            | 18                                | 0                          | 18                      |
| 1747.00   | 34005         | 0.78            | 42                                | 0                          | 42                      |
| 1747.75   | 36890         | 0.85            | 59                                | 0                          | 59                      |
| 1748.00   | 37850         | 0.87            | 64                                | 10                         | 74                      |
| 1748.50   | 42210         | 0.97            | 73                                | 53                         | 126                     |

As previously mentioned, a 16+/- ac-ft detention pond is proposed at the northwest side of the property. The peak flow reaching the detention pond, represented by HEC-1 combination point CP-6, is contributed by Channel C-1, the west embankment channel, flow conveyed through the 42" RCP and subbasin OND6. The 10 year and 100 year flows reaching the detention pond are 79 cfs and 190 cfs respectively.

A 60" outlet pipe is proposed from the detention pond which ties into the existing 60" storm drain placed with the Harsch Development. A 25" restrictor plate is designed for the 60" outlet pipe to control the outflow. The peak 100-year outflow from the detention is calculated to be 41 cfs with a peak WSE of 1732.22 feet. The calculated freeboard for the detention basin in the interim condition is 2.78 feet (1735-1732.22). A stage-storage discharge curve was used to model the proposed detention basin in HEC-1. The outflow was calculated using the orifice equation. Please refer to **Appendix B-3** for sample calculations of the calculated outflows. Below is a summary table containing the information used in stage-storage discharge curve.

Table 4: Summary Table for Detention Basin Stage-Storage Discharge Curve

| ELEVATION | HEIGHT<br>(ft) | AREA<br>(ft2) | VOLUME<br>(ft3) | VOLUME<br>(acre-ft) | CUMMULATIVE VOLUME (acre/ft) | OUTFLOW<br>(ft3/s) |
|-----------|----------------|---------------|-----------------|---------------------|------------------------------|--------------------|
| 1725.25   | 0.0            | 0             | 0               | 0.00                | 0.00                         | 0                  |
| 1726.00   | 0.75           | 9360          | 3510            | 0.08                | 0.08                         | 0                  |
| 1728.00   | 2.0            | 53790         | 63150           | 1.45                | 1.53                         | 22                 |
| 1729.00   | 1.0            | 76290         | 65040           | 1.49                | 3.02                         | 27                 |
| 1730.00   | 1.0            | 82060         | 79175           | 1.82                | 4.84                         | 32                 |
| 1732.00   | 2.0            | 93665         | 175725          | 4.03                | 8.88                         | 40                 |
| 1734.00   | 2.0            | 105690        | 199355          | 4.58                | 13.45                        | 46                 |
| 1735.00   | 1.0            | 112360        | 109025          | 2.50                | 15.95                        | 49                 |

HEC-1 combination point C18 is the combination of the outflow from the detention basin and the referenced subbasins. The 10-year and 100-year flow at combination point



C18 is 62 cfs and 123 cfs. The referenced hydrology from Addendum #1 for the Harsch Development calculated a 100-year discharge of 120 cfs at this combination point. The difference in the flows computed at CP-18 is only 3 cfs (2.5%). The existing 60" storm drain is analyzed for flow greater than 120 cfs and has the capacity for the additional flow. The analysis completed will be discussed in further detail in **Section D.** 

The remaining two onsite subbasins, OND14 and OND15, discharge into existing channels to the north. The 10-year and 100-year peak flows at CP-11 are 15 cfs and 31 cfs respectively. It should be noted that the flow reaching the northeast corner of the property after the proposed improvements is lower than the existing condition peak flow (27/65 cfs) at this location.

The discussion on the development of the hydrologic parameters is included in **Appendix B-4**. The interim drainage condition HEC-1 model is included in **Appendix B-2**. **Table 2** below shows the summary of the flows in interim condition.

Table 5: Summary Table for Interim Condition

| BASIN  | AREA<br>(ac) | Q <sub>100</sub><br>(cfs) | Q <sub>10</sub><br>(cfs) |
|--------|--------------|---------------------------|--------------------------|
| OND1   | 0.94         | 3                         | 1                        |
| OND2   | 3.70         | 8                         | 4                        |
| OND3   | 1.38         | 4                         | 2                        |
| OND4   | 11.67        | 27                        | 13                       |
| OND5   | 5.03         | 12                        | 6                        |
| OND6   | 9.90         | 23                        | 11                       |
| OND7   | 5.87         | 16                        | 8                        |
| OND8   | 14.26        | 33                        | 16                       |
| OND9   | 1.06         | 3                         | 2                        |
| OND10  | 4.28         | 10                        | 5                        |
| OND11  | 9.60         | 24                        | 12                       |
| OND12  | 2.77         | 8                         | 4                        |
| OND13  | 4.70         | 12                        | 6                        |
| OND14  | 11.12        | 31                        | 15                       |
| OND15  | 21.47        | 57                        | 28                       |
| DETPD  | 5.14         | 16                        | 8                        |
| OFFEX1 | 42.20        | 48                        | 14                       |
| OFFEX2 | 9.63         | 13                        | 4                        |
| OFFEX3 | 16.40        | 21                        | 8                        |
| OFFEX4 | 7.61         | 14                        | 6                        |
| OFFEX5 | 5.11         | 10                        | 4                        |
| CP-1   | NA           | 15                        | 5                        |
| CP-2   | NA           | 68                        | 22                       |
| CP-3   | NA           | 70                        | 22                       |
| CP-4   | NA           | 79                        | 26                       |
| CP-5   | NA           | 40                        | 19                       |
| CP-6   | NA           | 190                       | 79                       |
| CP-7   | NA           | 23                        | 8                        |
| CP-9   | NA           | 51                        | 23                       |
| CP-10  | NA           | 90                        | 42                       |
| CP-10A | NA           | 55                        | 25                       |
| CP-11  | NA           | 31                        | 15                       |
| C18    | NA           | 123                       | 62                       |
| C18B   | NA           | 133                       | 67                       |



### C. Developed Condition Hydrology

The developed condition hydrology was analyzed assuming that onsite and offsite basins were developed. The developed curve numbers for the offsite basins were assumed to be industrial based on its current land use and the surrounding properties. Please refer to **Appendix B-4** for the development of the hydrologic parameters. It should be noted that developed condition produced higher runoff, and therefore was used in the design of the drainage facilities. **Figure 6 Developed Condition Drainage Map** shows the onsite and offsite basins for the project site under developed drainage condition. This figure is included in **Appendix B-3**.

The drainage patterns of the onsite and offsite basins are consistent with the drainage patterns discussed in the interim drainage condition. Only one modification was made to the drainage patterns in the developed condition hydrology. The shallow ponding area located within subbasin OFFD3 was removed from the HEC-1 model. Therefore, the flow produced by OFFD3 and OND9 will now combine with the flow in Channel C-2 at HEC-1 combination point CP-8. HEC-1 combination point CP-8 is the combination of subbasins OND8, OND9 and OFFD3. The remaining flow contributions to Channel C-2 remain unchanged.

The 10-year and 100-year peak flow reaching the equalizer basin in developed conditions is 60 cfs and 127 cfs respectively. The peak WSE in the equalizer basin was determined by the HEC-1 model to be 1748.19 feet. This WSE is 0.44 feet above the spillway height. It was determined that 67 cfs will be conveyed through the 42" RCP into the detention basin whereas 26 cfs will flow north combining with subbasin OND14 at HEC-1 combination point CP-11. The peak flow (10-year/100-year) at this combination point is 15/39 cfs. The peak flow reaching the northeast corner of the property is less than existing drainage condition peak flows of 27/65 cfs.

The 10-year and 100-year peak flow reaching the detention basin in developed conditions is 119 cfs and 254 cfs respectively. The 100-year WSE in the detention basin determined by the HEC-1 model is 1733.80ft, resulting in a freeboard of 1.2 feet. The outflow though the 25" opening is 45 cfs, resulting in the 100-year peak flow at HEC-1 combination point C18 to be 126 cfs. The proposed development will add an additional 6 cfs (additional 5%) to the existing 60" storm drain. A hydraulic analysis was performed on the additional flow anticipated to be conveyed through the existing 60" storm drain. This will be discussed in further detail in **Section D**.



Table 6: Summary Table for Developed Condition

| BASIN<br>ID | AREA<br>(ac) | Q <sub>100</sub><br>(cfs) | Q <sub>10</sub><br>(cfs) |
|-------------|--------------|---------------------------|--------------------------|
| OND1        | 0.94         | 3                         | 1                        |
| OND2        | 3.70         | 8                         | 4                        |
| OND3        | 1.38         | 4                         | 2                        |
| OND4        | 11.67        | 27                        | 13                       |
| OND5        | 5.03         | 12                        | 6                        |
| OND6        | 9.90         | 23                        | 11                       |
| OND7        | 5.87         | 16                        | 8                        |
| OND8        | 14.26        | 33                        | 16                       |
| OND9        | 1.06         | 3                         | 2                        |
| OND10       | 4.28         | 10                        | 5                        |
| OND11       | 9.60         | 24                        | 12                       |
| OND12       | 2.77         | 8                         | 4                        |
| OND13       | 4.70         | 12                        | 6                        |
| OND14       | 11.12        | 31                        | 15                       |
| OND15       | 21.47        | 57                        | 28                       |
| DETPD       | 5.14         | 16                        | 8                        |
| OFFD1       | 42.20        | 87                        | 39                       |
| OFFD2       | 9.63         | 23                        | 10                       |
| OFFD3       | 16.40        | 35                        | 16                       |
| OFFD4       | 7.61         | 19                        | 9                        |
| OFFD5       | 5.11         | 13                        | 6                        |
| CP-1        | NA           | 25                        | 11                       |
| CP-2        | NA           | 120                       | 54                       |
| CP-3        | NA           | 121                       | 54                       |
| CP-4        | NA           | 131                       | 59                       |
| CP-5        | NA           | 40                        | 19                       |
| CP-6        | NA           | 254                       | 119                      |
| CP-7        | NA           | 37                        | 17                       |
| CP-8        | NA           | 70                        | 33                       |
| CP-9        | NA           | 89                        | 41                       |
| CP-10       | NA           | 127                       | 60                       |
| CP-10A      | NA           | 92                        | 43                       |
| CP-11       | NA           | 39                        | 15                       |
| C18         | NA           | 126                       | 68                       |
| C18B        | NA           | 136                       | 74                       |

The discussion on the development of the hydrologic parameters is included in **Appendix B-4**. The developed drainage condition HEC-1 model is included in **Appendix B-3**. Please refer to **Appendix E** for the proposed grading plans.



#### D. Hydraulics

#### **HEC-RAS Model for Channel C-1**

HEC-RAS was used to model Channel C-1 (from station 10+00 to 20+00) which begins as an unlined 10 feet wide channel, 3:1 side slopes with a minimum depth of 3 ft. The channel then transitions to a 10 feet wide concrete bottom section, with riprap lined banks with 3:1 side slopes with a minimum depth of 3 feet until the channel discharges into the detention basin. Please refer to proposed grading plans included in **Appendix E** for the cross-section details and locations.

Boundary conditions for Channel C-1 were set to anticipate the effects of the proposed grading. The upstream boundary condition was set to normal depth with the channel slope of 0.40%. The downstream boundary condition was set to normal depth with the channel slope of 6.00% which represents the slope of the access road entering the detention basin. This slope was the most critical condition to ensure the velocities meet CCRFCD criteria at the terminus of the model.

The HEC-RAS model was ended at station 38+74.10 because the runoff in Channel C-1 will spread across the access road and over the grouted riprap into the detention basin. The geometry data used in HEC-RAS model is consistent with the proposed grading plans.

The HEC-RAS model simulated under mixed flow regime using the flows summarized in the table below.

| STATION | FLOW (cfs) | NOTES                |
|---------|------------|----------------------|
| 1100    | 3          | flow of OND1         |
| 1200    | 33         | sum of CP-1 and OND2 |
| 2000    | 120        | flow at CP-2         |
| 2200    | 121        | flow at CP-3         |
| 2587.70 | 131        | flow at CP-4         |

Table 7: Summary of flows used for Channel C-1 HEC-RAS model

The results of the analysis shows that the maximum velocity in the unlined channel and the concrete/riprap channel are less than 5 feet/sec and 10feet/sec respectively. The freeboard calculations for Channel C-1 are located in **Appendix C-4**. Superelevation was calculated from station 20+50 through 23+73.86 because of the channel bend.

Please refer to Figure7 – Cross Section and Drainage Facility Map in Appendix C-1 for channel stationing and Appendix C-2 for the HEC-RAS model. An electronic copy of the HEC-RAS models is also included in Appendix F.



#### **HEC-RAS Model for Channel C-2**

HEC-RAS was used to model Channel C-2 (from station 10+00 to 26+69.88) which begins as an unlined 10 feet wide channel, 3:1 side slopes with a minimum depth of 3 ft. The channel then transitions to a 10 feet wide concrete bottom section, with riprap lined banks with 3:1 side slopes with a minimum depth of 3 feet (from station 20+00 to 25+45). The channel then transitions to a 10 feet wide concrete bottom section, with riprap lined banks with 3:1 side slopes with a minimum depth of 4 feet until the channel discharges into the equalizer basin. Please refer to proposed grading plans included in **Appendix E** for the cross-section details and locations.

The upstream boundary condition was set to normal depth with the channel slope of 0.40%. The downstream boundary condition was set to known WSE of 1748.19 which represents the peak WSE in the equalizer basin. The geometry data used in HEC-RAS model is consistent with the proposed grading plans.

The HEC-RAS model simulated under mixed flow regime using the flows summarized in the table below.

Table 8: Summary of flows used for Channel C-2 HEC-RAS model

| STATION | FLOW (cfs) | NOTES                 |
|---------|------------|-----------------------|
| 1000    | 80         | sum of CP-8 and OND10 |
| 2000    | 89         | flow at CP-9          |
| 2319.91 | 92         | flow at CP-10A        |

The results of the analysis shows that the maximum velocity in the unlined channel and the concrete/riprap channel are less than 5 feet/s and 10feet/s respectively. The freeboard calculations for Channel C-2 are located in **Appendix C-4**. Superelevation was calculated through the channel bend.

Please refer to Figure 7 – Cross-Section and Drainage Facility Map in Appendix C-1 for channel stationing and Appendix C-2 for the HEC-RAS model. An electronic copy of the HEC-RAS models is also included in Appendix F.

#### FlowMaster Calculations

FlowMaster was used to calculate normal depth and velocity at the cross-sections shown on Figure7- Cross-Section and Drainage Facility Map included in Appendix C-1. Freeboard was calculated on the channels along the perimeter of the proposed landfill. The cross-sections on the top of the landfill were analyzed to show the peak flow is contained within the cross-section. The embankment channels were also analyzed using the FlowMaster to the show the containment of flow. The embankment channels are grouted riprap lined with 10' feet wide, 3:1 side slopes and depth of 1 foot. The velocities within these embankment channels are less than 15 feet /sec meeting the CCRFCD criteria.



Please refer to **Appendix C-5** for the FlowMaster calculations and the proposed grading plans included in **Appendix E** for the cross-section details.

#### 42" Storm Drain

WSPG was used to analyze the 42" storm drain. Under developed condition, 67 cfs was calculated to enter the 42" storm drain based on the stage-storage discharge curve that was previously discussed in **Section III-B**. The upstream boundary condition uses a WSE of 1748.19 feet which was taken from HEC-1 model at the equalizer basin. The downstream boundary condition uses a WSE of 1733.8 feet which was taken from HEC-1 model at the detention basin.

Please refer to **Appendix C-6** for the WSPG model and the proposed grading plans included in **Appendix E** for the storm drain alignment, stationing and inverts.

#### 60" Storm Drain

WSPG was used to analyze the proposed 60" storm drain that ties into the existing 60" storm drain built with the Harsch Development. The outflow from the detention pond was calculated to be 45 cfs determined from the stage-storage discharge curve. At HEC-1 combination point C18 in the developed conditions, the peak flow is 126 cfs. The referenced WSPG model was revised to show the changes in the existing storm drain due to the addition of 6 cfs. In the model, stations 2899.20 thru 1144.65 were directly referenced from the above mentioned study.

The peak outflow from the detention pond was 45 cfs and the peak flow at combination point C18 is 126 cfs. Therefore, 81 cfs was introduced at station 2899.20 where the existing inlet is located (126-45 = 81 cfs). As shown in the chart below, the 60" storm drain has adequate capacity to convey additional 6 cfs with minimal differences in the HGL and EGL between the proposed storm drain flow and the original flow calculated in the referenced study.





Exhibit 3: 60" Storm Drain Analysis Chart

#### **Riprap Calculations**

Riprap calculations were performed to show that 12" riprap will withstand the shear stress acting on the side slopes of Channel C-1 and Channel C-2. The shear stress calculations were conducted on stations 20+00 thru 38+74.10 of Channel C-1 and stations 20+00 thru 26+69.88 for Channel C-2.

PBS&J sized the riprap based on critical shear stress calculations. The results of proposed HEC-RAS model were used to calculate the average boundary shear stress on the channel bed ( $\tau$ 0) using the following equation:

 $\tau o = \lambda DSf$ 

where  $\lambda$  is the density of water (62.4 lb/ft2), D is the flow depth, and Sf is the frictional slope).

The critical shear stress ( $\tau$ cr) for the riprap bed was calculated based on the following equation:

 $\tau cr = 0.06 (\lambda s - \lambda w) d Tan \Phi$ 

where  $\lambda s$  is the density of the riprap (149.76 lb/ft2, specific gravity = 2.4),  $\lambda w$  is the density of water (62.4 lb/ft2), d is the median diameter of the riprap, and  $\Phi$  is the angle



of repose, which is based on Figure 705A of the Clark County Regional Flood Control District (CCRFCD) design manual.

PBS&J computed the shear stress on the banks and side slopes  $(\tau m)$  using the following equation:

 $\tau m = 0.75 \lambda DSf$  $\tau m = 0.75 \tau o$ 

where to is average boundary shear stress on the bed as discussed above.

The critical shear stress  $(\tau s)$  on the banks and side slopes is calculated based on the following equation:

$$\tau_s = \tau_{cr} \sqrt{1 - \frac{Sin^2 \theta}{Sin^2 \phi}}$$

where  $\tau$ cr is critical shear stress on the bed as discussed above, and  $\theta$  is bank side slope.

PBS&J selected the riprap sizes such that the critical stress for banks is always greater than the shear stress for banks with a factor of safety always higher than 3 (refer to **Appendix C-8** for supporting calculations).

#### **IV. Conclusions**

This study presents the findings of a detailed evaluation of existing, interim, and developed drainage conditions for the proposed landfill.

This study investigated the onsite and offsite drainage conditions and determined that the site will be able to convey the 100-year peak flow rate through the proposed drainage facilities.

The study shows that the flood protection facilities designed within this study will improve/perpetuate existing drainage patterns.

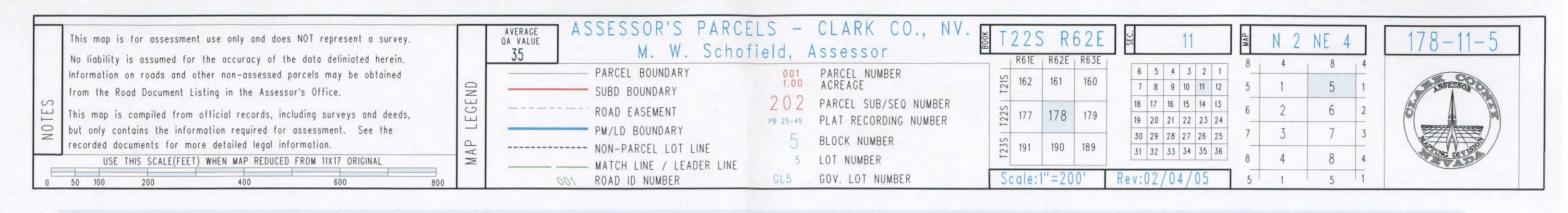
A copy of the grading plans are included Appendix E.

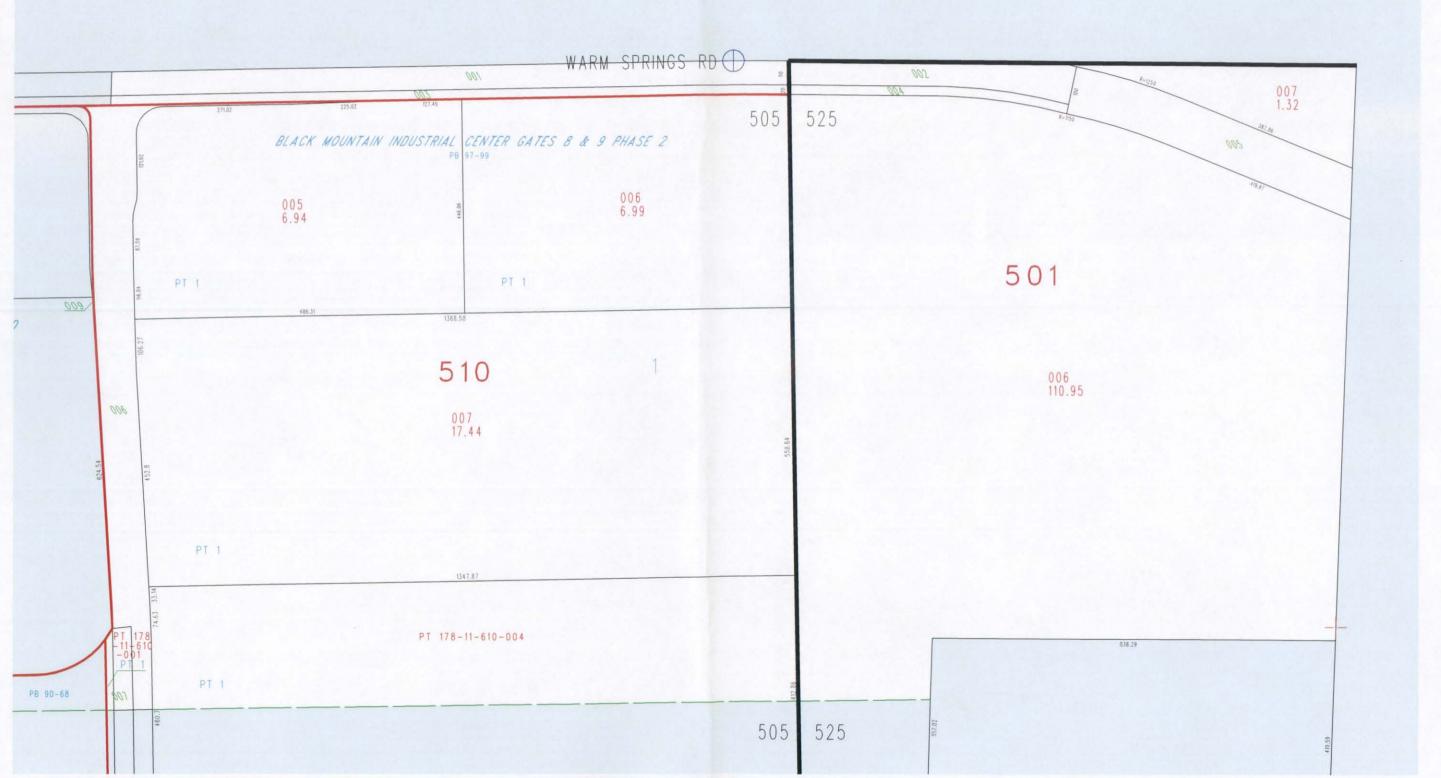


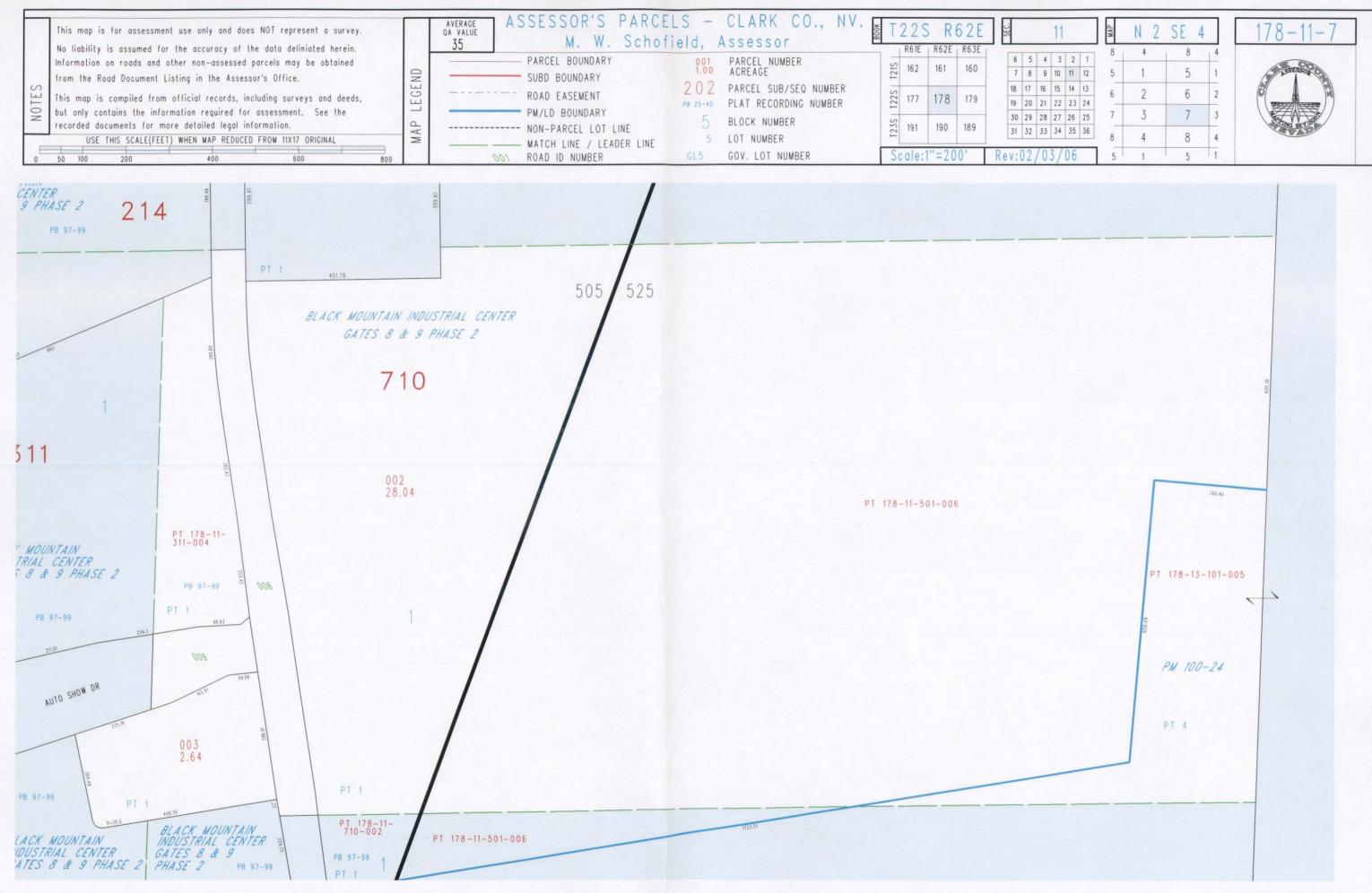
#### V. References

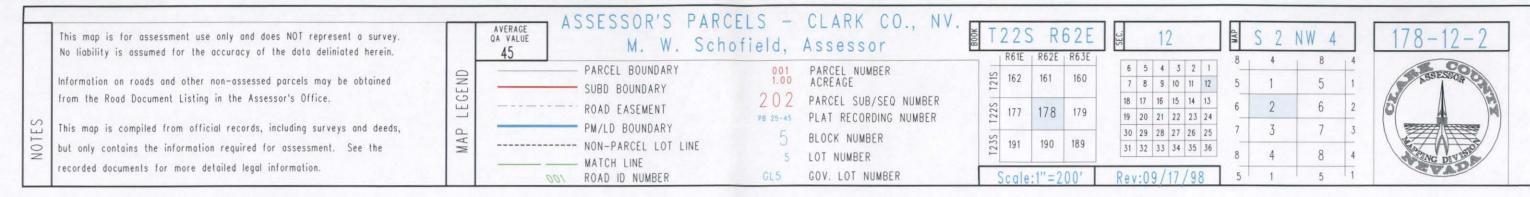
- Clark County Regional Flood Control District Hydrologic Criteria and Drainage Design Manual. Prepared for: Clark County Regional Flood Control District. Adopted August 12, 1999.
- 2. FlowMaster Version 6.1, Haestad Methods, Inc. 1999.
- 3. HEC-1 Flood Hydrograph Package Version 4.1. U.S. Army Corps of Engineers, Hydrologic Engineering Center, September 1990.
- 4. CCRFCD Master Plan Update of the Las Vegas Valley 2002. Prepared for Clark County Regional Flood Control District. Prepared by PBS&J and VTN, 2002.
- 5. Soil Survey of Las Vegas Valley Area Nevada 1985. United States Department of Agriculture, Soil Conservation Service
- 6. Addendum #1 to the Technical Drainage Study for Henderson Commerce Center Two (Formerly known as Harsch). Prepared by PBS&J, February 2003.
- 7. Update to the Technical Drainage Study for Henderson Commerce Center (Formerly known as Harsch Development). Prepared by PBS&J, February 2005.

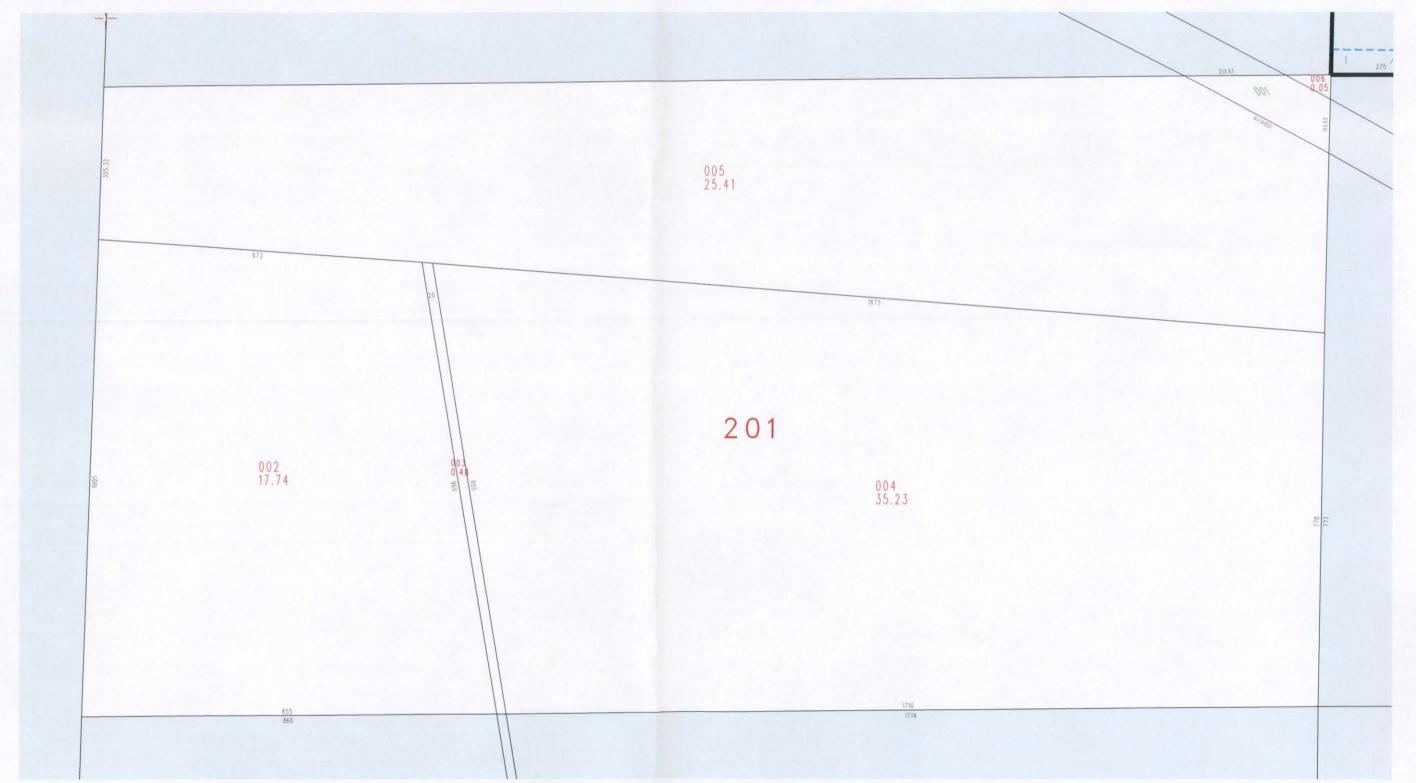
Appendix A: General Information Figures

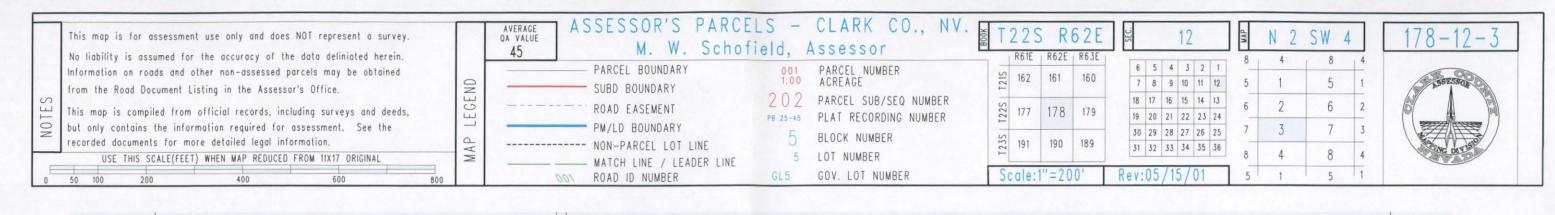


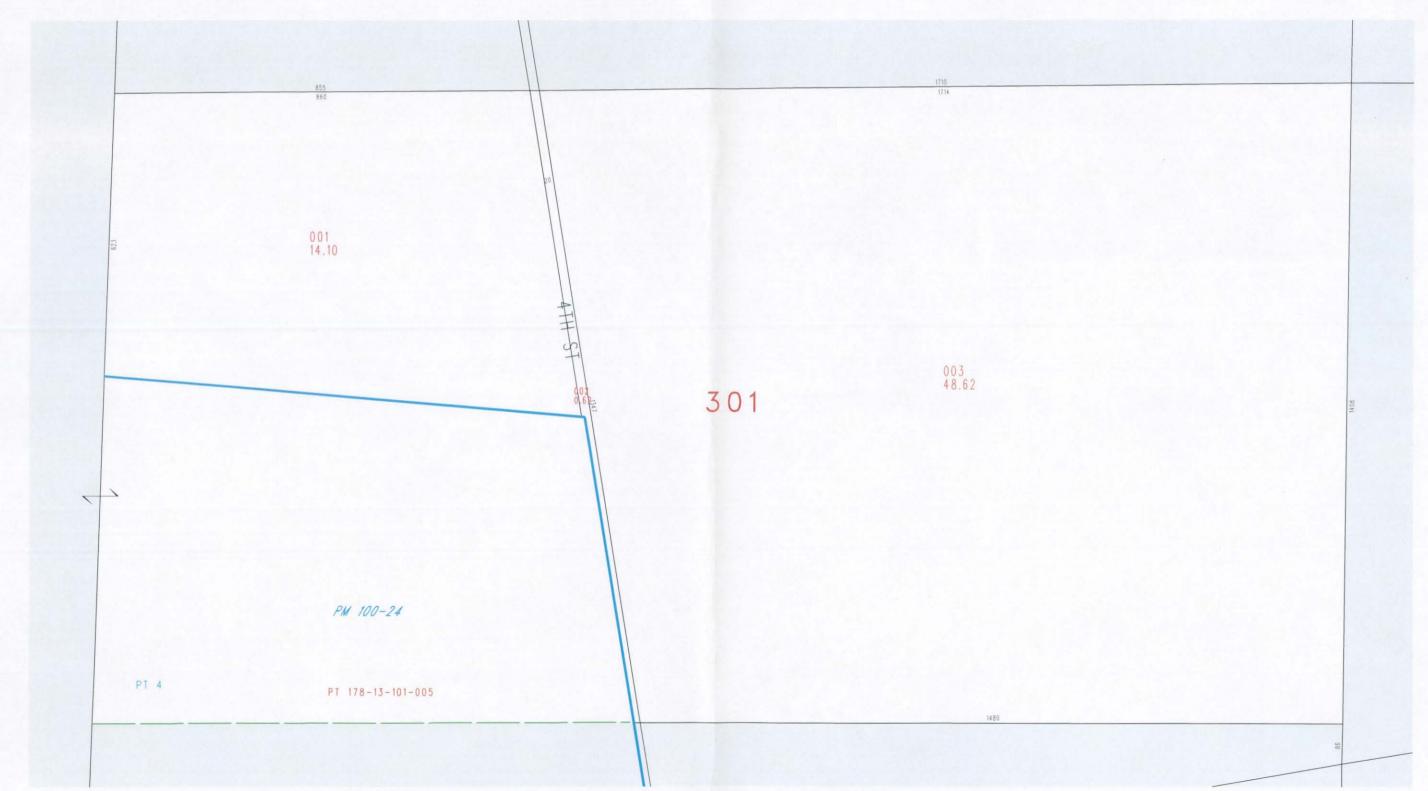




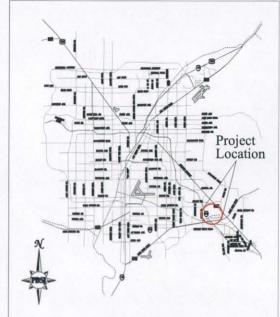














## **GRAPHIC SCALE**



( IN FEET ) 1 inch =800 ft.

511963.19

SEPTEMBER 2006

FIGURE 1 AREA/ VICINITY MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



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ENGINEERING PLANNING SURVEYING CONSTRUCTION SERVICES



FIGURE 2: CCRFCD FLOOD CONTROL FACILITIES MAP

| ID /<br>River<br>Mile | Status       | Facility Description  | Length<br>(fL) | Flow<br>(cfs) | HEC-1<br>Node | HEC-1<br>Model                          | Area<br>(sq.mi.) | Chang<br>Slop<br>(%) |
|-----------------------|--------------|---|----------------|---------------|---------------|---|------------------|----------------------|
| CIBH                  |              | C-1 CHANNEL - BOULDER HWY   |                |               |               |   |                  |                      |
| 0000                  | P1           | Conc Chni 30'W 6'D 2:1 SS   | 2140           | 3224          | CP22          | C1SDN3                                  |                  |                      |
| 0040                  | P1           | 3: 15' X 6' RCBC @ Horizon Dr   | 10000000       | 100000        |               |   | 3.19             | 1.00                 |
| 0042                  | P1           | Conc Chnl 30'W 6'D 2:1 SS   | 100            | 3194          | CP21          | C1SDN3                                  | 3.11             | 1.00                 |
| 0071                  | E            | 10' X 4' RCBC @ Equestrian Dr   | 100            | 2842          | CP21          | C1SDN3                                  | 3.11             | 1.00                 |
| 0071                  | PI           | 3: 14' X 6' RCBC @ Equestrian Dr  | 100            |               | CP20          | C1SDN3                                  | 2.77             | 1.00                 |
| 0073                  | P1           | Conc Chnl 30'W 6'D 2:1 SS   | 100            | 2842          | CP20          | C1SDN3                                  | 2.77             | 1.00                 |
| 0111                  | P1           | Conc Chnl 20'W 6'D 2:1 SS   |                | 2842          | CP20          | C1SDN3                                  | 2.77             | 0.80                 |
| 0148                  | E            | 5: 8' X 4' RCBC @ Robert Way  | 1960           | 1937          | CP17          | C1SDN3                                  | 1.53             | 0.80                 |
| 0150                  | E            | Earth Chnl 80'-90'W 5'D 2:1 SS with Drop Structures                       | 120            | 1832          | CP16          | C1SDN3                                  | 1.42             | 1.00                 |
| 0150                  | PO           | Cons Chall 407M 412 0.4 CO  | 1745           | 1832          | CP16          | C1SDN3                                  | 1.42             | 1.30                 |
| C1CH                  | PU           | Conc Chril 40"W 4"D 2:1 SS<br>C-1 CHANNEL                                 | 1745           | 1832          | CP16          | C1SDN3                                  | 1.42             | 1.30                 |
|                       |              |   | 2000           |               |               |   |                  |                      |
| 0040                  | P2           | Conc Chnl 40'W 10'D 0:1 SS  | 4200           | 7324          | CP61*         | C1SDN4                                  | 11.92            | 1.00                 |
| 0125                  | P2           | Conc Chni 40'W 10'D 0:1 SS  | 2100           | 7324          | CP61*         | C1SDN4                                  | 11.92            | 1.00                 |
| 0159                  | E            | Energy Dissipator   |                | 7324          | CP61*         | C1SDN4                                  | 11.92            |                      |
| 0161                  | E            | Earth Chnl 30'-60'W 7'-20'D with Gabion 2:1 SS                            | 2750           | 7324          | CP61°         | C1SDN4                                  | 11.92            | 2.00                 |
| 0161                  | P0           | Conc Chnl 40'W 8'D 0:1 SS   | 2750           | 7325          | CP61*         | C1SDN4                                  | 11.92            | 2.00                 |
| 0213                  | E            | Energy Dissipator   |                | 7324          | CP61*         | C1SDN4                                  | 11.92            |                      |
| 0215                  | E            | 2: 12' X 9' RCBC @ Lake Mead Dr   | 270            | 7324          | CP61*         | C1SDN4                                  | 11.92            | 3.20                 |
| 0220                  | E            | Conc Chnl 15'W 9'D 1:1 SS: West Floodwall                                 | 2560           | 7324          | CP61*         | C1SDN4                                  | 11.92            | 2.30                 |
| 0269                  | E            | Conc Chni 15'W 7'D 2:1 SS: West Floodwall                                 | 1740           | 7324          | CP61*         | C1SDN4                                  | 11.92            | 2.30                 |
| 0284                  | E            | Conc Chni 15'W 9'D 1:1 SS: West Floodwall                                 | 1760           | 7324          | CP61*         | C1SDN4                                  | 11.92            | 1.70                 |
| 0335                  | E            | Conc Chnl 50'W 12'D 0:1 SS  | 280            | 7324          | CP61*         | C1SDN4                                  | 11.92            | 1.20                 |
| 0340                  | E            | Conc Chni 40-50'W 12'D 0:1 SS   | 300            | 7324          | CP61*         | C1SDN4                                  | 11.92            | 1.20                 |
| 0346                  | E            | Conc Chnl 40'W 6'D 2:1 SS: West Floodwall                                 | 290            | 7324          | CP61          | C1SDN4                                  | 11.92            | 1.20                 |
| 0351                  | E            | 4: 12' X 7' RCBC @ Warm Springs Rd  | 100            | 7175          | CP59          | C1SDN4                                  | 11.25            | 1.00                 |
| 0353                  | E            | Conc Chnl 14.5'W 8'D 2:1 SS: West Floodwall                               | 1245           | 6961          | CPC1D         | C1SDN4                                  | 10,44            | 0.84                 |
| 0377                  | E            | Conc Chnl 15'W 10'D 2:1 SS: West Floodwall                                | 815            | 6961          | CPC1D         | C1SDN4                                  | 10.44            | 0.84                 |
| 0392                  | E            | Conc Chnl 50'W 14'D 0:1 SS  | 325            | 6961          | CPC1D         | C1SDN4                                  | 10.44            | 0.70                 |
| 0398                  | E            | Junction Structure  | 70             | 6961          | CPC1D         | C1SDN4                                  | 10.44            | 0.70                 |
| 0400                  | E            | Conc Chnl 39.5'W 9'-14'D 0:1 SS   | 450            | 5919          | CP51          | C1SDN4                                  | 8.52             | 2.70                 |
| 0408                  |              | Conc Chnl 25'W 9'D 2:1 SS   | 1650           | 5919          | CP51          | C1SDN4                                  | 8.52             | 2.00                 |
| 0439                  |              | Single Span Bridge @ Burkholder Blvd                                      | 100            | 5919          | CP51          | C1SDN4                                  | 8.52             | 2.00                 |
| 0441                  |              | Conc Chnl 25'W 9'D 2:1 SS   | 500            | 5666          | CP27          | C1SDN4                                  | 6.48             |                      |
| 0455                  |              | Conc Chni 25'W 7.5'D 2:1 SS   | 2695           | 5666          | CP27          | C1SDN3                                  | 6.48             | 2.00                 |
| 0502                  |              | Conc Chnl 25'W 7'D 2:1 SS   | 1100           | 5666          | CP27          | 100000000000000000000000000000000000000 |                  | 2.60                 |
| 0523                  |              | Conc Chnl 39'W 8'D 0:1 SS with Junction Structure                         | 310            | 5630          | CP26          | C1SDN3                                  | 6.48             | 2.50                 |
| 0528                  |              | Conc Chnl 25'W 7'D 2:1 SS   | 1340           | 4876          |               | C1SDN3                                  | 6.33             | 2.00                 |
| 0554                  |              | 3: 20' X 7' RCBC @ Boulder Hwy  | 350            | 1000          | CP23          | C1SDN3                                  | 5.33             | 2.00                 |
| 0561                  |              | Conc Chnl 20'W 6'D 0:1 SS   |                | 4828          | CPC1BH        | C1SDN3                                  | 5.26             | 2.40                 |
| 0600                  |              | 3: 10' X 7' RCBC @ Horizon Dr   | 1801<br>436    | 1765          | CP14          | C1SDN3                                  | 2.08             | 2.00                 |
| 0603                  |              | Conc Chnl 30'W 6'D 0:1 SS   |                | 1765          | CP14          | C1SDN3                                  | 2.08             | 1.20                 |
| 0604                  |              | Bridge 36'W 8.5'D @ UPRR  | 520            | 1765          | CP14          | C1SDN3                                  | 2.08             | 5.34                 |
| 0613                  |              | Conc Chnl 12.5'W 6'D 2:1 SS   | 1717           | 1765          | CP14          | C1SDN3                                  | 2.08             | 1.00                 |
| 0641                  | THE PARTY IN | Conc Chril 12.5 W 6 D 2:1 SS  | 1470           | 1765          | CP14          | C1SDN3                                  | 2.08             | 2.40                 |
| 0672                  | 100          | 4: 10' X 5' RCBC @ Vermillion Dr  | 1645           | 1641          | CP13          | C1SDN3                                  | 1.84             | 2.70                 |
| 0674                  |              | Conc Chnl 25'W 6'D 2:1 SS   | 115            | 1641          | CP13          | C1SDN3                                  | 1.84             | 0.50                 |
| 0686                  |              | NDOT Sediment Basin   | 630            | 1641          | CP13          | C1SDN3                                  | 1.84             | 0.70                 |
| CIDC                  | _            | C-1 CHANNEL - DRAKE CHANNEL   |                | 1239          | CP12          | C1SDN3                                  | 1.43             |                      |
| 0000                  |              |   | 141            |               |               |   |                  |                      |
| 0013                  |              | Conc Chnl 25'W 5'-14'D 0:1 SS   | 700            | 1778          | CP55          | C1SDN3                                  | 1.92             | 2.70                 |
| 0013                  |              | Earth Chni 10°W 5'D with Conc 2:1 SS                                      | 650            | 1778          | CP55          | C1SDN3                                  | 1.92             | 2.70                 |
| 0026                  | 100          | Conc Chnl 16'W 5'D 2:1 SS   | 650            | 1778          | CP55          | C1SDN3                                  | 1.92             | 2.70                 |
|                       |              | Conc Chnl 20.5'W 5'D 0:1 SS South Wall, 2:1 SS North Wall                 | 300            | 1778          | CP55          | C1SDN3                                  | 1.92             | 2.70                 |
| 0031                  |              | Conc Chnl 26'W 5'D 0:1 SS South Wall, 2:1 SS North Wall                   | 750            | 1778          | CP55          | C1SDN3                                  | 1.92             | 2.70                 |
| 0.10                  |              | Junction Structure  | 200            | 1778          | CP55          | C1SDN3                                  | 1.92             |                      |
| 0049                  |              | 2: 12' X 6' RCBC @ Racetrack Rd   | 92             | 1628          | CP54          | C1SDN3                                  | 1.69             | 0.50                 |
| 0051                  | 1            | Earth Chnl 20'-50'W 20'-10'D 2:1 SS with 9'-12' Gabion Drop<br>Structures | 2640           | 1628          | CP54          | C1SDN3                                  | 1.69             | 0.50                 |
| 0101                  |              | Earth Chnl 20'-50'W 20'-10'D 2:1 SS with 9'-12' Gabion Drop<br>Structures | 3660           | 1486          | CP53          | C1SDN3                                  | 1.44             | 0.50                 |
| 170                   |              | Soil Cement Levee 7.5'  | 2950           | 1132          | CP52          | C1SDN3B                                 | 6.39             | 2.90                 |
| 226                   |              | Soil Cement Levee 5'  | 3800           | 1132          | CP52          | C1SDN3B                                 | 6.39             | 2.90                 |
| 298                   |              | 48" RCPC Outlet   | 226            | 90            | DB5           | C1SDN3B                                 | 5.41             | 0.50                 |
| 302                   |              | 20,789 cfs PMF Spillway   |                | 20789         | C1-54         | C1SDN3B                                 | 5.41             |                      |
| 303                   | E 8          | 380 ac-ft East C-1 Detention Basin  |                |               |               |   |                  |                      |

| ID / River<br>Mile | Status | Facility Description                                | Length<br>(ft.) | Flow<br>(cfs) | HEC-1<br>Node | HEC-1<br>Model | Tributary<br>Area<br>(sq.mi.) | Channe<br>Slope<br>(%) ** |
|--------------------|--------|---|-----------------|---------------|---------------|----------------|-------------------------------|---------------------------|
| C1E1               |        | C-1 CHANNEL - EQUESTRIAN TRIBUTARY 1                |                 |               |               |                |                               |                           |
| 0000               | P1     | Energy Dissipator                                   |                 | 688           | CP30          | C1SDN3B        | 1.21                          |                           |
| 0002               | P1     | Conc Chnl 10'W 4.5'D 2:1 SS                         | 2200            | 688           | CP30          | C1SDN3B        | 1.21                          | 1.40                      |
| C1EQ               |        | C-1 CHANNEL - EQUESTRIAN D.B. OUTFALL               | 2500            | 000           | CF30          | CIGUNGO        | 1,21                          | 1,40                      |
| 0000               | P1     | Conc Chnl 10'W 5.5'D 2:1 SS                         | 3920            | 1097          | CP48          | C1SDN3         | 1.38                          | 1.40                      |
| 0074               | E      | 9: 45" X 29" HERCP                                  | 220             | 679           | CP46          | C1SDN3B        | 7.82                          | 0.50                      |
| 0078               | E      | Grass Chnl 40'W 4.5'D 5:1 SS                        | 1760            | 679           | CP46          | C1SDN3B        | 7.82                          | 1.50                      |
| 0112               | E      | Earth Chnl 45'-80'W 4'D 2:1 SS with Drop Structures | 1445            | 679           | CP46          | C1SDN3B        | 7.82                          | 1.40                      |
| 0139               | E      | 5' X 4' RCB   | 586             | 224           | DB4           | C1SDN3B        | 7.06                          | 1.90                      |
| 0151               | E      | Energy Dissipator                                   | 500             | 224           | DB4           | C1SDN3B        | 7.06                          | 1.00                      |
| 0152               | E      | 48" RCPC Outlet                                     | 325             | 224           | DB4           | C1SDN3B        | 7.06                          | 0.40                      |
| 0158               | E      | 39,100 cts PMF Spillway                             |                 | 39100         | CP44          | C1SDN3B        | 7.06                          | 0.10                      |
| 0159               | E      | 409 ac-ft Equestrian Detention Basin                |                 | 5196          | CP44          | C1SDN3B        | 7.06                          |                           |
| 0202               | E      | Conc Chnl 20'W 8.0'D 2:1 SS                         | 5000            | 3115          | CP38          | C1SDN3B        | 4.35                          | 2.40                      |
| 0297               | Ε      | Rip Rap Levee 10'                                   | 9000            | 3115          | CP38          | C1SDN3B        | 3.49                          | 2.00                      |
| C1FK               |        | C-1 CHANNEL - FOUR KIDS                             |                 | 0110          | 0100          | CIODINOD       | 0.40                          | 2.00                      |
| 0000               | P2     | 10' X 5' RCB  | 770             | 935           | CP72B         | C1SDN3         | 1.00                          | 2.50                      |
| 0014               | E      | Earth Chnl 21'W 4'-5'D with Rock 0:1 SS             | 1280            | 935           | CP72B         | C1SDN3         | 1.00                          | 1.80                      |
| 0039               | E      | 12' X 4' RCBC @ Eagle Rock Rd                       | 70              | 935           | CP72B         | C1SDN3         | 1.00                          | 2.70                      |
| 0040               | P1     | Conc Chnl 10'W 4.5'D 2:1 SS                         | 1750            | 935           | CP72B         | C1SDN3         | 1.00                          | 2.70                      |
| 0073               | E      | 4: 6' X 3' RCBC @ Lake Mead Dr                      | 160             | 721           | CP72A         | C1SDN3         | 0.78                          | 2.00                      |
| 0076               | P1     | Conc Chnl 10'W 5'D 0:1 SS                           | 1400            | 721           | CP72A         | C1SDN3         | 0.78                          | 3.00                      |
| C1GW               |        | C-1 CHANNEL - GREENWAY                              | 1,00            | 121           | OI TEN        | CIODIO         | 9.10                          | 0.00                      |
| 0000               | E      | 16' X 6' RCBC @ Pueblo Blvd                         | 114             | 920           | CP25          | C1SDN3         | 1.01                          | 1.00                      |
| 0002               | E      | Conc Chnl 6'W 9.5'D 1:1 SS                          | 1170            | 920           | CP25          | C1SDN3         | 1.01                          | 0.40                      |
| 0024               | E      | 2: 12' X 4' RCBC @ Boulder Hwy                      | 200             | 920           | CP25          | C1SDN3         | 1.01                          | 0.40                      |
| 0028               | E      | Conc Chnl 15'W 4'D 1:1 SS                           | 490             | 920           | CP25          | C1SDN3         | 1.01                          | 0.40                      |
| 0037               | E      | 2: 12' X 4' RCBC                                    | 40              | 920           | CP25          | C1SDN3         | 1.01                          | 0.90                      |
| 0038               | E      | Conc Chnl 15.3'W 4.8'D 1:1 SS                       | 450             | 920           | CP25          | C1SDN3         | 1.01                          | 0.70                      |
| 0047               | E      | 2: 12' X 4' RCBC @ Mona Ln                          | 70              | 568           | CP24          | C1SDN3         | 0.63                          | 0.60                      |
| 0048               | E      | Conc Chni 17'W 4'D 1:1 SS                           | 685             | 568           | CP24          | C1SDN3         | 0.63                          | 1,60                      |
| 0061               | E      | 2: 12' X 4' RCBC @ Greenway Rd                      | 190             | 568           | CP24          | C1SDN3         | 0.63                          | 1.00                      |
| 0064               | E      | Earth Chnl 16'-20'W 6'-9'D 0:1 SS                   | 300             | 568           | CP24          | C13DN3         | 0.63                          | 1.20                      |
| 0064               | P0     | Conc Chnl 15'W 4'D 0:1 SS                           | 300             | 568           | CP24          | C1SDN3         | 0.63                          | 1.20                      |
| 0070               | E      | 2: 12' X 4' RCBC @ Van Wagenen Ave                  | 85              | 568           | CP24          | C1SDN3         | 0.63                          | 0.80                      |
| 0072               | E      | Earth Chnl 28'W 3'-8'D 2:1 SS                       | 470             | 568           | CP24          | C1SDN3         | 0.63                          | 0.80                      |
| 0072               | P0     | Conc Chnl 15'W 4.5'D 0:1 SS                         | 470             | 568           | CP24          | C1SDN3         | 0.63                          | 0.80                      |
| 0081               |        | 3: 9.5' X 6.5' CMAP @ UPRR                          | 50              | 568           | CP24          | C1SDN3         | 0.63                          | 0.80                      |
| CIIT               |        | C-1 CHANNEL - ITHACA                                |                 | -             |               |                |                               | -                         |
| 0000               |        | 72" RCP Outlet                                      | 6200            | 424           | DB6           | C1SDN3B        | 3.42                          | 2.20                      |
| 0117               |        | 16,830 cfs PMF Spillway                             |                 | 16830         | CP64          | C1SDN3B        | 3.42                          |                           |
| 0118               |        | 310 ac-ft N.E. Detention Basin                      |                 | 1683          | CP64          | C1SDN3B        | 3.42                          |                           |
| 0155               |        | Soil Cement Levee 11'                               | 4000            | 1514          | C1-65         | C1SDN3B        | 2.54                          | 3.00                      |
| 0273               |        | Soil Cement Levee 11'                               | 400             | 1514          | C1-65         | C1SDN3B        | 2.54                          | 3.00                      |
| C1LM               |        | C-1 CHANNEL - LAKE MEAD                             |                 |               |               |                |                               |                           |
| 0000               |        | Conc Chnl 10'W 6'D 2:1 SS                           | 2525            | 1385          | CP71          | C1SDN3         | 1.96                          | 0.90                      |
| 0048               |        | 2: 11' X 6' RCBC @ Mohawk Dr                        | 60              | 1385          | CP71          | C1SDN3         | 1.96                          | 0.90                      |
| 0049               |        | Conc Chnl 10'W 6'D 2:1 SS                           | 1560            | 1385          | CP71          | C1SDN3         | 1.96                          | 0.90                      |
| 0079               | 1      | 2: 11' X 6' RCBC @ Pawnee Ln                        | 60              | 1385          | CP71          | C1SDN3         | 1.96                          | 0.90                      |
| 0083               |        | Conc Chnl 10'W 6'D 2:1 SS                           | 570             | 1385          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0090               |        | 2: 11' X 6' RCBC @ Navajo Dr                        | 60              | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0092               |        | Conc Chril 10'W 6'D 2:1 SS                          | 325             | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0098               |        | 2: 11' X 6' RCBC @ Shoshone Dr                      | 60              | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0099               |        | Conc Chnl 10'W 6'D 2:1 SS                           | 345             | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0105               |        | 2: 11' X 6' RCBC @ Center St                        | 100             | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0107               |        | Conc Chnl 10'W 6'D 2:1 SS                           | 555             | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0118               |        | 2: 11' X 6' RCBC @ Entrance                         | 50              | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0119               |        | Conc Chnl 10'W 6'D 2:1 SS                           | 295             | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0124               |        | 2: 11' X 6' RCBC @ Entrance                         | 50              | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0125               |        | Conc Chnl 10'W 6'D 2:1 SS                           | 870             | 1305          | CP70          | C1SDN3         | 1.77                          | 0.90                      |
| 0142               |        | 15' X 6' RCBC @ Warm Springs Rd                     | 125             | 1054          | CP69          | C1SDN3         | 1.44                          | 0.90                      |
| 0144               |        | Conc Chnl 10'W 4.5'D 2:1 SS                         | 655             | 682           | CP67          | C1SDN3         | 0.81                          | 0.90                      |
| 0156               |        | 11' X 6' RCBC @ Ash St                              | 60              | 682           | CP67          | C1SDN3         | 0.81                          | 0.90                      |
| 0158               |        | Conc Chni 10'W 4.5'D 2:1 SS                         | 1305            | 682           | CP67          | C1SDN3         | 0.81                          | 0.90                      |
| 0182               |        | 11' X 6' RCBC @ Ivy St                              | 60              | 682           | CP67          | C1SDN3         | 0.81                          | 0.90                      |
| 0184               | P1     | Conc Chnl 10'W 4.5'D 2:1 SS                         | 900             | 682           | CP67          | C1SDN3         | 0.81                          | 0.90                      |

| ID / River<br>Mile | Status   | Facility Description  | Length<br>(fL) | Flow<br>(cfs) | HEC-1<br>Node      | HEC-1<br>Model   | Tributary<br>Area<br>(eq.mi.) | Channel<br>Slope<br>(%) ** |
|--------------------|----------|---|----------------|---------------|--------------------|------------------|-------------------------------|----------------------------|
| LLMW               |          | LAKE LAS VEGAS - MAGIC WAY                                      |                |               |                    |                  |                               |                            |
| 0003               | PO       | Conc Chnl 10'W 6'D 2:1 SS                                       | 6670           | 1932          | CP80               | C1SDN3           | 3.52                          | 3.50                       |
| 0129               | E        | 6: 8' X 3' RCBC   | 160            | 1842          | CP79               | C1SDN3           | 3.04                          | 1.00                       |
| 0132               | PO       | Conc Chnl 15'W 5'D 2:1 SS                                       | 3720           | 1564          | CP77               | C1SDN3           | 2.30                          | 3.10                       |
| 0203               | E        | Conc Chnl 35'W 5'-6'D 0.5:1 SS                                  | 3000           | 1515          | C1-85              | C1SDN3           | 2.06                          | 3.10                       |
| PTBR               |          | PITTMAN WASH - BURNS  |                |               |                    |                  |                               |                            |
| 0029               | E        | Rip Rap Chnl 35'W 9'D 2:1 SS                                    | 2850           | 5448          | CPBR160            | PIT3SC           | 5.85                          | 0.68                       |
| 0029               | P1       | Rip Rap Chnl 60'W 9'D 3:1 SS                                    | 2850           | 5448          | CPBR160            | PIT3SC           | 5.85                          | 0.68                       |
| 0090               | E        | 2: 24' X 8.5' RCAC @ Weisner Way                                | 190            | 5448          | CPBR160            | PIT3SC           | 5.85                          | 0.90                       |
| 0091               | E        | Conc Chnl 25'W 9'D 2:1 SS                                       | 2570           | 5448          | CPBR160            | PIT3SC           | 5.85                          | 1.10                       |
| 0140               | E        | Conc Chnl 25'W 9'D 2:1 SS                                       | 1110           | 5254          | CPBR150            | PIT3SC           | 5.54                          | 0.50                       |
| 0160               | E        | Conc Chnl 10'W 8'D 2:1 SS                                       | 210            | 2881          | CPBR090            | PIT3SC           | 3.19                          | 1.00                       |
| 0164               | P1       | Conc Chnl 20'W 8'D 0:1 SS<br>Add 4: 16' X 4' RCBC @ Boulder Hwy | 250            | 2881          | CPBR090            | PIT3SC           | 3.19                          | 1.00                       |
| 0165               | E        |   | 330            | 2881          | CPBR090            | PIT3SC           | 3.19                          | 1.50                       |
| PTGB               |          | 2: 6' X 4' RCBC @ Boulder Hwy<br>PITTMAN WASH - GIBSON          | 330            | 2881          | CPBR090            | PIT3SC           | 3.19                          | 1.50                       |
| 0058               | P1       | Conc Chnl 15'W 5.5'D 2:1 SS                                     | 1560           | 1532          | CPBR080            | PITSC            | 1.76                          | 1.50                       |
| 0087               | P3       | 2: 10' X 6' RCB   | 660            | 1532          | CPBR080            | PIT3SC           | 1.76                          | 1.50                       |
| 0093               | E        | Earth/Conc Chnl 8'W 5'D 2:1 SS                                  | 550            | 1532          | CPBR080            | PIT3SC           | 1.76                          | 1.50                       |
| 0093               | P1       | Conc Chnl 30'W 5'D 0:1 SS                                       | 550            | 1532          | CPBR080            | PIT3SC           | 1.76                          | 1.50                       |
| PTGL               |          | PITTMAN GAS LINE  | - 550          | 1002          | OI DI IOOO         | 111000           | 1.70                          | 1.50                       |
| 0000               | Ε        | 72* RCP   | 1675           | 678           | CPPD030            | PIT3SC           | 0.69                          | 3.40                       |
| PTHR               |          | PITTMAN HORIZON RIDGE   |                |               |                    |                  |                               |                            |
| 0000               | P1       | Conc Chnl 15'W 5'D 2:1 SS                                       | 2300           | 1652          | CPPD170            | PIT3SC           | 1.49                          | 3.00                       |
| 0043               | P1       | 2: 12' X 6' RCBC @ UPRR   | 100            | 1371          | CPPD165            | PIT3SC           | 1.25                          | 2.00                       |
| 0044               | P1       | Conc Chnl 15'W 5.5'D 2:1 SS                                     | 1250           | 1371          | CPPD165            | PIT3SC           | 1.25                          | 1.20                       |
| 0049               | E        | 12' X 5' RCBC @ Lake Mead Dr                                    | 150            | 1345          | CPPD160            | PIT3SC           | 1.20                          | 1.20                       |
| 0067               | E        | 8' X 5' RCB   | 1800           | 1345          | CPPD160            | PIT3SC           | 1.20                          | 2.60                       |
| 0104               | P1       | Conc Chnl 15'W 4.5'D 2:1 SS                                     | 1825           | 1345          | CPPD160            | PIT3SC           | 1.20                          | 4.90                       |
| 0139               | E        | 36* RCP @ Horizon Ridge Pkwy                                    | 100            | 1065          | CPPD135            | PIT3SC           | 0.89                          | 7.00                       |
| 0139               | P1<br>P1 | 12' X 6' RCBC @ Horizon Ridge Pkwy                              | 100            | 1065          | CPPD135            | PIT3SC           | 0.89                          | 7.00                       |
| 0140               | Pi       | Conc Chnl 15'W 4'D 2:1 SS                                       | 3425 .         | 1065          | CPPD135            | PIT3SC           | 0.89                          | 4.00                       |
| 0203               | Pt       | 84* RCP Outlet  | 200            | 882           | CPPD125            | PIT3SC           | 0.72                          | 4.00                       |
| 0205               | P1       | 882 cfs Spillway  |                | 882<br>882    | CPPD125<br>CPPD125 | PIT3SC           | 0.72                          |                            |
| 0210               | E        | 2.5 ac-ft Pittman Horizon Ridge Debris Basin<br>Natural Wash    | 2950           | 882           | CPPD125<br>CPPD125 | PIT3SC           | 0.72                          | 7.00                       |
| PTIS               | _        | PITTMAN WASH - INTERSTATE                                       | 2950           | 002           | CPPD125            | PIT3SC           | 0.72                          | 7.00                       |
| 0000               | P1       | Conc Chnl 30'W 6'D 2:1 SS                                       | 2100           | 4530          | CPPD150            | PIT3SC           | 5.90                          | 3.00                       |
| 0007               | P1       | 4: 14' X 6' RCBC @ I-515  | 200            | 4530          | CPPD150            | PIT3SC           | 5.90                          | 1.40                       |
| 8000               | P1       | Conc Chnl 30'W 6.5'D 2:1 SS                                     | 150            | 4530          | CPPD150            | PIT3SC           | 5.90                          | 1.40                       |
| 0014               | P1       | 4: 14' X 6' RCBC @ I-515  | 150            | 4530          | CPPD150            | PIT3SC           | 5.90                          | 1.40                       |
| 0015               | P1       | Conc Chnl 30'W 6.5'D 2:1 SS                                     | 250            | 4261          | CPPD150            | PIT3SC           | 5.24                          | 1.40                       |
| 0023               | E        | Conc Chnl 40°W 7°D 2:1 SS                                       | 110            | 3497          | CPPD140            | PIT3SC           | 3.68                          | 3.00                       |
| 0028               | E        | 4: 8' X 8' RCBC @ I-515   | 350            | 3497          | CPPD140            | PIT3             | 3.68                          | 2.80                       |
| 0029               | E        | Conc Chnl 30'W 5'D 2:1 SS                                       | 1100           | 2520          | CPPD070            | PIT3             | 2.57                          | 3.00                       |
| 0050               | E        | Conc Chnl 30'W 5'D 2:1 SS                                       | 380            | 2520          | CPPD070            | PIT3SC           | 2.57                          | 3.00                       |
| 0055               | E        | 2: 7' X 7' RCBC @ UPRR  | 1000           | 2520          | CPPD070            | PIT3SC           | 2.57                          | 3.00                       |
| 0056               | E        | Conc Chnl 30'W 5'D 2:1 SS                                       | 650            | 2520          | CPPD070            | PIT3SC           | 2.57                          | 3.80                       |
| 0068               | E        | Rip Rap Chnl 35'W 6'D 2:1 SS                                    | 1000           | 2520          | CPPD070            | PIT3SC           | 2.57                          | 1.10                       |
| 0087               | E        | Conc Chnl 35'W 6'D 2:1 SS                                       | 800            | 2380          | CPPD060            | PIT3SC           | 2.36                          | 2.50                       |
| 0102               | E        | Rip Rap Chnl 35'W 6'D 2:1 SS                                    | 3390           | 2380          | CPPD060            | PIT3SC           | 2.36                          | 1.10                       |
| 0184               | E        | 2: 6' X 6' RCB  | 950            | 1365          | CPPD045            | PIT3SC           | 1.17                          | 3.50                       |
| 0197               | E        | Conc Chnl 9'W 4'D 3:1 SS  | 750            | 1962          | CPPD050            | PIT3SC           | 1.86                          | 5.00                       |
| 0198               | E        | 3: 60* RCP @ Horizon Ridge Pkwy<br>Conc Chnl 10*W 4*D 2:1 SS    | 150<br>3150    | 681<br>681    | CPPD030<br>CPPD030 | PIT3SC<br>PIT3SC | 0.69                          | 3.00                       |
|                    |          |   | 0.00           | 501           | 0.1900             | 1,1000           | 0.03                          | 1.30                       |
|                    |          |   |                |               |                    |                  |                               |                            |

| ID / River<br>Mile | Status | Facility Description              | Length<br>(fL) | Flow<br>(cfs) | HEC-1<br>Node | HEC-1<br>Model | Area<br>(sq.mi.) | Channel<br>Slope<br>(%) ** |
|--------------------|--------|-----------------------------------|----------------|---------------|---------------|----------------|------------------|----------------------------|
| PTPA               |        | PITTMAN PABCO                     |                |               |               |                |                  |                            |
| 0000               | P1     | Conc Chni 30'W 6.5'D 2:1 SS       | 12430          | 2251          | CPLW120       | PIT3SC         | 4.69             | 0.30                       |
| 0235               | E      | 10' X 5' RCBC @ Pabco             | 140            | 302           | PABCODB       | PIT3SC         | 1.28             | 2.30                       |
| 0236               | P1     | Conc Chnl 12'W 3'D 2:1 SS         | 950            | 302           | PABCODB       | PIT3SC         | 1.28             | 1.70                       |
| 0254               | E      | 1: 10' X 6' RCBC @ Warm Springs   | 90             | 302           | PABCODB       | PIT3SC         | 1.28             | 1,70                       |
| 0255               | P1     | Conc Chnl 12'W 3'D 2:1 SS         | 280            | 302           | PABCODB       | PIT3SC         | 1.28             | 1.70                       |
| 0260               | E      | 2: 6' X 4' RCBC @ Boulder Hwy     | 61             | 302           | PABCODB       | PIT3SC         | 1.28             | 1.70                       |
| 0262               | P1     | Conc Chnl 12'W 3'D 2:1 SS         | 45             | 302           | PABCODB       | PIT3SC         | 1.28             | 1.70                       |
| 0264               | E      | 2: 6' X 4' RCBC Outlet            | 230            | 302           | PABCODB       | PIT3SC         | 1.28             |                            |
| 0265               | P1     | 10,300 cfs PMF Spillway           |                | 10300         | CPPA030       | PIT3SC         | 1.28             |                            |
| 0266               | P1     | 53 ac-ft Pabco Detention Basin    |                | 1026          | CPPA030       | PIT3SC         | 1.28             |                            |
| PTPD               |        | PITTMAN PIONEER DETENTION         |                |               |               |                |                  |                            |
| 0000               | P1     | Conc Chnl 12'W 4'D 2:1 SS         | 500            | 668           | CPPD145       | PIT3SC         | 0.54             | 3.00                       |
| 0010               | E      | 2: 60" RCP @ UPRR                 | 50             | 668           | CPPD145       | PIT3SC         | 0.54             | 1.50                       |
| 0012               | E      | Rip Rap Chnl 18'W 4.3'D 2:1 SS    | 300            | 668           | CPPD145       | PIT3SC         | 0.54             | 3.30                       |
| 0018               | E      | 9' X 4' RCBC @ Las Palmas         | 100            | 668           | CPPD145       | PIT3SC         | 0.54             | 0.90                       |
| 0020               | E      | Rip Rap Chnl 18'W 4.3'D 2:1 SS    | 2275           | 668           | CPPD145       | PIT3SC         | 1.00             | 3.60                       |
| 0063               | E      | 72* RCP                           | 1650           | 556           | PPD130        | PIT3SC         | 0.40             | 2.80                       |
| PTRR               | 1230   | PITTMAN RAILROAD                  | 100000         | 1             | 510/92304     |                |                  |                            |
| 0000               | P2     | 14' X 8' RCB                      | 1070           | 1092          | CPPD110       | PIT3SC         | 1.57             | 1.40                       |
| 0020               | P2     | Conc Chnl 14'W 6'D 0:1 SS         | 890            | 1092          | CPPD110       | PIT3SC         | 1.57             | 3.00                       |
| 0027               | P2     | 14' X 8' RCB                      | 850            | 1092          | CPPD110       | PIT3SC         | 1.57             | 1.20                       |
| 0035               | P2     | Conc Chnl 10'W 6'D 2:1 SS         | 5350           | 1092          | CPPD110       | PIT3SC         | 1.57             | 1.20                       |
| 0115               | P2     | 12' X 6' RCB                      | 100            | 563           | CPPD090       | PIT3SC         | 0.81             | 1.30                       |
| 0116               | P2     | Conc Chnl 10'W 5'D 2:1 SS         | 3850           | 563           | CPPD090       | PIT3SC         | 0.81             | 0.80                       |
| PTVW               |        | PITTMAN WASH - VAN WAGENEN        | 1              |               |               |                |                  |                            |
| 0000               | P1     | Conc Chnl 25'W 6'D 2:1 SS         | 1460           | 2848          | CPBR090       | PIT3           | 3.19             | 1.50                       |
| 0025               | E      | 12' X 8' RCB                      | 1650           | 1160          | CPBR030       | PIT3SC         | 1.07             | 1.00                       |
| 0055               | E      | 12' X 6' RCB                      | 2770           | 840           | CPBR020       | PIT3SC         | 0.07             | 1.00                       |
| 0107               | E      | 96* RCP                           | 1260           | 840           | CPBR020       | PIT3           | 0.71             | 0.85                       |
| 0130               | E      | 90° RCP                           | 750            | 840           | CPBR020       | PIT3           | 0.71             | 1.07                       |
| 0144               | E      | 8' X 5' RCBC @ Commercial Way     | 70             | 840           | CPBR020       | PIT3           | 0.71             | 1.32                       |
| 0145               | E      | 84" RCP                           | 620            | 553           | CPBR010       | PIT3           | 3.46             | 1.32                       |
| 0157               | Ε      | 90* RCP                           | 300            | 553           | CPBR010       | PIT3           | 0.46             | 1.29                       |
| 0163               | 8      | 72* RCP                           | 2030           | 444           | PTVW0185      | PIT3SC         | 7.66             | 0.95                       |
| 0180               | E      | 60° RCP                           | 510            | 444           | PTVW0185      | PIT3SC         | 7.66             | 0.28                       |
| 0183               | E      | 60" RCP Outlet                    | 150            | 444           | PTVW0185      | PIT3           | 7.66             |                            |
| 0184               | E      | 35,500 ds PMF Spillway            |                | 35500         | CPPD190       | PIT3           | 7.66             |                            |
| 0185               | E      | 390 ac-ft Pioneer Detention Basin |                | 5857          | CPPD190       | PIT3           | 7.66             |                            |
| 0186               | E      | 6 Span Bridge 120'W 7'D @ UPRR    | 20             | 5857          | CPPD190       | PIT3           | 7.66             | 1.30                       |
| PTWH               |        | PITTMAN WEST HORIZON              | 100            |               | Service and   |                | -24              | 1000                       |
| 0000               | P1     | Conc Chnl 12'W 5'D 2:1 SS         | 500            | 1365          | CPPD045       | PIT3           | 1.17             | 4.00                       |
| 0010               | P1     | 12' X 6' RCBC @ Horizon Dr        | 50             | 1365          | CPPD045       | PIT3           | 1.17             | 4.00                       |
| 0011               | P1     | Conc Chnl 12'W 5'D 2:1 SS         | 6300           | 1365          | CPPD045       | PIT3           | 1.17             | 4.10                       |
|                    |        |                                   |                |               |               |                |                  |                            |
|                    |        |                                   |                |               |               |                |                  |                            |
|                    |        |                                   |                |               |               |                |                  |                            |

...RCB

...RCP

### FLOOD CONTROL FACILITIES INVENTORY TO ACCOMPANY FIGURE 2

\*The HEC-1 node shown identifies the controlling concentration point for the associated facility and is located upstream of this facility due to decreasing peak flow with increasing tributary area caused by storm distribution transitions, depth area reduction factors, or attenuation of flow from routing.

\*\*As-built or design slopes were used when available. All other slopes are based on existing topography. The user should verify the facility slope listed prior to performing any facility specific analysis.



2002 LAS VEGAS VALLEY FLOOD CONTROL MASTER PLAN UPDATE FACILITY INVENTORY FIGURE F-22

| L   | Street Name Designator AA BB | Existing FacilityE             |                   | Construction                                     | Features                   |
|-----|------------------------------|--------------------------------|-------------------|--|----------------------------|
| E   | Parent Stream Name           | Proposed or Modified FacilityP | Bottom WidthW     | Cast in Place Concrete PipeCIPCP                 | Reinforced Concrete Box    |
| G   | Stream Name                  | Contingency Level              |                   | Corrugated Metal Arch Pipe Culvert               | Reinforced Concrete Box Cu |
| E   | ID / River Mile 00 00        | Category BP0                   | DepthD            | Corrugated Metal Pipe Culvert                    | Reinforced Concrete Pipe   |
| AI. | Distance above confluence    | Master PlanP1                  |                   | High Density Polyethylene HDPE                   | Reinforced Concrete Pipe C |
| N   | With parent stream           | Preliminary DesignP2           | Side Slope, H:VSS | Helical Elliptical Reinforced Concrete PipeHERCP | Storm Sewer Pipe           |
| D   | Miles in tenths              | Design P3                      |                   | Reinforced Concrete Arch PipeRCAC                | cioni conor i ponimina     |



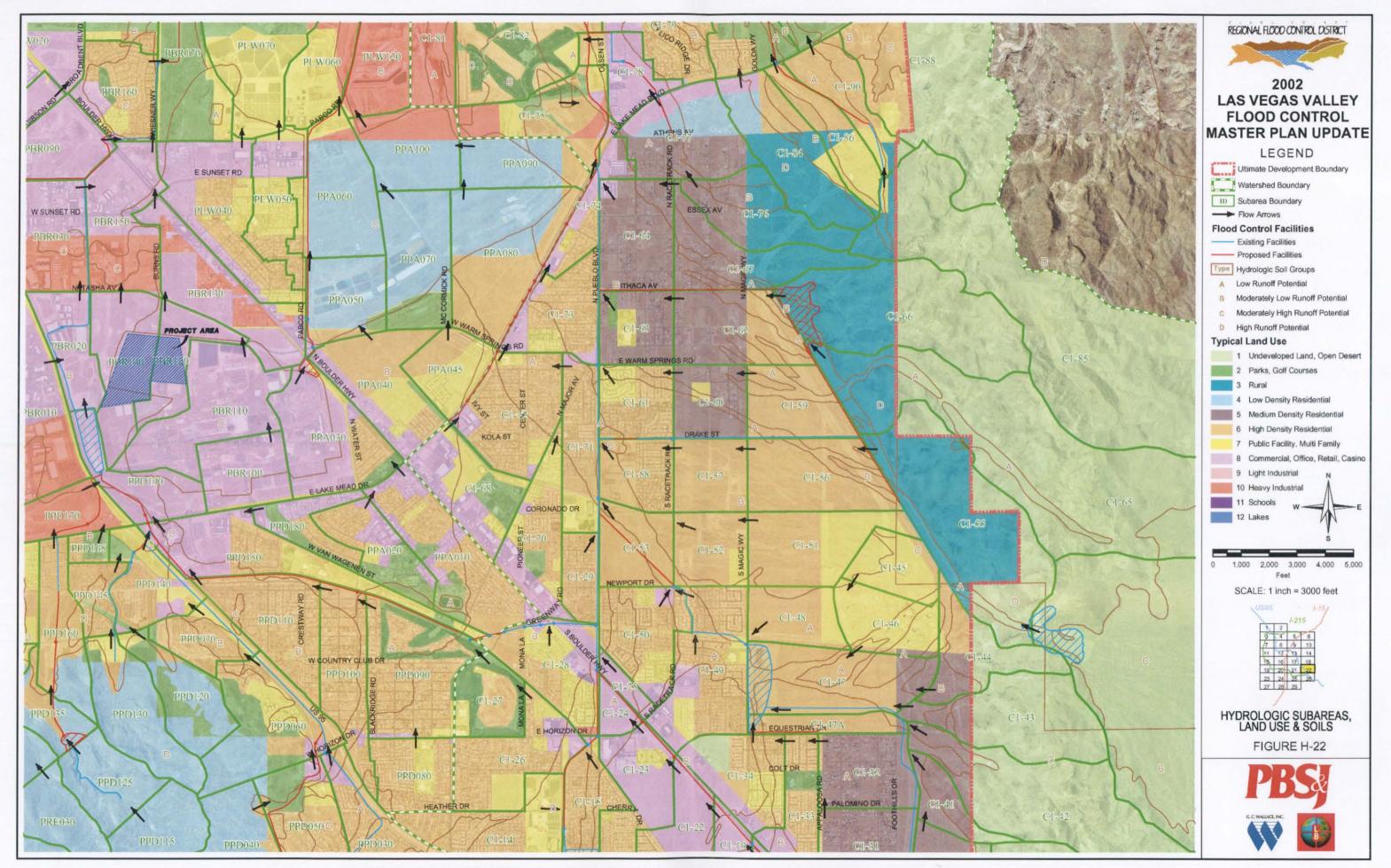


FIGURE 2A: HYDROLOGIC SUBAREAS LAND USE & SOILS MAP

120 | figures dwn Sen 21 2006 - 3: 35pm

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Appendix B: Hydrologic Calculations

Appendix B-1: Existing Condition Hydrology

|  |                     |          |        |                   | HY           | DROLC                            | GIC C       | RITER            | IA AND                          | DRAINAG              | E DESIG                       | N MANU                        | AL                |              |             |                            |         |
|--|---------------------|----------|--------|-------------------|--------------|----------------------------------|-------------|------------------|---------------------------------|----------------------|-------------------------------|-------------------------------|-------------------|--------------|-------------|----------------------------|---------|
| PBS&J<br>File: TD  | S-Standard          | d Form 4 | .xls   |                   |              |                                  |             |                  |                                 | LANDFILL             | gy                            |                               |                   | BY:<br>DATE: |             | KP 10/5/00                 | 6       |
| SUB-BASIN<br>DATA  |                     |          |        |                   |              | INITI                            | AL / OVERL  | AND              |                                 | TRAVEL TIME (Tt)     |                               |                               |                   | Тс           | Tc<br>Check | Tlag                       | REMARKS |
| DESIG:   | DEV/UN.<br>(D or U) | CN       | K (2)  | AREA<br>Ac<br>(3) | AREA<br>Mi^2 | INITIAL<br>LENGTH<br>Feet<br>(4) | SLOPE % (5) | Ti<br>Min<br>(6) | TRAVEL<br>LENGTH<br>Feet<br>(7) | SLOPE<br>%<br>(8)    | V1<br>VELOCITY<br>FPS<br>(9a) | V2<br>VELOCITY<br>FPS<br>(9b) | Tt<br>Min<br>(10) | Min<br>(13)  | Min (14)    | Tlag=<br>0.6Tc/60<br>Hours |         |
| ONEX1  | U                   | 81.9     | 0.6911 | 32.76             | 0.0512       | 252                              | 4.0         | 7.4              | 2082                            | 1.4                  | 1.78                          | 3.5                           | 12.2              | 19.5         | N/A         | 0.20                       |         |
| ONEX2  | U                   | 86.7     | 0.7544 | 28.77             | 0.0450       | 300                              | 5.0         | 6.3              | 2415                            | 0.8                  | 1.35                          | 2.7                           | 18.1              | 24.4         | N/A         | 0.24                       |         |
| ONEX3  | U                   | 91.0     | 0.8112 | 22.12             | 0.0346       | 200                              | 2.5         | 5.4              | 711                             | 3.0                  | 2.56                          | 5.1                           | 3.9               | 9.4          | N/A         | 0.09                       |         |
| ONEX4  | U                   | 87.3     | 0.7624 | 28.27             | 0.0442       | 300                              | 4.8         | 6.2              | 1751                            | 1.5                  | 1.82                          | 3.6                           | 10.4              | 16.6         | N/A         | 0.17                       |         |
| ONEX5  | U                   | 91.0     | 0.8112 | 1.06              | 0.0017       | 50                               | 1.3         | 3.4              | 453                             | 1.9                  | 2.05                          | 4.1                           | 3.7               | 7.0          | N/A         | 0.07                       |         |
| OFFEX1   | U                   | 77.6     | 0.6343 | 42.20             | 0.0659       | 278                              | 2.5         | 10.3             | 2213                            | 2.0                  | 2.09                          | 4.1                           | 10.9              | 21.1         | N/A         | 0.21                       |         |
| OFFEX2   | U                   | 78.5     | 0.6462 | 9.63              | 0.0150       | 195                              | 3.6         | 7.4              | 942                             | 1.8                  | 1.99                          | 3.9                           | 6,1               | 13.5         | N/A         | 0.14                       |         |
| OFFEX3   | U                   | 82.0     | 0.6924 | 16.40             | 0.0256       | 300                              | 0.3         | 18.3             | 1245                            | 1.7                  | 1.92                          | 3.8                           | 7.6               | 25.9         | N/A         | 0.26                       |         |
| OFFEX4   | U                   | 85.0     | 0.7320 | 7.61              | 0.0119       | 300                              | 1.0         | 11.5             | 750                             | 1.9                  | 2.02                          | 4.0                           | 5.2               | 16.6         | N/A         | 0.17                       |         |
| OFFEX5   | U                   | 85.0     | 0.7320 | 5.11              | 0.0080       | 300                              | 1.3         | 10.4             | 625                             | 1.6                  | 1.87                          | 3.7                           | 5.0               | 15.4         | N/A         | 0.15                       |         |
| Tc = Ti + Tt         Eqn. 601         For the travel time (Tt) calculations (Sec. 602.1),         Undeveloped         V1 = 14.8*(\$/100)^41/2           Ti = 1.8 (1.1 - K) L^4/2 / \$^1/3         Eqn. 602         V1 applies to the first 500 feet of travel distance;         Undeveloped         V2 = 29.4*(\$/100)^41/2           K = 0.0132 (CN) - 0.39         Eqn. 603         V2 applies to the remaining travel distance.         Undeveloped         V2 = 29.4*(\$/100)^41/2           Tc Check = L/180+10         Eqn. 604         Min Tc = 10 mins for undeveloped basins           Tt = 500/V1+ (Travel Length-500)/V2         Min Tc = 5 mins for developed basins |                     |          |        |                   |              |                                  |             |                  |                                 | Developed  Developed | V1 = 20.2*(S<br>V2 = 30.6*(S  |                               |                   |              |             |                            |         |
| REFER  | ENCE:               |          |        |                   |              |                                  |             |                  |                                 |                      |                               |                               |                   | STAND        | ARD FORM    | 4                          |         |

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 050CT06 TIME 19:48:16

U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKR- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRANT7 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUMMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ INFESTED SAT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

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HEC-1 INPUT
                                                                                                                                                                                            PAGE 1
                                          ID.....1....2.....3.....4.....5.....6.....7.....8......9.....10
*** FREE ***
                                           *DIAGRAM
                                                    EASTSIDE LANDFILL IMPROVEMENTS
                                          ID ID ID ID IT IN IO JR
                                                    EASTSIDE LANDFILL IMPROVEMENTS
EXISTING CONDITION MODEL
INPUT FILE = EXISTING_SDN3.DAT
SEPTEMBER 2006
DESIGN STORM = 100-YEAR 6-HR STORM
STORM DISTRIBUTION = SDN #3
MODELED BY PBS&J
                                                                     0
                                                                                  0
                                                                                              300
                    10
                                                    PREC
                                                               1.00 0.60
                                                                                             0.58
                                                ONEX1
EXISTING ONSITE BASIN
0.0512
2.79
.000 .020 .057
.130 .130 .130
.190 .197 .199
                    13
14
15
16
17
18
19
20
21
22
23
24
25
26
                                          KK
KM
BA
PC
PC
PC
PC
PC
PC
PC
PC
PC
                                                                   .020
.130
.197
.256
.590
                                                                               .057
.130
.199
.270
.710
.876
.987
                                                                                              .070
.133
.200
.278
.744
                                                                                                                         .108
.142
.204
.283
.812
                                                                                                                                                    .130
.158
.229
.322
.835
                                                                                                            .087
.140
.201
.281
                                                                                                                                       .124
.148
.214
.295
.819
.937
                                                     .251
                                                     .860
                                                                                               888
                                                                 .985
.999
81.9
                                                     .982
                                                                                              .989
                                                    0.20
                    27
28
29
30
31
                                                OFFEX1
                                                EXISTING OFFSITE BASIN
0.0659
0 77.6
                                          KKROFF1-ON1
KM ROUTE OFFEX1 FLOW TO CP-1
RK 2250 0.016 0.030
                    32
33
34
                                          KM
RK
                    35
36
37
                                                   EXISTING OFFSITE BASIN
.0150
0 78.5
                                          KM
BA
LS
                    38
                                                                                             HEC-1 INPUT
                                                                                                                                                                                            PAGE 2
                 LINE
                                          ID.....1.....2......3......4......5......6......7.....8......9.....10
                                          KKROFF2-CP1
KM ROUTE OFFEX2 FLOW TO CP-1
RK 2070 0.020 0.030 0 TRAP
                    40
41
42
                                                                                                                       15
                                                                                                                                        3
                    43
44
45
                                                  CP-1
COMBINE ONEX1 AND OFFEX1
                                          KM
HC
*
                     46
47
48
                                           KKRCP1-C18
                                          KM ROUTE CP-1 FLOW TO C18
RK 705 0.008 0.030
                                                                                                                                     3
                                                                                                0 TRAP 20
                                           Referenced from PBSJ

"Addendum #1 to the Technical Drainage Study for Henderson Commmerce
Center Two (Formerly known as HARSCH)" (February 2003)
                                          KK OPFD-14
KM OPSITE DEVELOPED BASIN OPFD-14
KM REPERENCED FROM EG02
BA 0.0028
PB 2.79
LS 0 88
                     49
50
51
52
53
54
```

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55
                                              UD 0.200
                                              KK RT-B14

KM ROUTE OFFD-14 THROUGH BMIC-1

RK 1050 0.014 0.013 0 TRAP
       56
57
58
                                                                                                                                                                                           15
                                                                                                                                                                                                                      10
                                              KK BMIC-1
KM ONSITE DEVELOPED BASIN BMIC-1
KM REFERENCED FROM EG02
       59
60
61
62
63
64
65
                                               KM
KM
BA
PB
LS
UD
                                                          0.0141
2.79
0
                                                                                                 92
                                                              0.081
                                                           C15
COMBINE RT-B14 AND BMIC-1
                                                                                                                                           HEC-1 INPUT
                                                                                                                                                                                                                                                                                                                              PAGE 3
LINE
                                              ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
                                                          RT-14
ROUTE C15 THROUGH BMIC-2
450 0.018 0.013
       69
70
71
                                                                                                                                                   O TRAD
                                                                                                                                                                                              15
                                                                                                                                                                                                                      10
                                              KK BMIC-2
KM ONSITE DEVELOPED BASIN BMIC-2
KM REFERENCED FROM EG02
BA 0.0118
PB 2.79
LS 0 92
UD 0.073
                                             KK
KM
HC
*
                                                             C16
COMBINE RT-14 AND BMIC-2
      79
80
81
      82
83
84
                                                           RT-15
ROUTE C16 THROUGH SCH-2
400 0.019 0.013
                                                                                                                                                                                             15 10
                                                                                                                                                    0 TRAP
                                                         SCH-2

ONSITE DEVELOPED BASIN SCH-2

REFERENCED FROM EG02

0.0065

2.79

0 92

0.060
                                              KK
KM
KM
BA
PB
LS
UD
       92
93
94
                                                             C17
COMBINE RT-15 AND SCH-2
                                                            RT-16
ROUTE C17 THROUGH BMIC-3
750 0.013 0.013 0 TRAP 15
      95
96
97
                                                                                                                                                                                                                               10
                                              KK BMIC-3
KM ONSITE DEVELOPED BASIN BMIC-3
KM REPERENCED FROM EG02
BA 0.0106
PB 2.79
LS 0 92
UD 0.062
                                                                                                                                           HEC-1 INPUT
                                                                                                                                                                                                                                                                                                                             PAGE 4
LINE
                                              ID.....1....2....3....4.....5....6.....7....8.....9.....10
                                            KK MGDEV-2
KM MILGARD MANUFACTURING ONSITE BASIN
KM REFERENCED FROM EG02
BA 0.0093
PB 2.79
LS 0 92
UD 0.075
*
                                               KK
KM
HC
*
                                                           C18
COMBINE RT-16, BMIC-3, MGDEV-2 AND CP-1
                                             KK
KM
BA
PB
LS
UD
                                                             ONEX2
                                                           EXISTING ONSITE BASIN
   116
117
118
119
120
                                                             .0450
2.79
0
0.24
                                              Referenced from PBSJ
*Addendum #1 to the Technical Drainage Contact Technic
                                              * *Addendum #1 to the Technical Drainage Study for Henderson Commmerce * Center Two (Formerly known as HARSH)* (February 2003)
                                              KK HR3

KM HARSCH ONSITE BASIN

BA 0.0014

PB 2.79

LS 0 92

UD 0.049
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HR2
HARSCH ONSITE BASIN
0.0016
2.79
                                           KK
KM
BA
PB
LS
UD
                    133
134
135
136
137
138
                                                HR1
HARSCH ONSITE BASIN
0.0015
2.79
                                           KK
KM
BA
PB
LS
UD
                                                    0.05
                                                                      92
                                                                                            HEC-1 INPUT
                                                                                                                                                                                          PAGE 5
                  LINE
                                           {\tt ID},\ldots,1,\ldots,2,\ldots,3,\ldots,4,\ldots,5,\ldots,6,\ldots,7,\ldots,8,\ldots,9,\ldots,10
                                           KK CHRI
KM COMBINE HR3, HR2, HR1
KM THESE FLOWS ARE DISCHARGED INTO THE ONSITE
KM STORM DRAIN SYSTEM LABELED ALIGNMENT "H1"
KM ON FIGURE 7
HC 3
*
                    139
140
141
142
143
144
                                                  C18B
COMBINE C18, CHR1 AND ONEX2
3
                    145
146
147
                                                   ONEX4
EXISTING ONSITE BASIN
.0442
2.79
0 87.3
0.17
                                                 OFFEX5
EXISTING OFFSITE BASIN
.0080
0 85.0
0.15
                    154
155
156
157
158
                                           KK
KM
BA
LS
UD
                                           KKROFF5-CP3
KM ROUTE OFFEX5 FLOW TO CP-3
RK 1692 0.019 0.030 0 TRAP
                                                                                                                          10
                                                   CP-3
COMBINE ONEX4 AND OFFEX5
2
                                                   ONEX3
EXISTING ONSITE BASIN
.0346
2.79
0 91.0
0.09
                    165
166
167
168
169
170
                                           KK
KM
BA
PB
LS
UD
                                           KK OFFEX4
KM EXISTI
BA .0119
LS 0
UD 0.17
                                                   EXISTING OFFSITE BASIN
.0119
0 85.0
0.17
                                                                                            HEC-1 INPUT
                                                                                                                                                                                       PAGE 6
                  LINE
                                           \texttt{ID},\ldots,1,\ldots,2,\ldots,3,\ldots,4,\ldots,5,\ldots,6,\ldots,7,\ldots,8,\ldots,9,\ldots,10
                    176
177
178
179
180
181
                                                 OFFEX3
EXISTING OFFSITE BASIN
.0256
2.79
                                           KK
KM
BA
PB
LS
UD
*
                                                                  82.0
                                                     0.26
                    182
183
184
185
186
                                           KK
KM
BA
LS
UD
                                                    ONEX5
                                                   EXISTING ONSITE BASIN .0017 0 91.0
                                                   CP-2
COMBINE OFFEX3 AND ONEX5
                                                  FEX3POND

COLLECTS FLOW FROM OFFEX3 AND ONEX5

1 STOR -1
0 0.47 1.37 2.71 4.5
1766 1767 1768 1769 177
0 0.01 0.02 0.03 0.0
                                          KKOFI
KM
RS
SV
SE
SQ
                    190
191
192
193
194
195
                    196
                                          22
1
                      SCHEMATIC DIAGRAM OF STREAM NETWORK
 INPUT
LINE
                    (V) ROUTING (--->) DIVERSION OR PUMP FLOW
                    (.) CONNECTOR
                                                   (<---) RETURN OF DIVERTED OR PUMPED FLOW
      13
                                       OFFEX1
V
V
```

| 32             | 7                   | ROFF1-ON                       |                    |         |          |       |     |
|----------------|---------------------|--------------------------------|--------------------|---------|----------|-------|-----|
| 35             |                     |                                | OFFEX2             |         |          |       |     |
| 40             | *                   |                                | V<br>V<br>ROFF2-CP |         |          |       |     |
|                |                     |                                |                    |         |          |       |     |
| 43             | CP-1<br>V<br>V      |                                |                    |         |          |       |     |
| 46             | RCP1-C18            |                                |                    |         |          |       |     |
| 49             |                     | OFFD-14                        |                    |         |          |       |     |
| 56             |                     | V<br>V<br>RT-B14               |                    |         |          |       |     |
|                |                     | 9                              | mura 1             |         |          |       |     |
| 59             |                     |                                | BMIC-1             |         |          |       |     |
| 66             | *                   | C15.<br>V<br>V                 |                    |         |          |       |     |
| 69             |                     | RT-14                          |                    |         |          |       |     |
| 72             | *                   | :                              | BMIC-2             |         |          |       |     |
| 79             |                     | C16.                           |                    |         |          |       |     |
| 82             |                     | V<br>V<br>RT-15                |                    |         |          |       |     |
|                |                     |                                | SCH-2              |         |          |       |     |
| 85             | *:                  |                                | SCH-2              |         |          |       |     |
| 92             |                     | C17.<br>V                      |                    |         |          |       |     |
| 95             |                     | RT-16                          |                    |         |          |       |     |
| 98             |                     |                                | BMIC-3             |         |          |       |     |
| 105            | 1                   |                                | Ĭ                  | MGDEV-2 |          |       |     |
| 112            | C18                 |                                |                    |         |          |       |     |
|                | **                  |                                |                    |         |          |       |     |
| 115            | - 2                 | ONEX2                          |                    |         |          |       |     |
| 121            | *                   | :                              | HR3                |         |          |       |     |
| 127            |                     | :                              | :                  | HR2     |          |       |     |
| 133            | Y<br>2              |                                |                    | 1       | HR1      |       |     |
| 139            | -                   |                                | CHR1.              |         |          |       |     |
| 145            | C18B                |                                |                    |         |          |       |     |
| 148            |                     | ONEX4                          |                    |         |          |       |     |
|                |                     | ONEAG                          |                    |         |          |       |     |
| 154            |                     |                                | OFFEX5<br>V        |         |          |       |     |
| 159            |                     | 1                              | ROFF5-CP           |         |          |       |     |
| 162            | *                   | CP-3.                          |                    |         |          |       |     |
| 165            | *                   |                                | ONEX3              |         |          |       |     |
| 171            | į.                  |                                | :                  | OFFEX4  |          |       |     |
| 176            | - :                 | 1                              |                    |         | OFFEX3   |       |     |
|                |                     |                                |                    |         |          |       |     |
| 182            |                     | #                              |                    |         |          | ONEX5 |     |
| 187            |                     | į.                             | Ş.                 |         | CP-2.    |       |     |
| 190            | · ×                 |                                | *                  | (*      | OFFEX3PO |       |     |
|                |                     |                                | THIS LOCATIO       | N       |          |       | *** |
| * FLOO         | DD HYDROGRAP<br>JUN | PH PACKAGE<br>1 1998<br>NN 4.1 | (HEC-1) *          |         |          |       | *   |
| *     * RIIN T | VERSIO              |                                | 9:48:16 *          |         |          |       | :   |
| *              |                     |                                | *******            |         |          |       | *** |
|                |                     |                                |                    |         |          |       |     |

U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

EXISTING CONDITION MODEL
INPUT FILE = EXISTING\_SDN3.DAT
SEPTEMBER 2006
DESIGN STORM = 100-YEAR 6-HR STORM
STORM DISTRIBUTION = SDN #3
MODELED BY PBS6J

11 10

OUTPUT CONTROL VARIABLES

IPENT 5 PRINT CONTROL

IPLOT 0 PLOT CONTROL

QSCAL 0. HYDROGRAPH PLOT SCALE

Tip

COMPUTATION INTERVAL .08 HOURS TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
DRAINAGE AREA
PRECIPITATION DEPTH
LENGTH, ELEVATION
FLOW
STORAGE VOLUME
SURFACE AREA
TEMPERATURE

SQUARE MILES INCHES FEET CUBIC FEET PER SECOND ACRE-FEET ACRES DEGREES FAHRENHEIT

MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS JP

1

MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
1.00 .60 .58

\*\*\* FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES TIME TO PEAK IN HOURS

RATIOS APPLIED TO PRECIPITATION

| OPERATION       | STATION  | AREA | PLAN |               | RATIO 1<br>1.00 | RATIO 2<br>.60 | RATIO 3     | ECIPITATION |
|-----------------|----------|------|------|---------------|-----------------|----------------|-------------|-------------|
| HYDROGRAPH AT   | ONEX1    | .05  | 1    | FLOW<br>TIME  | 47.<br>3.67     | 17.<br>3.67    | 16.<br>3.67 |             |
| HYDROGRAPH AT + | OFFEX1   | .07  | 1    | FLOW<br>TIME  | 48.<br>3.67     | 14.<br>3.67    | 13.<br>3.67 |             |
| ROUTED TO       |          |      |      |               | 47.<br>3.75     |                |             |             |
| HYDROGRAPH AT   |          |      |      | FLOW<br>TIME  | 13.<br>3.58     | 4.<br>3.58     | 4.<br>3.58  |             |
| ROUTED TO       | ROFF2-CP | .01  | 1    | FLOW<br>TIME  | 13.<br>3.67     | 4.<br>3.75     | 4.<br>3.75  |             |
| 3 COMBINED AT   | CP-1     | .13  | 1    | FLOW<br>TIME  | 105.<br>3.67    | 33.<br>3.75    | 30.<br>3.75 |             |
| ROUTED TO       | RCP1-C18 | .13  | 1    | FLOW<br>TIME  | 101.<br>3.67    | 32.<br>3.75    | 29.<br>3.83 |             |
| HYDROGRAPH AT + | OFFD-14  | .00  | 1    | FL/OW<br>TIME | 3.<br>3.58      | 2.<br>3.67     | 1.<br>3.67  |             |
| ROUTED TO       |          |      |      |               | 3.              |                |             |             |
| HYDROGRAPH AT   | BMIC-1   | .01  | 1    | FLOW<br>TIME  | 26.<br>3.50     | 13.<br>3.50    | 12.<br>3.50 |             |
| 2 COMBINED AT   | C15      | .02  | 1    | FLOW<br>TIME  | 28.<br>3.50     | 14.<br>3.50    | 13.<br>3.50 |             |
| ROUTED TO       | RT-14    | .02  | 1    | FLOW<br>TIME  | 27.<br>3.50     | 13.<br>3.50    | 13.<br>3.50 |             |
| HYDROGRAPH AT   | BMIC-2   | .01  | 1    | FLOW<br>TIME  | 22.<br>3.50     | 11.<br>3.50    | 11.<br>3.50 |             |
| 2 COMBINED AT   | C16      | .03  | 1    | FLOW<br>TIME  | 50.<br>3.50     | 25.<br>3.50    | 24.<br>3.50 |             |
| ROUTED TO       | RT-15    | .03  | 1    | FLOW<br>TIME  | 49.<br>3.50     | 24.<br>3.50    | 23.<br>3.50 |             |
| HYDROGRAPH AT   | SCH-2    | .01  | 1    | FLOW<br>TIME  | 13.<br>3.50     | 7.<br>3.50     | 6.<br>3.50  |             |
|                 |          |      |      |               |                 |                |             |             |

| 2 COMBINED      | C17                                | .04             | 1    | FLOW<br>TIME | 61.<br>3.50                     | 31.<br>3.50       | 29.<br>3.50 |              |                     |                   |        |   |
|-----------------|------------------------------------|-----------------|------|--------------|---------------------------------|-------------------|-------------|--------------|---------------------|-------------------|--------|---|
| ROUTED TO       | RT-16                              | .04             | 1    | FLOW<br>TIME | 59.<br>3.50                     | 29.<br>3.50       | 27.<br>3.50 |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT<br>BMIC-3                       | .01             | 1    | FLOW<br>TIME | 21.<br>3.50                     | 11.<br>3.50       | 10.<br>3.50 |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT<br>MGDEV-2                      | .01             | 1    | FLOW<br>TIME | 17.<br>3.50                     | 9.<br>3.50        | 8.<br>3.50  |              |                     |                   |        |   |
| 4 COMBINE       | O AT                               | .19             | 1    | FLOW<br>TIME | 162.<br>3.58                    | 57.<br>3.58       | 53.<br>3.50 |              |                     |                   |        |   |
| HYDROGRAPH      | AT ONEX2                           | .05             | 1    | FLOW<br>TIME | 49.<br>3.67                     | 21.<br>3.67       | 20.<br>3.67 |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT HR3                             | .00             | 1    | FLOW<br>TIME | 3.<br>3.50                      | 1.                | 1.<br>3.50  |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT<br>HR2                          | .00             | 1    | FLOW<br>TIME | 4.<br>3.50                      | 2.<br>3.50        | 2.<br>3.50  |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT HR1                             | .00             | 1    | FLOW<br>TIME | 3.<br>3.50                      | 2.<br>3.50        | 2.<br>3.50  |              |                     |                   |        |   |
| 3 COMBINED      | O AT CHR1                          | .00             | 1    | FLOW<br>TIME | 10.<br>3.50                     | 5.<br>3.50        | 5.<br>3.50  |              |                     |                   |        |   |
| 3 COMBINED      | O AT C18B                          | .24             | 1    | FLOW<br>TIME | 212.<br>3.58                    | 78.<br>3.67       | 73.<br>3.58 |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT ONEX4                           | .04             | 1    | FLOW<br>TIME | 56.<br>3.58                     | 25.<br>3.58       | 23.<br>3.58 |              |                     |                   |        |   |
| HYDROGRAPH      | AT OFFEX5                          | .01             | 1    | FLOW<br>TIME | 10.                             | 4.                | 4.          |              |                     |                   |        |   |
| ROUTED TO       | ROFF5-CP                           | .01             | 1    | FLOW<br>TIME | 9.<br>3.67                      | 4.<br>3.67        | 3.<br>3.67  |              |                     |                   |        |   |
| 2 COMBINED      | O AT CP-3                          | .05             | 1    | FLOW<br>TIME | 65.<br>3.58                     | 27.<br>3.58       | 26.<br>3.58 |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT ONEX3                           | .03             | 1    | FLOW<br>TIME | 59.<br>3.50                     | 29.<br>3.50       | 28.<br>3.50 |              |                     |                   |        |   |
| HYDROGRAPH      | AT OFFEX4                          | .01             | 1    | FLOW         | 14.                             | 6.                | 5.          |              |                     |                   |        |   |
| HYDROGRAPH<br>+ | AT OFFEX3                          | .03             | 1    | TIME         | 3.58                            | 8.                | 7.          |              |                     |                   |        |   |
| HYDROGRAPH      | AT ONEX5                           | ,00             | 1    | TIME         | 3.67                            | 3.75              | 3.75        |              |                     |                   |        |   |
| 2 COMBINED      | O AT CP-2                          | .03             | 1    | TIME         | 3.50                            | 3.50              | 3.50        |              |                     |                   |        |   |
| ROUTED TO       | OFFEX3PO                           | .03             | 1    | TIME         | 0.                              | 3.75              | 3.75        |              |                     |                   |        |   |
|                 |                                    |                 | **   | STAGE        | 5.92<br>AGES IN FEET<br>1768.34 | 1767.24           | 1767.18     |              |                     |                   |        |   |
| 1               |                                    |                 |      | TIME         | Y OF KINEMAT                    | 6.58<br>IC WAVE - | MUSKINGU    | M-CUNGE ROUT | ING                 |                   |        |   |
|                 | ISTAQ ELEMENT                      | DT              |      | PEAK         | LOW IS DIRECT                   | VOLUME            | WITHOUT B.  | INTERPOL     | INTERVAL<br>TIME TO |                   |        |   |
|                 |                                    | (MIN)           |      | (CFS)        | PEAK<br>(MIN)                   | (IN)              | (MIN)       | (CFS)        | PEAK<br>(MIN)       | (IN)              |        |   |
| I               | OR PLAN = 1 RATI                   | O= 1.00<br>2.18 |      | 46.96        | 222.91                          | .96               | 5.00        | 46.94        | 225.00              | .96               |        |   |
| CONTINUITY      | SUMMARY (AC-FT) -                  | INFLOW=         | .337 | 75E+01 E     | XCESS= .0000                    | E+00 OUTF         | LOW= .338   | 0E+01 BASIN  | STORAGE=            | .3651E-05 PERCENT | ERROR= | 2 |
|                 | FOR PLAN = 1 RATI                  | O= .60<br>3.08  |      | 13.76        | 228.58                          | .30               | 5.00        | 13.59        | 230.00              | .30               |        |   |
| CONTINUITY      | SUMMARY (AC-FT) -                  | INFLOW=         | .106 | 51E+01 E     | XCESS= .0000                    | E+00 OUTF         | LOW= .106   | 5E+01 BASIN  | STORAGE=            | .3304E-05 PERCENT | ERROR= | 4 |
|                 | FOR PLAN = 1 RATI                  | 0= .58<br>3.12  |      | 12.50        | 227.50                          | .28               | 5.00        | 12.40        | 230.00              | .28               |        |   |
| CONTINUITY      | SUMMARY (AC-FT) -                  | INFLOW=         | .969 | 6E+00 E      | XCESS= .0000                    | E+00 OUTF         | LOW= .973   | 3E+00 BASIN  | STORAGE=            | ,3663E-05 PERCENT | ERROR= | 4 |
| 1               | FOR PLAN = 1 RATI<br>ROFF2-CP MANE | 0= 1.00<br>2.57 |      | 13.17        | 219.45                          | 1,01              | 5.00        | 13.07        | 220.00              | 1.01              |        |   |
|                 |                                    |                 |      |              |                                 |                   |             |              |                     |                   |        |   |

| CONTINUITY SUMMARY   | (AC-FT) - INF  | FLOW= .   | .8075E+00  | EXCESS=  | .0000E+00  | OUTFLOW=   | .8108E+00   | BASIN   | STORAGE=   | .2611E-05 PE  | RCENT 1 | ERROR=                         | 4    |
|--|--|---|--|--|--|--|---|---|--|---|---------|--------------------------------|------|
| FOR PLAN<br>ROFF2-CH   | N = 1 RATIO=<br>MANE   | .60<br>3.75   | 3.97   | 225.   | 11   | .33  | 5.00  | 3.97  | 225.00   | .33   |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | FLOW= .   | .2625E+00  | EXCESS=  | .0000E+00  | OUTFLOW=   | .2649E+00   | BASIN   | STORAGE=   | .1921E-05 PE  | RCENT 1 | ERROR=                         | 9    |
| FOR PLAN<br>ROFFZ-CE   | 1 = 1 RATIO=<br>MANE   | .58<br>3.93   | 3.71   | 222.   | 59   | .30  | 5.00  | 3.61  | 225.00   | .30   |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | LOW= .  | .2406E+00  | EXCESS=  | .0000E+00  | OUTFLOW=   | .2435E+00   | BASIN   | STORAGE=   | .2215E-05 PE  | RCENT I | ERROR=                         | -1.2 |
| FOR PLAN   | 1 = 1 RATIO= 1<br>MANE   | .00   | 104.64   | 221.   | 47 1   | .06  | 5.00 10   | 1.21  | 220.00   | 1.07  |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | LOW= .  | 7492E+01   | EXCESS=  | .0000E+00  | OUTFLOW=   | .7497E+01   | BASIN   | STORAGE=   | .6376E-05 PE  | RCENT I | ERROR=                         | 1    |
| FOR PLAN   | = 1 RATIO=<br>MANE   | .60<br>1.09   | 32.76  | 226.   | 76   | .36  | 5.00 3  | 1.80  | 225.00   | .36   |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | LOW= .  | 2533E+01   | EXCESS=  | .0000E+00  | OUTFLOW=   | .2534E+01   | BASIN   | STORAGE=   | .6774E-05 PE  | RCENT H | ERROR=                         | .0   |
| FOR PLAN<br>RCP1-C18   |  | .58<br>1.10   | 29.80  | 226.   | 94   | .33  | 5.00 2  | 8,60  | 230.00   | .33   |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | LOW= .  | 2330E+01   | EXCESS=  | .0000E+00  | OUTFLOW=   | .2331E+01   | BASIN   | STORAGE=   | .6358E-05 PE  | RCENT E | ERROR=                         | .0   |
|  | = 1 RATIO= 1<br>  MANE   | .00   | 3.39   | 218.   | 69 1   | . 64   | 5.00  | 3.37  | 220.00   | 1.63  |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | LOW= .  | 2438E+00   | EXCESS=  | .0000E+00  | OUTFLOW=   | .2442E+00   | BASIN   | STORAGE=   | .7570E-08 PE  | RCENT E | ERROR=                         | -,2  |
|  | = 1 RATIO=<br>MANE   | .60<br>1.71   | 1.51   | 223.   | 43   | .71  | 5.00  | 1.50  | 220.00   | .71   |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | LOW= .  | 1061E+00   | EXCESS=  | .0000E+00  | OUTFLOW=   | .1063E+00   | BASIN   | STORAGE=   | .7638E-08 PE  | RCENT E | ERROR=                         | 2    |
|  | = 1 RATIO=<br>MANE   | .58<br>1.76   | 1.42   | 222.   | 80   | . 67   | 5.00  | 1.41  | 220.00   | .67   |         |                                |      |
| CONTINUITY SUMMARY   | (AC-FT) - INF  | LOW= .  | 9979E-01   | EXCESS=  | .0000E+00  | OUTFLOW=   | .9993E-01   | BASIN   | STORAGE=   | .5886E-08 PE  | RCENT E | ERROR=                         | -,1  |
| FOR PLAN   |  | 200   |  |  |  |  |   |   |  |   |         |                                |      |
|  | = 1 RATIO= 1<br>MANE   | .37   | 27.93  | 210.   | 77 1   | .91  | 5.00 2  | 7.32  | 210.00   | 1.91  |         |                                |      |
|  | MANE   | .37   |  |  |  |  |   |   |  |   | RCENT F | ERROR=                         | .0   |
| RT-14 CONTINUITY SUMMARY FOR PLAN  | MANE   | .37<br>LOW= .   |  | EXCESS=  | .0000E+00  | OUTFLOW=   | .1721E+01   |   |  |   | RCENT F | ERROR=                         | .0   |
| RT-14 CONTINUITY SUMMARY FOR PLAN  | MANE  (AC-FT) - INF  = 1 RATIO= MANE   | .37<br>LOW= .<br>.60<br>.42   | 1720E+01   | EXCESS=  | .0000E+00  | OUTFLOW=   | .1721E+01<br>5.00 1   | BASIN   | STORAGE=   | .7751E-08 PE  |         |                                | .0   |
| RT-14 CONTINUITY SUMMARY FOR PLAN RT-14 CONTINUITY SUMMARY FOR PLAN  | MANE  (AC-FT) - INF  = 1 RATIO= MANE   | .37 *LOW=60 .42 *LOW= .   | 1720E+01   | EXCESS= 211. EXCESS=   | .0000E+00  | OUTFLOW=   | .1721E+01<br>5.00 1<br>.8205E+00  | BASIN   | STORAGE=   | .7751E-08 PE  |         |                                |      |
| RT-14 CONTINUITY SUMMARY FOR PLAN RT-14 CONTINUITY SUMMARY FOR PLAN  | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE   | .37 "LOW=60 .42 "LOW= .   | 1720E+01<br>13.81<br>8203E+00<br>13.17   | EXCESS=  211.  EXCESS=  210.   | .0000E+00  | OUTFLOW= .91 OUTFLOW=  | .1721E+01 5.00 1 .8205E+00 5.00 1   | BASIN<br>3.40<br>BASIN<br>2.73  | STORAGE= 210.00 STORAGE= 210.00  | .7751E-08 PEI .91 .6549E-08 PEI .86   | RCENT E | ERROR=                         |      |
| RT-14 CONTINUITY SUMMARY  FOR PLAN RT-14 CONTINUITY SUMMARY  FOR PLAN RT-14 CONTINUITY SUMMARY  FOR FLAN   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE   | .37 LOW=60 .42 LOW=58 .41 LOW= .  | 1720E+01<br>13.81<br>8203E+00<br>13.17   | EXCESS=  211.  EXCESS=  210.   | .0000E+00 01 .0000E+00 75  | OUTFLOW= .91 OUTFLOW= .86 OUTFLOW=   | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00   | BASIN<br>3.40<br>BASIN<br>2.73  | STORAGE= 210.00 STORAGE= 210.00  | .7751E-08 PEI .91 .6549E-08 PEI .86   | RCENT E | ERROR=                         | .0   |
| RT-14 CONTINUITY SUMMARY  FOR PLAN RT-14 CONTINUITY SUMMARY  FOR PLAN RT-14 CONTINUITY SUMMARY  FOR FLAN   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE   | .37 *LOW=60 .42 *LOW=58 .41 *LOW= .   | 1720E+01 13.81 8203E+00 13.17 7778E+00 49.16   | EXCESS=  211.  EXCESS=  210.   | .0000E+00 01 .0000E+00 75 .0000E+00  | OUTFLOW= 91 OUTFLOW= .86 OUTFLOW=  | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00   | BASIN 3.40 BASIN 2.73 BASIN 8.56  | STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00  | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI   | RCENT E | ERROR=<br>ERROR=               | .0   |
| CONTINUITY SUMMARY  FOR PLAN  RT-14  CONTINUITY SUMMARY  FOR PLAN  RT-14  CONTINUITY SUMMARY  FOR PLAN  RT-15  CONTINUITY SUMMARY  FOR PLAN  FOR PLAN  FOR PLAN  FOR PLAN  FOR PLAN  FOR PLAN  | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  | .37 LOW=60 .42 LOW=58 .41 LOW=00 .36 LOW= .   | 1720E+01  13.81 8203E+00  13.17 7778E+00  49.16 2959E+01   | EXCESS=  211.  EXCESS=  210.  EXCESS=  210.  | .0000E+00 01 .0000E+00 75 .0000E+00  | OUTFLOW= .86 OUTFLOW= .93 OUTFLOW=   | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01  | BASIN 3.40 BASIN 2.73 BASIN 8.56 BASIN  | STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI   | RCENT E | ERROR=<br>ERROR=               | .0   |
| CONTINUITY SUMMARY  FOR PLAN  RT-14  CONTINUITY SUMMARY  FOR PLAN  RT-14  CONTINUITY SUMMARY  FOR PLAN  RT-15  CONTINUITY SUMMARY  FOR PLAN  FOR PLAN  FOR PLAN  FOR PLAN  FOR PLAN  FOR PLAN  | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  | .37   | 1720E+01  13.81 8203E+00  13.17 7778E+00  49.16 2959E+01  24.51  | EXCESS=  211.  EXCESS=  210.  EXCESS=  210.  | .0000E+00 01 .0000E+00 75 .0000E+00 62 1 .0000E+00                           | OUTFLOW= 91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW=                               | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2   | BASIN 3.40 BASIN 2.73 BASIN 8.56 BASIN 4.04   | STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE=   | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI  | RCENT F | ERROR= ERROR=                  | .0   |
| CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-15   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE   | .37 .37 .37 .37 .37 .37 .37 .37 .37 .37   | 1720E+01  13.81 8203E+00  13.17 7778E+00  49.16 2959E+01  24.51 1419E+01                                 | EXCESS=  211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.                         | .0000E+00 01 .0000E+00 75 .0000E+00 62 1 .0000E+00                           | OUTFLOW= 91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW=                               | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2   | BASIN                                     | STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=   | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI .93  | RCENT F | ERROR= ERROR=                  | .0   |
| CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-15   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE   | .37 .37 .37 .37 .37 .37 .37 .37 .37 .37   | 1720E+01 13.81 8203E+00 13.17 7778E+00 49.16 2959E+01 24.51 1419E+01 23.31                               | EXCESS=  211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.                         | .0000E+00 01 .0000E+00 75 .0000E+00 62 1 .0000E+00 82 .0000E+00              | OUTFLOW= .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .93                          | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2 .1420E+01 5.00 2                            | BASIN 3.40 BASIN 2.73 BASIN 4.04 BASIN BASIN BASIN  | STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=   | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI .93 .8611E-08 PEI                                      | RCENT F | ERROR= ERROR= ERROR=           | .0   |
| CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-15   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF                                | .37  LOW=60 .42  LOW=58 .41  .00 .36  LOW=60 .35  LOW=58 .35                          | 1720E+01 13.81 8203E+00 13.17 7778E+00 49.16 2959E+01 24.51 1419E+01 23.31                               | EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=                | .0000E+00 01 .0000E+00 75 .0000E+00 62 1 .0000E+00 82 .0000E+00              | OUTFLOW= 91 OUTFLOW= 86 OUTFLOW= 93 OUTFLOW= 88 OUTFLOW=                     | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2 .1420E+01 5.00 2                            | BASIN 3.40 BASIN 2.73 BASIN 8.56 BASIN 4.04 BASIN BASIN BASIN BASIN                             | STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI .93 .8611E-08 PEI                                      | RCENT F | ERROR= ERROR= ERROR=           | .0   |
| CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-15   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF                                  | .37  CLOW=60 .42  .58 .41  CLOW=58 .41  CLOW=60 .36  .55 .58 .35  CLOW=60 .55 .58 .35 | 1720E+01 13.81 8203E+00 13.17 7778E+00 49.16 2959E+01 24.51 1419E+01 23.31 1347E+01 60.94                | EXCESS=  211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.          | .0000E+00 01 .0000E+00 75 .0000E+00 82 .0000E+00 84 .0000E+00                | OUTFLOW= 91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .88 OUTFLOW= .88              | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2 .1420E+01 5.00 2 .1347E+01 5.00 5           | BASIN 3.40 BASIN 22.73 BASIN BASIN 4.04 BASIN BASIN BASIN BASIN BASIN BASIN                     | STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI .93 .8611E-08 PEI .88                                  | RCENT F | ERROR= ERROR= ERROR= ERROR=    | .0   |
| CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-16  CONTINUITY SUMMARY  FOR PLAN RT-16  CONTINUITY SUMMARY  FOR PLAN RT-16   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1  MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF | .37  **LOW=   | 1720E+01 13.81 8203E+00 13.17 7778E+00 49.16 2959E+01 24.51 1419E+01 23.31 1347E+01 60.94                | EXCESS=  211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.          | .0000E+00 01 .0000E+00 75 .0000E+00 82 .0000E+00 84 .0000E+00                | OUTFLOW= 91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .88 OUTFLOW= .94 OUTFLOW=     | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2 .1420E+01 5.00 2 .1347E+01 5.00 5           | BASIN 3.40 BASIN 22.73 BASIN BASIN 4.04 BASIN BASIN BASIN BASIN BASIN BASIN                     | STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=  210.00 STORAGE=   | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI .93 .8611E-08 PEI .88 .8421E-08 PEI                    | RCENT F | ERROR= ERROR= ERROR= ERROR=    | .0   |
| CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-16  CONTINUITY SUMMARY  FOR PLAN RT-16  CONTINUITY SUMMARY  FOR PLAN RT-16   | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  | .37  **LOW=   | 1720E+01 13.81 8203E+00 13.17 7778E+00 49.16 2959E+01 24.51 1419E+01 23.31 1347E+01 60.94 3645E+01 30.36 | EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.  EXCESS=  211.          | .0000E+00 01 .0000E+00 75 .0000E+00 82 .0000E+00 84 .0000E+00 13 1 .0000E+00 | OUTFLOW= 91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .88 OUTFLOW= .94 OUTFLOW= .94 | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2 .1420E+01 5.00 2 .1347E+01 5.00 5 .3647E+01 | BASIN | STORAGE=  210.00   | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI .93 .8611E-08 PEI .88 .8421E-08 PEI 1.95 .3120E-07 PEI | RCENT F | ERROR=  ERROR=  ERROR=  ERROR= | .0   |
| CONTINUITY SUMMARY  FOR PLAN RT-14  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-15  CONTINUITY SUMMARY  FOR PLAN RT-16  CONTINUITY SUMMARY  FOR PLAN RT-16 | MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  = 1 RATIO= 1 MANE  (AC-FT) - INF  = 1 RATIO= MANE  (AC-FT) - INF  | .37  **LOW=   | 1720E+01 13.81 8203E+00 13.17 7778E+00 49.16 2959E+01 24.51 1419E+01 23.31 1347E+01 60.94 3645E+01 30.36 | EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.  EXCESS=  211.  EXCESS= | .0000E+00 01 .0000E+00 75 .0000E+00 82 .0000E+00 84 .0000E+00 13 1 .0000E+00 | OUTFLOW= 91 OUTFLOW= 86 OUTFLOW= 93 OUTFLOW= 88 OUTFLOW= 94 OUTFLOW= 93      | .1721E+01 5.00 1 .8205E+00 5.00 1 .7780E+00 5.00 4 .2959E+01 5.00 2 .1420E+01 5.00 2 .1347E+01 5.00 5 .3647E+01 | BASIN 3.40 BASIN 22.73 BASIN 8.56 BASIN 4.04 BASIN BASIN BASIN BASIN 8.94 BASIN BASIN BASIN     | STORAGE=  210.00  STORAGE= | .7751E-08 PEI .91 .6549E-08 PEI .86 .6560E-08 PEI 1.94 .9128E-08 PEI .93 .8611E-08 PEI .88 .8421E-08 PEI 1.95 .3120E-07 PEI | RCENT F | ERROR=  ERROR=  ERROR=  ERROR= | .0   |

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2413E+00 EXCESS= .0000E+00 OUTFLOW= .2419E+00 BASIN STORAGE= .4920E-06 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .58 ROFF5-CP MANE 2.92 3.61 221.61 .53 5.00 3.45 220.00 .53

CONTINUITY SUMMARY (AC-FT) - INFLOW: .2254E+00 EXCESS: .0000E+00 OUTFLOW: .2260E+00 BASIN STORAGE: .3400E-06 PERCENT ERROR: -.2

\*\*\* NORMAL END OF HEC-1 \*\*\*

### **OFFEX3 Shallow Pondind Area**

| ELEVATION | AREA (ft2) | VOLUME (ft3) | VOLUME (ac-ft) | CUMULATIVE VOLUME (ac-ft) | OUTFLOW (cfs) |
|-----------|------------|--------------|----------------|---------------------------|---------------|
| 1766      | 10475      | 0            | 0.00           | 0.00                      | 0             |
| 1767      | 30499      | 20487        | 0.47           | 0.47                      | 0.01          |
| 1768      | 47931      | 39215        | 0.90           | 1.37                      | 0.02          |
| 1769      | 68570      | 58250.5      | 1.34           | 2.71                      | 0.03          |
| 1770      | 89398      | 78984        | 1.81           | 4.52                      | 0.04          |

Note: Area was determined from 1' topography using AutoCAD

## **LEGEND**

ONSITE BASIN BOUNDARY

OFFSITE BASIN BOUNDARY

OFFSITE BASIN LABEL

REFERENCED BASIN BOUNDARY

ONEX1 ONSITE BASIN LABEL

REFERENCED BASIN LABEL

HEC-1 COMBINATION POINT

DISCHARGE POINT

FLOW DIRECTION TOPOGRAPHY BOUNDARY

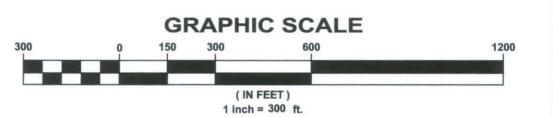
EXISTING LANDFILL BOUNDARY

# NOTES

"ADDENDUM #1 TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMERCE CENTER TWO (FORMERLY KNOWN AS HARSCH)" PREPARED BY PBS&J (FEBRUARY 2003) WAS USED FOR REFERENCED BASINS

| BASIN ID | AREA (ac) | Q <sub>100</sub> (cfs) | Q <sub>10</sub> (cfs) |
|----------|-----------|------------------------|-----------------------|
| ONEX1    | 32.76     | 47                     | 17                    |
| ONEX2    | 28.77     | 49                     | 21                    |
| ONEX3    | 22.12     | 59                     | 29                    |
| ONEX4    | 28.27     | 56                     | 25                    |
| ONEX5    | 1.06      | 3                      | 2                     |
| OFFEX1   | 42.20     | 48                     | 14                    |
| OFFEX2   | 9.63      | 13                     | 4                     |
| OFFEX3   | 16.40     | 21                     | 8                     |
| OFFEX4   | 7.61      | 14                     | 6                     |
| OFFEX5   | 5.11      | 10                     | 4                     |
| CP-1     | NA        | 105                    | 33                    |
| CP-2     | NA        | 23                     | 8                     |
| CP-3     | NA        | 65                     | 27                    |
| C18      | NA        | 162                    | 57                    |
| C18B     | NA        | 212                    | 78                    |





511963.19

OCTOBER 2006

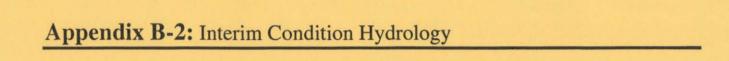
FIGURE 4 EXISTING CONDITION DRAINAGE MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



2270 Corporate Circle Telephone: 702/263-7275 Fax: 702/263-7200

ENGINEERING PLANNING. SURVEYING CONSTRUCTION SERVICES



### HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL PBS&J EASTSIDE LANDFILL File: TDS-Standard Form 4.xls BY: 10/5/06 Interim Condition Hydrology DATE: SUB-BASIN INITIAL / OVERLAND TRAVEL TIME Tc REMARKS To Tlag DATA TIME (TI) (Tt) Check TRAVEL V1 V2 Tlag= DESIG: DEV./UN. AREA AREA LENGTH SLOPE Ti LENGTH SLOPE VELOCITY VELOCITY Tt 0.6Tc/60 FPS (D or U) Feet Feet FPS Hours (2) (4) (5) (6) (7) (9b) (10) (13) OND1 D 87.7 0.94 0.0015 130 33.0 2.1 247 0.4 1.28 1.9 3.2 5.3 12.1 OND2 D 3.70 0.0058 137 33.0 2.2 910 0.4 1.28 1.9 10.1 15.8 OND3 D 88.6 0.7795 1.38 0.0022 156 33.0 2.2 360 1.0 2.02 3.1 3.0 5.2 12.9 0.05 2.6 OND4 D 89.7 0.7940 11.67 0.0182 240 2.0 6.8 1276 3.26 4.9 5.2 12.0 18.4 0.12 1.7 7.6 2.07 3.1 12.0 14.9 OND5 D 91.0 0.8112 5.03 0.0079 300 573 1.1 4.4 0.12 1.4 3.0 1407 0.6 1.56 2.4 11.7 15.6 18.2 OND6 D 91.0 0.8112 0.0155 70 0.16 9.90 D 158 33.0 2.1 1345 1.8 2.67 4.0 6.6 8.7 18.4 0.09 OND7 90.8 0.8086 5.87 0.0092 0.0223 33.0 1.9 2382 0.4 1.28 1.9 22.7 24.6 23.9 0.24 OND8 D 90.3 0.8020 14.26 128 Use Tlag = 0.15 See Note OND9 U 91.0 0.8112 0.0017 50 1.3 3.4 453 1.9 2.05 4.1 3.7 7.0 N/A 0.07 1.06 33.0 0.4 1.28 1.9 12.5 17.3 OND10 D 91.0 0.8112 4.28 0.0067 119 1.8 1190 14.2 0.14 OND11 D 91.0 0.8112 9.60 0.0150 220 1.6 6.6 1050 LI 2.12 3.2 6.8 13.4 17.1 0.13 OND12 D 91.4 0.8165 2.77 0.0043 138 33.0 1.9 610 1.5 2.47 3.7 3.9 5.7 14.2 0.06 OND13 D 91.0 0.8112 4.70 0.0073 95 33.0 1.6 714 0.4 1.28 1.9 8.4 9.9 14.5 0.10 OND14 U 91.0 0.8112 11.12 0.0174 122 1.0 5.7 559 5.0 3.31 6.6 2.7 8.4 N/A 0.08 OND15 U 91.0 0.8112 21.47 0.0335 200 2.5 5.4 711 3.0 2.56 5.1 3.9 9.4 N/A 0.09 DETPD D 91.4 0.8165 5.14 0.0080 60 8.3 2.0 35 34.0 11.78 17.8 0.0 2.0 10.5 0.02 2213 OFFEX1 U 77.6 0.6343 42.20 0.0659 278 2.5 10.3 2.0 2.09 4.1 10.9 21.1 N/A 0.21 OFFEX2 U 78.5 0.6462 9.63 0.0150 195 3.6 7.4 942 1.8 1.99 3.9 6.1 13.5 N/A 0.14 OFFEX3 0.0256 300 0.3 18.3 1245 1.7 1.92 3.8 7.6 25.9 U 82.0 0.6924 16.40 N/A 0.26 OFFEX4 U 0.7320 0.0119 1.0 11.5 750 1.9 2.02 4.0 5.2 N/A 0.17 85.0 7.61 16.6 U 85.0 0.7320 1.3 10.4 625 1.6 1.87 3.7 5.0 15.4 0.15 OFFEX5 5.11 0.0080 300 N/A For the travel time (Tt) calculations (Sec. 602.1), Tc = Ti + TtEqn. 601 Undeveloped V1 = 14.8\*(S/100)^1/2 Developed V1 = 20.2\*(S/100)^1/2 Ti = 1.8 (1.1 - K) L^1/2 / S^1/3 Egn. 602 V1 applies to the first 500 feet of travel distance; K = 0.0132 (CN) - 0.39 V2 applies to the remaining travel distance. Undeveloped V2 = 29.4\*(S/100)^1/2 Eqn. 603 Developed V2 = 30.6\*(S/100)^1/2 Tc Check = L/180+10 Egn. 604 Tlag = 0.6 Tc Egn. 612 Min Tc = 10 mins for undeveloped basins Tt = 500/V1+ (Travel Length-500)/V2 Min Tc = 5 mins for developed basins Note: The lag time or basin OND8 was changed to 0.15 hrs because the velocities were not accurate for the cross section. Please refer to the FlowMaster cross section located in Appendix B-3 for the time calculations. STANDARD FORM 4 REFERENCE:

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 27SEP06 TIME 19:18:46

U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

 X
 X
 XXXXXXX
 XXXXXX
 XX
 XX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKR- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRANT? VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUMMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ INFESSERS AT DESIRED CALCULATION INVERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```
1
                                                                                                  HEC-1 INPUT
                                                                                                                                                                                                      PAGE 1
                   LINE
                                             ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 *** FREE ***
                                              *DIAGRAM
                                                        RAM
EASTSIDE LANDFILL IMPROVEMENTS
INTERIM CONDITION MODEL
INPUT FILE = 1NT_SDN3.DAT
SEPTEMBER 2006
DESIGN STORM = 100-YEAR 6-HR STORM
STORM DISTRIBUTION = SDN #3
MODELED BY PBS&J
                                              ID ID ID ID ID IT IN IO JR
                                                                           0
                                                                                                    300
                       10
11
12
                                                        PREC 1.00 0.60
                                                                                                 0.58
                       13
14
15
16
17
18
19
20
21
22
23
24
25
26
                                             KK KM BA PB PC PC PC PC PC LS UD
                                                   CND9
EXISTING ONSITE BASIN
0.0017
2.79
.000 .020 .057
130 .130 .130
.190 .197 .199
.251 .256 .270
.499 .590 .710
.860 .868 .876
.982 .985 .987
.998 .999 1.00
                                                                      .020
.130
.197
.256
.590
.868
.985
.999
91.0
                                                                                                                  .140
.201
.281
.781
.910
                                                        0.07
                       27
28
29
30
31
                                             KK
KM
BA
LS
UD
*
                                                    OFFEX3
                                                    EXISTING OFFSITE BASIN 0.0256
                                                                      82.0
                                                        0.26
                       32
33
34
                                              KK
KM
HC
*
                                                      COMBINE OND9 AND OFFD3
                                                    DEVELOPED ONSITE BASIN
0.0223
                                                        0.15
                                                                                                  HEC-1 INPUT
                   LINE
                                             \mathtt{ID}.\dots..1\dots..2\dots..3\dots..4\dots..5\dots..6\dots..7\dots..8\dots..9\dots..10
                                              KKROND8-CP-9
                       41
42
                                                      ROUTE OND8 TO CP-9
1190 0.004 0.025
                                                                                                       0 TRAP 10
                                                                                                                                                 3
                                                    DEVELOPED ONSITE BASIN
                                                                      91.0
                                                       0.14
                                                   EXISTING OFFSITE BASIN 0.0080
                       48
49
50
51
52
                                             KK
KM
BA
LS
UD
                                                                    85.0
                                                       0.15
                       53
54
55
                                             KK
KM
HC
                                                      COMBINE RCP8-CP9, OFFD5 AND OND10
                                              KKRCP9-CP-10

KM ROUTE CP-9 TO CP-10

RK 725 0.015 0.015
                                                                                                      0 TRAP
                                                                                                                              10
```

```
KK OND12
KM DEVELOPED ONSITE BASIN
BA 0.0043
LS 0 91.4
UD 0.06
  64
65
66
                             COMBINE CP-9 AND OND12
                      KK OND11

KM DEVELOPED ONSITE BASIN

BA 0.0150

LS 0 91.0

UD 0.13
   67
68
69
70
71
                      KK OND13
KM DEVELOPED ONSITE BASIN
BA 0.0073
LS 0 91.0
UD 0.10
  72
73
74
75
76
                                                                   HEC-1 INPUT
                                                                                                                                                          PAGE 3
LINE
                      ID.....1.....2.....3.....4.....5......6.....7.....8......9.....10
                             \ensuremath{\text{CP-10}} COMBINE CP-10A, OND11 AND OND13 ^3
   77
78
79
                      80
81
82
83
84
85
86
                      KK DIVWEIR
KM DIVERT FLOW FROM EQ BASIN
DT DVPIPE
DI 0 59 74
DQ 0 59 64
   87
88
89
90
91
                                        59 74 126
59 64 73
                           OND14
DEVELOPED ONSITE BASIN
0.0174
0 91.0
   92
93
94
95
96
                             0.08
   97
98
99
                           CP-11
COMBINE WEIR FLOW AND OND14
                      KK OND1

KM DEVELOPED ONSITE BASIN

BA 0.0015

LS 0 87.7

UD 0.05

*
 100
101
102
103
104
                      KK OFFEX2
KM EXISTING OFFSITE BASIN
BA 0.0150
LS 0 78.5
UD 0.14
 110
111
112
                             CP-1
COMBINE OND1 AND OFFD2
2
                                                                   HEC-1 INPUT
                                                                                                                                                          PAGE 4
LINE
                      {\tt ID},\ldots,1,\ldots,2,\ldots,3,\ldots,4,\ldots,5,\ldots,6,\ldots,7,\ldots,8,\ldots,9,\ldots,10
                      KKRCP1-CP2
KM ROUTE CP-1 TO CP-2
RK 910 0.004 0.025
 113
114
115
                                                                        0 TRAP
                                                                                           10
                      KK OND2
KM DEVELOPED ONSITE BASIN
BA 0.0058
LS 0 87.7
UD 0.12
                      KK OFFEXI
KM EXISTING OFFSITE BASIN
BA 0.0659
LS 0 77.6
UD 0.21
 121
122
123
124
125
                      KK CP-2
KM COMBINE CP-1, OFFD1 AND OND2
HC 3
 126
127
128
                      KKRCP2-CP-3
KM ROUTE
RK 360 0.010 0.015
                                                                        0 TRAP 10 3
 132
133
134
                      KK OND3
KM DEVELOPED ONSITE BASIN
BA 0.0022
```

```
0 88.6
0.05
                                 CP-3
COMBINE CP-2 AND OND3
                        KKRCP3-CP4
KM ROUTE CP-3 TO CP-4
RK 1345 0.018 0.015
  141
142
                        KM
RK
*
                                                                              0 TRAP
                                                                                                  10
 143
144
145
146
147
                        KK
KM
BA
LS
UD
                              OND/
DEVELOPED ONSITE BASIN
0.0092
0 90.8
0.09
                                                                           HEC-1 INPUT
                                                                                                                                                                        PAGE 5
LINE
                        ID.....1....2.....3.....4.....5.....6.....7.....8.....9.....10
                        KK
KM
HC
*
                                CP-4
COMBINE CP-3 AND OND7
  149
150
                        KK OND4

KM DEVELOPED ONSITE BASIN

BA 0.0182

LS 0 89.7

UD 0.12

*
 151
152
153
154
155
                        KK
KM
BA
LS
UD
                              DEVELOPED ONSITE BASIN
0.0079
0 91.0
0.12
 161
162
163
                        KK
KM
HC
                                CP-5
COMBINE OND4 AND OND5
 164
165
166
167
168
                        KK
KM
BA
LS
UD
                              OND6
DEVELOPED ONSITE BASIN
0.0155
0 91.0
0.16
                             DVPIPE
RETURN FLOW FROM EQ BASIN PIPE
DVPIPE
                        KK RDVPIPE
KM ROUTE FLOW THROUGH 42" RCP
RK 1880 0.005 0.013 0 CIRC
                                                                                                  3.5
                             DETPD
DETENTION POND BASIN
0.0080
0 91.4
0.05
 175
176
177
178
179
                        KK
KM
BA
LS
UD
                               COMBINE CP-4, CP-5, OND6, DVPIPE AND DETPD 5
                                                                         HEC-1 INPUT
                                                                                                                                                                      PAGE 6
LINE
                        ID.....1.....2.....3.....4.....5.....6......7.....8.....9.....10
                        KK DETPOND
KM
RS 1
SV 0
SE 1725.25
 183
184
185
186
187
188
189
                        SQ
KO
                        * Referenced from PBSJ
*Addendum #1 to the Technical Drainage Study for Henderson Commmerce
*Center Two (Formerly known as HARSCH)* (February 2003)
                        KK OFFD-14
KM OFSITE DEVELOPED BASIN OFFD-14
KM REFERENCED FROM EG02
BA 0.0028
BE 2.79
LS 0 88
UD 0.200
 190
191
192
193
194
195
196
                        KK RT-B14
KM ROUTE
RK 1050
 197
198
199
                                ROUTE OFFD-14 THROUGH BMIC-1
1050 0.014 0.013 0 TRAP
                                                                                                      15
                                                                                                                 10
                        KK EMIC-1
KM ONSITE DEVELOPED BASIN BMIC-1
KM REPERENCED FROM EG02
BA 0.0141
PB 2.79
LS 0 92
UD 0.081
```

```
C15
COMBINE RT-B14 AND BMIC-1
2
                           RT-14
ROUTE C15 THROUGH BMIC-2
450 0.018 0.013
 211
212
                                                                 0 TRAP 15 10
                    RK
*
                    KK BMIC-2
KM ONSITE DEVELOPED BASIN BMIC-2
KM REFERENCED FROM BG02
 213
214
215
216
217
218
                         0.0118
2.79
0
                                                              HEC-1 INPUT
                                                                                                                                             PAGE 7
LINE
                    ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 219
                          C16
COMBINE RT-14 AND BMIC-2
 221
                          RT-15
ROUTE C16 THROUGH SCH-2
400 0.019 0.013
 224
                                                                  0 TRAP
                                                                                       15
                                                                                                  10
                         SCH-2
ONSITE DEVELOPED BASIN SCH-2
REFERENCED FROM EGO2
0.0065
2.79
                    KK
KM
KM
BA
PB
LS
UD
                           C17
COMBINE RT-15 AND SCH-2
                    KK
KM
HC
 234
235
                           RT-16
ROUTE C17 THROUGH BMIC-3
750 0.013 0.013
                                                                  0 TRAP
                                                                                    15
                                                                                              10
                        BMIC-3
ONSITE DEVELOPED BASIN BMIC-3
REFERENCED FROM BG02
0.0106
2.79
9 92
                    KK
KM
KM
BA
PB
LS
UD
                           0.062
 246
247
248
                    RK MGDEV-2

KM MILGARD MANUFACTURING ONSITE BASIN

RM REFERENCED FROM EGO2

0.0093

PB 2.79

LS 0 92

UD 0.075
 249
250
251
252
                                                              HEC-1 INPUT
                                                                                                                                             PAGE 8
LINE
                    ID......1.....2......3......4......5......6......7......8......9......10
                          C18 COMBINE RT-16, BMIC-3, BGDEV-2 AND OUTFLOW FROM DETENTION POND \frac{4}{}
                     Referenced from PBSJ
"Addendum #1 to the Technical Drainage Study for Henderson Commmerce
Center Two (Formerly known as HARSCH)" (February 2003)
 256
257
258
259
260
261
                         HR3
HARSCH ONSITE BASIN
0.0014
2.79
0 92
                           0.049
                         HR2
HARSCH ONSITE BASIN
0.0016
2.79
 262
263
264
265
266
267
                    KK
KM
BA
PB
LS
UD
*
                                           98
                           0.037
                    KK
KM
BA
PB
LS
UD
                         HARSCH ONSITE BASIN
0.0015
2.79
0 92
 269
270
271
272
273
                             0.05
                          CHR1
COMBINE HR3, HR2, HR1
THESE FLOWS ARE DISCHARGED INTO THE ONSITE
STORM DRAIN SYSTEM LABELED ALIGNMENT "H1"
ON FIGURE 7
                     . ........
```

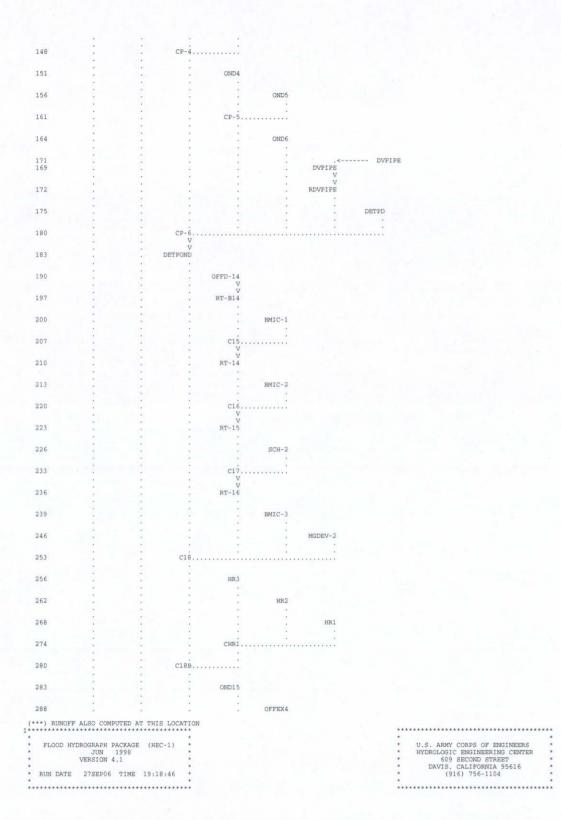
```
C18B
COMBINE C18 AND CHR1
2
                                                       HEC-1 INPUT
                                                                                                               PAGE 9
                         \texttt{ID},\ldots,1,\ldots,2,\ldots,3,\ldots,4,\ldots,5,\ldots,6,\ldots,7,\ldots,8,\ldots,9,\ldots,10
           LINE
                             OND15
DEVELOPED ONSITE BASIN
0.0335
0 91.0
0.09
            283
284
285
286
287
                         KK OFFEX4

KM EXISTING OFFSITE BASIN

BA 0.0119

LS 0 85.0

UD 0.17
            293
                         22
1
             SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT
                          (--->) DIVERSION OR PUMP FLOW
            (V) ROUTING
  NO.
            (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
   13
   27
                    OFFEX3
   32
   35
                         OND8
                     ROND8-CP
   40
   43
                                     OND10
   48
                                                OFFEX5
                         CP-9.....
   53
   56
                      RCP9-CP-
                                    OND12
   59
                       CP-10A.....
   64
                                     OND11
   67
   72
                                                OND13
                        CP-10.....
   77
                      EQBASIN
                                ----> DVPIPE
   92
                                     OND14
                        CP-11......
   97
  100
                                     OND1
                                                OFFEX2
  105
                                     CP-1.
  110
  113
                                  RCP1-CP2
  116
                                                  OND2
  121
                                                           OFFEX1
  126
                                     CP-2.
                                  RCP2-CP-
   129
   132
                                                  OND3
  137
                                     CP-3.....
  140
                                 RCP3-CP4
  143
                                                 OND7
```



EASTSIDE LANDFILL IMPROVEMENTS
INTERIM CONDITION MODEL
INPUT FILE = INT\_SIN3.DAT
SEPTEMBER 2006
DESIGN STORM = 100-YEAR 6-HR STORM
STORM DISTRIBUTION = SDN #3
MODELED BY PBS&J

```
5 PRINT CONTROL
0 PLOT CONTROL
0. HYDROGRAPH PLOT SCALE
                                                                             IPLOT
                  IT
                                                          HYDROGRAPH TIME DATA
                                                                                                              DATA
5 MINUTES IN COMPUTATION INTERVAL
1 0 STARTING DATE
0000 STARTING TIME
300 NUMBER OF HYDROGRAPH ORDINATES
2 0 ENDING DATE
0055 ENDING TIME
19 CENTURY MARK
                                                                           NDTIME
                                                                          ICENT
                                                               COMPUTATION INTERVAL
                                                                                                                                                   .08 HOURS
                                                                                TOTAL TIME BASE 24.92 HOURS
                                 ENGLISH UNITS
DRAINAGE AREA
PRECIPITATION DEPTH
LENGTH, ELEVATION
FLOW
STORAGE VOLUME
SURFACE AREA
TEMPERATURE
                                                                                                                            SOUARE MILES
                                                                                                                         SQUARE MILES
INCHES
FEET
CUBIC FEET PER SECOND
ACRE-FEET
ACRES
DEGREES FAHRENHEIT
                 JP
                                                        MULTI-PLAN OPTION
NPLAN
                                                                                                                              1 NUMBER OF PLANS
                 JR
                                                        MULTI-RATIO OPTION
                                                                RATIOS OF PRECIPITATION
1.00 .60 .58
  *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***
                                         ******
    183 KK
                                         * DETPOND *
                                          ***********
                                                        OUTPUT CONTROL VARIABLES

IPRNT 1 PRINT CONTROL

IPLOT 0 PLOT CONTROL
                                                                            IPRNT
IPLOT
QSCAL
                                                                                                                             0 PLOT CONTROL
0. HYDROGRAPH PLOT SCALE
                                                  HYDROGRAPH ROUTING DATA
                                                      STORAGE ROUTING
    185 RS
                                                                                                                   1 NUMBER OF SUBREACHES
STOR TYPE OF INITIAL CONDITION
-1.00 INITIAL CONDITION
.00 WORKING R AND D COEFFICIENT
                                                                            NSTPS
ITYP
                                                                                                        .0
    186 SV
                                                             STORAGE
                                                                                                                                                   .1
                                                                                                                                                                                 1.5
                                                                                                                                                                                                       3.0
                                                                                                                                                                                                                                             4.8
                                                                                                                                                                                                                                                                           8.9
                                                                                                                                                                                                                                                                                                              13.4
                                                                                                                                                                                                                                                                                                                                                     15.9
    187 SE
                                                         ELEVATION 1725.25 1726.00 1728.00 1729.00 1730.00 1732.00 1734.00 1735.00
    188 SQ
                                                       DISCHARGE 0.
                                                                                                                                     0. 22. 27.
                                                                                                                                                                                                                                             32.
                                                                                                                                                                                                                                                                             40.
                                                                                                                                                                                                                                                                                                              46.
                                                                                                                                                                                                               ***
  HYDROGRAPH AT STATION DETPOND
PLAN 1, RATIO = 1.00
                                                                                                                                                                                                                                                                      1728.2 * 1
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1727.7 * 1
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| 1 | 0355 |     | 37. |     | 1731.1 * |   | 1215 148 | 0.  |     |          | 1 | 2035 248 | 0. |     | 1726.0 |
|---|------|-----|-----|-----|----------|---|----------|-----|-----|----------|---|----------|----|-----|--------|
| 1 | 0400 | 49  | 38. | 7.7 | 1731.4 * |   | 1220 149 | 0.  | -1  | 1726.0 * | 1 | 2040 249 | 0. |     | 1726.0 |
| 1 | 0405 | 50  | 38. | 8.1 | 1731.6 * |   | 1225 150 | 0.  | .1  | 1726.0 * | 1 | 2045 250 | 0. |     | 1726.0 |
| 1 | 0410 | 51  | 39. | 8.3 | 1731.7 * | 1 | 1230 151 | 0.  | . 1 | 1726.0 * | 1 | 2050 251 | 0. | .1  | 1726.0 |
| 1 | 0415 | 52  | 39. | 8.5 | 1731.8 * | 1 | 1235 152 | 0.  | .1  | 1726.0 * | 1 | 2055 252 | 0. | .1  | 1726.0 |
| 1 | 0420 | 5.3 | 40. | 8.7 | 1731.9 * | 1 | 1240 153 | 0.  | .1  | 1726.0 * | 1 | 2100 253 | 0. | . 1 | 1726.0 |
| 1 | 0425 | 54  | 40. | 8.7 | 1731.9 * | 1 | 1245 154 | 0 - | .1  | 1726.0 * | 1 | 2105 254 | 0. |     | 1726.0 |
| 1 | 0430 | 55  | 40. | 8.8 | 1732.0 * |   | 1250 155 | 0.  | .1  | 1726.0 * | 1 | 2110 255 | 0. |     | 1726.0 |
| 1 | 0435 | 56  | 40. | 8.9 | 1732.0 * |   | 1255 156 | 0.  | .1  | 1726.0 * |   | 2115 256 | 0. |     | 1726.0 |
| 1 | 0440 | 57  | 40. | 9.0 | 1732.0 * |   | 1300 157 | 0.  | .1  | 1726.0 * | 1 | 2120 257 | 0. |     | 1726.0 |
|   |      |     |     |     |          |   |          |     |     |          |   |          |    |     |        |
| 1 | 0445 | 58  | 40. | 9.1 | 1732.1 * |   | 1305 158 | 0.  | .1  | 1726.0 * | 1 | 2125 258 | 0. |     | 1726.0 |
| 1 | 0450 | 59  | 40. | 9.2 | 1732.1 * |   | 1310 159 | 0.  | .1  | 1726.0 * |   | 2130 259 | 0. |     | 1726.0 |
| 1 | 0455 | 60  | 41. | 9.3 | 1732.2 * |   | 1315 160 | 0.  | .1  | 1726.0 * | 1 | 2135 260 | 0. |     | 1726.0 |
| 1 | 0500 | 61  | 41. | 9.4 | 1732.2 * | 1 | 1320 161 | 0.  | .1  | 1726.0 * | 1 | 2140 261 | 0. | . 1 | 1726.0 |
| 1 | 0505 | 62  | 41. | 9.4 | 1732.2 * | 1 | 1325 162 | 0.  | . 1 | 1726.0 * | 1 | 2145 262 | 0. | .1  | 1726.0 |
| 1 | 0510 | 63  | 41. | 9.4 | 1732.2 * | 1 | 1330 163 | 0.  | .1  | 1726.0 * | 1 | 2150 263 | 0. | . 1 | 1726.0 |
| 1 | 0515 | 64  | 41. | 9.3 | 1732.2 * | 1 | 1335 164 | 0.  | . 1 | 1726.0 * | 1 | 2155 264 | 0. | . 1 | 1726.0 |
| 1 | 0520 | 65  | 40. | 9.2 | 1732.1 * | 1 | 1340 165 | 0   |     | 1726.0 * | 1 | 2200 265 | 0. |     | 1726.0 |
| 1 | 0525 | 66  | 40. | 9.0 | 1732.1 * |   | 1345 166 | 0.  | .1  | 1726.0 * | 1 | 2205 266 | 0. |     | 1726.0 |
| 1 | 0530 | 67  | 40. | 8.9 | 1732.0 * |   | 1350 167 | 0.  |     | 1726.0 * | 1 | 2210 267 | 0. |     | 1726.0 |
| 1 | 0535 | 68  | 40. | 8.7 | 1731.9 * |   | 1355 168 | 0.  | .1  | 1726.0 * | 1 | 2215 268 | 0. |     | 1726.0 |
| 1 | 0540 | 69  | 39. | 8.5 | 1731.8 * |   |          |     | .1  | 1726.0 * | 1 | 2220 269 | 0. |     |        |
|   |      |     |     |     |          |   | 1400 169 | 0.  |     |          |   |          |    | .1  |        |
| 1 | 0545 | 70  | 39. | 8.3 | 1731.7 * |   | 1405 170 | 0.  | .1  | 1726.0 * | 1 | 2225 270 | 0. |     | 1726.0 |
| 1 | 0550 | 71  | 38. | 8.1 | 1731.6 * |   | 1410 171 | 0.  |     | 1726.0 * | 1 | 2230 271 | 0. |     | 1726.0 |
| 1 | 0555 | 72  | 38. | 7.8 | 1731.5 * |   | 1415 172 | 0.  | - 1 | 1726.0 * | 1 | 2235 272 | 0. |     | 1726.0 |
| 1 | 0600 | 73  | 38. | 7.6 | 1731.4 * |   | 1420 173 | 0.  | .1  | 1726.0 * | 1 | 2240 273 | 0. |     | 1726.0 |
| 1 | 0605 | 74  | 37. | 7.4 | 1731.3 * | 1 | 1425 174 | 0.  | .1  | 1726.0 * | 1 | 2245 274 | 0. |     | 1726.0 |
| 1 | 0610 | 75  | 37. | 7.2 | 1731.2 * | 1 | 1430 175 | 0.  | .1  | 1726.0 * | 1 | 2250 275 | 0. | .1  | 1726.0 |
| 1 | 0615 | 76  | 36. | 7.0 | 1731.0 * | 1 | 1435 176 | 0.  | . 1 | 1726.0 * | 1 | 2255 276 | 0. | .1  | 1726.0 |
| 1 | 0620 | 77  | 36. | 6.7 | 1730.9 * | 1 | 1440 177 | 0.  | . 1 | 1726.0 * | 1 | 2300 277 | 0. | .1  | 1726.0 |
| 1 | 0625 | 78  | 35. | 6.5 | 1730.8 * | 1 | 1445 178 | 0.  | .1  | 1726.0 * | 1 | 2305 278 | 0. |     | 1726.0 |
| 1 | 0630 | 79  | 35. | 6.3 | 1730.7 * |   | 1450 179 | 0.  | .1  | 1726.0 * | 1 | 2310 279 | 0. |     | 1726.0 |
| 1 | 0635 | 80  | 34. | 6.0 | 1730.6 * |   | 1455 180 | 0.  | .1  | 1726.0 * | 1 | 2315 280 | 0. |     | 1726.0 |
| 1 | 0640 | 81  | 34. | 5.8 | 1730.5 * |   | 1500 181 | 0.  |     | 1726.0 * | 1 | 2320 281 | 0. |     | 1726.0 |
| 1 | 0645 | 82  | 33. | 5.6 | 1730.4 * |   | 1505 182 | 0.  | .1  | 1726.0 * | 1 | 2325 282 | 0. |     | 1726.0 |
| 1 | 0650 | 83  | 33. |     | 1730.4   |   | 1510 183 |     |     | 1726.0 * | 1 | 2330 283 | 0. |     | 1726.0 |
| 1 |      |     |     | 5.3 |          |   |          | 0.  | .1  |          | 1 |          |    |     |        |
| 1 | 0655 | 84  | 33. | 5.1 | 1730.1 * |   | 1515 184 | 0.  |     | 1726.0 * |   | 2335 284 | 0. |     | 1726.0 |
| 1 | 0700 | 85  | 32. | 4.9 | 1730.0 * |   | 1520 185 | 0.  | .1  | 1726.0 * | 1 | 2340 285 | 0. |     | 1726.0 |
| 1 | 0705 | 86  | 32. | 4.7 | 1729.9 * |   | 1525 186 | 0.  | .1  | 1726.0 * | 1 | 2345 286 | 0. |     | 1726.0 |
| 1 | 0710 | 87  | 31. | 4.5 | 1729.8 * |   | 1530 187 | 0.  |     | 1726.0 * | 1 | 2350 287 | 0. |     | 1726.0 |
| 1 | 0715 | 88  | 30. | 4.3 | 1729.7 * |   | 1535 188 | 0.  | .1  | 1726.0 * | 1 | 2355 288 | 0. |     | 1726.0 |
| 1 | 0720 | 69  | 30. | 4.1 | 1729.6 * | 1 | 1540 189 | 0.  | .1  | 1726.0 * | 2 | 0000 289 | 0. | .1  | 1726.0 |
| 1 | 0725 | 90  | 29. | 3.9 | 1729.5 * | 1 | 1545 190 | 0.  | . 1 | 1726.0 * | 2 | 0005 290 | 0. | .1  | 1726.0 |
| 1 | 0730 | 91  | 29. | 3.7 | 1729.3 * | 1 | 1550 191 | 0.  | .1  | 1726.0 * | 2 | 0010 291 | 0. | . 1 | 1726.0 |
| 1 | 0735 | 92  | 28. | 3.5 | 1729.2 * | 1 | 1555 192 | 0.  | . 1 | 1726.0 * | 2 | 0015 292 | 0. |     | 1726.0 |
| 1 | 0740 | 93  | 28. | 3.3 | 1729.1 * |   | 1600 193 | 0.  |     | 1726.0 * | 2 | 0020 293 | 0. |     | 1726.0 |
| 1 | 0745 | 94  | 27. | 3.1 | 1729.0 * |   | 1605 194 | 0.  | .1  | 1726.0 * | 2 | 0025 294 | 0. |     | 1726.0 |
| 1 | 0750 | 95  | 27. | 2.9 | 1728.9 * |   | 1610 195 | 0.  | .1  | 1726.0 * | 2 | 0030 295 | 0. |     | 1726.0 |
| 1 |      | 96  | 26. | 2.7 | 1728.8 * |   | 1615 196 | 0.  |     | 1726.0 * | 2 | 0035 296 | 0. |     | 1726.0 |
| 1 | 0800 | 97  | 25. |     | 1728.7 * |   | 1620 197 |     |     | 1726.0 * | 2 | 0040 297 | 0. |     | 1726.0 |
| 1 | 0805 | 98  |     | 2.5 |          |   |          | 0.  | .1  |          | 2 |          |    |     |        |
| 1 |      |     | 25. | 2.4 | 1728.6 * |   | 1625 198 | 0.  | .1  | 1726.0 * |   | 0045 298 | 0. |     | 1726.0 |
| 1 | 0810 | 99  | 24. | 2.2 | 1728.4 * |   | 1630 199 | 0.  |     | 1726.0 * | 2 | 0050 299 | 0. |     | 1726.0 |
| 1 | 0815 | 100 | 24. | 2.0 | 1728.3 * | 1 | 1635 200 | 0.  | .1  | 1726.0 * | 2 | 0055 300 | 0. | .1  | 1726.0 |
|   |      |     |     |     |          |   |          |     |     |          |   |          |    |     |        |

| 1  | PEAK FLOW   | TIME |          |           | MAXIMUM AVE  | RAGE FLOW   |          |
|----|-------------|------|----------|-----------|--------------|-------------|----------|
|    |             |      |          | 6-HR      | 24-HR        | 72-HR       | 24.92-HR |
| +  | (CFS)       | (HR) |          |           |              |             |          |
|    |             |      | (CFS)    |           |              |             |          |
| +  | 41.         | 5.08 |          | 31.       | 9.           | 8.          | 8.       |
|    |             |      | (INCHES) | 1.944     | 2.126        | 2.126       | 2.126    |
|    |             |      | (AC-FT)  | 15.       | 17.          | 17.         | 17.      |
| PE | EAK STORAGE | TIME |          |           | MAXIMUM AVER | AGE STORAGE |          |
|    |             |      |          | 6-HR      | 24-HR        | 72-HR       | 24.92-HR |
| +  | (AC-FT)     | (HR) |          |           |              |             |          |
|    | 9.          | 5.08 |          | 5.        | 1.           | 1.          | 1.       |
| F  | PEAK STAGE  | TIME |          |           | MAXIMUM AVE  | RAGE STAGE  |          |
|    |             |      |          | 6-HR      | 24-HR        | 72-HR       | 24.92-HR |
| +  | (FEET)      | (HR) |          |           |              |             |          |
|    | 1732.22     | 5.08 |          | 1730.12   | 1727.10      | 1727.06     | 1727.06  |
|    |             |      | CUMULATI | VE AREA = | .15 SO MI    |             |          |

### HYDROGRAPH AT STATION DETPOND PLAN 1, RATIO = .60

| *** | *** | **** | **** | ******  | ******  | *****  | ***  | ****   | **** | **** | ******  | ******* | *****  | *** | ** | *** | **** | **** | ******  | ******  | ****** |
|-----|-----|------|------|---------|---------|--------|------|--------|------|------|---------|---------|--------|-----|----|-----|------|------|---------|---------|--------|
| DA  | MON | HRMN | ORD  | OUTFLOW | STORAGE | STAGE  | * 1  | OA MON | HRMN | ORD  | OUTFLOW | STORAGE | STAGE  | * 1 | DA | MON | HRMN | ORD  | OUTFLOW | STORAGE | STAGE  |
| 1   |     | 0000 | 1    | 0.      | .1      | 1726.0 | *    | 1      | 0820 | 101  | 1.      | .2      | 1726.1 | *   | 1  |     | 1640 | 201  | 0.      | .1      | 1726.0 |
| 1   |     | 0005 | 2    | 0.      | .1      | 1726.0 |      | 1      | 0825 | 102  | 1.      | .2      | 1726.1 | *   | 1  |     | 1645 | 202  | 0.      | .1      | 1726.0 |
| 1   |     | 0010 | 3    | 0.      | .1      | 1726.0 | *    | 1      | 0830 | 103  | 1.      | .2      | 1726.1 | *   | 1  |     | 1650 | 203  | 0.      | .1      | 1726.0 |
| 1   |     | 0015 | 4    | 0.      | .1      | 1726.0 | *    | 1      | 0835 | 104  | 1.      | .1      | 1726.1 | *   | 1  |     | 1655 | 204  | 0.      | .1      | 1726.0 |
| 1   |     | 0020 | 5    | 0.      | . 1     | 1726.0 | *    | 1      | 0840 | 105  | 1.      | .1      | 1726.1 | (*) | 1  |     | 1700 | 205  | 0.      | .1      | 1726.0 |
| 1   |     | 0025 | 6    | 0.      | .1      | 1726.0 | *    | 1      | 0845 | 106  | 1.      | .1      | 1726.1 |     | 1  |     | 1705 | 206  | 0.      | .1      | 1726.0 |
| 1   |     | 0030 | 7    | 0.      | . 1     | 1726.0 | *    | 1      | 0850 | 107  | 1.      | .1      | 1726.1 | *   | 1  |     | 1710 | 207  | 0.      | .1      | 1726.0 |
| 1   |     | 0035 | 8    | 0.      | .1      | 1726.0 | *    | 1      | 0855 | 108  | 1.      | .1      | 1726.1 | *   | 1  |     | 1715 | 208  | 0.      | .1      | 1726.0 |
| 1   |     | 0040 | 9    | 0.      | . 1     | 1726.0 | *    | 1      | 0900 | 109  | 1.      | .1      | 1726.1 | *   | 1  |     | 1720 | 209  | 0.      | .1      | 1726.0 |
| 1   |     | 0045 | 10   | 0.      | .1      | 1726.0 | *    | 1      | 0905 | 110  | 1.      | .1      | 1726.0 | *   | 1  |     | 1725 | 210  | 0.      | .1      | 1726.0 |
| 1   |     | 0050 | 11   | 0.      | .1      | 1726.0 | *    | 1      | 0910 | 111  | 0.      | .1      | 1726.0 | *   | 1  |     | 1730 | 211  | 0.      | .1      | 1726.0 |
| 1   |     | 0055 | 12   | 0.      | .1      | 1726.0 | *    | 1      | 0915 | 112  | 0.      | .1      | 1726.0 | *   | 1  |     | 1735 | 212  | 0.      | .1      | 1726.0 |
| 1   |     | 0100 | 13   | 0.      | .1      | 1726.0 | *    | 1      | 0920 | 113  | 0.      | .1      | 1726.0 | *   | 1  |     | 1740 | 213  | 0.      | .1      | 1726.0 |
| 1   |     | 0105 | 14   | 0.      | .1      | 1726.0 |      | 1      | 0925 | 114  | 0.      | .1      | 1726.0 | *   | 1  |     | 1745 | 214  | 0.      | .1      | 1726.0 |
| 1   |     | 0110 | 15   | 0.      | .1      | 1726.0 | *    | 1      | 0930 | 115  | 0.      | .1      | 1726.0 | *   | 1  |     | 1750 | 215  | 0.      | .1      | 1726.0 |
| 1   |     | 0115 | 16   | 0.      | .1      | 1726.0 | *    | 1      | 0935 | 116  | 0.      | .1      | 1726.0 | *   | 1  |     | 1755 | 216  | 0.      | .1      | 1726.0 |
| 1   |     | 0120 | 17   | 0.      | .1      | 1726.0 | *    | 1      | 0940 | 117  | 0.      | .1      | 1726.0 | *   | 1  |     | 1800 | 217  | 0.      | .1      | 1726.0 |
| 1   |     | 0125 | 18   | 0.      | .1      | 1726.0 | *    | 1      | 0945 | 118  | 0.      | . 1     | 1726.0 | *   | 1  |     | 1805 | 218  | 0.      | .1      | 1726.0 |
| 1   |     | 0130 | 19   | 0.      | .1      | 1726.0 | *    | 1      | 0950 | 119  | 0.      | .1      | 1726.0 | *   | 1  |     | 1810 | 219  | 0.      | .1      | 1726.0 |
| 1   |     | 0135 | 20   | 0.      | .1      | 1726.0 | *    | 1      | 0955 | 120  | 0.      | .1      | 1726.0 | *   | 1  |     | 1815 | 220  | 0.      | .1      | 1726.0 |
| 1   |     | 0140 | 21   | 0.      | .1      | 1726.0 | . 90 | 1      | 1000 | 121  | 0.      | .1      | 1726.0 | *   | 1  |     | 1820 | 221  | 0.      | .1      | 1726.0 |
| 1   |     | 0145 | 22   | 0.      | .1      | 1726.0 | W .  | 1      | 1005 | 122  | 0.      | .1      | 1726.0 | *   | 1  |     | 1825 | 222  | 0.      | .1      | 1726.0 |
| 1   |     | 0150 | 23   | 0.      | .1      | 1726.0 | - 10 | 1      | 1010 | 123  | 0.      | .1      | 1726.0 | *   | 1  |     | 1830 | 223  | 0.      | .1      | 1726.0 |
| 1   |     | 0155 | 24   | 1.      | .1      | 1726.1 | +    | 1      | 1015 | 124  | 0.      | .1      | 1726.0 | *   | 1  |     | 1835 | 224  | 0.      | .1      | 1726.0 |
| 1   |     | 0200 | 25   | 1.      | .1      | 1726.1 | *    | 1      | 1020 | 125  | 0.      | .1      | 1726.0 | *   | 1  |     | 1840 | 225  | 0.      | .1      | 1726.0 |
| 1   |     | 0205 | 26   | 1.      | . 1     | 1726.1 | *    | 1      | 1025 | 126  | 0.      | . 1     | 1726.0 | *   | 1  |     | 1845 | 226  | 0.      | . 1     | 1726.0 |
| 1   |     | 0210 | 27   | 1.      | .1      | 1726.1 | *    | 1      | 1030 | 127  | 0.      | . 1     | 1726.0 | *   | 1  |     | 1850 | 227  | 0.      | . 1     | 1726.0 |
| 1   |     | 0215 | 28   | 1.      | .1      | 1726.1 | *    | 1      | 1035 | 128  | 0.      | .1      | 1726.0 | *   | 1  |     | 1855 | 228  | 0.      | .1      | 1726.0 |
| 1   |     | 0220 | 29   | 1.      | .1      | 1726.1 | *    | 1      | 1040 | 129  | 0.      | .1      | 1726.0 | *   | 1  |     | 1900 | 229  | 0.      | .1      | 1726.0 |
| 1   |     | 0225 | 30   | 1.      | .2      | 1726.1 | *    | 1      | 1045 | 130  | 0.      | . 1     | 1726.0 | *   | 1  |     | 1905 | 230  | 0.      | . 1     | 1726.0 |
| 1   |     | 0230 | 31   | 1.      | .2      | 1726.1 | *    | 1      | 1050 | 131  | 0.      | .1      | 1726.0 | *   | 1  |     | 1910 | 231  | 0.      | .1      | 1726.0 |
| 1   |     | 0235 | 32   | 2.      | .2      | 1726.1 | *    | 1      | 1055 | 132  | 0.      | .1      | 1726.0 | +   | 1  |     | 1915 | 232  | 0.      | . 1     | 1726.0 |
| 1   |     | 0240 | 33   | 2.      | .2      | 1726.2 | *    | 1      | 1100 | 133  | 0.      | .1      | 1726.0 | *   | 1  |     | 1920 | 233  | 0.      | .1      | 1726.0 |
| 1   |     | 0245 | 34   | 2.      | .2      | 1726.2 | *    | 1      | 1105 | 134  | 0.      | .1      | 1726.0 |     | 1  |     | 1925 | 234  | 0.      | . 1     | 1726.0 |

| ### SPANOTS WOJSTUO GMO WAMH NOW AG * SDATS  #### SPANOTS WOJSTUO GMO WAMH NOM AG * SDATS  #### SPANOTS WOJSTUO GM | SAMOTS W | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0 |                                       | 1234678990511111111111111111111111111111111111 | 0000 I 00000 I |
|--|----------|---------------------------------------|--|---------------------------------------|--|--|
|  |          | TATS TA HYARDORUYH<br>SITAR ,I MAJY   |  |                                       |  |  |
| ***************************************  | *******  | IM Q2 21.                             | **************************************   | COMULATIVE                            | ******   | ******   |
|  | 1726.36  | 1726.37 1726.36                       |  | # # # # # # # # # # # # # # # # # # # | 4.25   | 1729.02  |
|  | AH-56.42 | 24-HR 72-HR                           | ян-9   |                                       | (AH)   | + (FEET)   |
|  |          | MAXIMUM AVERAGE STAGE                 |  |                                       | TIME   | PEAK STAGE   |
|  | .0       | 0 °0<br>HH-Z/, HH-DZ                  | .1   |                                       | (AH)   | (TT-DA) +  |
|  | AH-26.52 | MAXIMUM AVERAGE STORAGE               | AH-9   |                                       | TIME   | PEAK STORAGE   |
|  | 906.     | 900. 900.<br>.7 .7                    | 068.<br>.7   | (INCHES)                              |  |  |
|  | . 4      | . 4                                   | 14.  | (CES)                                 | 4.25   | . ZZ +   |
|  | RH-56.45 | 24-HR 72-HR                           | ян-9   |                                       | (AH)   | + (CES)  |
|  |          | MAXIMUM AVERAGE FLOW                  |  |                                       | TIME   | DEVK EPOM  |
| 0 9221 1 0 000 5500 2 0 9221 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 5700 5700 5700 5700 0 9221 1 0 000 570 |          | Column                                | 2   92L    2   2   2   2   2   2   2   2   2   | c.t. at.  2.1                         | 66 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6         | \$74.0 T \$74.0 T \$75.0 T  |

| 1 | 0145 22             | 01                 | 1726.0 * 1               | 1005 122             | 0.  | .1 | 1726.0 *             |     | 1825 222             | 0.  |    | 1726.0           |
|---|---------------------|--------------------|--------------------------|----------------------|-----|----|----------------------|-----|----------------------|-----|----|------------------|
| 1 | 0150 23<br>0155 24  | 01                 | 1726.0 * 1<br>1726.0 * 1 | 1010 123<br>1015 124 | 0.  | .1 |                      | 1   | 1830 223<br>1835 224 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 | 0200 25             | 11                 |                          | 1020 125             | 0.  | 1  |                      | 1   | 1840 225             | 0.  | .1 | 1726.0           |
| 1 | 0205 26             | 11                 | 1726.0 * 1               | 1025 126             | 0.  | .1 | 1726.0 *             | 1   | 1845 226             | 0.  | .1 | 1726.0           |
| 1 | 0210 27             | 11                 | 1726.1 * 1               | 1030 127             | 0.  | .1 |                      | 1   | 1850 227             | 0.  | .1 | 1726.0           |
| 1 | 0215 28             | 11                 | 1726.1 * 1<br>1726.1 * 1 | 1035 128             | 0.  | .1 | 1726.0 *             |     | 1855 228<br>1900 229 | 0.  |    | 1726.0           |
| 1 | 0220 29<br>0225 30  | 11                 | 1726.1 * 1<br>1726.1 * 1 | 1040 129<br>1045 130 | 0.  | .1 | 1726.0 *<br>1726.0 * | 1   | 1905 230             | 0.  |    | 1726.0<br>1726.0 |
| 1 | 0230 31             | 12                 | 1726.1 * 1               | 1050 131             | 0.  | .1 |                      | 1   | 1910 231             | 0.  | .1 |                  |
| 1 | 0235 32             | 12                 | 1726.1 * 1               | 1055 132             | 0.  | .1 |                      | 1   | 1915 232             | 0.  | .1 | 1726.0           |
| 1 | 0240 33             | 12                 | 1726.1 * 1               | 1100 133             | 0.  | .1 |                      | 1   | 1920 233<br>1925 234 | 0.  | .1 | 1726.0           |
| 1 | 0245 34<br>0250 35  | 22                 |                          | 1105 134<br>1110 135 | 0.  | .1 | 1726.0 *             |     | 1930 235             | 0.  | .1 | 1726.0           |
| 1 | 0255 36             | 22                 | 1726.2 * 1               | 1115 136             | 0.  | .1 | 1726.0 *             | 1   | 1935 236             | 0.  | .1 | 1726.0           |
| 1 | 0300 37             | 22                 | 1726.2 * 1               | 1120 137             | 0.  | .1 |                      | 1   | 1940 237             | 0.  | .1 | 1726.0           |
| 1 | 0305 38             | 22                 | 1726.2 * 1               | 1125 138             | 0.  | .1 |                      | 1   | 1945 238<br>1950 239 | 0.  | .1 | 1726.0           |
| 1 | 0310 39<br>0315 40  | 33<br>43           |                          | 1130 139<br>1135 140 | 0.  | .1 | 1726.0 *             |     | 1955 240             | 0.  | .1 | 1726.0<br>1726.0 |
| 1 | 0320 41             | 54                 |                          | 1140 141             | 0.  | .1 | 1726.0 *             | 1   | 2000 241             | 0.  | .1 | 1726.0           |
| 1 | 0325 42             |                    | 1726.7 * 1               | 1145 142             | 0.  | .1 | 1726.0 *             | 1   | 2005 242             | 0.  | .1 | 1726.0           |
| 1 |                     | 129                |                          | 1150 143             | 0.  | .1 | 1726.0 *<br>1726.0 * | 1   | 2010 243<br>2015 244 | 0.  |    | 1726.0<br>1726.0 |
| 1 |                     | 18. 1.3<br>22. 1.6 | 1728.1 * 1               | 1155 144<br>1200 145 | 0.  | .1 | 1726.0 *             | 1   | 2020 245             | 0.  | .1 | 1726.0           |
| 1 |                     | 23. 2.0            | 1728.3 * 1               | 1205 146             | 0.  | .1 | 1726.0 *             | 1   | 2025 246             | 0.  | .1 | 1726.0           |
| 1 | 0350 47             | 24. 2.2            | 1728.5 * 1               | 1210 147             | 0.  | .1 |                      | 1   | 2030 247             | 0.  | .1 | 1726.0           |
| 1 |                     | 25. 2.5<br>26. 2.6 | 1728.6 * 1<br>1728.7 * 1 | 1215 148<br>1220 149 | 0.  | .1 | 1726.0 *             |     | 2035 248<br>2040 249 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 |                     | 26. 2.7            |                          | 1225 150             | 0.  | .1 | 1726.0 *             | 1   | 2045 250             | 0.  | .1 | 1726.0           |
| 1 | 0410 51             | 26. 2.8            | 1728.9 * 1               | 1230 151             | 0.  | .1 | 1726.0 *             | 1   | 2050 251             | 0.  | .1 | 1726.0           |
| 1 |                     | 26. 2.8            | 1728.9 * 1               | 1235 152             | 0.  | .1 |                      | 1   | 2055 252             | 0.  | .1 | 1726.0           |
| 1 |                     | 26. 2.8<br>26. 2.8 | 1728.9 * 1<br>1728.9 * 1 | 1240 153<br>1245 154 | 0.  | .1 | 1726.0 * 1726.0 *    |     | 2100 253<br>2105 254 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 |                     | 26. 2.8            | 1728.8 * 1               | 1250 155             | 0.  | .1 | 1726.0 *             |     | 2110 255             | 0.  | .1 | 1726.0           |
| 1 |                     | 26. 2.7            | 1728.8 * 1               | 1255 156             | 0.  | .1 | 1726.0 *             |     | 2115 256             | 0.  |    | 1726.0           |
| 1 |                     | 26. 2.7            |                          | 1300 157<br>1305 158 | 0.  | .1 | 1726.0 *             | 1   | 2120 257<br>2125 258 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 |                     | 26. 2.7<br>26. 2.7 | 1728.8 * 1<br>1728.8 * 1 | 1310 159             | 0.  | .1 |                      | 1   | 2130 259             | 0.  | .1 | 1726.0           |
| 1 |                     | 26. 2.7            | 1728.8 * 1               | 1315 160             | 0.  | .1 | 1726.0 *             | 1   | 2135 260             | 0.  | .1 | 1726.0           |
| 1 |                     | 26. 2.7            | 1728.8 * 1               | 1320 161             | 0.  | .1 | 1726.0 *             | 1   | 2140 261             | 0.  | .1 | 1726.0           |
| 1 |                     | 26. 2.6            | 1728.7 * 1<br>1728.7 * 1 | 1325 162             | 0.  | .1 | 1726.0 *<br>1726.0 * | 1   | 2145 262<br>2150 263 | 0.  | .1 | 1726.0           |
| 1 |                     | 25. 2.6<br>25. 2.5 | 1728.7 * 1<br>1728.6 * 1 | 1330 163<br>1335 164 | 0.  | .1 | 1726.0 *             | 1   | 2155 264             | 0.  | .1 | 1726.0           |
| 1 |                     | 25. 2.4            | 1728.6 * 1               | 1340 165             | 0.  | .1 | 1726.0 *             | 1   | 2200 265             | 0.  | .1 | 1726.0           |
| 1 |                     | 25. 2.3            | 1728.5 * 1               | 1345 166             | 0.  | .1 | 1726.0 *             | 1   | 2205 266             | 0.  | .1 | 1726.0           |
| 1 |                     | 24. 2.2<br>24. 2.1 | 1728.4 * 1<br>1728.4 * 1 | 1350 167<br>1355 168 | 0.  | .1 | 1726.0 *             | 1   | 2210 267<br>2215 268 | 0.  | .1 | 1726.0           |
| 1 |                     | 23. 1.9            | 1728.3 * 1               | 1400 169             | 0.  | .1 |                      |     | 2220 269             | 0.  | .1 | 1726.0           |
| 1 | 0545 70             | 23. 1.8            | 1728.2 * 1               | 1405 170             | 0.  | .1 | 1726.0 *             | 1   | 2225 270             | 0.  | .1 | 1726.0           |
| 1 |                     | 22. 1.7            | 1728.1 * 1               | 1410 171             | 0.  | .1 | 1726.0 *<br>1726.0 * | 1   | 2230 271<br>2235 272 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 |                     | 22. 1.5<br>20. 1.4 | 1728.0 * 1<br>1727.8 * 1 | 1415 172<br>1420 173 | 0.  | .1 | 1726.0 *             | 1   | 2240 273             | 0.  | .1 | 1726.0           |
| î |                     | 18. 1.3            | 1727.7 * 1               | 1425 174             | 0.  | .1 | 1726.0 *             | 1   | 2245 274             | 0.  | .1 | 1726.0           |
| 1 |                     | 17. 1.2            | 1727.5 * 1               | 1430 175             | 0.  | .1 | 1726.0 *             |     | 2250 275             | 0.  | .1 | 1726.0           |
| 1 |                     | 15. 1.1<br>14. 1.0 | 1727.4 * 1<br>1727.3 * 1 | 1435 176<br>1440 177 | 0.  | .1 |                      | 1   | 2255 276<br>2300 277 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 |                     | 139                | 1727.1 * 1               | 1445 178             | 0.  | .1 | 1726.0 *             | î   | 2305 278             | 0.  | .1 | 1726.0           |
| 1 | 0630 79             | 118                | 1727.0 * 1               | 1450 179             | 0.  | .1 | 1726.0 *             | 1   | 2310 279             | 0.  | .1 | 1726.0           |
| 1 |                     | 108                | 1726.9 * 1               | 1455 180             | 0.  | .1 | 1726.0 *             | 1   | 2315 280             | 0.  | .1 | 1726.0           |
| 1 | 0640 81<br>0645 82  | 97                 |                          | 1500 181<br>1505 182 | 0.  | .1 | 1726.0 *             | 1   | 2320 281<br>2325 282 | 0.  | .1 | 1726.0           |
| 1 | 0650 83             | 86                 |                          | 1510 183             | 0.  | .1 | 1726.0 *             | 1   | 2330 283             | 0.  | .1 | 1726.0           |
| 1 | 0655 84             | 75                 | 1726,6 * 1               | 1515 184             | 0.  | .1 | 1726.0 *             | 1   | 2335 284             | 0.  | .1 | 1726.0           |
| 1 | 0700 85             | 65                 | 1726.6 * 1               | 1520 185             | 0.  | .1 | 1726.0 *             |     | 2340 285<br>2345 286 | 0.  | .1 | 1726.0           |
| 1 | 0705 86<br>0710 87  | 65<br>54           | 1726.5 * 1<br>1726.5 * 1 | 1525 186<br>1530 187 | 0.  | .1 | 1726.0 *             | 1   | 2345 286 2350 287    | 0.  | .1 | 1726.0<br>1726.0 |
| 1 | 0715 88             | 54                 | 1726.4 * 1               | 1535 188             | 0.  | .1 | 1726.0 *             | 1   | 2355 288             | 0.  | .1 | 1726.0           |
| 1 | 0720 89             | 44                 | 1726.4 * 1               | 1540 189             | 0.  | .1 |                      | 2   | 0000 289             | 0.  | .1 | 1726.0           |
| 1 | 0725 90<br>0730 91  | 43<br>33           | 1726.3 * 1<br>1726.3 * 1 | 1545 190<br>1550 191 | 0.  | .1 |                      | 2   | 0005 290<br>0010 291 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 | 0735 92             | 33                 | 1726.3 * 1               | 1555 192             | 0.  | .1 | 1726.0 *             | 2   | 0015 292             | 0.  | .1 | 1726.0           |
| 1 | 0740 93             | 33                 | 1726.3 * 1               | 1600 193             | 0.  | .1 | 1726.0 *             | 2   | 0020 293             | 0.  | .1 | 1726.0           |
| 1 | 0745 94             | 22                 | 1726.2 * 1               | 1605 194             | 0.  | .1 | 1726.0 *             | 2   | 0025 294             | 0.  | .1 | 1726.0           |
| 1 | 0750 95<br>0755 96  | 22                 | 1726.2 * 1<br>1726.2 * 1 | 1610 195<br>1615 196 | 0.  | .1 | 1726.0 *<br>1726.0 * | 2   | 0030 295<br>0035 296 | 0.  | .1 | 1726.0           |
| 1 | 0800 97             | 22                 | 1726.2 * 1               | 1620 197             | 0.  | .1 | 1726.0 *             | 2   | 0040 297             | 0.  | .1 | 1726.0           |
| 1 | 0805 98             | 22                 | 1726.1 * 1               | 1625 198             | 0.  | .1 | 1726.0 *             | 2   | 0045 298             | 0.  | .1 | 1726.0           |
| 1 | 0810 99<br>0815 100 | 12                 | 1726.1 * 1<br>1726.1 * 1 | 1630 199             | 0.  | .1 |                      | 2   | 0050 299<br>0055 300 | 0.  | .1 | 1726.0<br>1726.0 |
| 1 | 0815 100            | 12                 | 1726.1 * 1               | 1635 200             | .01 |    | 1720.0 *             | de. | 0035 500             | 0.5 |    | 1120.0           |

|    | PEAK FLOW         | TIME         |                              |                   | MAXIMIM A  | VERAGE FLOW            |                  |
|----|-------------------|--------------|------------------------------|-------------------|------------|------------------------|------------------|
| ,  | The Lucia         |              |                              | 6-HR              | 24-HR      | 72-HR                  | 24.92-HR         |
| +  | (CFS)             | (HR)         |                              | 0.111             | 24 1111    | ( * ++++               |                  |
| +  | 26.               | 4.25         | (CFS)<br>(INCHES)<br>(AC-FT) | 13.<br>.838<br>7. | .852<br>7. | 3.<br>.852<br>7.       | 3.<br>.852<br>7. |
| PE | EAK STORAGE       | TIME         |                              | 6-HR              | MAXIMUM AV | ERAGE STORAGE<br>72-HR | 24.92-HR         |
| +  | (AC-FT)<br>3.     | (HR)<br>4.25 |                              | 1.                | 0.         | 0.                     | 0.               |
| I  | PEAK STAGE        | TIME         |                              | 6-HR              | MAXIMUM A  | VERAGE STAGE<br>72-HR  | 24.92+HR         |
| +  | (FEET)<br>1728.88 | (HR)<br>4.25 |                              | 1727.35           | 1726.34    | 1726.33                | 1726.33          |
|    |                   |              | CUMULATIV                    | E AREA =          | .15 SQ M   | I                      |                  |

<sup>\*\*\*</sup> FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION=  $\,1\,$ 

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES TIME TO FEAK IN HOURS

OPERATION STATION AREA PLAN RATIO 1 RATIO 2 RATIO 3 1.00 .60 .58

HYDROGRAPH AT + OND9 .00 1 FLOW 3. 2. 1.

|                    |          |     |   | TIME              | 3.50                | 3.50        | 3.50        |
|--------------------|----------|-----|---|-------------------|---------------------|-------------|-------------|
| HYDROGRAPH AT      | OFFEX3   | .03 | 1 | FLOW<br>TIME      | 21.                 | 8.<br>3.75  | 7.<br>3.75  |
| 2 COMBINED AT      | CP-7     | .03 | 1 | FLOW              | 23.                 | 8.          | 8.          |
| HYDROGRAPH AT      | OND8     | .02 | 1 | TIME              | 3.67                | 3.75        | 3.75        |
| ROUTED TO          | ROND8-CP | .02 | 1 | TIME              | 3.58                | 3.58        | 3.58        |
| HYDROGRAPH AT      |          |     |   | TIME              | 3.67                | 3.67        | 3.67        |
| +<br>HYDROGRAPH AT | OND10    | .01 | 1 | FLOW              | 3.58                | 3.58        | 3.58        |
| +<br>3 COMBINED AT | OFFEX5   | .01 | 1 | FLOW .            | 10.<br>3.58         | 4.<br>3.58  | 4.<br>3.58  |
| *                  | CP-9     | .04 | 1 | FLOW<br>TIME      | 51.<br>3.58         | 23.<br>3.67 | 22.<br>3.67 |
| ROUTED TO          | RCP9-CP- | .04 | 1 | FLOW<br>TIME      | 50.<br>3.58         | 23.<br>3.67 | 22.<br>3.67 |
| HYDROGRAPH AT      | OND12    | .00 | 1 | FLOW<br>TIME      | 8.<br>3.50          | 4.<br>3.50  | 4.<br>3.50  |
| 2 COMBINED AT      | CP-10A   | .04 | 1 | FLOW<br>TIME      | 55.<br>3.58         | 25.<br>3.67 | 24.<br>3.67 |
| HYDROGRAPH AT      | OND11    | .01 | 1 | FLOW<br>TIME      |                     | 12.<br>3.58 | 11.<br>3.58 |
| HYDROGRAPH AT      | OND13    | .01 | 1 | FLOW<br>TIME      | 12.                 | 6.<br>3.50  | 6.          |
| 3 COMBINED AT      | CP-10    | .06 | 1 | FLOW              | 90.                 | 42.         | 40.         |
| ROUTED TO          | EOBASIN  | .06 | 1 | TIME              | 3.58                |             | 3.58        |
|                    |          |     |   | TIME<br>PEAK STAG | 3.83<br>SES IN FEET | 3.83        | 3.83        |
|                    |          |     | 1 | STAGE             | 1747.53<br>3.83     | 3.83        | 3.83        |
| DIVERSION TO       | DVPIPE   | .06 | 1 | FLOW<br>TIME      | 54.<br>3.83         | 27.<br>3.83 | 26.<br>3.83 |
| HYDROGRAPH AT      | DIVWEIR  | .06 | 1 | FLOW<br>TIME      | 0.                  | 0.          | 0.          |
| HYDROGRAPH AT +    | OND14    | .02 | 1 | FLOW<br>TIME      | 31.<br>3.50         | 15.<br>3.50 | 14.<br>3.50 |
| 2 COMBINED AT      | CP-11    | .08 | 1 | FLOW<br>TIME      | 31.<br>3.50         | 15.<br>3.50 | 14.<br>3.50 |
| HYDROGRAPH AT      | OND1     | .00 | 1 | FLOW<br>TIME      | 3.                  | 1.<br>3.50  | 1.<br>3.50  |
| HYDROGRAPH AT      | OFFEX2   | .01 | 1 | FLOW              | 13.                 | 4           | 4.<br>3.58  |
| 2 COMBINED AT      | CP-1     | .02 | 1 | TIME              | 15.                 | 5.          | 4.          |
| ROUTED TO          | RCP1-CP2 | 00  | 1 | TIME              | 3,58                |             | 3.58        |
| HYDROGRAPH AT      |          | .02 |   | FLOW<br>TIME      | 14.<br>3.58         |             | 3.67        |
| +<br>HYDROGRAPH AT | OND2     | .01 | 1 | FLOW<br>TIME      | 8.<br>3.58          | 4.<br>3.58  | 3.58        |
| *                  | OFFEX1   | .07 | 1 | FLOW<br>TIME      | 48.<br>3.67         | 14.<br>3.67 | 13.<br>3.67 |
| 3 COMBINED AT      | CP-2     | .09 | 1 | FLOW<br>TIME      | 68.<br>3.67         | 22.<br>3.67 | 20.<br>3.67 |
| ROUTED TO          | RCP2-CP- | .09 | 1 | FLOW<br>TIME      | 68.<br>3.67         | 21.<br>3.67 | 19.<br>3.67 |
| HYDROGRAPH AT      | OND3     | .00 | 1 | FLOW<br>TIME      | 4.<br>3.50          | 3.50        | 2.<br>3.50  |
| 2 COMBINED AT      | CP-3     | .09 | 1 | FLOW<br>TIME      | 70.<br>3.67         |             | 20.<br>3.67 |
| ROUTED TO          | RCP3-CP4 | .09 | 1 | FLOW              | 69.                 |             | 19.         |

|               |         |     |    | TIME         | 3.67                            | 3.67        | 3.75        |
|---------------|---------|-----|----|--------------|---------------------------------|-------------|-------------|
| HYDROGRAPH AT | OND7    | .01 | 1  | FLOW<br>TIME | 16.<br>3.50                     | 8.<br>3.50  | 7.<br>3.50  |
| 2 COMBINED AT | CP-4    | .10 | 1  | FLOW<br>TIME | 79.<br>3.58                     | 26.<br>3.67 | 24.<br>3.67 |
| HYDROGRAPH AT | OND4    | .02 | 1  | FLOW<br>TIME | 27.<br>3.58                     | 13.<br>3.58 | 12.<br>3.58 |
| HYDROGRAPH AT | OND5    | .01 | 1  | FLOW<br>TIME | 12.<br>3.58                     | 6.<br>3.58  | 6.<br>3.58  |
| 2 COMBINED AT | CP-5    | .03 | 1  | FLOW<br>TIME | 40.<br>3.58                     | 19.<br>3.58 | 18.<br>3.58 |
| HYDROGRAPH AT | OND6    | .02 | 1  | FLOW<br>TIME | 23.<br>3.58                     | 11.<br>3.58 | 11.<br>3.58 |
| HYDROGRAPH AT | DVPIPE  | .00 | 1  | FLOW<br>TIME | 54.<br>3.83                     | 27.<br>3.83 | 26.<br>3.83 |
| ROUTED TO     | RDVPIPE | .00 | 1  | FLOW<br>TIME | 54.<br>3.83                     | 27.<br>3.83 | 26.<br>3.83 |
| HYDROGRAPH AT | DETPD   | .01 | 1  | FLOW<br>TIME | 16.<br>3.50                     | 8.<br>3.50  | 8.          |
| 5 COMBINED AT | CP-6    | .15 | 1  | FLOW<br>TIME | 190.<br>3.58                    | 79.<br>3.58 | 74.<br>3.58 |
| ROUTED TO     | DETPOND | .15 | 1  | FLOW<br>TIME | 41.<br>5.08                     | 27.<br>4.25 | 26.<br>4.25 |
|               |         |     | ** |              | AGES IN FEET<br>1732.22<br>5.08 | **          | 1728.88     |
| HYDROGRAPH AT | OFFD-14 | .00 | 1  | FLOW<br>TIME | 3.                              | 2.          | 1.          |
| ROUTED TO     | RT-B14  | .00 | 1  | FLOW<br>TIME | 3.3.67                          | 1.          | 1. 3.67     |
| HYDROGRAPH AT | BMIC-1  | .01 | 1  | FLOW<br>TIME | 26.<br>3.50                     | 13.<br>3.50 | 12.         |
| 2 COMBINED AT | C15     | .02 | 1  | FLOW<br>TIME | 28.<br>3.50                     | 14.<br>3.50 | 13.<br>3.50 |
| ROUTED TO     | RT-14   | .02 | 1  | FLOW<br>TIME | 27.<br>3.50                     | 13.<br>3.50 | 13.         |
| HYDROGRAPH AT | BMIC-2  | .01 | 1  | FLOW<br>TIME | 22.<br>3.50                     | 11.         | 11.<br>3.50 |
| 2 COMBINED AT | C16     | .03 | 1  | FLOW<br>TIME | 50.<br>3.50                     | 25.         | 24.<br>3.50 |
| ROUTED TO     | RT-15   | .03 | 1  | FLOW<br>TIME | 49.                             | 24.         | 23.         |
| HYDROGRAPH AT | SCH-2   | .01 | 1  | FLOW         | 13.<br>3.50                     | 3.50<br>7.  | 3.50        |
| 2 COMBINED AT | C17     | .04 | 1  | TIME         | 61.<br>3.50                     |             | 3.50        |
| ROUTED TO     | RT-16   | .04 | 1  | FLOW         | 59.<br>3.50                     | 29          | 27          |
| HYDROGRAPH AT | BMIC-3  | .01 | 1  | TIME         | 21.                             | 11.         | 10.         |
| HYDROGRAPH AT | MGDEV-2 | .01 | 1  | TIME         | 3.50                            | 3.50        | 3.50        |
| 4 COMBINED AT | C18     | .20 | 1  | TIME         | 3.50<br>123.                    | 3.50<br>62. | 3.50        |
| HYDROGRAPH AT | HR3     | .00 | 1  | FLOW         | 3.50                            | 1.          | 1.          |
| HYDROGRAPH AT | HR2     | .00 | 1  | TIME         | 3.50                            | 3.50        | 3.50        |
| HYDROGRAPH AT | HR1     | .00 | 1  | TIME         | 3.50                            | 3.50        | 3.50        |
| 3 COMBINED AT | CHR1    | ,00 | 1  | TIME         | 3.50                            | 3.50        | 3.50        |
|               |         |     |    |              |                                 |             |             |

|                   |                      |                      |             | TIME                                    |             | 3.50         | 3.50        | 3.50              |                               |                 |                            |          |     |
|-------------------|----------------------|----------------------|-------------|---|-------------|--------------|-------------|-------------------|-------------------------------|-----------------|----------------------------|----------|-----|
| 2 COMBIN          | ED AT                | C18B                 | .21         | 1 FLOW                                  |             | 133.<br>3.50 | 67.<br>3.50 | 64.<br>3.50       |                               |                 |                            |          |     |
| HYDROGRAP         |                      | OND15                | .03         | 1 FLOW                                  |             | 57.          | 28          | 27.               |                               |                 |                            |          |     |
|                   |                      | ONDIS                | .03         | TIME                                    |             | 3.50         | 3.50        | 3.50              |                               |                 |                            |          |     |
| HYDROGRAP<br>+    |                      | OFFEX4               | .01         | 1 FLOW<br>TIME                          |             | 14.<br>3.58  | 6.<br>3.58  | 5.<br>3.58        |                               |                 |                            |          |     |
| 1                 |                      |                      |             |   |             |              |             |                   | -CUNGE ROUT                   | TING            |                            |          |     |
|                   |                      |                      |             | (                                       | FLOW IS     | DIRECT       | RUNOFF W    |                   | SE FLOW) INTERPOL COMPUTATION |                 |                            |          |     |
|                   | ISTAQ                | ELEMENT              | DT          | PEAK                                    | TIME<br>PEA |              | VOLUME      | DT                | PEAK                          | TIME TO<br>PEAK | VOLUME                     |          |     |
|                   |                      |                      | (MIN)       | (CFS)                                   | (M          | IIN)         | (IN)        | (MIN)             | (CFS)                         | (MIN)           | (IN)                       |          |     |
|                   | ROND8-CF             | N = 1 RATIO=<br>MANE | 1.62        | 32.92                                   | 217.        | 65           | 1.82        | 5.00              | 31.53                         | 220.00          | 1.82                       |          |     |
| CONTINUIT         | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .2161E+01                               | EXCESS=     | .00001       | e+00 OUTFLO | OW= .2168         | E+01 BASIN                    | STORAGE=        | .6696E-06 PERCENT          | ERROR=   | -,3 |
|                   | FOR PLAN             | N = 1 RATIO=         | .60         | 15.86                                   | 219.        | 44           | .84         | 5.00              | 15.62                         | 220.00          | .84                        |          |     |
| CONTINUIT         | y summary            | (AC-FT) - I          | NFLOW=      | 9996E+00                                | EXCESS=     | .0000        |             |                   | E+01 BASIN                    | STORAGE=        | .5867E-06 PERCENT          | ERROR=   | 3   |
|                   |                      | V = 1 RATIO=         |             |   |             |              |             | 31/2 2-23/8       |                               |                 |                            |          |     |
|                   | ROND8-CF             |                      | 2.07        | 14.96                                   | 218.        | 61           | .80         | 5.00              | 14.69                         | 220.00          | .80                        |          |     |
| CONTINUIT         | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .9454E+00                               | EXCESS=     | .0000E       | E+00 OUTFLO | OW= .9483         | E+00 BASIN                    | STORAGE=        | .6885E-06 PERCENT          | * EFROR= | - 3 |
|                   | POR PLAN<br>RCP9-CP- | N = 1 RATIO=<br>MANE | 1.00        | 50.82                                   | 216.        | 00           | 1.74        | 5.00              | 49.63                         | 215.00          | 1.75                       |          |     |
| CONTINUIT         | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .3439E+01                               | EXCESS=     | .00001       | E+00 OUTFLO | OW= .3440         | E+01 BASIN                    | STORAGE=        | .3381E-06 PERCENT          | ERROR=   | .0  |
|                   | FOR PLAN             | r = 1 RATIO=         | .60         |   |             |              |             |                   |                               |                 |                            |          |     |
|                   | RCP9-CP-             | MANE                 | .50         | 23.33                                   | 220.        | 56           | .79         | 5.00              | 23.32                         | 220.00          | .79                        |          |     |
| CONTINUIT         | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .1560E+01                               | EXCESS=     | .00001       | +00 OUTFLO  | OW= .1561         | E+01 BASIN                    | STORAGE=        | .3045E-06 PERCENT          | ERROR=   | .0  |
|                   | FOR PLAN<br>RCP9-CP- | I = 1 RATIO=<br>MANE | .58<br>.57  | 21.96                                   | 220.        | 31           | .75         | 5.00              | 21.96                         | 220.00          | .75                        |          |     |
| CONTINUIT         | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .1473E+01                               | EXCESS=     | .0000E       | +00 OUTFL   | OW= .1474         | E+01 BASIN                    | STORAGE=        | .3331E-06 PERCENT          | ERROR=   | .0  |
|                   | FOR PLAN             | = 1 RATIO=           | 1.00        | 14.82                                   | 218.        | 3.4          | 1.07        | 5.00              | 14.37                         | 215.00          | 1.07                       |          |     |
| CONTINUIT         | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | 9363E+00                                | EXCESS=     | .00007       | +00 OUTFL   |                   | E+00 BASIN                    | STORAGE=        | .2101E-06 PERCENT          | ERROR=   | - 2 |
| 0.00112.2110.2.2. |                      | = 1 RATIO=           |             | .,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | INCLIDE-    | .00001       |             | 311- 12300        | D100 D1011                    | 0101010         | 12-V-12-00   1-13-10-11-11 | Littor-  |     |
|                   | RCP1-CP2             |                      | 2.17        | 4.84                                    | 219.        | 55           | .36         | 5.00              | 4.79                          | 220.00          | .36                        |          |     |
| CONTINUIT         | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .3181E+00                               | EXCESS=     | .0000E       | +00 OUTFLO  | OW= .3191         | E+00 BASIN                    | STORAGE=        | .2143E-06 PERCENT          | ERROR=   | 3   |
|                   | FOR PLAN<br>RCP1-CP2 | = 1 RATIO=<br>  MANE | .58<br>2.23 | 4.38                                    | 220.        | 13           | .33         | 5.00              | 4.37                          | 220.00          | .33                        |          |     |
| CONTINUITY        | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .2929E+00                               | EXCESS=     | .0000E       | +00 OUTFLO  | OW= .2937         | E+00 BASIN                    | STORAGE=        | .1728E-06 PERCENT          | ERROR=   | 3   |
|                   |                      | = 1 RATIO=           |             |   |             |              |             |                   |                               |                 |                            |          |     |
|                   | RCP2-CP-             |                      |             |   |             |              |             |                   |                               |                 | 1.02                       |          |     |
| CONTINUITY        |                      |                      |             | .4810E+01                               | EXCESS=     | .00001       | 00 OUTFLO   | OW= .4810         | E+01 BASIN                    | STORAGE=        | .9178E-07 PERCENT          | ERROR=   | .0  |
|                   | FOR PLAN<br>RCP2-CP- | 1 = 1 RATIO=<br>MANE | .60         | 21.49                                   | 220.        | 45           | .34         | 5.00              | 21.35                         | 220.00          | .34                        |          |     |
| CONTINUITY        | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .1596E+01                               | EXCESS=     | .00001       | +00 OUTFLO  | OW= .1596         | E+01 BASIN                    | STORAGE=        | .8670E-07 PERCENT          | ERROR=   | .0  |
|                   | FOR PLAN             | = 1 RATIO=           | .58         | 19.59                                   | 220         | 58           | 31          | 5.00              | 19.38                         | 220.00          | .31                        |          |     |
| CONTINUITO        | Y SUMMARY            | (AC-FT) - T          |             |   |             |              |             |                   |                               |                 | .8727E-07 PERCENT          | ERROP-   | .0  |
|                   |                      | = 1 RATIO=           |             |   | -CAMAD      |              | OF OUT DO   |                   | MIGIN                         |                 | TENCENT                    | andre-   |     |
|                   | RCP3-CP4             |                      | .61         | 69.46                                   | 220.        | 77           | 1.04        | 5.00              | 69.27                         | 220.00          | 1.04                       |          |     |
| CONTINUITY        | Y SUMMARY            | (AC-FT) - I          | NFLOW=      | .5012E+01                               | EXCESS=     | .00001       | E+00 OUTFLO | OW= .5015         | E+01 BASIN                    | STORAGE=        | .4675E-06 PERCENT          | ERROR=   | 1   |
|                   | FOR PLAN<br>RCP3-CP4 | 1 = 1 RATIO=<br>MANE | .60         | 22.00                                   | 222.        | 28           | .35         | 5.00              | 21.43                         | 220.00          | .35                        |          |     |
| COMPUTABLITATI    | V CIBBIATO           | (AC PE) T            | MET ON-     | 16050.01                                | nyanaa      | 0000         | . 00 OUMBI  | 264 1.50 <i>6</i> | D.O. DECEN                    | CMOD 3 OF       | ACAER OF PROGRAM           | PROPER   |     |

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1685E+01 EXCESS= .0000E+00 OUTFLOW= .1686E+01 BASIN STORAGE= .4645E-06 PERCENT ERROR= -.1

| co | FOR PLAN<br>RCP3-CP4 | = 1 RATIO=<br>MANE   | 1.00        | 20.05      | 221     | .90       | .32      | 5.00       | 19.47    | 225.00   | .32               |        |    |
|----|----------------------|----------------------|-------------|------------|---------|-----------|----------|------------|----------|----------|-------------------|--------|----|
| co |                      |                      |             |            |         |           |          |            |          |          |                   |        |    |
|    | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 1550E+01 1 | EXCESS= | .0000E+00 | OUTFLOW: | = .1551E+0 | 01 BASIN | STORAGE= | .4728E-06 PERCENT | ERROR= | 1  |
|    | FOR PLAN<br>RDVPIPE  | = 1 RATIO= 1<br>MANE | 1.00        | 54.03      | 231     | .40 -1    | .00      | 5.00       | 54.01    | 230.00   | -1.00             |        |    |
|    | FOR PLAN<br>RDVPIPE  | = 1 RATIO=<br>MANE   | .60<br>1.27 | 27.47      | 231     | .34 -1    | .00      | 5.00       | 27.45    | 230.00   | -1.00             |        |    |
|    | FOR PLAN<br>RDVPIPE  | = 1 RATIO=<br>MANE   | .58<br>1.18 | 26.15      | 231     | .54 -1    | .00      | 5.00       | 26.12    | 230.00   | -1.00             |        |    |
|    | FOR PLAN<br>RT-B14   | = 1 RATIO= 1<br>MANE | 1.00        | 3.39       | 218     | . 69 1    | .64      | 5.00       | 3,37     | 220.00   | 1.63              |        |    |
| co | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 2438E+00 1 | EXCESS= | .0000E+00 | OUTFLOW: | = .2442E+( | 00 BASIN | STORAGE= | .7570E-08 PERCENT | ERROR= | 2  |
|    | FOR PLAN<br>RT-B14   | = 1 RATIO=<br>MANE   | .60<br>1.71 | 1.51       | 223     | .43       | .71      | 5.00       | 1.50     | 220.00   | .71               |        |    |
| co | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 1061E+00 I | EXCESS= | .0000E+00 | OUTFLOW: | = .1063E+0 | 00 BASIN | STORAGE= | .7638E-08 PERCENT | ERROR= | 2  |
|    | FOR PLAN<br>RT-B14   | = 1 RATIO=<br>MANE   | .58<br>1.76 | 1.42       | 222     | .80       | .67      | 5.00       | 1.41     | 220.00   | .67               |        |    |
| co | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 9979E-01 1 | EXCESS= | .0000E+00 | OUTFLOW: | = .9993E-0 | 01 BASIN | STORAGE= | .5886E-03 PERCENT | ERROR= | 1  |
|    |                      | = 1 RATIO= 1<br>MANE | .00         | 27.93      | 210     | .77 1     | .91      | 5.00       | 27.32    | 210.00   | 1.91              |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 1720E+01 I | EXCESS= | .0000E+00 | OUTFLOW: | = .1721E+0 | )1 BASIN | STORAGE= | .7751E-08 PERCENT | ERROR= | .0 |
|    |                      | = 1 RATIO=<br>MANE   | .60         | 13.81      | 211.    | .01       | .91      | 5.00       | 13.40    | 210.00   | .91               |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 8203E+00 1 | EXCESS= | .0000E+00 | OUTFLOW: | = .8205E+0 | 00 BASIN | STORAGE= | .6549E-08 PERCENT | ERROR= | .0 |
|    |                      | = 1 RATIO=<br>MANE   | .58         | 13.17      | 210.    | .75       | .86      | 5.00       | 12.73    | 210.00   | .86               |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 7778E+00 1 | EXCESS= | .0000E+00 | OUTFLOW: | = ,7780E+0 | 00 BASIN | STORAGE= | .6560E-08 PERCENT | ERROR= | .0 |
|    |                      | = 1 RATIO= 1<br>MANE | .36         | 49.16      | 210.    | 62 1      | .93      | 5.00       | 48.56    | 210.00   | 1.94              |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW=       | 2959E+01 H | EXCESS= | .0000E+00 | OUTFLOW: | = .2959E+0 | )1 BASIN | STORAGE= | .9128E-08 PERCENT | ERROR= | .0 |
|    |                      | = 1 RATIO=<br>MANE   | .60         | 24.51      | 210.    | 82        | .93      | 5.00       | 24.04    | 210.00   | .93               |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 1419E+01 H | EXCESS= | .0000E+00 | OUTFLOW: | = .1420E+0 | )1 BASIN | STORAGE= | .8611E-08 PERCENT | ERROR= | .0 |
|    |                      | = 1 RATIO=<br>MANE   | .58<br>.35  | 23.31      | 210.    | 84        | .88      | 5.00       | 22.85    | 210.00   | .88               |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 1347E+01 E | EXCESS= | .0000E+00 | OUTFLOW: | = .1347E+0 | )1 BASIN | STORAGE= | .8421E-08 PERCENT | ERROR= | .0 |
|    |                      | = 1 RATIO= 1<br>MANE | .53         | 60.94      | 211.    | 13 1      | .94      | 5.00       | 58.94    | 210.00   | 1.95              |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | LOW=        | 3645E+01 E | EXCESS= | .0000E+00 | OUTFLOW: | : .3647E+0 | 1 BASIN  | STORAGE= | .3120E-07 PERCENT | ERROR= | 1  |
|    |                      | = 1 RATIO=<br>MANE   | .60         | 30.36      | 211.    | 36        | .93      | 5.00       | 28.90    | 210.00   | .93               |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 1751E+01 E | EXCESS= | .0000E+00 | OUTFLOW: | : .1752E+0 | )1 BASIN | STORAGE= | .3374E-07 PERCENT | ERROR= | 1  |
|    |                      | = 1 RATIO=<br>MANE   | .58         | 28.82      | 211.    | .06       | .89      | 5.00       | 27.44    | 210.00   | .89               |        |    |
| CO | NTINUITY SUMMARY     | (AC-FT) - INF        | FLOW= .     | 1661E+01 I | EXCESS= | .0000E+00 | OUTFLOW: | = .1663E+0 | )1 BASIN | STORAGE= | .3305E-07 PERCENT | ERROR= | 1  |

## **LEGEND**

ONSITE BASIN BOUNDARY OFFSITE BASIN BOUNDARY REFERENCED BASIN BOUNDARY ONSITE BASIN LABEL OFFSITE BASIN LABEL REFERENCED BASIN LABEL HEC-1 COMBINATION POINT DISCHARGE POINT

## NOTES

FLOW DIRECTION

REFERENCED BASIN BOUNDARY

EXISTING LANDFILL BOUNDARY

"ADDENDUM #1 TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMERCE CENTER TWO (FORMERLY KNOWN AS HARSCH)" PREPARED BY PBS&J (FEBRUARY 2003) WAS USED FOR REFERENCED BASINS

|   | BASIN ID | AREA (ac) | Q <sub>100</sub> (cfs) | Q <sub>10</sub> (cfs) |
|---|----------|-----------|------------------------|-----------------------|
|   | OND1     | 0.94      | 3                      | 1                     |
|   | OND2     | 3.70      | 8                      | 4                     |
|   | OND3     | 1.38      | 4                      | 2                     |
|   | OND4     | 11.67     | 27                     | 13                    |
|   | OND5     | 5.03      | 12                     | 6                     |
|   | OND6     | 9.90      | 23                     | 11                    |
|   | OND7     | 5.87      | 16                     | 8                     |
|   | OND8     | 14.26     | 33                     | 16                    |
|   | OND9     | 1.06      | 3                      | 2                     |
|   | OND10    | 4.28      | 10                     | 5                     |
|   | OND11    | 9.60      | 24                     | 12                    |
|   | OND12    | 2.77      | 8                      | 4                     |
|   | OND13    | 4.70      | 12                     | 6                     |
|   | OND14    | 11.12     | 31                     | 15                    |
|   | OND15    | 21.47     | 57                     | 28                    |
|   | DETPD    | 5.14      | 16                     | 8                     |
|   | OFFEX1   | 42.20     | 48                     | 14                    |
|   | OFFEX2   | 9.63      | 13                     | 4                     |
|   | OFFEX3   | 16.40     | 21                     | 8                     |
|   | OFFEX4   | 7.61      | 14                     | 6                     |
|   | OFFEX5   | 5.11      | 10                     | 4                     |
|   | CP-1     | NA        | 15                     | 5                     |
|   | CP-2     | NA        | 68                     | 22                    |
|   | CP-3     | NA        | 70                     | 22                    |
|   | CP-4     | NA        | 79                     | 26                    |
|   | CP-5     | NA        | 40                     | 19                    |
|   | CP-6     | NA        | 190                    | 79                    |
|   | CP-7     | NA        | 23                     | 8                     |
|   | CP-9     | NA        | 51                     | 23                    |
|   | CP-10    | NA        | 90                     | 42                    |
|   | CP-10A   | NA        | 55                     | 25                    |
| [ | CP-11    | NA        | 31                     | 15                    |
|   | C18      | NA        | 123                    | 62                    |



(IN FEET) 1 inch = 300 ft.

511963.19

OCTOBER 2006

FIGURE 5 INTERIM CONDITION DRAINAGE MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



2270 Corporate Circle Henderson, Nevada 89074-6382 Telephone: 702/263-7275 Fax: 702/263-7200

ENGINEERING PLANNING. SURVEYING CONSTRUCTION SERVICES

Appendix B-3: Developed Condition Hydrology

### HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL PBS&J EASTSIDE LANDFILL File: TDS-Standard Form 4.xls BY: **Developed Condition Hydrology** DATE: 10/5/06 SUB-BASIN INITIAL / OVERLAND TRAVEL TIME REMARKS Tc TC Tiag DATA TIME (Ti) Check TRAVEL INITIAL V1 V2 Tlag= LENGTH LENGTH DESIG: DEV/UN. CN AREA AREA SLOPE TI SLOPE VELOCITY VELOCITY Tt 0.6Tc/60 (D or U) Ac MI^2 Feet Feet **FPS** FPS Hours (2) (3) (4) (5) (6) (7) (8) (9a) (9b) (10) (13) (14) ONDI D 87.7 0.7676 0.0015 130 33.0 2.1 247 0.4 1 28 19 3.2 5.3 12.1 0.94 0.05 OND2 D 87.7 0.7676 0.0058 137 33.0 2.2 910 0.4 1.28 1.9 10.1 12.2 15.8 0.12 3.70 OND3 D 88.6 0.7795 1.38 0.0022 156 33.0 2.2 360 1.0 2.02 3.1 3.0 5.2 12.9 0.05 OND4 89.7 0.7940 0.0182 2.0 6.8 1276 2.6 3.26 4.9 5.2 12.0 18.4 0.12 D 11.67 240 OND5 D 91.0 0.8112 5.03 0.0079 300 1.7 7.6 573 1.1 2.07 3.1 4.4 12.0 14.9 0.12 OND6 D 91.0 0.8112 9.90 0.0155 70 1.4 3.9 1407 0.6 1.56 2.4 11.7 15.6 18.2 0.16 1345 OND7 D 90.8 0.8086 5.87 0.0092 158 33.0 2.1 1.8 2.67 4.0 6.6 8.7 18.4 0.09 OND8 D 90.3 0.8020 14.26 0.0223 128 33.0 1.9 2382 0.4 1.28 1.9 22.7 24.6 23.9 0.24 Use Tlag = 0.15 See Note 0.8112 0.0017 3.4 453 2.05 OND9 U 91.0 1.06 50 1.3 1.9 4.1 3.7 7.0 N/A 0.07 0.8112 0.0067 119 33.0 1.8 1190 0.4 1.28 12.5 17.3 OND10 D 91.0 4.28 1.9 14.2 0.14 0.0150 1050 OND11 91.0 0.8112 220 1.6 6.6 2.12 13.4 17.1 0.13 D 9.60 1.1 3.2 6.8 0.8165 0.0043 138 33.0 1.9 610 2.47 OND12 91.4 1.5 3.7 3.9 14.2 D 2.77 5.7 0.06 OND13 D 91.0 0.8112 4.70 0.0073 95 33.0 1.6 714 0.4 1.28 1.9 8.4 9.9 14.5 0.10 0.8112 0.0174 122 1.0 5.7 559 3.31 OND14 U 91.0 11.12 5.0 6.6 2.7 8.4 N/A 0.08 OND15 U 91.0 0.8112 21.47 0.0335 200 2.5 5.4 711 3.0 2.56 5.1 3.9 9.4 N/A 0.09 DETPD D 91.4 0.8165 5.14 0.0080 60 8.3 2.0 35 34.0 11.78 17.8 0.0 2.0 10.5 0.02 OFFD1 D 88.2 0.7742 42.20 0.0659 278 2.5 7.2 2213 2.0 2.85 4.3 9.5 16.7 23.8 0.17 OFFD2 D 88.6 0.7795 9.63 0.0150 195 3.6 5.3 942 1.8 2.71 4.1 4.9 10.1 16.3 0.10 OFFD3 D 89.9 0.7967 16.40 0.0256 300 0.3 13.6 1245 1.7 2.63 4.0 6.3 19.9 18.6 0.19 OFFD4 0.8112 0.0119 300 1.0 9.0 750 1.9 2.76 4.2 13.0 15.8 D 91.0 7.61 4.0 0.13 OFFD5 D 91.0 0.8112 5.11 0.0080 300 1.3 8.2 625 1.6 2.56 3.9 3.8 12.0 15.1 0.12 Tc = Ti + Tt Eqn. 601 For the travel time (Tt) calculations (Sec. 602.1), Undeveloped V1 = 14.8\*(S/100)^1/2 V1 = 20.2\*(S/100)^1/2 Ti = 1.8 (1.1 - K) L^1/2 / S^1/3 Eqn. 602 V1 applies to the first 500 feet of travel distance; K = 0.0132 (CN) - 0.39 Eqn. 603 V2 applies to the remaining travel distance. Undeveloped V2 = 29.4\*(S/100)^1/2 Developed $V2 = 30.6*(S/100)^{1/2}$ Tc Check = L/180+10 Eqn. 604 Tlag = 0.6 Tc Eqn. 612 Min Tc = 10 mins for undeveloped basins Tt = 500/V1+ (Travel Length-500)/V2 Min Tc = 5 mins for developed basins Note: The lag time or basin OND8 was changed to 0.15 hrs because the velocities were not accurate for the cross section. Please refer to the FlowMaster cross section located in Appendix B-3 for the time calculations. REFERENCE: STANDARD FORM 4

\* FLOOD HYDROGRAPH PACKAGE (HEC-1) JUN 1998 VERSION 4.1 RUN DATE 27SEP06 TIME 18:51:46

U.S. ARMY CORPS OF ENGINEERS HYDROLOGIC ENGINEERING CENTER 609 SECOND STREET DAVIS, CALIFORNIA 95616 (916) 756-1104

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKR- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRANT? VERSION NEW OPPIONS: DAMBREAK OUTFLOW SUMMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE PREQUENCY, DSS:READ INFE SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```
1
                                                                                                        HEC-1 INPUT
                                                                                                                                                                                                                 PAGE 1
                    LINE
                                                 ID.....1....2.....3.....4.....5.....6.....7....8.....9....10
  *** FREE ***
                                                *DIAGRAM

ID EASTSIDE LANDFILL IMPROVEMENTS

ID DEVLOPED CONDITION MODEL

ID INPUT FILE = DEV_SDN3.DAT

ID SEPTEMBER 2006

ID DESIGN STORM = 100-YEAR 6-HR STORM

ID STORM DISTRIBUTION = SDN #3

ID MODELED BY PBS&J
                                                ID ID ID ID ID IT IN IO JR
                                                                         0 0
                                                                                                          300
                        10
11
12
                                                            PREC
                                                                      1.00 0.60 0.58
                        13
14
15
16
17
18
19
20
21
22
23
24
25
26
                                                 KK KM BA PB PC PC PC PC PC LS UD *
                                                       OND8
DEVELOPED ONSITE BASIN
0.0223
2.79
.000 .020 .057
.130 .130 .130
.190 .197 .199
.561 .256 .270
                                                                           .020
.130
.197
.256
.590
                                                                                         .057
.130
.199
.270
.710
.876
.987
                                                                                                                        .087
.140
.201
.281
.781
                                                                                                                                       .108
.142
.204
.283
.812
                                                                                                                                                      .124
.148
.214
.295
.819
.937
.993
                                                             .251
.499
.860
.982
                                                                          .985
                                                            .998
                                                            0.15
                        27
28
29
30
31
                                                        0 91.0
0.07
                                                        OFFD3
DEVELOPED OFFSITE BASIN
0.0256
                                                 KK
KM
BA
LS
UD
                         32
33
34
35
36
                        37
38
39
                                                         COMBINE OND9 AND OFFD3
                                                                                                      HEC-1 INPUT
                                                                                                                                                                                                                 PAGE 2
                     LINE
                                                 {\tt ID}.\dots..1.\dots.2\dots..3\dots..4\dots..5\dots..6\dots..7\dots..8\dots..9\dots..10
                                                         COMBINE CP-7 AND OND8
                                                 KKRCP8-CP-9
KM ROUTE CP-8 TO CP-9
RK 1190 0.004 0.025
                         43
44
45
                                                                                                                                     10 3
                                                                                                             0 TRAP
                                                 KK
KM
BA
LS
                        46
47
48
                                                       DEVELOPED ONSITE BASIN
0.0067
0 91.0
                        49
50
                                                           0.14
                                                 UD
*
                                                       OFFD5
DEVELOPED OFFSITE BASIN
0.0080
0 91.0
0.12
                                                 KK
KM
BA
LS
UD
                        51
52
53
54
55
                         56
57
58
                                                         COMBINE RCP8-CP9, OFFD5 AND OND10
```

```
KKRCP9-CP-10

KM ROUTE CP-9 TO CP-10

RK 725 0.015 0.015 0 TRAP
   59
60
61
                                                                                                       10 3
                        KK OND12
KM DEVELOPED ONSITE BASIN
BA 0.0043
LS 0 91.4
UD 0.06
   62
63
64
65
66
                         KK CP-10A
KM COMBINE CP-9 AND OND12
HC 2
   67
68
69
                        KK OND11

KM DEVELOPED ONSITE BASIN

BA 0.0150

LS 0 91.0

UD 0.13
   70
71
72
73
74
                                                                         HEC-1 INPUT
                                                                                                                                                                             PAGE 3
                         ID.....1.....2......3......4......5.....6......7......8......9.....10
LINE
                         KK OND13
KM DEVELOPED ONSITE BASIN
BA 0.0073
LS 0 91.0
UD 0.10
                         RK CP-10
RM COMBINE CP-10A, OND11 AND OND13
HC 3
   80
81
82
                        KK EQBASIN

KM EQUALIZER BASIN TO SPLIT FLOW NORTH AND

RM TO THE DETENTION POND

RS 1 STOR -1

SA 0 0.08 0.70 0.78 0.85 0.87 0.97

SE 1744.5 1745 1746 1747 1747.75 1748 1748.5

SQ 0 0 0 18 42 59 74 126
   83
84
85
86
87
88
89
                        KK DIVWEIR
KM DIVERT FLOW FROM EQ BASIN
DT DVPIPE
DI 0 59 74 126
DQ 0 59 64 73
   90
91
92
93
94
                              OND14
DEVELOPED ONSITE BASIN
0.0174
0 91.0
0.08
   95
96
97
98
99
                         KK
KM
BA
LS
UD
                         KK CP-11
KM COMBINE WEIR FLOW AND OND14
HC 2
 100
101
102
                        KK OND1
KM DEVELOPED ONSITE BASIN
BA 0.0015
LS 0 87.7
UD 0.05
  103
104
105
106
107
                        KK OFFD2

KM DEVELOPED OFFSITE BASIN

BA .0150

LS 0 00.6

UD 0.10
 108
109
110
111
112
                                                                          HEC-1 INPUT
                                                                                                                                                                             PAGE 4
LINE
                         {\tt ID}.\dots..1,\dots..2,\dots..3,\dots..4,\dots..5,\dots..6,\dots..7,\dots..8,\dots..9,\dots..10
 113
114
115
                         KK CP-1
KM COMBINE OND1 AND OFFD2
HC 2
                         KKRCP1-CP2

KM ROUTE CP-1 TO CP-2

RK 910 0.004 0.025 0 TRAP
                                                                                                      10 3
                        KK OND2

KM DEVELOPED ONSITE BASIN

BA 0.0058

LS 0 87.7

UD 0.12
 120
121
122
123
                         KK OFFD1
KM DEVELOPED OFFSITE BASIN
BA 0.0659
LS 0 88.2
UD 0.17
  125
126
127
128
  129
130
131
                                CP-2
COMBINE CP-1, OFFD1 AND OND2
  132
133
134
                         KKRCP2-CP-3
                         KM ROUTE
RK 360 0.010 0.015 0 TRAP 10
```

```
OND3
DEVELOPED ONSITE BASIN
0.0022
0 88.6
0.05
                       KK
KM
HC
*
                               CP-3
COMBINE CP-2 AND OND3
2
141
142
                       KKRCP3-CP4

KM ROUTE CP-3 TO CP-4

RK 1345 0.018 0.015
143
144
145
                                                                         0 TRAP 10
                                                                         HEC-1 INPUT
                                                                                                                                                                       PAGE 5
                        ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
146
147
148
149
150
                             OND7
DEVELOPED ONSITE BASIN
0.0992
0 90.8
0.09
                       KK
KM
BA
LS
UD
151
152
153
                       KK
KM
HC
                               CP-4
COMBINE CP-3 AND OND7
2
                             OND4
DEVELOPED ONSITE BASIN
0.0182
0 89.7
0.12
                       KK
KM
BA
LS
UD
                             OND5
DEVELOPED ONSITE BASIN
0.0079
0 91.0
0.12
159
160
161
162
163
                       KK
KM
BA
LS
UD
                               CP-5
COMBINE OND4 AND OND5
2
164
165
166
                             OND6
DEVELOPED ONSITE BASIN
0.0155
0 91.0
0.16
                       KK DVPIPE
KM RETURN FLOW FROM EQ BASIN PIPE
DR DVPIPE
                       KK RDVPIPE
KM ROUTE FLOW THROUGH 42° RCP
RK 1880 0.005 0.013 0 CIRC
175
176
177
                                                                                                   3.5
                       KK DETPD

KM DETENTION POND BASIN

BA 0.0080

LS 0 91.4

UD 0.05
                                                                        HEC-1 INPUT
                                                                                                                                                                         PAGE 6
                        ID.....1.....2.....3.....4.....5.....6.....7.....8......9.....10
                       KK
KM
HC
                               \ensuremath{\text{CP-6}} COMBINE CP-4, CP-5, OND6, DVPIPE AND DETPD 5
184
185
                       KK DETPOND
KM
RS 1
SV 0
SE 1725.25
SQ 0
KO 1
186
187
188
189
190
191
192
                        Referenced from PBSJ

"Addendum #1 to the Technical Drainage Study for Henderson Commmerce
Center Two (Formerly known as HARSCH)" (February 2003)
                       RK OFFD-14
RM OFSITE DEVELOPED BASIN OFFD-14
RM REFERENCED FROM EG02
BA 0.0028
PB 2.79
LS 0 88
UD 0.200
193
194
195
196
197
198
199
                       KK RT-B14

KM ROUTE OFFD-14 THROUGH BMIC-1

RK 1050 0.014 0.013 0 TRAP
                                                                                                       15
                                                                                                                     10
                       KK BMIC-1

KM ONSITE DEVELOPED BASIN BMIC-1

KM REFERENCED FROM EG02

BA 0.0141
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```
2.79
0
0.081
 207
208
209
                       PB
LS
UD
 210
211
212
                               COMBINE RT-B14 AND BMIC-1
                               RT-14
ROUTE C15 THROUGH BMIC-2
450 0.018 0.013
 213
214
215
                                                                        0 TRAP
                                                                                               15 10
                                                                       HEC-1 INPUT
                                                                                                                                                                 PAGE 7
LINE
                       ID.....1....2.....3.....4.....5.....6.....7.....8.....9.....10
                       KK BMIC-2
RM ONSITE DEVELOPED BASIN BMIC-2
RM REFERENCED FROM EGG2
BA 0.0118
PB 2.79
LS 0 92
UD 0.073
*
 216
217
218
 219
220
221
222
                       KK
KM
HC
                               C16
COMBINE RT-14 AND BMIC-2
 226
227
228
                       KK
KM
RK
*
                               RT-15
ROUTE C16 THROUGH SCH-2
400 0.019 0.013
                                                                           0 TRAP
                               SCH-2
ONSITE DEVELOPED BASIN SCH-2
REFERENCED FROM EG02
 229
230
231
232
233
234
235
                       KK
KM
KM
BA
PB
LS
UD
                             0.0065
2.79
0.060
                                                 92
 236
237
238
                               C17
COMBINE RT-15 AND SCH-2
                       KK
KM
HC
 239
240
241
                       KK
KM
RK
                               RT-16
ROUTE C17 THROUGH BMIC-3
750 0.013 0.013 0 TRAP
                       KK BMIC-3
KM ONSITE DEVELOPED BASIN BMIC-3
KM REFERENCED FROM BG02
BA 0.0106
PB 2.79
LS 0 92
UD 0.062
 242
243
244
245
246
247
248
                            MGDEV-2
MILGARD MANUFACTURING ONSITE BASIN
REFERENCED FROM EG02
0.0093
2.79
                        PAGE 8
                       ID.....1.....2.....3.....4.....5.....6.....7.....8......9.....10
LINE
 256
257
258
                               COMBINE RT-16, BMIC-3, BGDEV-2 AND OUTFLOW FROM DETENTION POND
                        Referenced from PBSJ
* "Addendum #1 to the Technical Drainage Study for Henderson Commmerce
* Center Two (Formerly known as HARSCH)" (February 2003)
                       KK HR3
KM HARSCH ONSITE BASIN
BA 0.0014
PB 2.79
LS 0 92
UD 0.049
 259
260
261
262
263
264
 265
266
267
268
269
270
                            HR2
HARSCH ONSITE BASIN
0.0016
2.79
0 98
0.037
                       KK
KM
BA
PB
LS
UD
                             HR1
HARSCH ONSITE BASIN
0.0015
2.79
                       KK
KM
BA
PB
LS
UD
                                 0.05
                                 CHR1
                               CHRI
COMBINE HR3, HR2, HR1
THESE FLOWS ARE DISCHARGED INTO THE ONSITE
STORM DRAIN SYSTEM LABELED ALIGNMENT "H1"
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KM ON FIGURE 7
HC 3
                       .
                          C18B
COMBINE C18 AND CHR1
2
                                                 HEC-1 INPUT
                                                                                                  PAGE 9
                      ID.....1.....2.....3.....4......5......6.....7.....8......9.....10
         LINE
                         OND15
DEVELOPED ONSITE BASIN
0.0335
0 91.0
0.09
                      KK OFFD4

RM DEVELOPED OFFSITE BASIN

BA 0.0119

LS 0 91.0

UD 0.13

*

ZZ
          291
292
293
294
295
          296
1
           SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT
LINE
          (V) ROUTING (--->) DIVERSION OR PUMP FLOW
  NO.
          (.) CONNECTOR
                          (<---) RETURN OF DIVERTED OR PUMPED FLOW
   13
                      OND9
   32
                                OFFD3
                      CP-7.....
   37
           CP-8.....
   40
   43
        RCP8-CP-
                     OND10
   46
   51
                                OFFD5
   56
   59
        RCP9-CP-
                     OND12
   62
          CP-10A.....
   67
                      OND11
   70
   75
                                OND13
   80
   83
         EQBASIN
         DIVWEIR DVPIPE
   92
90
   95
                     OND14
           CP-11.....
  100
  103
                      OND1
  108
                                OFFD2
  113
                      CP-i.....
                   RCP1-CP2
  116
  119
                                 OND2
  124
                                           OFFD1
  129
                      CP-2.....
  132
  135
                                 OND3
```

## EASTSIDE LANDFILL IMPROVEMENTS DEVLOPED CONDITION MODEL

| 140          | . CP-   | 3                                     |                   |           |           |  |   |
|--------------|---|---------------------------------------|-------------------|-----------|-----------|--|---|
| 143          | RCP3-CP                                       | 94                                    |                   |           |           |  |   |
| 146          | i   | OND7                                  |                   |           |           |  |   |
| 151          | ¥   |                                       |                   |           |           |  |   |
| 154          |   | OND4                                  |                   |           |           |  |   |
| 159          | * -   |                                       | OND5              |           |           |  |   |
| 164          |   |                                       |                   |           |           |  |   |
| 167          |   | * *                                   | OND6              |           |           |  |   |
| 174          |   |                                       |                   | -         | DVPIPE    |  |   |
| 172          |   |                                       | 7.51              | DVPIPE    |           |  |   |
| 175          |   |                                       | 0+0<br>0+0<br>(*) | RDVPIPE . |           |  |   |
| 178          | •   |                                       |                   | :         | DETPD     |  |   |
| 183          | CP-   | V                                     |                   |           | ********* |  |   |
| 186          | DETPON  | ID.                                   |                   |           |           |  |   |
| 193          |   | OFFD-14                               |                   |           |           |  |   |
| 200          | * * *   | . V<br>. RT-B14                       |                   |           |           |  |   |
| 203          |   |                                       | BMIC-1            |           |           |  |   |
| 210          |   | . C15                                 |                   |           |           |  |   |
| 213          |   | . V<br>V<br>. RT-14                   |                   |           |           |  |   |
| 216          |   | 1 1                                   | BMIC-2            |           |           |  |   |
| 223          |   | . C16                                 |                   |           |           |  |   |
| 226          | *   | . V<br>. V<br>. RT-15                 |                   |           |           |  |   |
| 229          |   |                                       | SCH-2             |           |           |  |   |
| 236          |   | . cı7                                 |                   |           |           |  |   |
| 239          | *   | . V<br>V<br>. RT-16                   |                   |           |           |  |   |
| 242          |   |                                       | BMIC-3            |           |           |  |   |
|              |   | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | (4)               | MODEL 2   |           |  |   |
| ***          |   | 185 8<br>185 8                        | 1 K               | MGDEV-2   |           |  |   |
| 256          |   | 8<br>:                                |                   |           |           |  |   |
| 259          |   | . HR3                                 |                   |           |           |  |   |
| 265          |   |                                       | HR2               |           |           |  |   |
| 271          |   |                                       |                   | HR1       |           |  |   |
| 277          | *   | . CHR1                                |                   |           |           |  |   |
| 283          |   | B                                     |                   |           |           |  |   |
| 286          | 2   | OND15                                 |                   |           |           |  |   |
| 291          |   |                                       | OFFD4             |           |           |  |   |
| 1*********   | OFF ALSO COMPUTED A                           | ***********                           |                   |           |           | ***************************************  |   |
| * FLOOD<br>* | HYDROGRAPH PACKAGE<br>JUN 1998<br>VERSION 4.1 | E (HEC-1) *                           |                   |           |           | * U.S. ARMY CORPS OF ENGINEERS  * HYDROLOGIC ENGINEERING CENTER  * 609 SECOND STREET |   |
| * RUN DAT    | TE 27SEP06 TIME                               | 18:51:46 *                            |                   |           |           | * DAVIS, CALIFORNIA 95616<br>* (916) 756-1104  |   |
| *******      | ***********                                   | *********                             |                   |           |           | ************   | 1 |

INPUT FILE = DEV\_SDN3.DAT SEPTEMBER 2006 DESIGN STORM = 100-YEAR 6-HR STORM STORM DISTRIBUTION = SDN #3 MODELED BY PBS&J

| 11   | IO   |                      | O              | JTPUT CON                | TROL VAR | IABLES         |             |        |  |            |           |                            |            |              |      |           |           |                            |
|------|------|----------------------|----------------|--------------------------|----------|----------------|-------------|--------|--|------------|-----------|----------------------------|------------|--------------|------|-----------|-----------|----------------------------|
|      |      |                      |                | I PRN<br>I PLC           | TT<br>T  | 5              | PRII<br>PLO | T CON  | TROL<br>PROL<br>PH PLOT SCA  | 10730      |           |                            |            |              |      |           |           |                            |
|      |      |                      |                |                          |          |                | HYDI        | ROGRAI | PH PLOT SCA  | ALE        |           |                            |            |              |      |           |           |                            |
|      | IT   |                      | H              | YDROGRAPH<br>NMI         | TIME DA  | TA 5           | MIN         | JTES I | IN COMPUTATE DATE TIME F HYDROGRAF   | TION INTER | RVAL      |                            |            |              |      |           |           |                            |
|      |      |                      |                | IDAT                     | E 1      | 0000           | STA         | RTING  | DATE   |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | N                        | IQ O     | 300            | NUM         | BER OF | HYDROGRAI  | PH ORDINAT | res       |                            |            |              |      |           |           |                            |
|      |      |                      |                | NDTIM                    | E 2      | 0055           | END:        | ING DA | ME   |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | ICENT                    |          | 19             | CEN         | PURY N | MARK   |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | COMPUTAT                 | ION INTE | RVAL           | 24.1        | OB HOU | JRS  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                |                          | AL TIME  | AGAG           | 24.         | Z HOL  | JRS  |            |           |                            |            |              |      |           |           |                            |
|      |      | ENG                  | LISH t         | JNITS<br>INAGE ARE       | A        | SQUA           | RE M        | LES    |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      | PREG           | INAGE ARE                | N DEPTH  | INCH           | ES          |        |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      | FLO            | STH, ELEV                |          | CUBI           | C FEI       | ET PER | R SECOND   |            |           |                            |            |              |      |           |           |                            |
|      |      |                      | SURI           | RAGE VOLU<br>PACE AREA   | PIE,     | ACRE:<br>DEGRI | S           | r.     |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      | TEM            | PERATURE                 |          | DEGR           | EES 1       | FAHREI | NHEIT  |            |           |                            |            |              |      |           |           |                            |
|      | JP   |                      | M              | JLTI-PLAN<br>NPLA        |          |                | NUM         | BER OF | PLANS  |            |           |                            |            |              |      |           |           |                            |
|      | ***  |                      |                |                          |          |                |             |        | 1 11110  |            |           |                            |            |              |      |           |           |                            |
|      | JR   |                      | M              |                          | OF PREC  | IPITAT:        |             |        |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | 1.00                     | .60      |                | .58         |        |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                |                          |          |                |             |        |  |            |           |                            |            |              |      |           |           |                            |
| ***  | ***  | *** *                | ** **          | *** ***                  | *** ***  | *** *          | ** *        | ** *** | *** *** *  | ** *** **  | *** ***   | *** ***                    | ***        | *** ***      | ***  | ** *** ** | * *** *** | *** ***                    |
|      |      |                      |                |                          |          |                |             |        |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      | ****           | *******                  |          |                |             |        |  |            |           |                            |            |              |      |           |           |                            |
| 186  | KK   | 4                    | DET            | POND *                   |          |                |             |        |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      | *****          | ******                   |          |                |             |        |  |            |           |                            |            |              |      |           |           |                            |
| 192  | ко   |                      | 01             | JTPUT CON                | TROL VAR | IABLES         |             |        |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | IPRN<br>IPLO             | T        | 1              | PRI         | T CON  | TROL   |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | QSCA                     |          |                |             |        | PH PLOT SCA  | LE         |           |                            |            |              |      |           |           |                            |
|      |      |                      | HYDI           | ROGRAPH R                | OUTING I | ATA            |             |        |  |            |           |                            |            |              |      |           |           |                            |
| 188  | RS   |                      | S              | PORAGE RO                | UTING    |                |             |        |  |            |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | NSTP                     | S        | STOR           | NUM         | BER OF | SUBREACHE  | S          |           |                            |            |              |      |           |           |                            |
|      |      |                      |                | RSVRI                    |          | -1.00          | INI         | TIAL ( | NITIAL CONDITION   | 10111011   |           |                            |            |              |      |           |           |                            |
|      |      |                      |                |                          |          |                |             |        | AND D COEF   |            |           |                            |            |              |      |           |           |                            |
| 189  | SV   |                      |                | STORAGE                  |          | .0             |             | .1     | 1.5  | 3.0        | 4.8       | 8.                         | 9          | 13.4         | 1    | 5.9       |           |                            |
| 190  | SE   |                      | EI             | LEVATION                 | 1725     | .25            | 1726        | .00    | 1728.00  | 1729.00    | 1730.00   | 1732.0                     | 0          | 1734.00      | 1735 | 5.00      |           |                            |
| 191  | SQ   |                      | D              | SCHARGE                  |          | 0.             |             | 0.     | 22.  | 27.        | 32.       | 40                         |            | 46.          |      | 49.       |           |                            |
|      |      |                      |                |                          |          |                |             |        |  | ***        |           |                            |            |              |      |           |           |                            |
| **** | **** | ****                 | ****           | ******                   | ******   | *****          | ***         | ****   | ******   | ******     | ******    | *****                      | ***        | ******       | **** | ******    | ******    | ******                     |
|      |      |                      |                |                          |          |                |             | 1      | TYDROGRAPH   | AT STATIC  | ON DETPON | ID                         |            |              |      |           |           |                            |
|      |      |                      |                |                          |          |                |             |        |  | RATIO      |           |                            |            |              |      |           |           |                            |
| **** | **** | *****                | ****           | ******                   | ******   | *****          | ****        | ****   | *******  | *******    | ******    | *****                      | ****       | ******       | **** | ******    | ******    | ******                     |
| DA   | MON  | HRMN                 | ORD (          | OUTFLOW                  | STORAGE  | STAG           | E * 1       | OA MOI | HRMN ORD   | OUTFLOW    | STORAGE   | STAGE                      | * DA       | MON HRMN     | ORD  | OUTFLOW   | STORAGE   | STAGE                      |
| 1    |      | 0000                 | 1              | 0.                       | .1       | 1726.          | *           | 1      | 0820 101   | 30.        | 4.3       | 1729.7                     | * 1        | 1640         | 201  | 0.        | .1        | 1726.0                     |
| 1    |      | 0005                 | 3              | 0.                       | .1       | 1726.0         | * 0         | 1      | 0825 102   | 30.        | 4.1       | 1729.6                     | * 1        | 1645         | 202  | 0.        | .1        | 1726.0                     |
| 1    |      | 0015                 | 4              |                          |          |                |             |        | 0835 104   | 29.        | 3.7       | 1729.4                     | * 1        | 1655         | 204  | 0.        | .1        | 1726.0                     |
| 1    |      | 0020                 | 5 6 7          | 0.                       | .1       | 1726.          | ) *         | 1      | 0840 105   | 28.        | 3.5       | 1729.1                     | * 1        | 1705         | 206  | 0.        | .1        | 1726.0                     |
| 1    |      | 0030                 | 7              | 0.                       | .1       | 1726.0         | ) *         | 1      | 0820 101<br>0825 102<br>0830 103<br>0835 104<br>0840 105<br>0845 106<br>0850 107<br>0855 108   | 27.<br>27. | 3.1       | 1729.0                     | * 1<br>* 1 | 1710<br>1715 | 207  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0040                 | 9              | 1                        | - 1      | 1726.          |             | 1      |  |            |           |                            |            |              |      |           |           |                            |
| 1    |      | 0045<br>0050<br>0055 | 11             | 1.                       | .2       | 1726.          | . +         | 1      | 0910 111   | 25.        | 2.4       | 1728.7<br>1728.6<br>1728.5 | * 1        | 1730         | 211  | 0.        | .1        | 1726.0<br>1726.0<br>1726.0 |
| 1    |      | 0100                 | 13             | 1.                       | .2       | 1726.          | *           | 1      | 0915 112 0920 113  | 24.        | 2.2       | 1728.5                     | * 1<br>* 1 | 1735<br>1740 | 212  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0105                 | 14             | 1.                       | .2       | 1726.          | *           | 1      | 0925 114   | 23.        | 1,9       | 1728.2                     | * 1        | 1745         | 214  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0115                 | 15<br>16<br>17 | 2.                       | .2       | 1726.          | *           | 1      | 0935 116   | 22.        | 1.6       | 1728.0                     | * 1        | 1755         | 216  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0120                 | 18             | 2.                       | .2       | 1726.          | 2 +         | 1      | 0940 117   | 18.        | 1.4       | 1727.7                     | * 1        | 1800         | 217  | 0.        | .1        | 1726.0                     |
| 1    |      | 0130                 | 19<br>20       | 2.                       | .2       | 1726.          | 2 *         | 1      | 0950 119   | 17.<br>15. | 1.2       | 1727.5                     | * 1        | 1810<br>1815 | 219  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0140                 | 21             | 4.                       | .3       | 1726.          | 3 *         | 1      | 1000 121   | 13.        | 1.0       | 1727.2                     | * 1        | 1820         | 221  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0150                 | 23             | 5.                       | .4       | 1726.          | 5 *         | 1      | 1010 123   | 11.        | .8        | 1727.1                     | * 1        | 1830         | 223  | 0.        | .1        | 1726.0                     |
| 1    |      |                      |                | 6.<br>6.<br>7.           | .5       | 1726.          | 5 *         | 1      | 1015 124   | 10.        | .7        | 1726.9                     | * 1        | 1835<br>1840 | 224  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0205                 | 26             | 7.                       | .5       | 1726.          | 6 *         | 1      | 1025 126   | 8.         | .6        | 1726.7                     | * 1        | 1845         | 226  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0215                 | 28             | 6.<br>7.<br>7.<br>7.     | .5       | 1726.          | 6 *         | 1      | 1035 128   | 6.         | .5        | 1726.6                     | * 1        | 1855         | 228  | 0.        | .1        | 1726.0                     |
| 1    |      | 0220                 | 30             | 8.<br>9.                 | .6       | 1726.          | 7 *         | 1      | 1040 129<br>1045 130   | 6.<br>5.   | .5        | 1726.5                     | * 1<br>* 1 | 1900         | 229  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0230                 | 31<br>32<br>33 | 10.                      | .7       | 1726.          | 9 *         | 1      | 1050 131   | 5.         | . 4       | 1726.4                     | * 1        | 1910         | 231  | 0.        | .1        | 1726.0                     |
| 1    |      | 0240                 | 33             | 11.                      | .8       | 1727.          | 0 *         | 1      | 1050 131<br>1055 132<br>1100 133<br>1105 134   | 4.         | .3        | 1726.3                     | * 1        | 1920         | 233  | 0.        | .1        | 1726.0<br>1726.0           |
| 1    |      | 0245                 | 34             | 12.<br>13.               | .9       | 1727.          | 2 *         | 1      | 11105 134  | 3.         | .3        | 1726.3                     | * 1        | 1925<br>1930 | 234  | 0.        | .1        | 1726.0                     |
| 1    |      | 0255                 | 36             | 13.<br>14.<br>15.<br>16. | 1.0      | 1727.          | 2 *         | 1      | 1115 136   | 3.         | .3        | 1726.3                     | * 1        | 1935         | 236  | 0.        | .1        | 1726.0                     |
| 1    |      | 0305                 | 38             | 15.                      | 1.0      | 1727.          | 3 *         | 1      | 1125 138   | 2.         | .2        | 1726.2                     | * 1        | 1945         | 238  | 0.        | .1        | 1726.0<br>1726.0<br>1726.0 |
| 1    |      | 0310                 | 39             | 16.                      | 1.1      | 1727.          | *           | 1      | 0905 110<br>0910 111<br>0910 111<br>0910 113<br>0920 113<br>0920 114<br>0930 115<br>0940 117<br>0945 118<br>0950 119<br>0955 120<br>1000 121<br>1005 122<br>1010 123<br>1015 124<br>1020 125<br>1030 127<br>1030 127<br>1031 128<br>1100 133<br>1105 134<br>1110 135<br>1120 137<br>1125 138<br>1130 139 | 2.         | .2        | 1726.2                     | - 1        | 1950         | 239  | 0.        | .1        | 1726.0                     |
|      |      |                      |                |                          |          |                |             |        |  |            |           |                            |            |              |      |           |           |                            |

|     |         |      |     |      |        |   |   |      |     |    |     | 10000  |     |   | 1055 04 |   |    |     | 4000   |
|-----|---------|------|-----|------|--------|---|---|------|-----|----|-----|--------|-----|---|---------|---|----|-----|--------|
| 1   | 0315 4  |      | 19. |      | 1727.8 |   |   | 1135 |     | 2. |     | 1726,2 |     |   | 1955 24 |   |    |     | 1726.0 |
| 1   | 0320 4  |      | 23. |      | 1728.2 |   |   | 1140 |     | 2. |     | 1726.2 |     |   | 2000 24 |   |    |     | 1726.0 |
| 1   |         | 12   | 25. |      | 1728.7 |   | 1 | 1145 |     | 1. |     | 1726.1 |     | 1 | 2005 24 |   |    | .1  |        |
| 1   | 0330 4  |      | 29. |      | 1729.4 |   | 1 | 1150 |     | 1. | .2  | 1726.1 |     | 1 | 2010 24 |   |    | -1  | 1726.0 |
| 1   | 0335 4  |      | 33. |      | 1730.1 |   |   | 1155 |     | 1. | .2  | 1726.1 |     |   | 2015 24 |   |    |     | 1726.0 |
| 1   | 0340 4  | 15   | 35. | 6.6  | 1730.9 |   | 1 | 1200 | 145 | 1. | .2  | 1726.1 |     |   | 2020 24 |   | 0. | -1  | 1726.0 |
| 1   | 0345 4  | 46   | 38. | 7.9  | 1731.5 | * | 1 | 1205 | 146 | 1. | .1  | 1726.1 |     | 1 | 2025 24 | 6 | 0. | .1  | 1726.0 |
| 1   | 0350 4  | 17   | 40. | 8.9  | 1732.0 |   | 1 | 1210 | 147 | 1. | .1  | 1726.1 |     | 1 | 2030 24 | 7 | 0. | .1  | 1726.0 |
| 1   | 0355 4  | 18   | 41. | 9.7  | 1732.4 |   | 1 | 1215 | 148 | 1. | .1  | 1726.1 | *   | 1 | 2035 24 | 8 | 0. | .1  | 1726.0 |
| 1   | 0400 4  | 19   | 42. | 10.3 | 1732.6 | * | 1 | 1220 | 149 | 1. | .1  | 1726.1 |     | 1 | 2040 24 | 9 | 0. | .1  | 1726.0 |
| 1   | 0405 5  | 50   | 43. |      | 1732.8 |   | 1 | 1225 | 150 | 1. | .1  | 1726.1 | . # | 1 | 2045 25 | 0 | 0. | .1  | 1726.0 |
| 1   |         | 51   | 43. |      | 1733.0 |   | 1 | 1230 |     | 1. | . 1 | 1726.1 | *   | 1 | 2050 25 | 1 |    | .1  | 1726.0 |
| 1   |         | 52   | 43. |      | 1733.1 |   | 1 | 1235 |     | 1. | .1  | 1726.0 |     | 1 | 2055 25 | 2 |    | . 1 | 1726.0 |
| 1   |         | 53   | 44. |      | 1733.2 |   | 1 | 1240 |     | 0. |     | 1726.0 |     |   | 2100 25 |   |    |     | 1726.0 |
| 1   |         | 54   | 44. |      | 1733.3 |   | 1 | 1245 |     | 0. |     | 1726.0 |     |   | 2105 25 |   |    |     | 1726.0 |
| 1   | 0430 5  |      | 44. |      | 1733.3 |   | 1 | 1250 |     | 0. |     | 1726.0 |     |   | 2110 25 |   |    |     | 1726.0 |
|     |         | 56   | 44. |      | 1733.4 |   | 1 | 1255 |     | 0. | .1  | 1726.0 |     |   | 2115 25 |   |    |     | 1726.0 |
| *   |         |      |     |      | 1733.4 |   | 1 |      |     |    | .1  | 1726.0 |     |   | 2120 25 |   |    |     | 1726.0 |
| 4   | 0440 5  |      | 44. |      |        |   | 1 | 1300 |     | 0. |     | 1726.0 |     |   | 2125 25 |   |    | .1  | 1726.0 |
|     |         | 8    | 45. |      | 1733.6 |   |   | 1305 |     | 0. | .1  |        |     |   | 2130 25 |   |    |     |        |
| 1   |         | 59   | 45. |      | 1733.6 |   | 1 | 1310 |     | 0. | .1  | 1726.0 |     |   |         |   |    |     | 1726.0 |
| 1   |         | 50   | 45. |      | 1733.7 |   |   | 1315 |     | 0. | .1  | 1726.0 |     |   | 2135 26 |   |    |     | 1726.0 |
| 1   |         | 51   | 45. |      | 1733.8 |   | 1 | 1320 |     | 0. | .1  | 1726.0 |     | 1 | 2140 26 |   |    |     | 1726.0 |
| 1   |         | 52   | 45. |      | 1733.8 |   | 1 | 1325 |     | 0. | .1  | 1726.0 |     |   | 2145 26 |   |    |     | 1726.0 |
| 1   |         | 53   | 45. |      | 1733.8 |   | 1 | 1330 |     | 0. | .1  | 1726.0 |     |   | 2150 26 |   |    |     | 1726.0 |
| 1   |         | 54   | 45. |      | 1733.8 |   | 1 | 1335 |     | 0. |     | 1726.0 |     |   | 2155 26 |   |    |     | 1726.0 |
| 1   | 0520 €  |      | 45. |      | 1733.7 |   | 1 | 1340 |     | 0. |     | 1726.0 |     |   | 2200 26 |   |    |     | 1726.0 |
| 1   | 0525 6  | 56   | 45. | 12.7 | 1733.7 |   | 1 | 1345 | 166 | 0. | .1  | 1726.0 | *   | 1 | 2205 26 |   | 0. | .1  | 1726.0 |
| 1   | 0530 6  | 57   | 45. | 12.6 | 1733.6 |   | 1 | 1350 | 167 | 0. | . 1 | 1726.0 | *   | 1 | 2210 26 | 7 | 0. | .1  | 1726.0 |
| 1   | 0535 6  | 68   | 45. | 12.4 | 1733.5 |   | 1 | 1355 | 168 | 0. | .1  | 1726.0 | *   | 1 | 2215 26 | 8 | 0. | .1  | 1726.0 |
| 1   | 0540 6  | 59   | 44. | 12.2 | 1733.4 |   | 1 | 1400 | 169 | 0. | -1  | 1726.0 | *   | 1 | 2220 26 | 9 | 0. | .1  | 1726.0 |
| 1   | 0545 7  | 70   | 44. | 12.0 | 1733.4 |   | 1 | 1405 | 170 | O. | . 1 | 1726.0 | *   | 1 | 2225 27 | 0 | 0. | .1  | 1726.0 |
| 1   | 0550 7  | 71   | 44. | 11.7 | 1733.3 | * | 1 | 1410 | 171 | 0. | 1   | 1726.0 | *   | 1 | 2230 27 | 1 | 0. | .1  | 1726.0 |
| 1   | 0555 7  | 72   | 43. | 11.5 | 1733.1 | * | 1 | 1415 | 172 | 0. | .1  | 1726.0 | *   | 1 | 2235 27 | 2 | 0. | .1  | 1726.0 |
| 1   | 0600 7  | 73   | 43. | 11.3 | 1733.0 |   | 1 | 1420 | 173 | 0. | .1  | 1726.0 |     | 1 | 2240 27 | 3 |    |     | 1726.0 |
| 1   | 0605 7  | 74   | 43. | 11.0 | 1732.9 |   | 1 | 1425 | 174 | 0. | .1  | 1726.0 |     | 1 | 2245 27 | 4 |    |     | 1726.0 |
| 1   |         | 75   | 42. |      | 1732.8 |   | 1 | 1430 |     | 0. | .1  | 1726.0 |     |   | 2250 27 |   |    |     | 1726.0 |
| 1   |         | 76   | 42. |      | 1732.7 |   | 1 | 1435 |     | 0. |     | 1726.0 |     |   | 2255 27 |   |    |     | 1726.0 |
| 3   |         | 77   | 42. |      | 1732.6 |   | 1 | 1440 |     | 0. |     | 1726.0 |     |   | 2300 27 |   |    |     | 1726.0 |
| 1   |         | 78   | 41. |      | 1732.5 |   | 1 | 1445 |     | 0. | .1  | 1726.0 |     | 1 | 2305 27 |   |    |     | 1726.0 |
| -   |         | 79   | 41. |      | 1732.4 |   | 1 | 1450 |     | 0. | 1.  | 1726.0 |     | 1 | 2310 27 |   |    |     | 1726.0 |
| 1   |         | 30   | 41. |      | 1732.2 |   | 1 | 1455 |     | 0. | .1  | 1726.0 |     |   | 2315 28 |   |    |     | 1726.0 |
| -   |         | 91   | 40. |      | 1732.1 |   | 1 | 1500 |     | 0. | . 1 | 1726.0 |     | 1 | 2320 28 |   |    |     | 1726.0 |
|     | 0645 8  |      | 40. |      | 1732.0 |   | 1 | 1505 |     | 0. | .1  | 1726.0 |     |   | 2325 28 |   |    | .1  | 1726.0 |
| - 1 | 0650 8  |      | 39. |      | 1731.9 |   |   | 1510 |     | 0. | .1  | 1726.0 |     |   | 2330 28 |   |    |     | 1726.0 |
| -   |         | 34   | 39. |      | 1731.9 |   | 1 | 1515 |     | 0. | .1  | 1726.0 |     |   | 2335 28 |   |    |     | 1726.0 |
| 1   |         |      |     |      |        |   | 1 |      |     |    |     | 1726.0 |     | 1 | 2335 28 |   |    |     | 1726.0 |
| 1   |         | 35   | 38. |      | 1731.6 |   |   | 1520 |     | 0. | -1  |        |     |   |         |   |    |     |        |
| 1   |         | 36   | 38. |      | 1731.5 |   | 1 | 1525 |     | 0. | -1  | 1726.0 |     |   | 2345 28 |   |    |     | 1726.0 |
| 1   |         | 37   | 37. |      | 1731.3 |   | 1 | 1530 |     | 0. | .1  | 1726.0 |     |   | 2350 28 |   |    |     | 1726.0 |
| 1   | 0715 8  |      | 37. |      | 1731.2 |   | 1 | 1535 |     | 0. | .1  | 1726.0 |     | 1 | 2355 28 |   |    |     | 1726.0 |
| 1   |         | 39   | 36, |      | 1731.1 |   | 1 | 1540 |     | 0. |     | 1726.0 |     |   | 0000 28 |   |    |     | 1726.0 |
| 1   |         | 90   | 36. |      | 1731.0 |   | 1 | 1545 |     | 0. | 1.3 | 1726.0 |     |   | 0005 29 |   |    |     | 1726.0 |
| 1   |         | 91   | 35. |      | 1730.9 |   | 1 | 1550 |     | 0. | .1  | 1726.0 |     | 2 | 0010 29 |   |    | .1  |        |
| 1   |         | 92   | 35. |      | 1730.7 |   | 1 | 1555 |     | 0. | . 1 | 1726.0 |     | 2 | 0015 29 |   |    | .1  | 1726.0 |
| 1   |         | 93   | 34. | 6.1  | 1730.6 |   | 1 | 1600 |     | 0. | .1  | 1726.0 |     | 2 | 0020 29 |   |    | . 1 | 1726.0 |
| 1   |         | 94   | 34. |      | 1730.5 |   | 1 | 1605 |     | 0. | . 1 | 1726.0 |     | 2 | 0025 29 |   |    |     | 1726.0 |
| 1   | 0750 9  | 95   | 34. | 5.6  | 1730.4 | * | 1 | 1610 | 195 | 0. | . 1 | 1726.0 | *   |   | 0030 29 |   | 0. | .1  | 1726.0 |
| 1   | 0755 9  | 96   | 33. | 5.4  | 1730.3 | * | 1 | 1615 | 196 | 0. | .1  | 1726.0 |     | 2 | 0035 29 | 6 |    | . 1 | 1726.0 |
| 1   |         | 97   | 33. |      | 1730.2 |   | 1 | 1620 |     | 0. | .1  | 1726.0 |     | 2 | 0040 29 |   |    | . 1 | 1726.0 |
| 1   |         | 98   | 32. |      | 1730.0 |   | 1 | 1625 |     | 0. | .1  | 1726.0 |     | 2 | 0045 29 |   |    | .1  | 1726.0 |
| 1   |         | 99   | 32. | 4.7  | 1729.9 |   | 1 | 1630 |     | 0. | . 1 | 1726.0 |     | 2 | 0050 29 |   |    | .1  | 1726.0 |
| 1   | 0815 10 |      | 31. |      | 1729.8 |   | 1 | 1635 |     | 0. |     | 1726.0 |     | 2 | 0055 30 |   |    | .1  | 1726.0 |
|     | 0022 20 | 4.00 |     |      |        |   |   |      |     |    |     |        |     | - |         |   |    |     |        |

| PEAK FLOW    | TIME |           |          | MAXIMUM AVE  |             |          |
|--------------|------|-----------|----------|--------------|-------------|----------|
|              |      |           | 6-HR     | 24-HR        | 72-HR       | 24.92-HR |
| + (CFS)      | (HR) |           |          |              |             |          |
|              |      | (CFS)     |          | 2.2          |             | -        |
| + 45.        | 5.17 |           | 38.      | 11.          | 11.         | 11.      |
|              |      | (INCHES)  | 2.342    | 2,786        | 2.786       | 2.786    |
|              |      | (AC-FT)   | 19.      | 22.          | 22.         | 22.      |
| PEAK STORAGE | TIME |           |          | MAXIMUM AVER | AGE STORAGE |          |
|              |      |           | 6~HR     | 24-HR        | 72-HR       | 24.92-HR |
| + (AC-FT)    | (HR) |           |          |              |             |          |
| 13.          | 5.17 |           | 8.       | 2.           | 2.          | 2.       |
| PEAK STAGE   | TIME |           |          | MAXIMUM AVE  | RAGE STAGE  |          |
|              |      |           | 6-HR     | 24-HR        | 72-HR       | 24.92-HR |
| + (FEET)     | (HR) |           |          |              |             |          |
| 1733.80      | 5.17 |           | 1731.59  | 1727.56      | 1727.50     | 1727.50  |
|              |      | CUMULATIV | E AREA = | .15 SQ MI    |             |          |

HYDROGRAPH AT STATION DETPOND

|        |      |     |         |         |        | *: |       |        |     |         |         |        | * |     |     |      |     |         |         |       |
|--------|------|-----|---------|---------|--------|----|-------|--------|-----|---------|---------|--------|---|-----|-----|------|-----|---------|---------|-------|
| OA MON | HRMN | ORD | OUTFLOW | STORAGE | STAGE  | :  | DA MO | N HRMN | ORD | OUTFLOW | STORAGE | STAGE  | * | DA  | MON | HRMN | ORD | OUTFLOW | STORAGE | STAG  |
| 1      | 0000 | 1   | 0.      | .1      | 1726.0 | *  | 1     | 0820   | 101 | 4.      | . 4     | 1726.4 | * | 1   |     | 1640 | 201 | 0.      | .1      | 1726. |
| 1      | 0005 | 2   | 0.      | -1      | 1726.0 | *  | 2     | 0825   | 102 | 4.      | .3      | 1726.3 | * | 1   |     | 1645 | 202 | 0.      | .1      | 1726. |
| 1      | 0010 | 3   | 0.      | .1      | 1726.0 | *  | 1     | 0830   | 103 | 3.      | .3      | 1726.3 | * | 1   |     | 1650 | 203 | 0.      | .1      | 1726. |
| 1      | 0015 | 4   | 0.      | -1      | 1726.0 | *  | 1     | 0835   | 104 | 3.      | .3      | 1726.3 | * | 1   |     | 1655 | 204 | 0.      | .1      | 1726. |
| 1      | 0020 | 5   | 0.      | .1      | 1726.0 |    | 1     | 0840   | 105 | 3.      | .3      | 1726.2 | * | 1   |     | 1700 | 205 | 0.      | .1      | 1726. |
| 1      | 0025 | 6   | 0.      | -1      | 1726.0 | *  | 1     | 0845   | 106 | 2.      | .2      | 1726.2 | * | 1   |     | 1705 | 206 | 0.      | .1      | 1726. |
| 1      | 0030 | 7   | 0.      | .1      | 1726.0 | *  | 1     | 0850   | 107 | 2.      | .2      | 1726.2 | * | 1   |     | 1710 | 207 | 0.      | . 1     | 1726. |
| 1      | 0035 | 8   | 0.      | .1      | 1726.0 |    | 1     | 0855   | 108 | 2.      | .2      | 1726.2 | * | 1   |     | 1715 | 208 | 0.      | .1      | 1726. |
| 1      | 0040 | 9   | 0.      | -1      | 1726.0 | *  | 1     | 0900   |     | 2.      | .2      | 1726.2 | * | 1   |     | 1720 | 209 | 0.      | .1      | 1726. |
| 1      | 0045 | 10  | 0.      | .1      | 1726.0 |    | 1     | 0905   | 110 | 2.      | .2      | 1726.1 |   | 1   |     | 1725 | 210 | 0.      | .1      | 1726. |
| 1      | 0050 | 11  | 0.      | .1      | 1726.0 | *  | 1     | 0910   | 111 | 1.      | .2      | 1726.1 | * | 1   |     | 1730 | 211 | 0.      | . 1     | 1726. |
| 1      | 0055 | 12  | 0.      | .1      | 1726.0 | *  | 1     | 0915   | 112 | 1.      | .2      | 1726.1 |   | 1   |     | 1735 | 212 | 0.      | .1      | 1726. |
| 1      | 0100 | 13  | 0.      | .1      | 1726.0 |    | 1     | 0920   |     | 1.      | .2      | 1726.1 |   | 1   |     | 1740 | 213 | 0.      | .1      | 1726. |
| 1      | 0105 | 14  | 0.      | .1      | 1726.0 |    | 1     | 0925   |     | 1.      | .2      | 1726.1 |   | 1   |     | 1745 | 214 | 0.      | . 1     | 1726  |
| 1      | 0110 | 15  | 0.      | . 1     | 1726.0 |    | 1     | 0930   |     | 1.      | .1      | 1726.1 | * | 1   |     | 1750 | 215 | 0.      | .1      | 1726. |
| 1      | 0115 | 16  | 0.      | .1      | 1726.0 |    | 1     | 0935   | 116 | 1.      | . 1     | 1726.1 |   | 1   |     | 1755 | 216 | 0.      | .1      | 1726. |
| 1      | 0120 | 17  | 0.      | .1      | 1726.0 |    | 1     | 0940   |     | 1.      | . 1     | 1726.1 | * | 1   |     | 1800 |     | 0.      | .1      | 1726. |
| 1      | 0125 | 18  | 0.      | -1      | 1726.0 |    | 1     | 0945   | 118 | 1.      | .1      | 1726.1 | * | 1   |     | 1805 |     | 0.      | . 1     | 1726. |
| 1      | 0130 | 19  | 0.      | .1      | 1726.0 | *  | 1     | 0950   | 119 | 1.      | .1      | 1726.1 | * | 1   |     | 1810 |     | 0.      | . 1     |       |
| 1      | 0135 | 20  | 0.      | . 1     | 1726.0 |    | 1     | 0955   | 120 | 1.      | .1      | 1726.1 | * | - 1 |     | 1815 | 220 | 0.      | . 1     | 1726. |
| 1      | 0140 | 21  | 0.      | .1      | 1726.0 | *  | 1     | 1000   |     | 1.      | .1      | 1726.0 | * | 1   |     | 1820 |     | 0       | . 1     | 1726. |
| 1      | 0145 | 22  | 0.      | .1      | 1726.0 |    | 1     | 1005   | 122 | 0.      | . 1     | 1726.0 | * | 1   |     | 1825 | 222 | 0.      | .1      | 1726. |
| 1      | 0150 | 23  | 1.      | .1      | 1726.0 |    | 1     | 1010   |     | 0.      | .1      | 1726.0 |   | 1   |     | 1830 | 223 | 0.      | . 1     | 1726. |
| 1      | 0155 | 24  | 1.      | .1      | 1726.1 |    | 1     | 1015   |     | 0.      | .1      | 1726.0 |   | 1   |     | 1835 |     | 0.      | -1      | 1726  |
| 1      | 0200 | 25  | 1.      | .1      | 1726.1 |    | 1     | 1020   |     | 0.      | .1      | 1726.0 |   | 1   |     | 1840 |     | 0.      | . 1     |       |
| 1      | 0205 | 26  | 1.      | . 1     | 1726.1 |    | 1     | 1025   |     | 0.      | .1      | 1726.0 |   | 1   |     | 1845 |     | 0.      | . 1     | 1726. |

|    | 1 0210<br>1 0215<br>1 0225<br>1 0235<br>1 0230<br>1 0245<br>1 0255<br>1 0300<br>1 0310<br>1 0310<br>1 0310<br>1 0310<br>1 0310<br>1 0350<br>1 0350 | 28<br>30<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31 | 1. 1. 1. 2. 2. 2. 3. 3. 4. 4. 4. 5. 6. 8. 13. 20. 24. 29. 30. 31. 31. 32. 32. 32. 32. 32. 32. 32. 32. 32. 32 | .2.2.2.2.2.3.3.3.3.3.3.3.3.3.3.3.3.3.3. |  |                     | 1030<br>1045<br>1055<br>1100<br>1115<br>1110<br>1111<br>1112<br>1112<br>111 | 128 133 134 135 137 138 139 141 142 143 145 156 157 158 159 160 151 177 178 179 181 189 189 189 199 199 199 199 199 19 | 0.<br>0.<br>0.<br>0.<br>0.       |                            | 1726.0 | *************************************** | 111111111111111111111111111111111111111 | 1850<br>1905<br>1910<br>1915<br>1925<br>1935<br>1940<br>2005<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2025<br>2020<br>2020<br>2025<br>2020<br>2020<br>2025<br>2020<br>2020<br>2020<br>2025<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2020<br>2 | 228 231 232 231 232 231 232 231 232 231 232 231 232 231 232 231 232 231 232 231 232 231 231 |       | 00.0000 |                                  | 1726.0 |    |
|----|--|--|--|---|--|---------------------|---|--|----------------------------------|----------------------------|---|---|---|---|---|-------|---|----------------------------------|--|----|
| 3  | PEAK FLOW  | TIME   | *******  | *****                                   | 6-HR   | MAXII               |   | ******<br>RAGE FLA<br>72-1   | WC                               | 24.92-HR                   | ******  | ***                                     | *****                                   | *****   | *****   | ***** | ***   | ******                           | ******   | 9  |
| +  | (CFS)<br>32,   | (HR)<br>5.00   | (CF  |   | 20.<br>1.266   | 1                   | 5.  | 1.3  | 5.                               | 5.<br>1.301                |   |   |   |   |   |       |   |                                  |  |    |
| Pi | EAK STORAGE  | TIME   | (AC-F  | FT)                                     | 4  | MIXAN               | JM AVER   | AGE STO  | RAGE                             | 10.                        |   |   |   |   |   |       |   |                                  |  |    |
| +  | (AC-FT)  | (HR)<br>5.00   |  |   | 6-HR<br>2.   |                     | 4-HR<br>1.  |  | HR<br>1.                         | 24.92-HR                   |   |   |   |   |   |       |   |                                  |  |    |
| 1  | PEAK STAGE   |  |  |   |  | MAXTI               | MIIM AVE  | RAGE ST  | AGE                              | 24.92-HR                   |   |   |   |   |   |       |   |                                  |  |    |
| +  | (FEET)<br>1730.08  | (HR)<br>5.00   |  |   | 728.29   |                     |   |  |                                  |                            |   |   |   |   |   |       |   |                                  |  |    |
|    |  |  | CUMUL  | ATIVE                                   | AREA =   | .15                 | SQ MI   |  |                                  |                            |   |   |   |   |   |       |   |                                  |  |    |
| ** | • • • • • • • • • • • •  | ******   | ******   | *****                                   | *******  | ****                |   |  |                                  | on Detpon                  |   | ***                                     | *****                                   | ****  | ****  | ***** | ****  | ******                           | *******  | E. |
| ** |  |  |  |   | *******  |                     | PL  | AN 1,  | RATIO                            | = .58                      |   | ***                                     | *****                                   | ****  | ****  | ***** | ****  |                                  | *******  |    |
|    | DA MON HRMN  | ORD OU   | TFLOW ST   | PORAGE                                  | STAGE *  | DA M                | ON HRMN   | ORD O  | UTFLOW                           | STORAGE                    | STAGE   | *                                       | DA MON                                  | HRMN  | ORD   | OUTFL | OW  | STORAGE                          | STAGE  |    |
|    | 1 0000<br>1 0005<br>1 0010<br>1 0025<br>1 0020<br>1 0025<br>1 0030<br>1 0035   | 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9                            | 0.<br>0.<br>0.<br>0.<br>0.   | .1<br>.1<br>.1<br>.1<br>.1<br>.1<br>.1  | 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * 1726.0 * | 1 1 1 1 1 1 1 1 1 1 | 0820<br>0825<br>0830<br>0835<br>0840<br>0845<br>0850<br>0855                | 101<br>102<br>103<br>104<br>105<br>106<br>107<br>108<br>109  | 3.<br>3.<br>3.<br>2.<br>2.<br>2. | .3 .3 .2 .2 .2 .2 .2 .2 .2 | 1726.3<br>1726.3<br>1726.3<br>1726.2<br>1726.2<br>1726.2<br>1726.2<br>1726.2<br>1726.2  | * * * * * * * *                         | 1 | 1640<br>1645<br>1650<br>1655<br>1700<br>1705<br>1710<br>1715<br>1720  | 201<br>202<br>203<br>204<br>205<br>206<br>207<br>208<br>209                                 |       | 0.  | .1<br>.1<br>.1<br>.1<br>.1<br>.1 | 1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0<br>1726.0   |    |
|    | 1 0045<br>1 0050<br>1 0055<br>1 0100   | 10<br>11<br>12<br>13   | 0.<br>0.<br>0.   | .1                                      | 1726.0 * 1726.0 * 1726.0 * 1726.0 *  | 1<br>1<br>1         | 0905<br>0910<br>0915<br>0920  | 110<br>111<br>112<br>113   | 1.<br>1.<br>1.                   | .2<br>.2<br>.2<br>.1       | 1726.1<br>1726.1<br>1726.1<br>1726.1  |   | 1<br>1<br>1                             | 1725<br>1730<br>1735<br>1740  | 210<br>211<br>212<br>213  |       | 0.  | .1<br>.1<br>.1                   | 1726.0<br>1726.0<br>1726.0<br>1726.0   |    |

| 1  | 0105 14  | 0.  | .1 1726.   | 0 * 1  | 0925 114 | 1. | .1  | 1726.1 * | 1 | 1745 214 | 0. | .1  | 1726.0 |
|----|----------|-----|------------|--------|----------|----|-----|----------|---|----------|----|-----|--------|
| 1  | 0110 15  | 0.  | .1 1726.   | 0 * 1  | 0930 115 | 1. | .1  | 1726.1 * | 1 | 1750 215 | 0. | . 1 | 1726.0 |
| 1  | 0115 16  | 0.  | .1 1726.   |        | 0935 116 | 1. | .1  | 1726.1 * | 1 | 1755 216 | 0. | . 1 | 1726.0 |
| 1  | 0120 17  | 0.  | .1 1726.   |        | 0940 117 | 1. | .1  | 1726.1 * | 1 | 1800 217 | 0. |     | 1726.0 |
|    |          |     |            |        |          |    |     |          | + |          |    | .1  |        |
| 1  | 0125 18  | 0.  | .1 1726.   | 0 * 1  | 0945 118 | 1. | - 1 | 1726.1 * | 1 | 1805 218 | 0. | .1  | 1726.0 |
| 1  | 0130 19  | 0.  | .1 1726.   |        | 0950 119 | 1. | .1  | 1726.0 * | 1 | 1810 219 | 0. | . 1 | 1726.0 |
| 1  | 0135 20  | 0.  | .1 1726.   | 0 * 1  | 0955 120 | 0. | . 1 | 1726.0 * | 1 | 1815 220 | 0. | .1  | 1726.0 |
| 1  | 0140 21  | 0.  | .1 1726.   |        | 1000 121 | 0. | .1  | 1726.0 * | 1 | 1820 221 | 0. | .1  | 1726.0 |
|    |          |     | .1 1/20.   | 0 - 1  |          | 0. |     |          | - |          |    |     |        |
| 1  | 0145 22  | 0.  | .1 1726.   |        | 1005 122 | 0. | .1  | 1726.0 * | 1 | 1825 222 | 0. | .1  | 1726.0 |
| 1  | 0150 23  | 0.  | .1 1726.   | 0 * 1  | 1010 123 | 0. | . 1 | 1726.0 * | 1 | 1830 223 | 0. | .1  | 1726.0 |
| 1  | 0155 24  | 1.  | .1 1726.   | 0 * 1  | 1015 124 | 0. | . 1 | 1726.0 * | 1 | 1835 224 | 0. | . 1 | 1726.0 |
| 1  | 0200 25  | 1.  | .1 1726.   | 1 * 1  | 1020 125 | 0. | .1  | 1726.0 * | 1 | 1840 225 | 0. | . 1 | 1726.0 |
| -  |          |     |            |        |          |    |     |          | - |          |    |     |        |
| 1  | 0205 26  | 1.  | .1 1726.   |        | 1025 126 | 0. | .1  | 1726.0 * | 1 | 1845 226 | 0. | .1  | 1726.0 |
| 1  | 0210 27  | 1.  | .1 1726.   | 1 * 1  | 1030 127 | 0. | .1  | 1726.0 * | 1 | 1850 227 | 0. | .1  | 1726.0 |
| 1  | 0215 28  | 1.  | .1 1726.   | 1 * 1  | 1035 128 | 0. | . 1 | 1726.0 * | 1 | 1855 228 | 0. | .1  | 1726.0 |
| 1  | 0220 29  | 1.  | .2 1726.   |        | 1040 129 | 0. | .1  | 1726.0 * | 1 | 1900 229 | 0. | .1  | 1726.0 |
| 1  |          |     |            |        |          | 0. |     | 1726.0 * | 4 |          | 0. |     |        |
|    | 0225 30  | 1.  | .2 1726.   | 1 " 1  | 1045 130 |    | .1  | 1726.0 " | 1 |          | 0. | .1  | 1726.0 |
| 1  | 0230 31  | 2.  | .2 1726.   | 1 * 1  | 1050 131 | 0. | . 1 | 1726.0 * | 1 | 1910 231 | 0. | .1  | 1726.0 |
| 1  | 0235 32  | 2.  | .2 1726.   | 2 * 1  | 1055 132 | 0. | . 1 | 1726.0 * | 1 | 1915 232 | 0. | . 1 | 1726.0 |
| 1  | 0240 33  | 2.  | .2 1726.   | 2 * 1  | 1100 133 | 0. | .1  | 1726.0 * | 1 | 1920 233 | 0. | .1  | 1726.0 |
| 1  | 0245 34  | 2.  | .2 1726.   | 2 * 1  | 1105 134 | 0. | .1  | 1726.0 * | 1 | 1925 234 | 0. | .1  | 1726.0 |
| -  |          |     | 2 1720.    |        |          |    |     | 1720.0   | 4 |          | 0. |     |        |
| 1  | 0250 35  | 3.  | .3 1726.   |        | 1110 135 | 0. | .1  | 1726.0 * | 1 | 1930 235 | 0. | .1  | 1726.0 |
| 1  | 0255 36  | 3.  | .3 1726.   | 3 * 1  | 1115 136 | 0. | .1  | 1726.0 * | 1 | 1935 236 | 0. | . 1 | 1726.0 |
| 1  | 0300 37  | 3.  | .3 1726.3  | 3 * 1  | 1120 137 | 0. | . 1 | 1726.0 * | 1 | 1940 237 | 0. | .1  | 1726.0 |
| 1  | 0305 38  | 4.  | .3 1726.   | 3 * 1  | 1125 138 | 0. | .1  | 1726.0 * | 1 | 1945 238 | 0. | .1  | 1726.0 |
| 1  | 0310 39  | 4.  | .4 1726.   |        | 1130 139 | 0. | .1  | 1726.0 * | 1 | 1950 239 | 0. | .1  | 1726.0 |
| 1  |          |     | . 4 1720.  |        |          |    |     | 1720.0   | 4 |          |    |     | 1720.0 |
| 1  | 0315 40  | 5.  | .4 1726.   | 5 * 1  | 1135 140 | 0. | .1  | 1726.0 * | 1 | 1955 240 | 0. | .1  | 1726.0 |
| 1  | 0320 41  | 8.  | .6 1726.   | 7 * 1  | 1140 141 | 0. | .1  | 1726.0 * | 1 | 2000 241 | 0. | .1  | 1726.0 |
| 1  | 0325 42  | 12. | .9 1727.   | 1 * 1  | 1145 142 | 0. | . 1 | 1726.0 * | 1 | 2005 242 | 0. | .1  | 1726.0 |
| 1  | 0330 43  | 19. | 1.3 1727.  | 7 * 1  | 1150 143 | 0. | .1  | 1726.0 * | 1 | 2010 243 | 0. | . 1 | 1726.0 |
| 1  | 0335 44  | 23. | 1.9 1728.  |        | 1155 144 | 0. | .1  | 1726.0 * | 1 | 2015 244 | 0. | .1  | 1726.0 |
| +  |          |     |            |        |          |    |     |          |   |          |    |     |        |
| 1  | 0340 45  | 25. | 2.5 1728.  |        | 1200 145 | 0. | .1  | 1726.0 * | 1 | 2020 245 | 0. | . 1 | 1726.0 |
| 1  | 0345 46  | 27. | 3.0 1729.  |        | 1205 146 | 0. | .1  | 1726.0 * | 1 | 2025 246 | 0. | .1  | 1726.0 |
| 1  | 0350 47  | 28. | 3.5 1729.3 | 2 * 1  | 1210 147 | 0. | .1  | 1726.0 * | 1 | 2030 247 | 0. | . 1 | 1726.0 |
| 1  | 0355 48  | 29. | 3.8 1729.  | 4 1    | 1215 148 | 0. | .1  | 1726.0 * | 1 | 2035 248 | 0. | . 1 | 1726.0 |
| 1  | 0400 49  | 30. | 4.1 1729.  |        | 1220 149 | 0. | .1  | 1726.0 * | 1 | 2040 249 | 0. | .1  | 1726.0 |
|    |          |     |            |        |          |    |     |          |   |          |    |     |        |
| 1  | 0405 50  | 30. | 4.3 1729.  | 7 * 1  | 1225 150 | 0. | .1  | 1726.0 * | 1 | 2045 250 | 0. | . 1 | 1726.0 |
| 1  | 0410 51  | 31. | 4.4 1729.  | 8 * 1  | 1230 151 | 0. | .1  | 1726.0 * | 1 | 2050 251 | 0. | .1  | 1726.0 |
| 1  | 0415 52  | 31. | 4.5 1729.1 | 8 * 1- | 1235 152 | 0. | . 1 | 1726.0 * | 1 | 2055 252 | 0. | . 1 | 1726.0 |
| 1  | 0420 53  | 31. | 4.5 1729.  |        | 1240 153 | 0. | .1  | 1726.0 * | 1 | 2100 253 | 0. | .1  | 1726.0 |
| 1  | 0425 54  | 31. | 4.5 1729.1 | 0 + 1  | 1245 154 | 0. | .1  | 1726.0 * | 4 | 2105 254 | 0. | .1  | 1726.0 |
| 1  |          |     |            |        |          |    |     | 1720.0   | + |          |    |     |        |
| 1  | 0430 55  | 31. | 4.5 1729.1 |        | 1250 155 | 0. | , 1 | 1726.0 * | 1 | 2110 255 | 0. | .1  | 1726.0 |
| 1  | 0435 56  | 31. | 4.6 1729.  |        | 1255 156 | 0. | .1  | 1726.0 * | 1 | 2115 256 | 0. | .1  | 1726.0 |
| 1  | 0440 57  | 31. | 4.6 1729.  | 9 * 1  | 1300 157 | 0. | . 1 | 1726.0 * | 1 | 2120 257 | 0. | .1  | 1726.0 |
| 1  | 0445 58  | 31. | 4.6 1729.5 |        | 1305 158 | 0. | .1  | 1726.0 * | 1 | 2125 258 | 0. | .1  | 1726.0 |
| 1  | 0450 59  | 31. | 4.6 1729.  |        | 1310 159 | 0. | .1  | 1726.0 * | 1 | 2130 259 | 0. | .1  | 1726.0 |
|    |          |     |            |        |          |    |     | 1720.0   |   |          |    |     | 1/26.0 |
| 1  | 0455 60  | 31. | 4.6 1729.  |        | 1315 160 | 0. | .1  | 1726.0 * | 1 | 2135 260 | 0. | . 1 | 1726.0 |
| 1  | 0500 61  | 31. | 4.6 1729.9 |        | 1320 161 | 0. | . 1 | 1726.0 * | 1 | 2140 261 | 0. | .1  | 1726.0 |
| 1  | 0505 62  | 31. | 4.6 1729.  | 9 * 1  | 1325 162 | 0. | . 1 | 1726.0 * | 1 | 2145 262 | 0. | .1  | 1726.0 |
| 1  | 0510 63  | 31, | 4.6 1729.1 |        | 1330 163 | 0. | . 1 | 1726.0 * | 1 | 2150 263 | 0. | .1  | 1726.0 |
| 1  | 0515 64  | 31. | 4.5 1729.1 |        | 1335 164 | 0. | .1  | 1726.0 * | 1 | 2155 264 | 0. | .1  | 1726.0 |
| 1  |          |     | 4.3 1729.1 |        |          |    | - 1 | 1720.0   | 4 |          |    |     | 1726.0 |
| 1  | 0520 65  | 31, | 4.4 1729.  |        | 1340 165 | 0. | .1  | 1726.0 * | 1 | 2200 265 | 0. | . 1 | 1726.0 |
| 1  | 0525 66  | 30. | 4.2 1729.  | 7 * 1  | 1345 166 | 0. | . 1 | 1726.0 * | 1 | 2205 266 | 0. | . 1 | 1726.0 |
| 1  | 0530 67  | 30. | 4.1 1729.  | 5 * 1. | 1350 167 | 0. | . 1 | 1726.0 * | 1 | 2210 267 | 0. | . 1 | 1726.0 |
| 1  | 0535 68  | 30. | 4.0 1729.5 |        | 1355 168 | 0. | .1  | 1726.0 * | 1 | 2215 268 | 0. | . 1 | 1726.0 |
| 1  | 0540 69  | 29. | 3.8 1729.4 |        | 1400 169 | 0. | . 1 | 1726.0 * | 1 | 2220 269 | 0. | . 1 | 1726.0 |
| +  |          |     | 3.0 1/23.  |        | 4400 400 |    |     |          |   | 2225 270 |    |     |        |
| 1  |          | 29. | 3.7 1729.  |        |          | 0. | .1  | 1726.0 * | - |          | 0. | .1  | 1726.0 |
| 1  | 0550 71  | 28. | 3.5 1729.  |        | 1410 171 | 0. | .1  | 1726.0 * | 1 | 2230 271 | 0. | . 1 | 1726.0 |
| 1  | 0555 72  | 28. | 3.3 1729.2 | 2 * 1  | 1415 172 | 0. | .1  | 1726.0 * | 1 | 2235 272 | 0. | .1  | 1726.0 |
| 1  | 0600 73  | 27. | 3.2 1729.  | * 1    | 1420 173 | 0. | . 1 | 1726.0 * | 1 | 2240 273 | 0. | . 1 | 1726.0 |
| .1 | 0605 74  | 27. | 3.0 1729.0 | . 1    | 1425 174 | 0. | . 1 | 1726.0 * | 1 | 2245 274 | 0. | . 1 | 1726.0 |
| 1  | 0610 75  | 26. | 2.8 1728.5 |        | 1430 175 | 0. | .1  | 1726.0 * | 1 | 2250 275 | 0. | .1  | 1726.0 |
| 1  | 0615 76  | 26. | 2.7 1728.1 |        | 1435 176 | 0. | .1  | 1726.0 * | 1 | 2255 276 | 0. | . 1 | 1726.0 |
| 1  |          |     | 2.7 1728.  |        |          |    |     |          | 1 |          |    |     | 1720.0 |
| 1  | 0620 77  | 25. | 2.5 1728.  |        |          | 0. | .1  | 1726.0 * | 1 | 2300 277 | 0. | .1  | 1726.0 |
| 1  | 0625 78  | 25. | 2.4 1728.  | 5 * 1  | 1445 178 | 0. | .1  | 1726.0 * | 1 | 2305 278 | 0. | .1  | 1726.0 |
| 1  | 0630 79  | 24. | 2.2 1728.  | 4 1    | 1450 179 | 0. | .1  | 1726.0 * | 1 | 2310 279 | 0. | . 1 | 1726.0 |
| 1  | 0635 80  | 24. | 2.0 1728.  |        | 1455 180 | 0. | .1  | 1726.0 * | 1 | 2315 280 | 0. | .1  | 1726.0 |
| 1  | 0640 81  | 23. | 1.9 1728.  |        | 1500 181 | 0. | .1  | 1726.0 * | 1 | 2320 281 | 0. | .1  | 1726.0 |
| 1  | 0645 82  | 23. | 1.7 1728.  |        | 1505 182 | 0. | .1  | 1726.0 * | 1 | 2325 282 | 0. | 1   | 1726.0 |
| 1  |          | 23. |            |        |          |    |     |          | 1 |          |    |     |        |
| 1  | 0650 83  | 22. | 1.6 1728.0 |        | 1510 183 | 0. | .1  | 1726.0 * | 1 | 2330 283 | 0. | .1  | 1726.0 |
| 1  | 0655 84  | 20. | 1.4 1727.  |        | 1515 184 | 0. | .1  | 1726.0 * | 1 | 2335 284 | 0. | . 1 | 1726.0 |
| 1  | 0700 85  | 18. | 1.3 1727.  |        | 1520 185 | 0. | .1  | 1726.0 * | 1 | 2340 285 | 0. | . 1 | 1726.0 |
| 1  | 0705 86  | 17. | 1.2 1727.  |        | 1525 186 | 0. | .1  | 1726.0 * | 1 | 2345 286 | 0. | . 1 | 1726.0 |
| 1  | 0710 87  | 15. | 1.1 1727.  |        | 1530 187 | 0. | .1  | 1726.0 * | 1 | 2350 287 | 0. | .1  | 1726.0 |
| 2  |          |     | 1 0 1727.4 |        |          |    |     |          | 4 |          |    |     | 1720.0 |
| 1  | 0715 88  | 14. | 1.0 1727.  |        | 1535 188 | 0. | .1  | 1726.0 * | 1 | 2355 288 | 0. | .1  | 1726.0 |
| 1  | 0720 89  | 12. | .9 1727.   | * 1    | 1540 189 | 0. | .1  | 1726.0 * | 2 | 0000 289 | 0. | . 1 | 1726.0 |
| 1  | 0725 90  | 11. | .8 1727.0  | * 1    | 1545 190 | 0. | .1  | 1726.0 * | 2 | 0005 290 | 0. | . 1 | 1726.0 |
| 1  | 0730 91  | 10. | .7 1726.9  | * 1.   | 1550 191 | 0. | .1  | 1726.0 * | 2 | 0010 291 | 0. | . 1 | 1726.0 |
| 1  | 0735 92  | 9.  | .7 1726.1  |        | 1555 192 | 0. | .1  | 1726.0 * | 2 | 0015 292 | 0. | .1  | 1726.0 |
| 1  |          |     |            |        |          |    |     | 1726.0 * | 2 |          | 0. |     |        |
| 1  | 0740 93  | 8.  | .6 1726.   |        | 2000 200 | 0. | .1  |          | 4 |          | 0. | . 1 | 1726.0 |
| 1  | 0745 94  | 7.  | .6 1726.   |        | 1605 194 | 0. | .1  | 1726.0 * | 2 | 0025 294 | 0. | .1  | 1726.0 |
| 1  | 0750 95  | 7.  | .5 1726.   |        | 1610 195 | 0. | .1  | 1726.0 * | 2 | 0030 295 | 0. | . 1 | 1726.0 |
| 1  | 0755 96  | 6.  | .5 1726.   |        | 1615 196 | 0. | .1  | 1726.0 * | 2 | 0035 296 | 0. | .1  | 1726.0 |
| 1  | 0800 97  | 5.  | .4 1726.   |        | 1620 197 | 0. | .1  | 1726.0 * | 2 | 0040 297 | 0. | . 1 | 1726.0 |
| 4  | 0805 98  | 5.  | .4 1726.4  |        | 1625 198 | 0. | .1  | 1726.0 * | 2 | 0045 298 | 0. | .1  | 1726.0 |
| 4  | 0810 99  |     |            |        | 1630 199 |    |     |          | 2 | 0050 299 |    |     | 1720.0 |
| 1  |          | 4.  | .4 1726.   |        |          | 0. | .1  | 1726.0 * |   |          | 0. | .1  | 1726.0 |
| 1  | 0815 100 | 4.  | .3 1726.4  | 4 * 1  | 1635 200 | 0. | .1  | 1726.0 * | 2 | 0055 300 | 0. | . 1 | 1726.0 |
|    |          |     |            | *      |          |    |     | *        |   |          |    |     |        |

| PEAK FLOW           | TIME         |                              | 6-HR                | MAXIMUM AV           | ERAGE FLOW<br>72-HR   | 24.92-HR     |
|---------------------|--------------|------------------------------|---------------------|----------------------|-----------------------|--------------|
| + (CFS)             | (HR)         | 12 62261                     | 0-111               | Se-1114              | 72-m                  | 24.92-111    |
| + 31.               | 5.00         | (CFS)<br>(INCHES)<br>(AC-FT) | 19.<br>1.200<br>10. | 1.229<br>10.         | 1.229<br>10.          | 1.229<br>10. |
| PEAK STORAGE        | TIME         |                              | 6-HR                | MAXIMUM AVE<br>24-HR | RAGE STORAGE<br>72-HR | 24.92-HR     |
| + (AC-FT) 5.        | (HR)<br>5.00 |                              | 2.                  | 1.                   | 1.                    | 1.           |
| PEAK STAGE          | TIME         |                              | 6-HR                | MAXIMUM AV<br>24-HR  | ERAGE STAGE<br>72-HR  | 24.92-HR     |
| + (FEET)<br>1729.88 | (HR)<br>5.00 |                              | 1728.14             | 1726.55              | 1726.53               | 1726.53      |
|                     |              | CUMULATIV                    | /E AREA =           | .15 SQ MI            |                       |              |

<sup>\*\*\*</sup> FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

| OPERATION     | STATION  | AREA | PLAN |              | RATIO 1<br>1.00                        | rios appli<br>ratio 2<br>.60 | ED TO PREC<br>RATIO 3<br>.58 | IPITATION |
|---------------|----------|------|------|--------------|--|------------------------------|------------------------------|-----------|
| HYDROGRAPH AT |          |      |      |              | 33.<br>3.58                            |                              |                              |           |
| HYDROGRAPH AT | OND9     |      |      |              | 3.                                     |                              |                              |           |
| HYDROGRAPH AT | OFFD3    | .03  |      |              | 35.<br>3.58                            |                              |                              |           |
| 2 COMBINED AT | CP-7     |      |      |              | 37.<br>3.58                            |                              |                              |           |
| 2 COMBINED AT | CP-8     |      |      |              | 70.<br>3.58                            |                              |                              |           |
| ROUTED TO     | RCP8-CP- | .05  |      |              | 67.<br>3.67                            |                              |                              |           |
| HYDROGRAPH AT |          |      |      |              | 10.<br>3.58                            |                              |                              |           |
| HYDROGRAPH AT |          |      |      |              | 13.                                    |                              |                              |           |
| 3 COMBINED AT | CP-9     |      |      |              | 89.<br>3.58                            |                              |                              |           |
| ROUTED TO     | RCP9-CP- |      |      |              |  |                              |                              |           |
| HYDROGRAPH AT |          |      |      |              | 8.                                     |                              |                              |           |
| 2 COMBINED AT | CP-10A   | .07  |      |              | 92.<br>3.58                            |                              |                              |           |
| HYDROGRAPH AT | OND11    | .01  | 1    |              | 24.<br>3.58                            |                              |                              |           |
| HYDROGRAPH AT | OND13    | .01  |      |              | 12.<br>3.50                            |                              |                              |           |
| 3 COMBINED AT | CP-10    | .09  | 1    |              | 127.<br>3.58                           |                              |                              |           |
| ROUTED TO     | EQBASIN  |      |      |              | 93.<br>3.75                            |                              |                              |           |
|               |          |      |      |              | 3.75<br>GES IN FEET<br>1748.19<br>3.75 |                              |                              |           |
| DIVERSION TO  | DVPIPE   | .09  |      |              | 3.75<br>67.<br>3.75                    |                              |                              |           |
| HYDROGRAPH AT | DIVWEIR  |      |      |              | 3.75<br>26.<br>3.75                    |                              |                              |           |
| HYDROGRAPH AT | OND14    |      |      |              | 2.1                                    |                              | 14.                          |           |
| 2 COMBINED AT | CP-11    | .11  | 1    | TIME         | 20                                     | 10                           | 3.50                         |           |
| HYDROGRAPH AT | OND1     | .00  | 1    | TIME         |  | 3.50<br>1.<br>3.50           | 3.50                         |           |
| HYDROGRAPH AT | OFFD2    |      |      | TIME<br>FLOW | 3.50<br>23.<br>3.50                    |                              |                              |           |
| 2 COMBINED AT | CP-1     | .02  |      | TIME         |  | 3.50<br>11.<br>3.50          | 10.<br>3.50                  |           |
| ROUTED TO     | RCP1-CP2 | .02  | 1    | TIME         |  |                              |                              |           |
| HYDROGRAPH AT | OND2     | .01  | 1    | TIME         |  | 11.<br>3.58                  |                              |           |
| HYDROGRAPH AT | OFFD1    |      |      | TIME         | 3.58                                   |                              | 3.58                         |           |
| 3 COMBINED AT |          |      |      | TIME         |  | 39.<br>3.58                  |                              |           |
| ROUTED TO     | RCP2-CP- |      |      | TIME         |  | 54.<br>3.58                  |                              |           |
|               | DUFF-UF- | .03  | *    | · MAN        | 4471                                   | 221                          | 30,                          |           |

|                 |          |     |    | TIME         | 3.58         | 3.58          | 3.58        |
|-----------------|----------|-----|----|--------------|--------------|---------------|-------------|
| HYDROGRAPH AT   | OND3     | .00 | 1  | FLOW<br>TIME | 4.<br>3.50   | 2.<br>3.50    | 2.<br>3.50  |
| 2 COMBINED AT + | CP-3     | .09 | 1  | FLOW<br>TIME | 121.<br>3.58 | 54.<br>3.58   | 51.<br>3.58 |
| ROUTED TO       | RCP3-CP4 | .09 | 1  | FLOW<br>TIME | 118.<br>3.58 | 52.<br>3.58   | 49.<br>3.58 |
| HYDROGRAPH AT   | OND7     | .01 | 1  | FLOW<br>TIME | 16.<br>3.50  | 8.<br>3.50    | 7.<br>3.50  |
| 2 COMBINED AT   | CP-4     | .10 | 1  | FLOW<br>TIME | 131.<br>3.58 | 59.<br>3.58   | 55.<br>3.58 |
| HYDROGRAPH AT   | OND4     | .02 | 1  | FLOW<br>TIME | 27.<br>3.58  | 13.<br>3.58   | 12.<br>3.58 |
| HYDROGRAPH AT   | OND5     | .01 | 1  | FLOW<br>TIME | 12.<br>3.58  | 6.<br>3.58    | 6.<br>3.58  |
| 2 COMBINED AT + | CP-5     | .03 | 1  | FLOW<br>TIME | 40.<br>3.58  | 19.<br>3.58   | 18.<br>3.58 |
| HYDROGRAPH AT   | OND6     | .02 | 1  | FLOW<br>TIME | 23.<br>3.58  | 11.           | 11.<br>3.58 |
| HYDROGRAPH AT   | DVPIPE   | .00 | 1  | FLOW<br>TIME | 67.<br>3.75  | 39.<br>3.83   | 37.<br>3.83 |
| ROUYED TO       | RDVPIPE  | .00 | 1  | FLOW<br>TIME | 67.<br>3.83  | 38.<br>3.83   | 36.<br>3.83 |
| HYDROGRAPH AT   | DETPD    | .01 | 1  | FLOW<br>TIME | 16.<br>3.50  | 8.<br>3.50    | 8.<br>3.50  |
| 5 COMBINED AT   | CP-6     | .15 | 1  | FLOW<br>TIME | 254.<br>3.58 | 119.          | 112.        |
| ROUTED TO       | DETPOND  | .15 | 1  | FLOW<br>TIME | 45.<br>5.17  | 32.<br>5.00   | 31.<br>5.00 |
|                 |          |     | ** | STAGE        | GES IN FEET  | **<br>1730.08 | 1729.88     |
| HYDROGRAPH AT   | OFFD-14  | .00 | 1  | TIME         | 5.17         | 5.00          | 5.00        |
| ROUTED TO       |          |     |    | TIME         | 3.58         | 3.67          | 3.67        |
| +               | RT-B14   | .00 | 1  | FLOW<br>TIME | 3.67         | 3.67          | 3.67        |
| HYDROGRAPH AT   | BMIC-1   | .01 | 1  | FLOW<br>TIME | 26.<br>3.50  | 13.<br>3.50   | 12.<br>3.50 |
| 2 COMBINED AT   | C15      | .02 | 1  | FLOW<br>TIME | 28.<br>3.50  | 14.<br>3.50   | 13.<br>3.50 |
| ROUTED TO       | RT-14    | .02 | 1  | FLOW<br>TIME | 27.<br>3.50  | 13.<br>3.50   | 13.<br>3.50 |
| HYDROGRAPH AT   | BMIC-2   | .01 | 1  | FLOW<br>TIME | 22.<br>3.50  | 11.<br>3.50   | 11.<br>3.50 |
| 2 COMBINED AT + | C16      | .03 | 1  | FLOW<br>TIME | 50.<br>3.50  | 25.<br>3.50   | 24.<br>3.50 |
| ROUTED TO       | RT-15    | .03 | 1  | FLOW<br>TIME | 49.<br>3.50  | 24.<br>3.50   | 23.<br>3.50 |
| HYDROGRAPH AT   | SCH-2    | .01 | 1  | FLOW<br>TIME | 13.<br>3.50  | 7.<br>3.50    | 6.<br>3.50  |
| 2 COMBINED AT   | C17      | .04 | 1  | FLOW<br>TIME | 61.<br>3.50  | 31.<br>3.50   | 29.<br>3.50 |
| ROUTED TO       | RT-16    | .04 | 1  | FLOW<br>TIME | 59.<br>3.50  | 29.<br>3.50   | 27.<br>3.50 |
| HYDROGRAPH AT   | BMIC-3   | .01 | 1  | FLOW<br>TIME | 21.<br>3.50  | 11.<br>3.50   | 10.<br>3.50 |
| HYDROGRAPH AT   | MGDEV-2  | .01 | 1  | FLOW<br>TIME | 17.<br>3.50  | 9.<br>3.50    | 8.<br>3.50  |
| 4 COMBINED AT   | C18      | .20 | 1  | FLOW<br>TIME | 126.<br>3.50 | 68.<br>3.50   | 65.<br>3.50 |
| HYDROGRAPH AT   | HR3      | .00 | 1  | FLOW         | 3.           | 1.            | 1.          |

|                   |                        |               | TIME           |         | 3.50            | 3.50              | 3.50             |             |          |              |        |        |    |
|-------------------|------------------------|---------------|----------------|---------|-----------------|-------------------|------------------|-------------|----------|--------------|--------|--------|----|
| HYDROGRAPH AT     | HR2                    | .00           | 1 FLOW<br>TIME |         | 4.<br>3.50      | 2.<br>3.50        | 2.<br>3.50       |             |          |              |        |        |    |
| HYDROGRAPH AT     | HR1                    | .00           | 1 FLOW<br>TIME |         | 3.<br>3.50      | 2.<br>3.50        | 2.<br>3.50       |             |          |              |        |        |    |
| 3 COMBINED AT     | CHR1                   | .00           | 1 FLOW         |         | 10.<br>3.50     | 5.<br>3.50        | 5.<br>3.50       |             |          |              |        |        |    |
| 2 COMBINED AT     | C18B                   | .21           | 1 FLOW         |         | 136.<br>3.50    | 74.<br>3.50       | 70.<br>3.50      |             |          |              |        |        |    |
| HYDROGRAPH AT     | OND15                  | .03           | 1 FLOW         |         | 57.             | 28.               | 27.              |             |          |              |        |        |    |
| HYDROGRAPH AT     | OFFD4                  | .01           | TIME<br>1 FLOW |         | 3.50<br>19.     | 9.                | 9.               |             |          |              |        |        |    |
| 1                 |                        |               | TIME           |         | 3.58<br>NEMATIC | 3.58<br>WAVE - MU | 3.58<br>SKINGUM- | -CUNGE ROUT | TING     |              |        |        |    |
| ISTAQ             | ELEMENT                | DT            |                |         | DIRECT R        | UNOFF WITH        | HOUT BAS         | SE FLOW)    | ATED TO  | VOLUME       |        |        |    |
| Total             | anname.                | (MIN)         |                | PEA     | K.              |                   |                  |             | PEAK     |              |        |        |    |
|                   | AN = 1 RATIO           | = 1.00        |                |         |                 |                   | (MIN)            | (CFS)       | (MIN)    | (IN)         |        |        |    |
|                   | - MANE                 | 1.36          |                |         |                 | 1.81              | 5.00             | 66.60       | 220.00   | 1.80         |        |        |    |
| CONTINUITY SUMMAR |                        |               | .4767E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .4776E         | 3+01 BASIN  | STORAGE= | .5556E-06 PI | ERCENT | ERROR= | 2  |
|                   | N = 1 RATIO            | = .60<br>1.75 | 33.06          | 218.    | 31              | .83               | 5.00             | 32.31       | 220.00   | .83          |        |        |    |
| CONTINUITY SUMMAR | RY (AC-FT) -           | INFLOW=       | .2194E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .2198E         | E+01 BASIN  | STORAGE= | .5369E-06 PI | ERCENT | ERROR= | 2  |
|                   | N = 1 RATIO            | = .58<br>1.71 | 31.11          | 219.    | 15              | .79               | 5.00             | 30.65       | 220.00   | .79          |        |        |    |
| CONTINUITY SUMMAR | RY (AC-FT) -           | INFL/OW=      | .2075E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .2079E         | E+01 BASIN  | STORAGE= | .5580E-06 PI | ERCENT | ERROR= | 2  |
|                   | N = 1 RATIO            | = 1.00        | 88.20          | 215.    | 76              | 1.82              | 5.00             | 86.53       | 215.00   | 1.82         |        |        |    |
| CONTINUITY SUMMAR | RY (AC-FT) -           | INFLOW=       | .6239E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .6240E         | +01 BASIN   | STORAGE= | .3111E-06 PE | ERCENT | ERROR= | .0 |
|                   | N = 1 RATIO            | = .60<br>.49  | 41.32          | 216.    | 17              | .84               | 5.00             | 41.28       | 220.00   | .84          |        |        |    |
| CONTINUITY SUMMAR |                        |               |                |         | .0000E+0        |                   |                  |             |          |              | ERCENT | ERROR= | .0 |
|                   | N = 1 RATIO            | = .58<br>.50  | 39.15          | 220.    | 28              | .80               | 5.00             | 39.15       | 220.00   | .80          |        |        |    |
| CONTINUITY SUMMAR | Y (AC-FT) - I          | INFLOW=       | .2735E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .2735E         | C+01 BASIN  | STORAGE= |              | ERCENT | ERROR= | .0 |
|                   | N = 1 RATIO            |               |                |         |                 |                   |                  |             |          |              |        |        |    |
|                   |                        |               | 25.01          |         |                 | 1.68              | 5.00             | 24.19       | 215.00   | 1.68         |        |        |    |
| CONTINUITY SUMMAR |                        |               | .1472E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .1478E         | 0+01 BASIN  | STORAGE= | .1971E-06 PH | ERCENT | ERROR= | 4  |
|                   | N = 1 RATIO:<br>2 MANE | 1.83          | 11.24          | 214.    | 86              | .74               | 5.00             | 11.22       | 215.00   | .74          |        |        |    |
| CONTINUITY SUMMAR | Y (AC-FT) - :          | INFLOW=       | .6495E+00      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .6514E         | +00 BASIN   | STORAGE= | .2695E-06 PE | ERCENT | ERROR= | 3  |
|                   | N = 1 RATIO:<br>2 MANE | = .58<br>1.82 | 10.72          | 214.    | 12              | .70               | 5.00             | 10.59       | 215.00   | .70          |        |        |    |
| CONTINUITY SUMMAR | Y (AC-FT) - :          | INFLOW=       | .6118E+00      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .6142E         | +00 BASIN   | STORAGE= | .1771E-06 PH | ERCENT | ERROR= | 4  |
|                   | N = 1 RATIO:<br>- MANE | = 1.00        | 119.25         | 215.    | 41              | 1.65              | 5.00             | 118.57      | 215.00   | 1.65         |        |        |    |
| CONTINUITY SUMMAR | Y (AC-FT) -            | INFLOW=       | .7768E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .7768E         | 0+01 BASIN  | STORAGE= | .8974E-07 PR | ERCENT | ERROR= | .0 |
|                   | N = 1 PATIO:<br>- MANE | 60<br>.29     | 53.80          | 215.    | 59              | .72               | 5.00             | 53.11       | 215.00   | .72          |        |        |    |
| CONTINUITY SUMMAR | Y (AC-FT) - :          | INFLOW=       | .3399E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .3399E         | 01 BASIN    | STORAGE= | .9188E-07 PE | ERCENT | ERROR= | .0 |
|                   | N = 1 RATIO:<br>- MANE | = .58<br>.34  | 50.63          | 215.    | 67              | .68               | 5.00             | 50.01       | 215.00   | .68          |        |        |    |
| CONTINUITY SUMMAR | Y (AC-FT) -            | INFLOW=       | .3201E+01      | EXCESS= | .0000E+0        | 0 OUTFLOW:        | = .3201E         | 0+01 BASIN  | STORAGE= | .8963E-07 PH | ERCENT | ERROR= | .0 |

FOR PLAN = 1 RATIO= 1.00

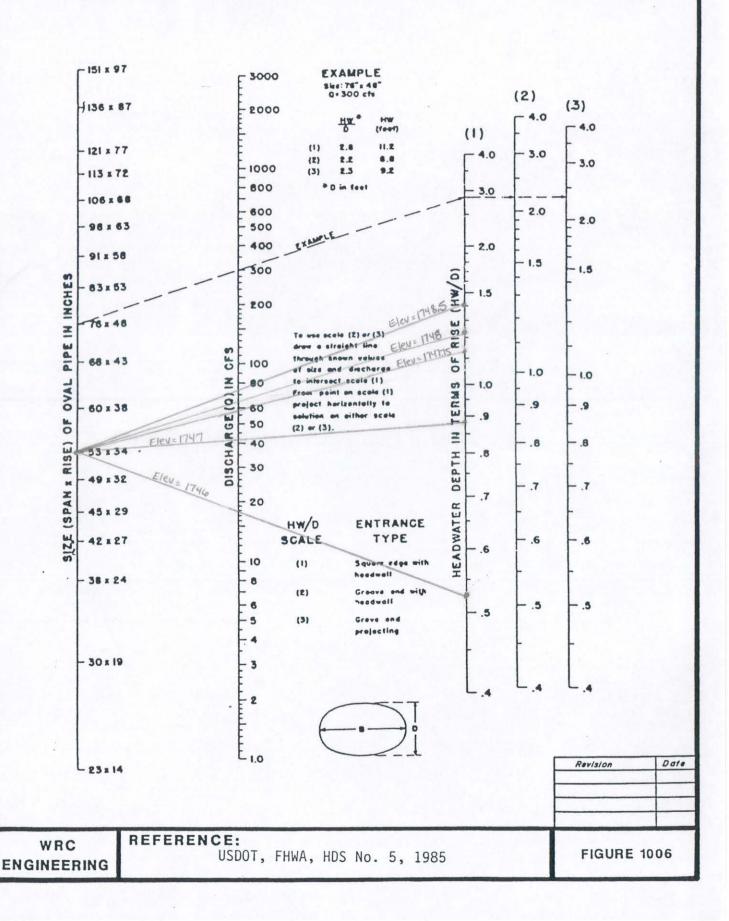
| CONTINU  | ITY SUMMARY  | (AC-PT) - IN   | FLOW=   | .7973E+01   | EXCESS=  | .0000E+00   | OUTFLOW=  | .7976E+  | 01 BASIN   | STORAGE=   | .3874E-06 PERCEN  | TT ERROR=  | .0 |
|--|--|--|---|---|--|---|---|--|--|--|---|--|----|
|  | FOR PLAN<br>RCP3-CP4   | = 1 RATIO=<br>MANE   | .60<br>.72  | 53.97   | 216  | .59   | .72   | 5.00   | 51.67  | 215.00   | .73   |  |    |
| CONTINU  | UTY SUMMARY  | (AC-FT) - IN   | FLOW=   | .3490E+01   | EXCESS=  | .0000E+00   | OUTFLOW=  | .3493E+  | 01 BASIN   | STORAGE=   | .4528E-06 PERCEN  | T ERROR=   | 1  |
|  | FOR PLAN<br>RCP3-CP4   | = 1 RATIO=<br>MANE   | .58<br>.79  | 50.57   | 216.   | .98   | .68   | 5.00   | 48.54  | 215.00   | .68   |  |    |
| CONTINU  | ITY SUMMARY  | (AC-FT) - IN   | FLOW=   | .3287E+01   | EXCESS=  | .0000E+00   | OUTFLOW=  | .3290E+  | 01 BASIN   | STORAGE=   | .4272E-06 PERCEN  | TT ERROR=  | 1  |
|  | FOR PLAN<br>RDVPIPE  | = 1 RATIO=<br>MANE   | 1.00  | 67.24   | 226  | .83 -1  | .00   | 5.00   | 66.79  | 230.00   | -1.00   |  |    |
|  | FOR PLAN<br>RDVPIPE  | = 1 RATIO=<br>MANE   | .60<br>1.18   | 38.60   | 232.   | .47 -1  | .00   | 5.00   | 38.25  | 230.00   | -1.00   |  |    |
|  | FOR PLAN<br>RDVPIPE  | = 1 RATIO=<br>MANE   | .58<br>1.15   | 36.67   | 232.   | .60 -1  | .00   | 5.00   | 36.35  | 230.00   | -1.00   |  |    |
|  | FOR PLAN<br>RT-B14   | = 1 RATIO=<br>MANE   | 1.00  | 3.39  | 218.   | .69 1   | . 64  | 5.00   | 3.37   | 220.00   | 1.63  |  |    |
| CONTINU  | ITY SUMMARY  | (AC-FT) - IN   | FLOW=   | .2438E+00   | EXCESS=  | 0000E+00  | OUTFLOW=  | .2442E+  | 00 BASIN   | STORAGE=   | .7570E-08 PERCEN  | T ERROR=   | 2  |
|  | FOR PLAN<br>RT-B14   | = 1 RATIO=<br>MANE   | .60<br>1.71   | 1.51  | 223.   | .43   | .71   | 5.00   | 1.50   | 220.00   | .71   |  |    |
| CONTINU  | ITY SUMMARY  | (AC-FT) - IN   | FLOW=   | .1061E+00   | EXCESS=  | .0000E+00   | OUTFLOW=  | .1063E+  | 00 BASIN   | STORAGE=   | .7638E-08 PERCEN  | TT ERROR=  | 2  |
|  | FOR PLAN<br>RT-B14   | = 1 RATIO=<br>MANE   | .58<br>1.76   | 1.42  | 222.   | .80   | .67   | 5.00   | 1.41   | 220.00   | .67   |  |    |
| CONTINU  | ITY SUMMARY  | (AC-FT) - IN   | FLOW=   | .9979E-01   | EXCESS=  | .0000E+00   | OUTFLOW=  | .9993E-  | 01 BASIN   | STORAGE=   | .5886E-08 PERCEN  | T ERROR=   | 1  |
|  | FOR PLAN<br>RT-14  | = 1 RATIO=<br>MANE   | 1.00  | 27.93   | 210.   | .77 1   | .91   | 5.00   | 27.32  | 210.00   | 1.91  |  |    |
|  |  |  |   |   |  |   |   |  |  |  |   |  |    |
| CONTINU  | ITY SUMMARY  | (AC-FT) - IN   | FLOW=   | .1720E+01   | EXCESS=  | .0000E+00   | OUTFLOW=  | .1721E+  | 01 BASIN   | STORAGE=   | .7751E-08 PERCEN  | T ERROR=   | .0 |
| CONTINU  |  | = 1 RATIO=   |   |   |  |   |   | .1721E+  | 01 BASIN<br>13.40  | STORAGE=   | .7751E-08 PERCEN  | T ERROR=   | .0 |
|  | FOR PLAN<br>RT-14  | = 1 RATIO=<br>MANE   | .60   | 13.81   | 211.   | 01  | .91   | 5.00   | 13.40  | 210.00   |   |  | .0 |
|  | FOR PLAN<br>RT-14<br>ITY SUMMARY   | = 1 RATIO=<br>MANE<br>(AC-FT) - IN:<br>= 1 RATIO=  | .60<br>.42<br>FLOW=   | 13.81<br>.8203E+00  | 211.<br>EXCESS=  | .0000E+00   | .91<br>OUTFLOW=   | 5.00   | 13.40  | 210.00   | .91   |  |    |
| CONTINU  | FOR PLAN<br>RT-14<br>ITY SUMMARY<br>FOR PLAN<br>RT-14  | = 1 RATIO=<br>MANE<br>(AC-FT) - IN<br>= 1 RATIO=<br>MANE   | .60<br>.42<br>FLOW=<br>.58<br>.41   | 13.81<br>.8203E+00  | 211.<br>EXCESS=  | .0000E+00   | .91<br>OUTFLOW=   | 5.00<br>.8205E+  | 13.40<br>00 BASIN<br>12.73   | 210.00<br>STORAGE=<br>210.00   | .91<br>.6549E-08 PERCEN   | T ERROR=   |    |
| CONTINU  | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-14  ITY SUMMARY FOR PLAN   | = 1 RATIO=<br>MANE<br>(AC-FT) - IN<br>= 1 RATIO=<br>MANE   | .60<br>.42<br>FLOW=<br>.58<br>.41   | 13.81<br>.8203E+00<br>13.17<br>.7778E+00  | 211.<br>EXCESS=<br>210.<br>EXCESS=   | .0000E+00   | .91 OUTFLOW= .86 OUTFLOW=   | 5.00<br>.8205E+  | 13.40<br>00 BASIN<br>12.73   | 210.00<br>STORAGE=<br>210.00   | .91<br>.6549E-08 PERCEN   | T ERROR=   | .0 |
| CONTINU  | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-15   | = 1 RATIO=<br>MANE<br>(AC-FT) - IN<br>= 1 RATIO=<br>MANE<br>(AC-FT) - IN<br>= 1 RATIO=<br>MANE   | .60<br>.42<br>FLOW=<br>.58<br>.41<br>FLOW=  | 13.81<br>.8203E+00<br>13.17<br>.7778E+00<br>49.16   | 211. EXCESS= 210.  | .0000E+00<br>.75<br>.0000E+00   | .91 OUTFLOW= .86 OUTFLOW=   | 5.00<br>.8205E+<br>5.00<br>.7780E+   | 13.40<br>00 BASIN<br>12.73<br>00 BASIN<br>48.56  | 210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00   | .91<br>.6549E-08 PERCEN<br>.86  | T ERROR=   | .0 |
| CONTINU  | FOR PLAN RT-14 ITY SUMMARY FOR PLAN RT-14 ITY SUMMARY FOR PLAN RT-15 ITY SUMMARY FOR PLAN  | = 1 RATIO=<br>MANE<br>(AC-FT) - IN<br>= 1 RATIO=<br>MANE<br>(AC-FT) - IN<br>= 1 RATIO=<br>MANE<br>(AC-FT) - IN   | .60<br>.42<br>FLOW=<br>.58<br>.41<br>FLOW=<br>1.00<br>.36<br>FLOW=                              | 13.81<br>.8203E+00<br>13.17<br>.7778E+00<br>49.16   | EXCESS=  210.  EXCESS=  210.  EXCESS=  | .0000E+00<br>.75<br>.0000E+00   | .91 OUTFLOW= .86 OUTFLOW=   | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00   | 13.40<br>00 BASIN<br>12.73<br>00 BASIN<br>48.56  | 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE=  | .91<br>.6549E-08 PERCEN<br>.86<br>.6560E-08 PERCEN  | T ERROR=   | .0 |
| CONTINUI   | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-15   | = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  | .60<br>.42<br>FLOW=<br>.58<br>.41<br>FLOW=<br>1.00<br>.36<br>FLOW=                              | 13.81<br>.8203E+00<br>13.17<br>.7778E+00<br>49.16<br>.2959E+01<br>24.51   | 211. EXCESS= 210. EXCESS= 210. EXCESS= 210.  | .0000E+00 .75 .0000E+00 .62 1 .0000E+00   | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW=  | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+  | 13.40<br>00 BASIN<br>12.73<br>00 BASIN<br>48.56<br>01 BASIN<br>24.04                                     | 210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00   | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN   | T ERROR=   | .0 |
| CONTINUI   | FOR PLAN RT-14 ITY SUMMARY FOR PLAN RT-14 ITY SUMMARY FOR PLAN RT-15 ITY SUMMARY FOR PLAN RT-15  | = 1 RATIO= MANE  (AC-FT) - IN   | .60<br>.42<br>FLOW=<br>.58<br>.41<br>FLOW=<br>1.00<br>.36<br>FLOW=<br>.60<br>.35                | 13.81 .8203E+00 13.17 .7778E+00 49.16 .2959E+01 24.51 .1419E+01   | 211. EXCESS= 210. EXCESS= 210. EXCESS= 210. EXCESS=                                      | .0000E+00 .75 .0000E+00 .62 1 .0000E+00   | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW=  | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00  | 13.40<br>00 BASIN<br>12.73<br>00 BASIN<br>48.56<br>01 BASIN<br>24.04                                     | 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE=  | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93   | T ERROR=   | .0 |
| CONTINUI CONTINUI CONTINUI                                 | FOR PLAN RT-14 ITY SUMMARY FOR PLAN RT-15 ITY SUMMARY FOR PLAN RT-15 ITY SUMMARY FOR PLAN RT-15 ITY SUMMARY  | = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  | .60 .42  FLOW= .58 .41  FLOW= .36  .60 .35  .60 .35   | 13.81 .8203E+00 13.17 .7778E+00 49.16 .2959E+01 24.51 .1419E+01 23.31   | 211. EXCESS= 210. EXCESS= 210. EXCESS= 210.  | .0000E+00 .75 .0000E+00 .62 1 .0000E+00 .82 .0000E+00                               | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .93                                    | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00<br>.1420E+                                       | 13.40 00 BASIN 12.73 00 BASIN 48.56 01 BASIN 24.04 01 BASIN 22.85  | 210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00                         | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93   | T ERROR= T ERROR= T ERROR=                       | .0 |
| CONTINUI CONTINUI CONTINUI                                 | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-15   | = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  | .60 .42 .58 .41 .58 .41 .50 .36 .60 .35 .51 .40   | 13.81 .8203E+00 13.17 .7778E+00 49.16 .2959E+01 24.51 .1419E+01 23.31   | 211. EXCESS= 210. EXCESS= 210. EXCESS= 210. EXCESS= 210.                                 | .0000E+00 .75 .0000E+00 .62 1 .0000E+00 .82 .0000E+00                               | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .88 OUTFLOW=                           | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00<br>.1420E+                                       | 13.40 00 BASIN 12.73 00 BASIN 48.56 01 BASIN 24.04 01 BASIN 22.85  | 210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00<br>STORAGE=<br>210.00                         | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93 .8611E-08 PERCEN  | T ERROR= T ERROR= T ERROR=                       | .0 |
| CONTINUI   | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-15   | = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE   | .60 .42 .58 .41 .60 .36 .60 .35 .41 .60 .36 .35 .35 .35 .35                                     | 13.81<br>.8203E+00<br>13.17<br>.7778E+00<br>49.16<br>.2959E+01<br>24.51<br>.1419E+01<br>23.31<br>.1347E+01<br>60.94 | 211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.                         | .0000E+00 .75 .0000E+00 .62 1 .0000E+00 .82 .0000E+00 .84 .0000E+00                 | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .93 OUTFLOW= .88 OUTFLOW=              | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00<br>.1420E+<br>5.00                               | 13.40 00 BASIN 12.73 00 BASIN 48.56 01 BASIN 24.04 01 BASIN 22.85 01 BASIN                               | 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE=  | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93 .8611E-08 PERCEN  | T ERROR= TT ERROR= TT ERROR=                     | .0 |
| CONTINUI   | FOR PLAN RT-14  ITY SUMMARY  FOR PLAN RT-15  ITY SUMMARY  FOR PLAN RT-15  ITY SUMMARY  FOR PLAN RT-15  ITY SUMMARY  FOR PLAN RT-16  ITY SUMMARY  FOR PLAN RT-16                        | = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-PT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE  | .60 .42 .60 .42 .60 .60 .60 .60 .60 .60 .60 .60 .60 .60   | 13.81 .8203E+00 13.17 .7778E+00 49.16 .2959E+01 24.51 .1419E+01 23.31 .1347E+01 60.94                               | 211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.  EXCESS=                | .0000E+00 .75 .0000E+00 .62 1 .0000E+00 .82 .0000E+00 .84 .0000E+00                 | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .88 OUTFLOW= .94 OUTFLOW=              | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00<br>.1420E+<br>5.00<br>.1347E+                    | 13.40 00 BASIN 12.73 00 BASIN 48.56 01 BASIN 24.04 01 BASIN 22.85 01 BASIN                               | 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE=                        | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93 .8611E-08 PERCEN .88 .8421E-08 PERCEN                           | T ERROR= TT ERROR= TT ERROR=                     | .0 |
| CONTINUI  CONTINUI  CONTINUI  CONTINUI  CONTINUI           | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-16  ITY SUMMARY FOR PLAN RT-16                             | = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE   | .60 .42 .60 .42 .60 .65 .60 .65   | 13.81 .8203E+00 13.17 .7778E+00 49.16 .2959E+01 24.51 .1419E+01 23.31 .1347E+01 60.94 .3645E+01 30.36               | 211. EXCESS= 210. EXCESS= 210. EXCESS= 210. EXCESS= 211. EXCESS= 211.                    | .0000E+00 .75 .0000E+00 .62 1 .0000E+00 .82 .0000E+00 .84 .0000E+00 .36             | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .93 OUTFLOW= .94 OUTFLOW= .93          | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00<br>.1420E+<br>5.00<br>.3647E+                    | 13.40 00 BASIN 12.73 00 BASIN 48.56 01 BASIN 24.04 01 BASIN 22.85 01 BASIN 58.94 01 BASIN                | 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00 STORAGE= 210.00                 | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93 .8611E-08 PERCEN .88 .8421E-08 PERCEN                           | T ERROR= TT ERROR= TT ERROR= TT ERROR= TT ERROR= | .0 |
| CONTINUI  CONTINUI  CONTINUI  CONTINUI  CONTINUI           | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-16  ITY SUMMARY FOR PLAN RT-16  ITY SUMMARY FOR PLAN RT-16 | = 1 RATIO= MANE  = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE               | .60 .42 .58 .41 .60 .35 .58 .41 .60 .35 .58 .35 .58 .58 .58 .58 .58 .58 .58 .58 .58 .5          | 13.81 .8203E+00 13.17 .7778E+00 49.16 .2959E+01 24.51 .1419E+01 23.31 .1347E+01 60.94 .3645E+01 30.36               | 211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.  EXCESS=  211.  EXCESS= | .0000E+00 .75 .0000E+00 .62 1 .0000E+00 .82 .0000E+00 .13 1 .0000E+00 .36           | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .94 OUTFLOW= .93 OUTFLOW=              | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00<br>.1420E+<br>5.00<br>.3647E+<br>5.00            | 13.40 00 BASIN 12.73 00 BASIN 48.56 01 BASIN 24.04 01 BASIN 22.85 01 BASIN 58.94 01 BASIN 28.90 01 BASIN | 210.00 STORAGE=        | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93 .8611E-08 PERCEN .88 .8421E-08 PERCEN 1.95 .3120E-07 PERCEN .93 | T ERROR= TT ERROR= TT ERROR= TT ERROR= TT ERROR= | .0 |
| CONTINUI  CONTINUI  CONTINUI  CONTINUI  CONTINUI  CONTINUI | FOR PLAN RT-14  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-15  ITY SUMMARY FOR PLAN RT-16  ITY SUMMARY FOR PLAN RT-16  ITY SUMMARY FOR PLAN RT-16 | = 1 RATIO= MANE  (AC-FT) - IN  = 1 RATIO= MANE | .60 .42 FLOW= .58 .41 FLOW= .50 .36 FLOW= .50 .35 FLOW= .50 .60 .65 FLOW= .60 .65 FLOW= .60 .65 | 13.81 .8203E+00 13.17 .7778E+00 49.16 .2959E+01 24.51 .1419E+01 23.31 .1347E+01 30.36 .1751E+01 28.82               | 211.  EXCESS=  210.  EXCESS=  210.  EXCESS=  210.  EXCESS=  211.  EXCESS=  211.          | .0000E+00 .75 .0000E+00 .62 1 .0000E+00 .82 .0000E+00 .13 1 .0000E+00 .36 .0000E+00 | .91 OUTFLOW= .86 OUTFLOW= .93 OUTFLOW= .93 OUTFLOW= .94 OUTFLOW= .93 OUTFLOW= | 5.00<br>.8205E+<br>5.00<br>.7780E+<br>5.00<br>.2959E+<br>5.00<br>.1420E+<br>5.00<br>.3647E+<br>5.00<br>.1752E+ | 13.40 00 BASIN 12.73 00 BASIN 48.56 01 BASIN 24.04 01 BASIN 22.85 01 BASIN 58.94 01 BASIN 28.90 01 BASIN | 210.00 STORAGE= 210.00 | .91 .6549E-08 PERCEN .86 .6560E-08 PERCEN 1.94 .9128E-08 PERCEN .93 .8611E-08 PERCEN .88 .8421E-08 PERCEN 1.95 .3120E-07 PERCEN .93 | T ERROR= TT ERROR= TT ERROR= TT ERROR= TT ERROR= | .0 |

.56 120.24 215.94 1.65 5.00 117.64 215.00 1.66

RCP3-CP4 MANE

\*\*\* NORMAL END OF HEC-1 \*\*\*

# NOMOGRAPH - INLET CONTROL ELLIPTICAL PIPE



#### **Equalizer Basin**

| ELEVATION | AREA (ft2) | AREA (ac-ft) | 42" ELLIPTICAL PIPE FLOW (cfs) | SPILLWAY OVERFLOW (cfs) | TOTAL DISCHARGE(cfs) |
|-----------|------------|--------------|--------------------------------|-------------------------|----------------------|
| 1744.50   | 0          | 0.00         | 0                              | 0                       | 0                    |
| 1745.00   | 3480       | 0.08         | 0                              | 0                       | 0                    |
| 1746.00   | 30510      | 0.70         | 18                             | 0                       | 18                   |
| 1747.00   | 34005      | 0.78         | 42                             | 0                       | 42                   |
| 1747.75   | 36890      | 0.85         | 59                             | 0                       | 59                   |
| 1748.00   | 37850      | 0.87         | 64                             | 10                      | 74                   |
| 1748.50   | 42210      | 0.97         | 73                             | 53                      | 126                  |

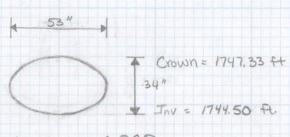
NOTE: 1) Areas were determined by using AutoCAD

<sup>2)</sup> The flow through the 42" elliptical pipe was calculated using the nomograph. See attached nomograph.
3) The flow overtopping the equalizer basin was calculated using the weir equation. See attached calculations.



Subject: 42" Elliptical RCP at Equalizer Basin
Sample Calculations

| COMP. BY:   |  |
|-------------|--|
| CHK.BY:     |  |
| DATE:       |  |
| SHEET NO .: |  |
| JOB NO ·    |  |



42" Elliptical RCP

Sample Calculation @ Elevation 1748.50

HW = 1748.5 - 1744.5 = 4 + 4 $D = \left(\frac{34''}{12}\right) = 2.83 + 4$ 

 $\frac{HW}{D} = \frac{4.0 \text{ ft}}{2.83 \text{ ft}} = 1.41$ 

Plot 1.41 on nomograph to get flow through elliptical pipe. .. Flow through elliptical pipe at elevation 1748.50 is 73 cfs

Wier Equation

Q = CLH3/2

Q= 2.7 (30F)(1748.50 - 1747.75)3/2 - 53 cfs

Total flow leaving equalizer basin at elevation 1748.50: Quotal = 73 cfs + 53 cfs = 126 cfs

### **Detention Basin**

| ELEVATION | HEIGHT (ft) | AREA (ft2) | VOLUME (ft3) | VOLUME (acre-ft) | CUMMULATIVE VOLUME (acre/ft) | OUTFLOW (ft3/s) |
|-----------|-------------|------------|--------------|------------------|------------------------------|-----------------|
| 1725.25   | 0.0         | 0          | 0            | 0.00             | 0.00                         | 0               |
| 1726.00   | 0.75        | 9360       | 3510         | 0.08             | 0.08                         | 0               |
| 1728.00   | 2.0         | 53790      | 63150        | 1.45             | 1.53                         | 22              |
| 1729.00   | 1.0         | 76290      | 65040        | 1.49             | 3.02                         | 27              |
| 1730.00   | 1.0         | 82060      | 79175        | 1.82             | 4.84                         | 32              |
| 1732.00   | 2.0         | 93665      | 175725       | 4.03             | 8.88                         | 40              |
| 1734.00   | 2.0         | 105690     | 199355       | 4.58             | 13.45                        | 46              |
| 1735.00   | 1.0         | 112360     | 109025       | 2.50             | 15.95                        | 49              |

Note: 1) Areas were determined by using AutoCAD

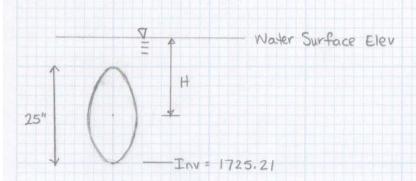
<sup>2)</sup> The outflow was calculated by using the orifice equation. See attached calculations.



Subject: Detention Basin Outlet

COMP. BY: \_\_\_\_\_\_
CHK.BY: \_\_\_\_\_
DATE: \_\_\_\_
SHEET NO.: \_\_\_\_\_
JOB NO.: \_\_\_\_

Q = 0.61 A J2g H



Center Elev of 25" orifice =  $1725.21 + \frac{25"}{12} = 1726.25$ 

Sample Calculation for Orifice Outlet

Water Surface Elev = 1728  $Q = 0.61 (\pi)(1.042 \, H)^2 \sqrt{2}(32.2)(1728 - 1726.25) = 22.08 \, cfs$ 

## **Worksheet for OND8 channel**

### **Project Description**

Friction Method Manning Formula Solve For Normal Depth

#### Input Data

 $\begin{array}{ccc} \text{Channel Slope} & 0.40000 & \% \\ \text{Discharge} & 33.00 & \text{ft}^3\text{/s} \end{array}$ 

Section Definitions

| anenkaliikeelekkii ee |      | u<br>Soller hours (State Work St.) | agreements.   |  |
|-----------------------|------|------------------------------------|---------------|--|
| Station (ft)          |      | Elevation (ft)                     | 9<br>(8 ) (5) |  |
|                       | 0+00 |                                    | 3.00          |  |
|                       | 0+09 |                                    | 0.00          |  |
|                       | 0+19 |                                    | 0.00          |  |
|                       | 0+25 |                                    | 1.52          |  |
|                       | 0+36 |                                    | 1.65          |  |
|                       | 0+46 |                                    | 3.00          |  |
|                       |      |                                    | li .          |  |

Roughness Segment Definitions

| Start Sta        | tion            | ding Station |           | Roughness Coeffi                                     | cient |
|------------------|-----------------|--------------|-----------|--|-------|
|                  | (0+00, 3.00)    | (0+          | 46, 3.00) |  | 0.025 |
| Results          |                 |              |           | n allines acentar photosoci<br>Rankon manana alla sa |       |
| Normal Depth     |                 | 0.87         | ft        |  |       |
| Elevation Range  | 0.00 to 3.00 ft |              |           |  |       |
| Flow Area        |                 | 11.20        | ft²       |  |       |
| Wetted Perimeter |                 | 16.12        | ft        |  |       |
| Top Width        |                 | 15.87        | ft        |  |       |
| Normal Depth     |                 | 0.87         | ft        |  |       |
| Critical Depth   |                 | 0.65         | ft        |  |       |
| Critical Slope   |                 | 0.01133      | ft/ft     |  |       |
| Velocity         |                 | 2.95         | ft/s      |  |       |
| Velocity Head    |                 | 0.14         | ft        |  |       |
| Specific Energy  |                 | 1.00         | ft        |  |       |
| Froude Number    |                 | 0.62         |           |  |       |

|                     | Worksheet f | or OND8  | channel     |   |
|---------------------|-------------|----------|-------------|---|
| Results             |             |          | A ALEXANDER | <del>-</del> -                                |
| Flow Type           | Subcritical |          |             |   |
| GVF Input Data      |             |          |             | eta an en |
| Downstream Depth    |             | 0.00     | ft          |   |
| Length              |             | 0.00     | ft          |   |
| Number Of Steps     |             | 0        |             |   |
| GVF Output Data     |             |          |             |   |
| Upstream Depth      |             | 0.00     | ft          |   |
| Profile Description |             |          |             |   |
| Profile Headloss    |             | 0.00     | ft          |   |
| Downstream Velocity |             | Infinity | ft/s        |   |
| Upstream Velocity   |             | Infinity | ft/s        |   |
| Normal Depth        |             | 0.87     | ft          |   |
| Critical Depth      |             | 0.65     | ft          |   |
| Channel Slope       |             | 0.00400  | ft/ft       |   |
| Critical Slope      |             | 0.01133  | ft/ft       |   |

### **Cross Section for OND8 channel**

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

#### Input Data

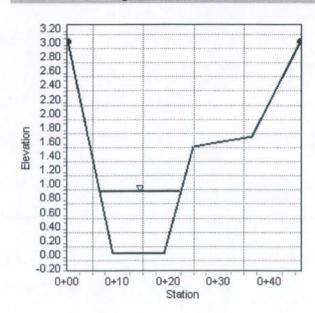
Channel Slope Normal Depth

Discharge

0.40000 % 0.87 ft

33.00 ft<sup>3</sup>/s

#### Cross Section Image



tenannel = 
$$\frac{\text{channel path length}}{\text{velocity}} = \frac{2382 \text{ ft}}{2.95 \text{ ft/s}} = \frac{807.5 \text{ sec}}{100 \text{ sec}} = \frac{13.5 \text{ min}}{100 \text{ sec}}$$

toverland = calculated from Standard form 4 = 1,9 min

# **LEGEND**

ONSITE BASIN BOUNDARY

OFFSITE BASIN BOUNDARY

REFERENCED BASIN BOUNDARY

OFFSITE BASIN LABEL

HEC-1 COMBINATION POINT

ND1 ONSITE BASIN LABEL

REFERENCED BASIN LABEL

DISCHARGE POINT

FLOW DIRECTION

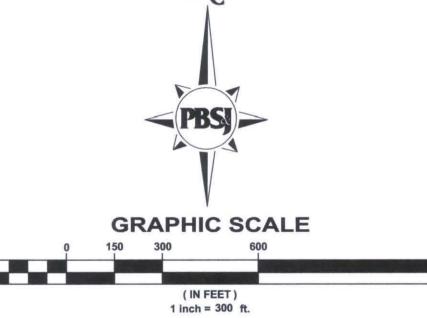
REFERENCED BASIN BOUNDARY

EXISTING LANDFILL BOUNDARY

# NOTES

"ADDENDUM #1 TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMERCE CENTER TWO (FORMERLY KNOWN AS HARSCH)" PREPARED BY PBS&J (FEBRUARY 2003) WAS USED FOR REFERENCED BASINS

| BASIN ID | AREA (ac) | Q <sub>100</sub> (cfs) | Q <sub>10</sub> (cfs) |  |
|----------|-----------|------------------------|-----------------------|--|
| OND1     | 0.94      | 3                      | 1                     |  |
| OND2     | 3.70      | 8                      | 4                     |  |
| OND3     | 1.38      | 4                      | 2                     |  |
| OND4     | 11.67     | 27                     | 13                    |  |
| OND5     | 5.03      | 12                     | 6                     |  |
| OND6     | 9.90      | 23                     | 11                    |  |
| OND7     | 5.87      | 16                     | 8                     |  |
| OND8     | 14.26     | 33                     | 16                    |  |
| OND9     | 1.06      | 3                      | 2                     |  |
| OND10    | 4.28      | 10                     | 5                     |  |
| OND11    | 9.60      | 24                     | 12                    |  |
| OND12    | 2.77      | 8                      | 4                     |  |
| OND13    | 4.70      | 12                     | 6                     |  |
| OND14    | 11.12     | 31                     | 15                    |  |
| OND15    | 21.47     | 57                     | 28                    |  |
| DETPD    | 5.14      | 16                     | 8                     |  |
| OFFD1    | 42.20     | 87                     | 39                    |  |
| OFFD2    | 9.63      | 23                     | 10                    |  |
| OFFD3    | 16.40     | 35                     | 16                    |  |
| OFFD4    | 7.61      | 19                     | 9                     |  |
| OFFD5    | 5.11      | 13                     | 6                     |  |
| CP-1     | NA        | 25                     | 11                    |  |
| CP-2     | NA        | 120                    | 54                    |  |
| CP-3     | NA        | 121                    | 54                    |  |
| CP-4     | NA        | 131                    | 59                    |  |
| CP-5     | NA        | 40                     | 19                    |  |
| CP-6     | NA        | 254                    | 119                   |  |
| CP-7     | NA        | 37                     | 17                    |  |
| CP-8     | NA        | 70                     | 33                    |  |
| CP-9     | NA        | 89                     | 41                    |  |
| CP-10    | NA        | 127                    | 60                    |  |
| CP-10A   | NA        | 92                     | 43                    |  |
| CP-11    | NA        | 39                     | 15                    |  |
| C18      | NA        | 126                    | 68                    |  |
| C18B     | NA        | 136                    | 74                    |  |



511963.19

OCTOBER 2006

FIGURE 6 DEVELOPED CONDITION DRAINAGE MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



2270 Corporate Circle Suite 100 Henderson, Nevada 89074-6382 Telephone: 702/263-7275 Fax: 702/263-7200

ENGINEERING PLANNING. SURVEYING CONSTRUCTION SERVICES



#### LEGEND

PROPERTY BOUNDARY
SOIL BOUNDARY

510

SOIL MAP SYMBOL



## **GRAPHIC SCALE**



i mon – i

SEPTEMBER 2006

FIGURE B-4 SOIL MAP

TECHNICAL DRAINAGE STUDY FOR EASTSIDE LANDFILL



2270 Corporate Circle Sulte 100 Henderson, Nevada 89074-6382 Telephone: 702/263-7275 Fax: 702/263-7200

ENGINEERING PLANNING SURVEYING CONSTRUCTION SERVICES

## **Curve Number Calculations**

Insert

Delete

| Eviction | Candition | Hydrology |
|----------|-----------|-----------|
|          |           |           |

| Basin Name | Soil Type | Hydrologic Group      | Land Use   | Curve No. | % of Composition |      |       |       | Composite<br>Curve No. |
|------------|-----------|-----------------------|--|-----------|------------------|------|-------|-------|------------------------|
| ONEX1      | 187       | 0 %A 100 %B 0 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 77.00     | 46%              | 46%  | 35.42 | 35.42 | **:                    |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 44%              | 90%  | 37.40 | 72.82 |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                   | 91.00     | 10%              | 100% | 9.10  | 81.92 | 81.9                   |
| ONEX2      | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 72%              | 72%  | 61.20 | 61.20 | -                      |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                   | 91.00     | 28%              | 100% | 25.48 | 86.68 | 86.7                   |
| ONEX3      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                   | 91.00     | 100%             | 100% | 91.00 | 91.00 | 91.0                   |
| ONEX4      | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 61%              | 61%  | 51.85 | 51.85 |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                   | 91.00     | 39%              | 100% | 35.49 | 87.34 | 87.3                   |
| ONEX5      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                   | 91.00     | 100%             | 100% | 91.00 | 91.00 | 91.0                   |
| OFFEX1     | 187       | 0 %A 100 %B 0 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 77.00     | 92%              | 92%  | 70.84 | 70.84 | _                      |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 8%               | 100% | 6.80  | 77.64 | 77.6                   |
| OFFEX2     | 187       | 0 %A 100 %B 0 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 77.00     | 81%              | 81%  | 62.37 | 62.37 |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 19%              | 100% | 16.15 | 78.52 | 78.5                   |
| OFFEX3     | 187       | 0 %A 100 %B 0 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 77.00     | 37%              | 37%  | 28.49 | 28.49 |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 63%              | 100% | 53.55 | 82.04 | 82.0                   |
| OFFEX4     | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 100%             | 100% | 85.00 | 85.00 | 85.0                   |
| OFFEX5     | 615       | 0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping | 85.00     | 100%             | 100% | 85.00 | 85.00 | 85.0                   |

### **Curve Number Calculations**

Insert

Delete

Interim Condition Hydrology

| Basin Name | Soil Type | Hydrologic Group                               | Land Use   | Curve No.      | % of Composition | Curve No.    |  |
|------------|-----------|--|--|----------------|------------------|--------------|--|
| OND1 187   |           | 0 %A 100 %B 0 %C 0 %D                          | Industrial (72% imp)   | 88.00          | 85%              | **           |  |
|            | 187       | 0 %A 100 %B 0 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 86.00 15%      |                  | 87.7         |  |
| OND2       | 187       | 0 %A 100 %B 0 %C 0 %D                          | Industrial (72% Imp)   | 88.00          | 87%              | -            |  |
|            | 187       | 0 %A 100 %B 0 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 86.00          | 13%              | 87.7         |  |
| OND3       | 187       | 0 %A 100 %B 0 %C 0 %D                          | Industrial (72% Imp)   | 88.00          | 94%              |              |  |
|            | 187       | 0 %A 100 %B 0 %C 0 %D                          | Impervious Area- Paved Parking Lots, Roofs, Driveways etc.   | 98.00          | 6%               | 88.6         |  |
| OND4       | 187       | 0 %A 100 %B 0 %C 0 %D                          | Industrial (72% Imp)   | 88.00          | 42%              |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 58%              | 89.7         |  |
| OND5       | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 100%             | 91.0         |  |
| OND6       | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 92%              |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 91.00          | 8%               | 91.0         |  |
| OND7       | 187       | 0 %A 100 %B 0 %C 0 %D                          | Industrial (72% Imp)   | 88.00          | 19%              | -            |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 76%              | -            |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Impervious Area- Paved Parking Lots, Roofs, Driveways etc.   | 98.00          | 6%               | 90.8         |  |
| OND8       | 187       | 0 %A 100 %B 0 %C 0 %D                          | Industrial (72% Imp)   | 88.00          | 21%              |              |  |
|            | 187       | 0 %A 100 %B 0 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 86.00          | 1%               |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 75%              |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 91.00          | 3%               | 90.3         |  |
| OND9       | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 100%             | 91.0         |  |
| OND10      | 615       |  |  | 95%            | **               |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 91.00          |                  |              |  |
| OND11      | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          |                  |              |  |
| OND12      | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 95%              | 91.0         |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Impervious Area- Paved Parking Lots, Roofs, Driveways etc.   | 98.00          | 5%               | 91.4         |  |
| OND13      | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 96%              |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 91.00          | 4%               | 91.0         |  |
| OND14      | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 100%             | 91.0         |  |
| OND15      | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 97%              | _            |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 91.00          | 3%               | 91.0         |  |
| DETPD      | 615       | 0 %A 0 %B 100 %C 0 %D                          | Industrial (72% Imp)   | 91.00          | 31%              |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Impervious Area- Paved Parking Lots, Roofs, Driveways etc.   | 98.00          | 5%               |              |  |
|            | 615       | 0 %A 0 %B 100 %C 0 %D                          | Newly Graded Areas (Pervious Areas Only, No Vegetation)  | 91.00          | 64%              | 91.4         |  |
| OFFEX1     | 187       | 0 %A 100 %B 0 %C 0 %D                          | Western Desert Urban Area - Natural Desert Landscaping   | 77.00          | 92%              |              |  |
| OFFERT     | 615       | 0 %A 0 %B 100 %C 0 %D                          | Western Desert Urban Area - Natural Desert Landscaping  Western Desert Urban Area - Natural Desert Landscaping | 85.00          | 8%               |              |  |
| OFFEX2     | 187       |  |  |                |                  | 77.6         |  |
| OFFERZ     | 615       | 0 %A 100 %B 0 %C 0 %D<br>0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping   | 77.00<br>85.00 |                  | 81%          |  |
| OFFEYA     |           |  | Western Desert Urban Area - Natural Desert Landscaping   |                | 19%              | 78.5         |  |
| OFFEX3     | 187       | 0 %A 100 %B 0 %C 0 %D                          | Western Desert Urban Area - Natural Desert Landscaping   | 77.00          | 37%              |              |  |
| OFFEY!     | 615       | 0 %A 0 %B 100 %C 0 %D                          | Western Desert Urban Area - Natural Desert Landscaping   | 85.00          | 63%              | 82.0         |  |
| OFFEX5     | 615       | 0 %A 0 %B 100 %C 0 %D<br>0 %A 0 %B 100 %C 0 %D | Western Desert Urban Area - Natural Desert Landscaping  Western Desert Urban Area - Natural Desert Landscaping | 85.00<br>85.00 | 100%             | 85.0<br>85.0 |  |

### **Curve Number Calculations**

Insert

Delete

Developed Condition Hydrology

| Basin Name | Soil Type | Hydrologic Group      | Land Use   | Curve No. | % of Composition | Composite<br>Curve No. |
|------------|-----------|-----------------------|--|-----------|------------------|------------------------|
| OND1 187   |           | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 85%              | 2                      |
|            | 187       | 0 %A 100 %B 0 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 86.00     | 15%              | 87.7                   |
| OND2       | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 87%              |                        |
|            | 187       | 0 %A 100 %B 0 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 86.00     | 13%              | 87.7                   |
| OND3       | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 94%              | _                      |
|            | 187.      | 0 %A 100 %B 0 %C 0 %D | Impervious Area- Paved Parking Lots, Roofs, Driveways etc. | 98.00     | 6%               | 88.6                   |
| OND4       | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 42%              | 44                     |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 58%              | 89.7                   |
| OND5       | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 100%             | 91.0                   |
| OND6       | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 92%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 91.00     | 8%               | 91.0                   |
| OND7       | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 19%              | 77                     |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 76%              | 77.                    |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Impervious Area- Paved Parking Lots, Roots, Driveways etc. | 98.00     | 6%               | 90.8                   |
| OND8       | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 21%              |                        |
|            | 187       | 0 %A 100 %B 0 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 86.00     | 1%               |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 75%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 91.00     | 3%               | 90.3                   |
| OND9       | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     |                  |                        |
| OND10      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 95%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 91.00     | 5%               | 91.0                   |
| OND11      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 100%             | 91.0                   |
| OND12      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 95%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Impervious Area- Paved Parking Lots, Roofs, Driveways etc. | 98.00     | 5%               | 91.4                   |
| OND13      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 96%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 91.00     | 4%               | 91.0                   |
| OND14      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 100%             | 91.0                   |
| OND15      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 97%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 91.00     | 3%               | 91.0                   |
| DETPD      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 31%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Impervious Area- Paved Parking Lots, Roofs, Driveways etc. | 98.00     | 5%               |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Newly Graded Areas (Pervious Areas Only, No Vegetation)    | 91.00     | 64%              | 91.4                   |
| OFFD1      | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 92%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 8%               | 88.2                   |
| OFFD2      | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 81%              | +-:                    |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 19%              | 88.6                   |
| OFFD3      | 187       | 0 %A 100 %B 0 %C 0 %D | Industrial (72% Imp)                                       | 88.00     | 37%              |                        |
|            | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 63%              | 89.9                   |
| OFFD4      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 100%             | 91.0                   |
| OFFD5      | 615       | 0 %A 0 %B 100 %C 0 %D | Industrial (72% Imp)                                       | 91.00     | 100%             | 91.0                   |

#### Rainfall Methodology

#### A. Point Rainfall

According to Figure 513 of the Criteria Manual the site is located outside the McCarran Rainfall area. The 100-year, 6-hour rainfall depth duration frequency values for areas located outside the McCarran Airport Rainfall area were obtained from Figure 506 of the Criteria Manual. According to Figure 506, the rainfall depth for the 100-year 6-hour event is 1.95 inches. This value was adjusted according to Table 501 by 1.43, for a 100-year recurrence interval. The adjusted rainfall depth is 2.79 inches and was calculated as follows: (1.95)(1.43) = 2.79 inches. According to Figure 503, the rainfall depth for the 10-year 6-hour event is 1.35 inches. This value was adjusted according to Table 501 by 1.24, for a 10-year recurrence interval. The adjusted rainfall depth is 1.67 inches and is calculated as follows: (1.35)(1.24) = 1.67 inches.

The HEC-1 multi-ratio option (HEC 1990) was used to model the 10-year and 100-year design storms in the HEC-1 input file. The HEC-1 JR card was used to specify the ratio by which to multiply the 100-year precipitation values (point rainfall). The 10-year and 100-year ratios are 0.60 and 1.00, respectively (see calculation for 10-year ratio included in this appendix).

#### B. Storm Distribution

Table 503 in the Criteria Manual specifies that the 6-hour storm distribution, SDN 3 should be used for drainage areas less than eight square miles.

## **Runoff Methodology**

#### A. Lag Time

The Criteria Manual's Standard Form 4 was completed to determine the time of concentration for each drainage basin. For all basins which comprise less than 1 square mile, the time of concentration was calculated as follows:

$$T_c = T_i + T_t$$

Where: Tc = Time of Concentration

Ti = Initial, inlet or overland flow time Tt = Travel time in the ditch, gutter, etc.

The time of concentration is the sum of the initial flow time,  $T_i$  and the travel time,  $T_t$ . The minimum  $T_c$  recommended for non-urban watersheds is 10 minutes and 5 minute minimum for urban watersheds.

Initial flow time was calculated as follows:

$$Ti = 1.8(1.1 - K)Lo^{1/2}/S^{1/3}$$

Where: Ti = Initial overland flow time (in minutes)

K = 0.0132CN - 0.39CN = Curve Number

Lo = Length of overland flow (maximum 500 feet)

S = Average basin slope (in percent)

The lag time was calculated as follows:

 $T_{lag} = 0.6T_c$  (in hours)

Travel time is calculated as follows:

$$T_t = L_t/(60 \text{ V})$$

Where:

 $T_t$  = Travel time in the ditch, gutter, etc. (minutes)

 $L_t = Travel Length (feet)$ 

V = Average velocity of flow (ft/s)

Now,

 $V = CS^{1/2}$   $C = 1.49/nR^{2/3}$ 

R = A/P

Where:

V= Average Velocity (fps)

S = Average Slope (ft/ft0)

n = Manning's Roughness Coefficient

R = Hydraulic Radius (ft)

P = Wetted perimeter

A = Area of Flow (sq ft)

Two sets of coefficients were determined, one for developed conditions (Urbanized Areas) and the other for undeveloped (Non-Urbanized Areas) conditions. The following coefficients shall be used for developed areas (Urbanized Areas). For the first developed conditions velocity (V1), the appropriate coefficient (C = 20.2) represents street flow with n = 0.016 and a depth in the gutter of 0.3 feet. For the second developed conditions velocity (V2), the appropriate coefficient (C=30.6) represents curb height street flow. As may be noted, V2 is approximately equal to 1.5 times V1. Typically, drainage areas are delineated such that the channelized flow considered in the calculations of travel times is within streets and other minor water courses and does not include significant lengths of major improved floodway and channels in the travel distance for the time of concentration.

The second set of coefficients shall be used in existing areas (Non-Urbanized Areas). For the first undeveloped conditions velocity (V1), the appropriate coefficient C=14.8) represents wide channel flow with D=0.25 feet and n=0.04. For the second undeveloped conditions velocity (V2), the appropriate coefficient C=29.4) represents wide channel flow with D=0.7 feet and n=0.04. The time of concentration for the first design point in an urbanized basin using this procedure should not exceed the time of concentration calculated using below equation, which was developed using rainfall/runoff data collected in urbanized regions.

$$t_c = L / 180 + 10 (604)$$

Where t<sub>c</sub> = Time of Concentration at the First Design Point in an Urban Watershed (min)

L = Watershed Length (ft)

If the above equation results in a lesser time of concentration at the first design point and thus would govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream reaches. The minimum to recommended for urbanized areas is 5 minutes.

Subbasin OND8 time of concentration was adjusted because the velocities calculated by the above mentioned formulas did not accurately represent to channel velocity. A channel cross section for this basin is included in Appendix B-3. The velocity determined by using FlowMaster was 2.95ft/s. The Standard Form 4 channel velocity was calculated to be 1.9 ft/s. By using the velocity calculated by Flowmaster, the time of concentration reduced to 15 minutes. Please refer to Appendix B-3 for the calculations for the time of concentration.

#### B. Soils - Curve Number Determination

Soils information, for the onsite and offsite drainage basins, was obtained from the Soil Conservation Service (SCS) Soil Survey of Las Vegas Valley Area, Nevada, 1985. The project site and offsite basin is depicted on a SCS survey map and is included in this appendix, see **Figure B-4: Soil Map**. The soil types were matched to the corresponding SCS Curve Number (CN) for use in the Standard Form 4 and the HEC-1 analysis. The corresponding CN's for these soils are from Table 602 of the Criteria Manual. The onsite and offsite basins are composed of soil types #187 and #615 with a corresponding hydrologic group of B and C respectively.

In developed condition, the proposed landfill was classified as industrial because the landfill is planned to have a type II layer on the top. Since industrial has an imperviousness of 72%, this was assumed to be an appropriate curve number. The curve numbers for industrial are more conservative than curve numbers for gravel which would represent the type II material.

Imperviousness and newly graded curve numbers were also used to appropriately classify the designed drainage facilities around the landfill.

#### C. Routing

Routing in improved channels or storm drains were performed using the Kinematic method. Kinematic routing requires the following input parameters: roughness coefficient, base width, side slope, slope, and reach length. Kinematic routing was used for subbasins delineated by PBS&J within this TDS.

# PRECIPITATION ADJUSTMENT RATIOS

| Recurrence<br>Interval | Ratio to<br>NOAA Atlas 2 |
|------------------------|--------------------------|
| 2-year                 | 1.00                     |
| 5-year                 | 1.16                     |
| 10-year                | 1.24                     |
| 25-year                | 1.33                     |
| 50-year                | 1.39                     |
| 100-year               | 1.43                     |

NOTE: 1. Multiply the values obtained from the NOAA Atlas 2 by the above ratios to obtain the adjusted precipitation values.

- NOAA Atlas 2 values for use with TR-55 shall not be adjusted by the above ratios.
- 3. Tables 505 and 506 require no adjustments.

Revision Date

WRC ENGINEERING REFERENCE:

USACE, Los Angeles District, 1988

TABLE 501

# SIX-HOUR STORM DISTRIBUTIONS

| Percent of        |       |      |      |              | Percent of        |       |       |
|-------------------|-------|------|------|--------------|-------------------|-------|-------|
| Total Storm Depth |       |      |      |              | Total Storm Depth |       |       |
| Storm Time        | 00110 |      |      | Storm Time   |                   |       |       |
| (In Minutes)      | SDN3  | SDN4 | SDN5 | (In Minutes) | SDN3              | SDN4  | SDN5  |
| 0                 | 0.0   | 0.0  | 0.0  | 185          | 32.2              | 37.6  | 43.0  |
| 5                 | 2.0   | 2.0  | 2.0  | 190          | 35.2              | 41.5  | 47.7  |
| 10                | 5.7   | 5.8  | 5.9  | 195          | 40.9              | 46.2  | 51.4  |
| 15                | 7.0   | 7.5  | 8.0  | 200          | 49.9              | 53.0  | 56.1  |
| 20                | 8.7   | 9.9  | 11.0 | 205          | 59.0              | 61.0  | 63.0  |
| 25                | 10.8  | 12.6 | 14.4 | 210          | 71.0              | 71.0  | 71.0  |
| 30                | 12.4  | 13.7 | 15.0 | 215          | 74.4              | 73.2  | 72.0  |
| 35                | 13.0  | 14.5 | 16.0 | 220          | 78.1              | 75.6  | 73.1  |
| 40                | 13.0  | 14.9 | 16.8 | 225          | 81.2              | 78.2  | 75.2  |
| 45                | 13.0  | 15.1 | 17.1 | 230          | 81.9              | 79.9  | 77.9  |
| 50                | 13.0  | 15.5 | 18.0 | 235          | 83.5              | 81.3  | 79.0  |
| 55                | 13.0  | 15.6 | 18.2 | 240          | 85.1              | 82.3  | 79.5  |
| 60                | 13.0  | 15.9 | 18.7 | 245          | 85.6              | 83.0  | 80.4  |
| 65                | 13.3  | 16.2 | 19.0 | 250          | 86.0              | 83.5  | 81.0  |
| 70                | 14.0  | 16.9 | 19.7 | 255          | 86.8              | 84.4  | 82.0  |
| 75                | 14.2  | 17.2 | 20.2 | 260          | 87.6              | 85.1  | 82.6  |
| 80                | 14.8  | 17.9 | 21.0 | 265          | 88.8              | 86.4  | 84.0  |
| 85                | 15.8  | 18.9 | 22.0 | 270          | 91.0              | 88.5  | 85.9  |
| 90                | 17.2  | 20.1 | 23.0 | • 275        | 92.6              | 90.8  | 88.9  |
| 95                | 18.1  | 21.1 | 24.1 | 280          | 93.7              | 92.4  | 91.0  |
| 100               | 19.0  | 22.0 | 25.0 | 285          | 95.0              | 94.4  | 93.8  |
| 105               | 19.7  | 22.8 | 25.9 | 290          | 97.0              | 96.8  | 96.6  |
| 110               | 19.9  | 23.2 | 26.5 | 295          | 97.6              | 97.3  | 97.0  |
| 115               | 20.0  | 24.0 | 28.0 | 300          | 98.2              | 97.8  | 97.4  |
| 120               | 20.1  | 24.6 | 29.0 | 305          | 98.5              | 98.2  | 97.9  |
| 125               | 20.4  | 25.2 | 30.0 | 310          | 98.7              | 98.4  | 98.1  |
| 130               | 21.4  | 26.0 | 30.5 | 315          | 98.9              | 98.6  | 98.3  |
| 135               | 22.9  | 26.9 | 30.9 | 320          | 99.0              | 98.8  | 98.5  |
| 140               | 24.1  | 27.6 | 31.0 | 325          | 99.3              | 99.1  | 98.9  |
| 145               | 24.9  | 28.3 | 31.7 | 330          | 99.3              | 99.2  | 99.0  |
| 150               | 25.1  | 28.6 | 32.1 | 335          | 99.4              | 99.3  | 99.2  |
| 155               | 25.6  | 29.2 | 32.7 | 340          | 99.5              | 99.4  | 99.3  |
| 160               | 27.0  | 30.2 | 33.3 | 345          | 99.8              | 99.7  | 99.6  |
| 165               | 27.8  | 31.2 | 34.6 | 350          | 99.8              | 99.8  | 99.7  |
| 170               | 28.1  | 32.1 | 36.1 | 355          | 99.9              | 99.9  | 99.9  |
| 175               | 28.3  | 33.2 | 38.1 | 360          | 100.0             | 100.0 | 100.0 |
| 180               | 29.5  | 35.2 | 40.8 |              |                   |       |       |
|                   |       |      |      |              |                   |       |       |

Notes: 1. For drainage areas less than 8 square miles in size, use SDN 3.

For drainage areas greater than or equal to 8 square miles and less than 12 square miles in size, use SDN 4.

3. For drainage areas greater than or equal to 12 square miles, use SDN 5.

4. A graphical representation of these values is presented on Figure 515.

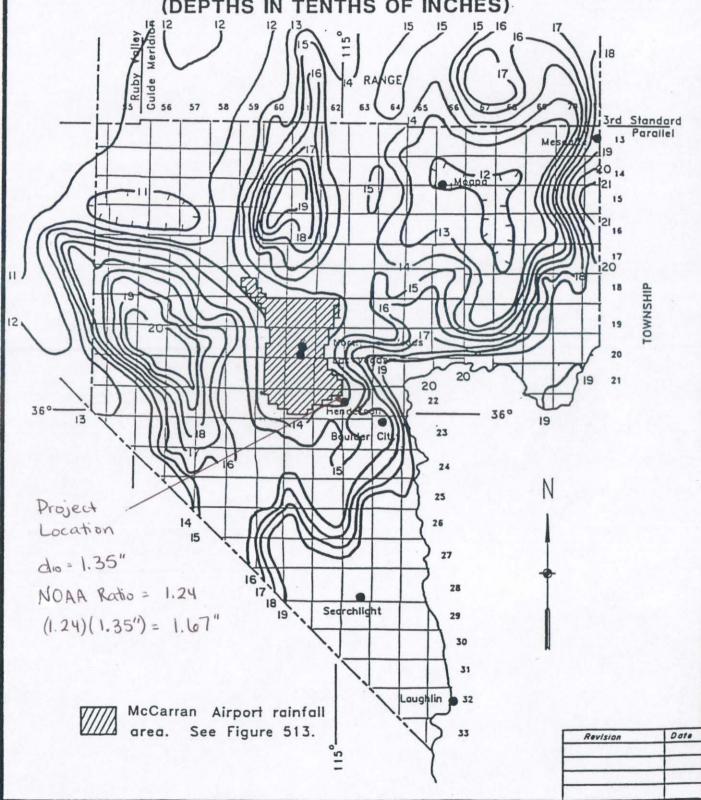
Revision Date

REFERENCE:

TABLE 503

# RAINFALL DEPTH-DURATION-FREQUENCY 10-YEAR, 6-HOUR

(DEPTHS IN TENTHS OF INCHES)



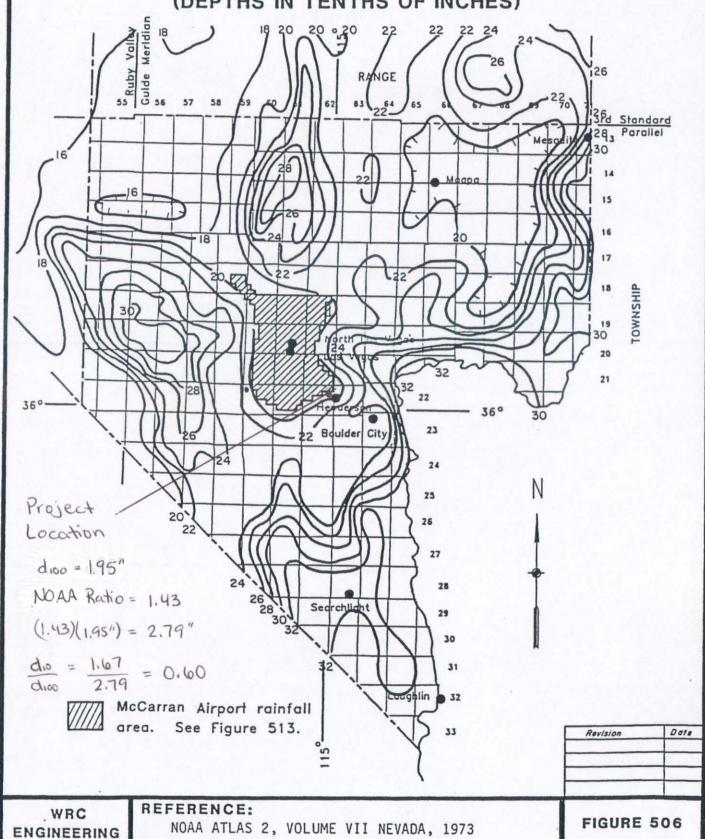
WRC ENGINEERING REFERENCE:

NOAA ATLAS 2, VOLUME VII NEVADA, 1973

FIGURE 503

# RAINFALL DEPTH-DURATION-FREQUENCY 100-YEAR, 6-HOUR

(DEPTHS IN TENTHS OF INCHES)



This unit is used mainly as habitat for desert wildlife and for recreation. It is also used for urban development.

This unit is well suited to the construction of dwellings.

Unless the density of housing is too high, septic tank absorption fields normally function well on this unit.

Roads can easily be constructed and maintained on

www unit.

The main limitations for lawns and landscaping are the subbles and pebbles throughout the soil. Topsoil is seeded for best results when landscaping, particularly in used for lawns. Lawn grasses, shrubs, and trees that are not sensitive to lime-induced chlorosis are well set to use in landscaping. Annual applications of iron the lates reduce the effects of chlorosis.

This map unit is in capability subclass VIIs, contrigated, and in horticultural group 2.

184—Caliza very gravelly sandy loam, 2 to 8
percent slopes. This very deep, well drained soil is on
prosional fan remnants. It formed in alluvium derived
tem various kinds of rock.

typically, the surface layer is light brown very gravelly loam about 3 inches thick. The upper 13 inches of underlying material is light brown very gravelly sandy and the lower part to a depth of 60 inches or more part brown, stratified very gravelly coarse sand to very loamy sand.

included in this unit is about 5 percent Aztec soils on account fan remnants. The percentage varies from one

was to another.

Permeability of the Caliza soil is moderately rapid.

Assable water capacity is very low. Effective rooting

per is 60 inches or more. Runoff is medium, and the

stand of water erosion is slight. The hazard of soil

stand is moderate. This soil is subject to rare periods

the boding during prolonged, high-intensity storms.

The boding and deposition are common along

sembanks.

the unit is used mainly as habitat for desert wildlife of for recreation. It is also used for urban development. The main limitation for construction of dwellings is the used of flooding.

the used to protect onsite sewage disposal systems

m flooding.

Channeling and deposition can be minimized and laborance costs reduced by protecting roads from

STATE OF THE PERSON NAMED IN

The main limitation for lawns and landscaping is the main of pebbles in the soil. Topsoil is needed for best when landscaping, particularly in areas used for Lawn grasses, shrubs, and trees that are not lime-induced chlorosis are well suited to use the effects of chlorosis.

map unit is in capability subclasses IVs, irrigated, with nonirrigated. It is in horticultural group 2.

187—Caliza extremely cobbly fine sandy loam, 2 to 8 percent slopes. This very deep, well drained soil is on inset fan remnants. It formed in alluvium derived from various kinds of rock.

Typically, about 85 percent of the surface is covered with a desert pavement of cobbles, stones, and pebbles. The surface layer is a light brown extremely cobbly fine sandy loam about 2 inches thick. The upper 12 inches of the underlying material is light brown and pink very gravelly sandy loam, and the lower part to a depth of 60 inches or more is light brown and pink, stratified material that averages very gravelly loamy coarse sand. In some areas of similar included soils, the surface layer is extremely stony fine sandy loam.

Included in this unit are about 5 percent Arizo soils, flooded, in channels; 5 percent Pittman soils on erosional fan remnants; and 5 percent Aztec soils on erosional fan remnants. Included areas make up about 15 percent of the total acreage. The percentage varies from one area to another.

Permeability of this Caliza soil is moderately rapid.

Available water capacity is low. Effective rooting depth is 60 inches or more. Runoff is medium, and the hazard of water erosion is slight. The hazard of soil blowing is moderate if the surface is disturbed.

This unit is used mainly as habitat for desert wildlife and for recreation. It is also used for urban development.

This unit is well suited to the construction of dwellings.
Unless the density of housing is too high, septic tank
absorption fields normally function well on this unit.

Roads can easily be constructed and maintained on this unit.

The main limitation for lawns and landscaping is the stones, cobbles, and pebbles on the surface and throughout the soil. Topsoil is needed for best results when landscaping, particularly in areas used for lawns. Lawn grasses, shrubs, and trees that are not sensitive to lime-induced chlorosis are well suited to use in landscaping. Annual applications of iron chelates reduce the effects of chlorosis.

Intermittent streams form the drainageways in this unit. These drainageways are subject to rare or occasional periods of high-velocity flooding. Care should be taken during urbanization to accommodate the runoff from the drainageways. If drains become plugged during a major flood, accelerated erosion and damage to roads, buildings, and other structures can occur.

This map unit is in capability subclass VIIs, nonirrigated, and in horticultural group 2.

190—Dalian very gravelly fine sandy loam, 2 to 4 percent slopes. This very deep, well drained soil is on fan skirts. It formed in alluvium derived dominantly from limestone and dolomite.

Typically, 65 percent of the surface is covered with a weakly developed desert pavement of pebbles. The surface layer is light yellowish brown very gravelly fine

The main limitations for lawns and landscaping are the presence of pebbles throughout the soil and the very low available water capacity of the Weiser soil. Topsoil is needed for best results when landscaping, particularly in areas used for lawns. Frequent irrigation of lawns, gardens, and most other plantings is needed because of the limited available water capacity of the soil. Lawn grasses, shrubs, and trees that are not sensitive to lime-induced chlorosis are well suited to use in landscaping. Annual applications of iron chelates reduce the effects of chlorosis.

Intermittent streams form the drainageways in this unit. These drainageways are subject to rare or occasional periods of high-velocity flooding. Care should be taken during urbanization to accommodate the runoff from the drainageways. If drains become plugged during a major flood, accelerated erosion and damage to roads, buildings, and other structures can occur.

This map unit is in capability subclasses IVs, irrigated, and VIIs, nonirrigated. It is in horticultural group 2.

545—Weiser-Goodsprings complex, 2 to 4 percent slopes. This map unit is on erosional fan remnants.

This unit is 60 percent Weiser extremely gravelly fine sandy loam, 2 to 4 percent slopes, and 25 percent Goodsprings very gravelly fine sandy loam, 2 to 4 percent slopes. The Weiser and Goodsprings soils are on summits and shoulders of the fan remnants. The components of this unit are so intricately intermingled that it was not practical to map them separately at the scale used.

Included in this unit are about 5 percent Las Vegas soils and 10 percent Skyhaven soils on relict alluvial flats. Included areas make up about 15 percent of the total acreage. The percentage varies from one area to another.

The Weiser soil is very deep and well drained. It formed in alluvium derived dominantly from limestone and dolomite. Typically, 90 percent of the surface layer is covered with a desert pavement of pebbles. There is a dark desert varnish on the exposed surfaces of the rock fragments. The surface layer is light yellowish brown extremely gravelly fine sandy loam about 1 inch thick. The underlying material to a depth of 63 inches is light brown extremely gravelly fine sandy loam and very gravelly fine sandy loam, averaging extremely gravelly fine sandy loam.

Permeability of the Weiser soil is moderately rapid. Available water capacity is very low. Effective rooting depth is 60 inches or more. Runoff is medium, and the hazard of water erosion is slight. The hazard of soil blowing is moderate if the desert pavement is disturbed.

The Goodsprings soil is shallow and well drained. It formed in alluvium derived from various kinds of rock. Typically, 90 percent of the surface is covered with a desert pavement of pebbles. The surface layer is light brown very gravelly fine sandy loam about 5 inches

thick. The upper 10 inches of the underlying material is pink gravelly fine sandy loam, the next 37 inches is pinkish white, strongly lime-cemented hardpan, and the lower part to a depth of 60 inches or more is pink extremely gravelly loamy fine sand. Depth to the hardpan ranges from 9 to 20 inches.

Permeability of the Goodsprings soil is moderate above the hardpan. Available water capacity is very low. Effective rooting depth is 9 to 20 inches. Runoff is medium, and the hazard of water erosion is slight. The hazard of soil blowing is high if the desert pavement is disturbed.

This unit is used as habitat for desert wildlife and for recreation.

This unit is limited for roads because of the depth to the hardpan in areas of the Goodsprings soil. Roads should be designed to minimize cuts. Heavy equipment is needed for excavation.

This map unit is in capability subclass VIIs, nonirrigated. The Weiser soil is in horticultural group 2, and the Goodsprings soil is in horticultural group 6.

600—Slickens. Slickens consists of accumulations of fine-textured material such as that separated in ore-mill operations. It is largely freshly ground rock that commonly has undergone chemical treatment during the milling process. Slickens is commonly confined in specially constructed basins.

This map unit is in capability subclass VIIIs, nonirrigated.

605—Dumps. Dumps consists of areas of smoothed or uneven accumulations of waste rock and general refuse.

This map unit is in capability subclass VIIIs, nonirrigated.

**610—Pits, gravel.** Pits, gravel, consists of open excavations from which soil material and gravel have been removed, exposing rock, a hardpan, or other material.

This map unit is in capability subclass VIIIs, nonirrigated.

615—Urban land. Urban land consists of areas covered by asphalt, concrete, and buildings or other urban structures.

This map unit is in capability subclass VIIIs, nonirrigated.

630—Badland. Badland is moderately steep to very steep barren land dissected by many intermittent drainage channels that have cut into soft geologic material. The areas ordinarily are not stony. Local relief generally ranges from 25 to 100 feet. Potential runoff is very high, and erosion is active. Some small included areas of identifiable soils support vegetation.

#### HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

# RUNOFF CURVE NUMBERS (URBAN AREAS<sup>1</sup>)

| Cover description  |   |    | 0  | mbers for<br>soil group— |    |
|--|---|----|----|--------------------------|----|
| Cover type and hydrologic condition                                      | Average percent<br>impervious area <sup>2</sup> | A  | В  | С                        | D  |
| Fully developed urban areas (vegetation established)                     |   |    |    |                          |    |
| Open space (lawns, parks, golf courses, cemeteries, etc.) <sup>2</sup> : |   |    |    |                          |    |
| Poor condition (grass cover < 50%)                                       |   | 68 | 79 | 86                       | 89 |
| Fair condition (grass cover 50% to 75%)                                  |   | 49 | 69 | 79                       | 84 |
| Good condition (grass cover > 75%)                                       |   | 39 | 61 | 74                       | 80 |
| Impervious areas:  |   |    |    |                          |    |
| Paved parking lots. roofs, driveways, etc.                               |   |    |    |                          |    |
| (excluding right-of-way).  |   | 98 | 98 | 98                       | 98 |
| Streets and roads:   |   |    |    |                          |    |
| Paved: curbs and storm sewers (excluding                                 |   |    |    |                          |    |
| right-of-way)  |   | 98 | 98 | 98                       | 98 |
| Paved: open ditches (including right-of-way)                             |   | 83 | 89 | 92                       | 93 |
| Gravel (including right-of-way)  |   | 76 | 85 | 89                       | 91 |
| Dirt (including right-of-way)  |   | 72 | 82 | 87                       | 89 |
| Western desert urban areas:  |   |    |    |                          |    |
| Natural desert landscaping (pervious areas only)                         |   | 63 | 77 | 85                       | 88 |
| Artificial desert landscaping (impervious weed                           |   |    |    |                          |    |
| barrier, desert shrub with 1- to 2-inch sand                             |   |    |    |                          |    |
| or gravel mulch and basin borders)                                       |   | 96 | 96 | 96                       | 96 |
| Urban districts:   |   |    |    |                          |    |
| Commercial and business  | 85  | 89 | 92 | 94                       | 95 |
| Industrial Residential districts by average lot size:                    | 72  | 81 | 88 | 91                       | 93 |

#### See Table 602A

Developing urban areas

| 77 | 86 | 91    | 94       |
|----|----|-------|----------|
|    | 77 | 77 86 | 77 86 91 |

<sup>1</sup> Average runoff condition, and  $I_* = 0.2S$ .

| Date |
|------|
|      |
|      |
|      |
|      |
|      |

WRC ENGINEERING REFERENCE:

SCS TR-55, USDA, June 1986.

TABLE 602 1 of 4

<sup>2</sup> The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system. Impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using Figure 603.

<sup>3</sup> CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.

<sup>4</sup> Composite CN's for natural desert landscaping should be computed using Figure 603 based on the impervious area percentage (CN #98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.

<sup>5</sup> Composite CN's to use for the design of temporary measures during grading and construction should be computed using Figure 603 based on the degree of development impervious area percentage) and the CN's for the newly graded pervious areas.

# HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

# **RUNOFF CURVE NUMBERS** (SEMIARID RANGELANDS1)

| Cover description                              |                                      |      |    | mbers for<br>soil group— |      |
|--|--------------------------------------|------|----|--------------------------|------|
| Cover type                                     | Hydrologic<br>condition <sup>2</sup> | A3 · | В  | С                        | D    |
| Herbaceous-mixture of grass, weeds, and        | Poor                                 |      | 80 | 87                       | 93   |
| low-growing brush, with brush the              | Fair                                 |      | 71 | 81                       | 89   |
| minor element.                                 | Good                                 |      | 62 | 74                       | 85   |
| Oak-aspen-mountain brush mixture of oak brush, | Poor                                 |      | 66 | 74                       | 79   |
| aspen, mountain mahogany, bitter brush, maple, | Fair                                 |      | 48 | 57                       | 63   |
| and other brush.                               | Good                                 |      | 30 | 41                       | 48   |
| Pinyon-juniper-pinyon, juniper, or both;       | Poor                                 |      | 75 | 85                       | 89   |
| grass understory.                              | Fair                                 |      | 58 | 73                       | 80   |
|  | Good                                 |      | 41 | 61                       | . 71 |
| Sagebrush with grass understory.               | Poor                                 |      | 67 | 80                       | 85   |
|  | Fair                                 |      | 51 | 63                       | 70   |
|  | Good                                 |      | 35 | 47                       | 55   |
| Desert shrub—major plants include saltbush,    | Poor                                 | 63   | 77 | 85                       | 88   |
| greasewood, creosotebush, blackbrush, bursage, | Fair                                 | 55   | 72 | 81                       | 86   |
| palo verde, mesquite, and cactus.              | Good                                 | 49   | 68 | 79                       | 84   |

Average runoff condition, and I = 0.2S.

Revision Date

WRC ENGINEERING REFERENCE:

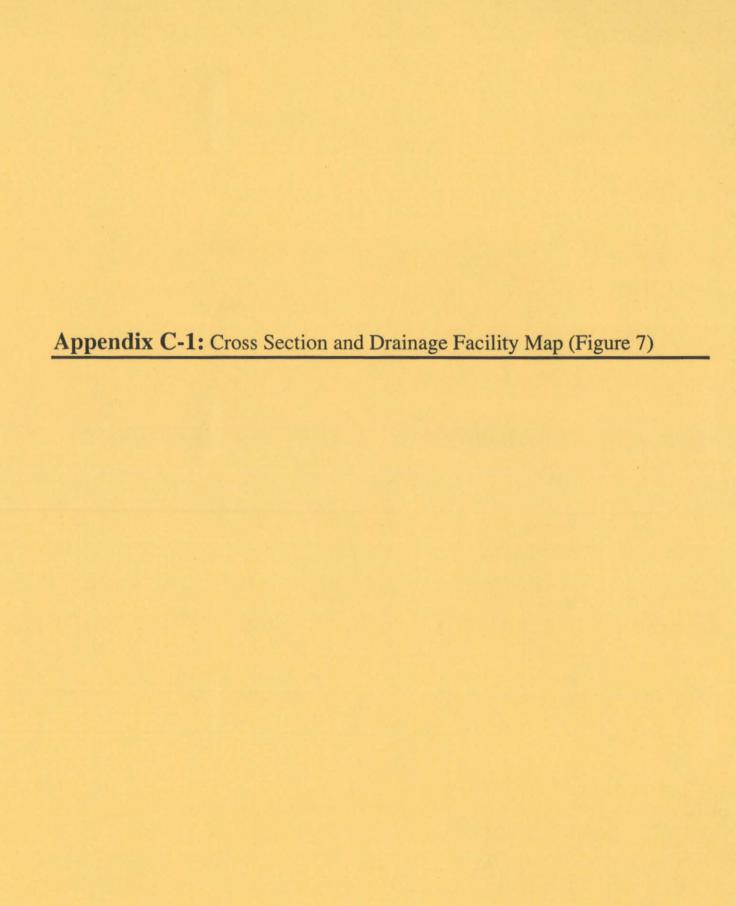
SCS TR-55, USDA, June 1986.

TABLE 602 4 of 4

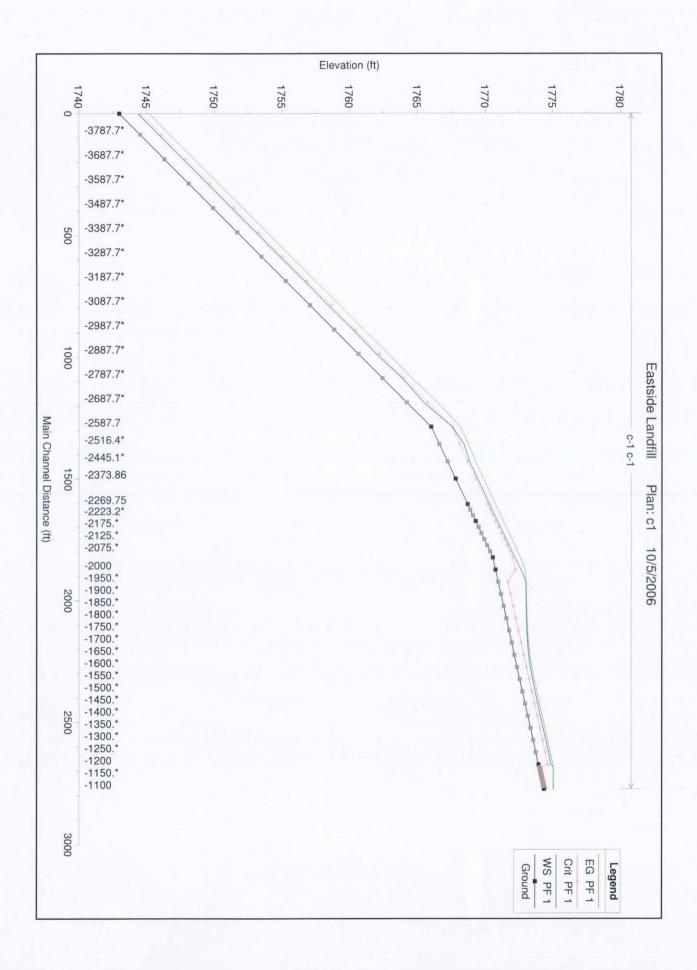
<sup>&</sup>lt;sup>2</sup> Poor: <30% ground cover (litter, grass, and brush overstory). Fair: 30 to 70% ground cover. Good: >70% ground cover.

<sup>\*</sup>Curve numbers for group A have been developed only for desert shrub.

Appendix C: Hydraulic Calculations



Appendix C-2: HEC-RAS Model for Channel C-1

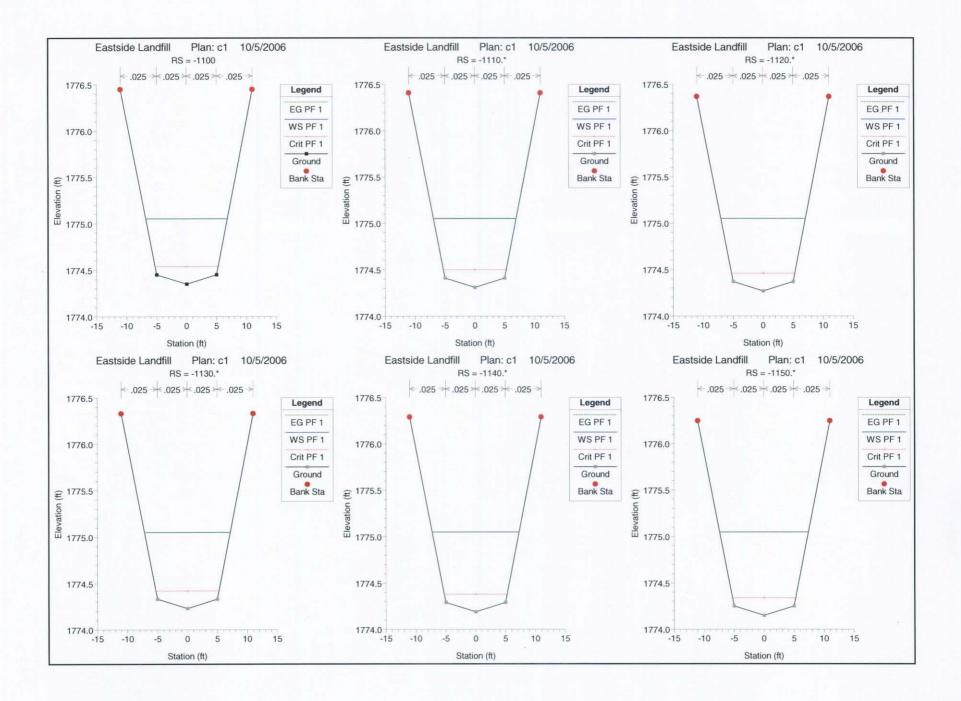


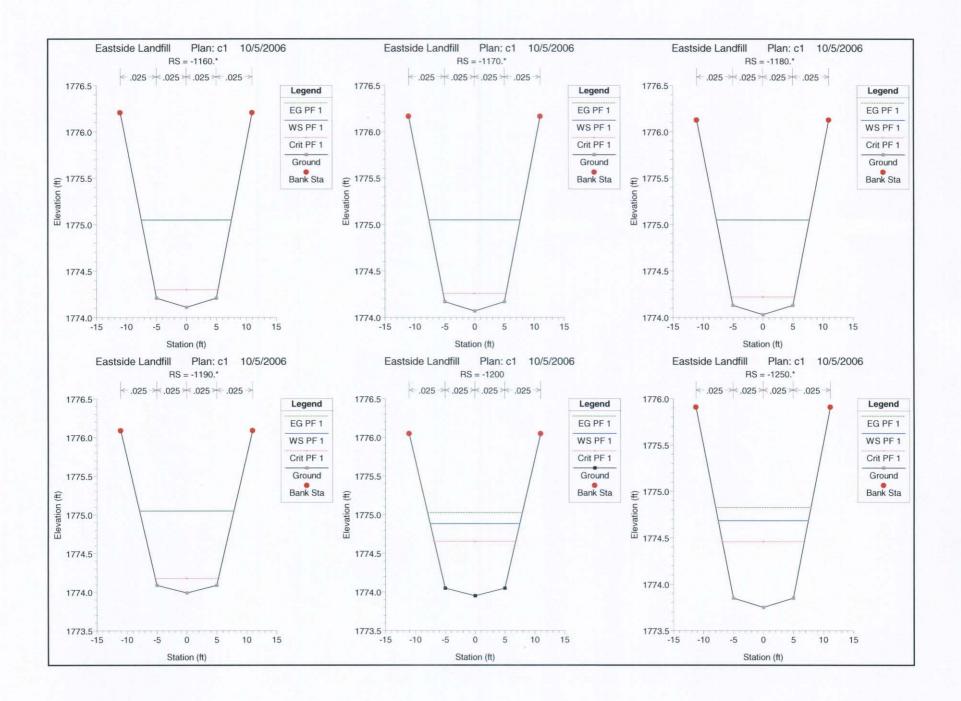
HEC-RAS Plan: c1 River: c-1 Reach: c-1 Profile: PF 1

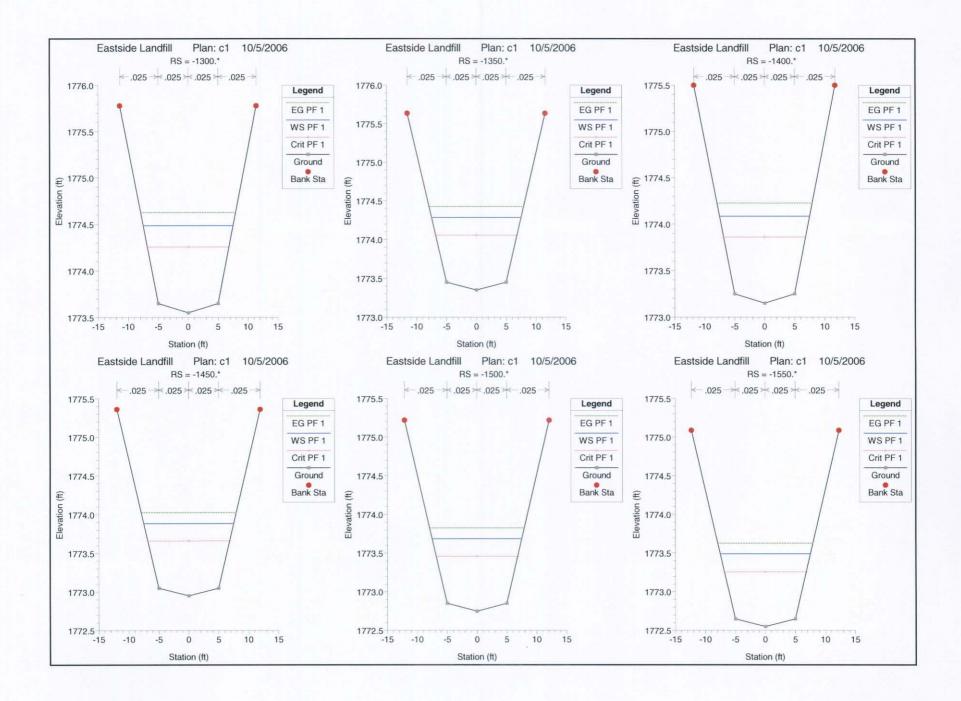
| Reach | River Sta | Profile | Q Total | Min Ch El                                   | W.S. Elev                               | Crit W.S.                               | E.G. Elev                               | E.G. Slope                              | Vel Chnl     | Flow Area      | Top Width      | Froude # Chl | Max Chl Dpth | Frctn Slope |
|-------|-----------|---------|---------|---|---|---|---|---|--------------|----------------|----------------|--------------|--------------|-------------|
|       |           |         | (cfs)   | (ft)  | (ft)                                    | (ft)                                    | (ft)                                    | (ft/ft)                                 | (ft/s)       | (sq ft)        | (ft)           |              | (ft)         | (ft/ft)     |
| ⊱1    | -1100     | PF 1    | 3.00    | 1774.35                                     | 1775.05                                 | 1774.54                                 | 1775.06                                 | 0.000097                                | 0.39         | 7.62           | 13.62          | 0.09         | 0.70         | 0.000087    |
| ×1    | -1110.*   | PF 1    | 3.00    | 1774.31                                     | 1775.05                                 | 1774.50                                 | 1775.05                                 | 0.000079                                | 0.37         | 8.16           | 13.85          | 0.08         | 0.74         | 0.000072    |
| >1    | -1120.*   | PF 1    | 3.00    | 1774.27                                     | 1775.05                                 | 1774.46                                 | 1775.05                                 | 0.000065                                | 0.34         | 8.71           | 14.09          | 0.08         | 0.78         | 0.000059    |
| >-1   | -1130.*   | PF 1    | 3.00    | 1774.23                                     | 1775.05                                 | 1774.42                                 | 1775.05                                 | 0.000054                                | 0.32         | 9.27           | 14.33          | 0.07         | 0.82         | 0.000049    |
| c-1   | -1140.*   | PF 1    | 3.00    | 1774.19                                     | 1775.05                                 | 1774.38                                 | 1775.05                                 | 0.000045                                | 0.30         | 9.84           | 14.56          | 0.07         | 0.86         | 0.000042    |
| c-1   | -1150.*   | PF 1    | 3.00    | 1774.15                                     | 1775.05                                 | 1774.34                                 | 1775.05                                 | 0.000038                                | 0.29         | 10.42          | 14.80          | 0.06         | 0.90         | 0.000035    |
| c-1   | -1160.*   | PF 1    | 3.00    | 1774.11                                     | 1775.05                                 | 1774.30                                 | 1775.05                                 | 0.000033                                | 0.27         | 11.02          | 15.04          | 0.06         | 0.94         | 0.000030    |
| c-1   | -1170.*   | PF 1    | 3.00    | 1774.07                                     | 1775.05                                 | 1774.26                                 | 1775.05                                 | 0.000028                                | 0.26         | 11.62          | 15.28          | 0.05         | 0.98         | 0.000026    |
| c-1   | -1180.*   | PF 1    | 3.00    | 1774.03                                     | 1775.05                                 | 1774.22                                 | 1775.05                                 | 0.000024                                | 0.25         | 12.23          | 15.52          | 0.05         | 1.02         | 0.000022    |
| c-1   | -1190.*   | PF 1    | 3.00    | 1773.99                                     | 1775.05                                 | 1774.18                                 | 1775.05                                 | 0.000021                                | 0.23         | 12.86          | 15.76          | 0.05         | 1.06         | 0.000930    |
| c-1   | -1200     | PF 1    | 33.00   | 1773.95                                     | 1774.89                                 | 1774.66                                 | 1775.03                                 | 0.004001                                | 3.01         | 10.96          | 15.02          | 0.62         | 0.94         | 0.003997    |
| c-1   | -1250.*   | PF 1    | 33.00   | 1773.75                                     | 1774.69                                 | 1774.46                                 | 1774.83                                 | 0.003994                                | 3.01         | 10.97          | 15.03          | 0.62         | 0.94         | 0.003997    |
| c-1   | -1300.*   | PF 1    | 33.00   | 1773.55                                     | 1774.49                                 | 1774.26                                 | 1774.63                                 | 0.004001                                | 3.01         | 10.96          | 15.01          | 0.62         | 0.94         | 0.004001    |
| c-1   | -1350.*   | PF 1    | 33.00   | 1773.35                                     | 1774.29                                 | 1774.06                                 | 1774.43                                 |   | 3.01         | 10.96          | 15.01          | 0.62         | 0.94         | 0.004001    |
| c-1   | -1400.*   | PF 1    | 33.00   | 1773.15                                     | 1774.09                                 | 1773.86                                 | 1774.23                                 |   | 3.01         | 10.96          | 15.02          | 0.62         | 0.94         | 0.003999    |
| c-1   | -1450.*   | PF 1    | 33.00   | 1772.95                                     | 1773.89                                 | 1773.66                                 | 1774.03                                 |   | 3.01         | 10.96          | 15.03          | 0.62         | 0.94         | 0.003991    |
| c-1   | -1500.*   | PF 1    | 33.00   | 1772.75                                     | 1773.69                                 |   | 1773.83                                 | 100000000000000000000000000000000000000 | 3.01         | 10.98          | 15.03          | 0.62         | 0.94         | 0.003964    |
| c-1   | -1550.*   | PF 1    | 33.00   | 1772.55                                     | 1773.49                                 |   | 1773.63                                 |   | 3.00         | 11.01          | 15.03          | 0.62         | 0.94         | 0.003872    |
| c-1   | -1600.*   | PF 1    | 33.00   | 1772.35                                     | 1773.30                                 | 1773.06                                 | 1773.44                                 |   | 2.96         | 11.15          | 15.09          | 0.61         | 0.95         | 0.003603    |
| c-1   | -1650.*   | PF 1    | 33.00   | 1772.15                                     | 1773.13                                 |   | 1773.25                                 | -                                       | 2.85         | 11.57          | 15.26          | 0.58         | 0.98         | 0.003045    |
| c-1   | -1700.*   | PF 1    | 33.00   | 1771.95                                     | 1772.99                                 |   | 1773.10                                 |   | 2.64         | 12.49          | 15.61          | 0.52         | 1.04         | 0.002262    |
| c-1   | -1750.*   | PF 1    | 33.00   | 1771.75                                     | 1772.89                                 | 900000000000000000000000000000000000000 | 1772.98                                 |   | 2.33         | 14.14          | 16.23          | 0.44         | 1.14         | 0.001510    |
| c-1   | -1800.*   | PF 1    | 33.00   | 1771.55                                     | 1772.83                                 |   | 1772.89                                 |   | 2.00         | 16.48          | 17.08          | 0.36         | 1.28         | 0.000962    |
| c-1   | -1850.*   | PF 1    | 33.00   | 1771.35                                     | 1772.79                                 |   | 1772.84                                 |   | 1.70         | 19.37          | 18.07          | 0.29         | 1.44         | 0.000611    |
| c-1   | -1900.*   | PF 1    | 33.00   | 1771.15                                     | 1772.77                                 |   | 1772.81                                 | 0.000495                                | 1.46         | 22.68          | 19.14          | 0.24         | 1.62         | 0.000396    |
| c-1   | -1950.*   | PF 1    | 33.00   | 1770.95                                     | 1772.76                                 |   | 1772.78                                 |   | 1.25         | 26.33          | 20.24          | 0.19         | 1.81         | 0.000318    |
| c-1   | -2000     | PF 1    | 33.00   | 1770.75                                     | 1772.75                                 | 7011107200                              | 100000000000000000000000000000000000000 |   | 1.09         | 30.25          | 21.38          | 0.16         | 2.00         | 0.002312    |
| c-1   | -2050     | PF 1    | 120.00  | 1770.55                                     | 1772.18                                 | 100000000000000000000000000000000000000 | 1772.61                                 |   | 5.28         | 22.72          | 19.15          | 0.85         | 1.62         | 0.008406    |
| c-1   | -2075.*   | PF1     | 120.00  | 1770.34                                     | 1771.96                                 |   | 1772.40                                 | -                                       | 5.28         | 22.71          | 19.14          | 0.86         | 1.62         | 0.008448    |
| c-1   | -2100.*   | PF 1    | 120.00  | 1770.13                                     |   |   | 1772.19                                 |   | 5.30         | 22.63          | 19.12          | 0.86         | 1.62         | 0.008522    |
| c-1   | -2125.*   | PF 1    | 120.00  | 1769.92                                     | 1771.54                                 |   | 100000000000000000000000000000000000000 |   | 5.32         | 22.55          | 19.09          | 0.86         | 1.62         | 0.008425    |
| c-1   | -2150.*   | PF 1    | 120.00  | 1769.70                                     | 1771.33                                 |   | 1771.76                                 | -                                       | 5.25         | 22.84          | 19.19          | 0.85         | 1.63         | 0.008248    |
| c-1   | -2175.*   | PF1     | 120.00  | 1769.49                                     | 1771.13                                 |   | 1771.55                                 |   | 5.23         | 22.93          | 19.21          | 0.84         | 1.64         | 0.008390    |
| c-1   | -2200     | PF 1    | 121.00  | 1769.28                                     | 1770.90                                 |   | 1771.35                                 |   | 5.33         | 22.68          | 19.14          | 0.86         | 1.62         | 0.008570    |
| c-1   | -2223.2*  | PF 1    | 121.00  | 1769.08                                     | 1770.70                                 | 100000000000000000000000000000000000000 | 1771.15                                 |   | 5.33         | 22.70          | 19.14          | 0.86         | 1.62         | 0.008546    |
| c-1   | -2246.5*  | PF 1    | 121.00  | 1768.88                                     | 1770.51                                 | 1770.37                                 | 1770.95                                 |   | 5.32         | 22.73          | 19.15          | 0.86         | 1.63         | 0.008505    |
| c-1   | -2269.75  | PF 1    | 121.00  | 1768.68                                     | 1770.31                                 | 1770.17                                 | 1770.75                                 |   | 5.31         | 22.79          | 19.17          | 0.86         | 1.63         | 0.008450    |
| c-1   | -2373.86  | PF 1    | 121.00  | 1767.80                                     | 1769.43                                 |   | 1769.87                                 |   | 5.30         | 22.85          | 19.19          | 0.86         | 1.63         | 0.008410    |
| c-1   | -2445.1*  | PF 1    | 121.00  | 1767.20                                     | 1768.83<br>1768.42                      | O.M. Barrell                            | 1769.27<br>1768.74                      |   | 5.29         | 22.87<br>26.49 | 19.20<br>20.29 | 0.85<br>0.70 | 1.63         | 0.006934    |
| c-1   | -2516.4*  | PF 1    | 121.00  | 1766.60                                     | 1768.42                                 |   | 1768.74                                 |   | 4.57<br>6.12 | 21.42          | 18.73          | 1.01         | 1.82         | 0.008089    |
| c-1   | -2587.7   | PF 1    | 131.00  | 1766.00                                     | 100000000000000000000000000000000000000 |   |   | -                                       | -            |                |                |              | 1.56         |             |
| c-1   | -2687.7*  | PF 1    | 131.00  | 1764.21                                     | 1765.47                                 |   | 1766.49                                 |   | 8.09         | 16.19          | 16.98          | 1.46         | 1.26         | 0.015943    |
| c-1   | -2787.7*  | PF 1    | 131.00  | 1762.42<br>1760.64                          | 1763.87<br>1761.97                      | 1763.98<br>1762.20                      | 1764.57<br>1762.86                      |   | 6.71<br>7.58 | 19.53<br>17.27 | 18.12<br>17.36 | 1.14         | 1.45         | 0.018227    |
| c-1   | -2887.7*  |         |         | - 1900-00-00-00-00-00-00-00-00-00-00-00-00- |   |   |   |   | 7.58         |                |                | 1/2/2/2/1/   |              |             |
| c-1   | -2987.7*  | PF 1    | 131.00  | 1758.85                                     | 1760.25                                 | 1760.41                                 | 1761.02                                 | 0.016441                                | 7.03         | 18.63          | 17.82          | 1.21         | 1.40         | 0.018032    |

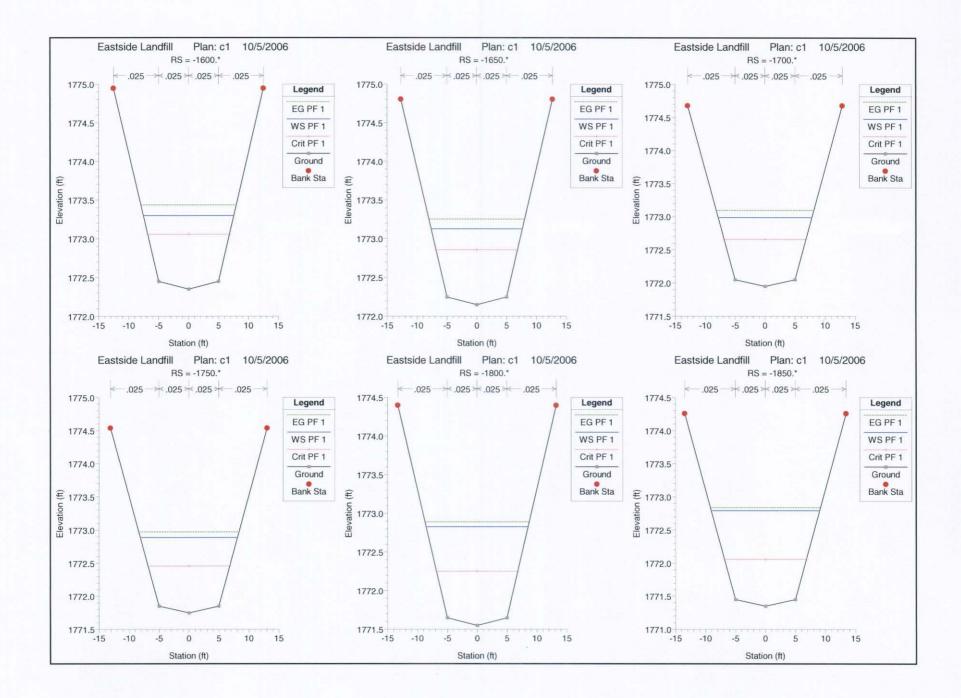
HEC-RAS Plan: c1 River: c-1 Reach: c-1 Profile: PF 1 (Continued)

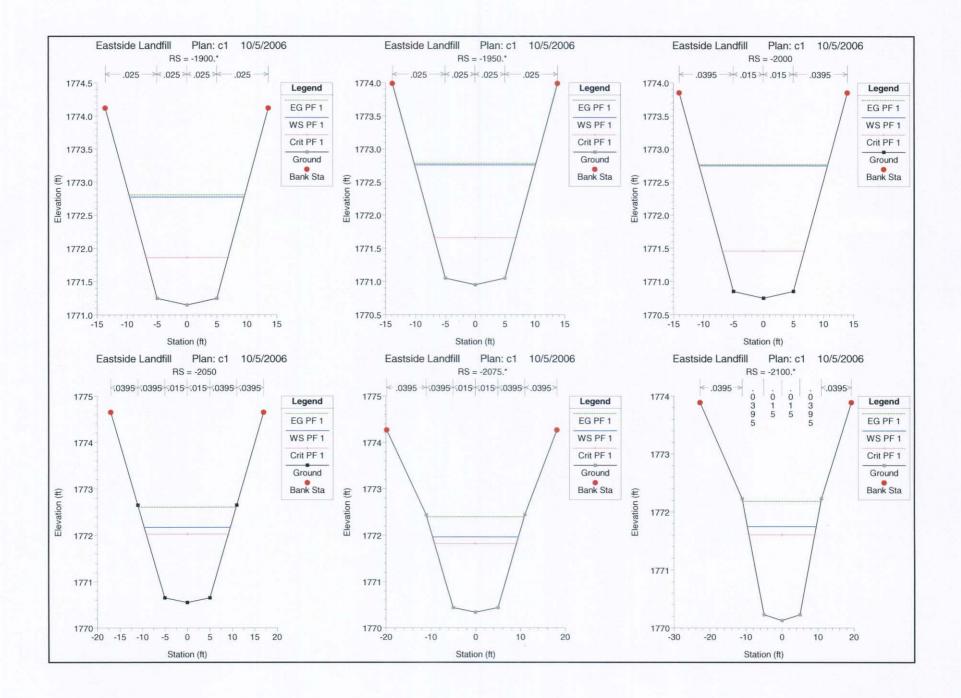
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl | Max Chl Dpth | Frctn Slope |
|-------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|--------------|-------------|
|       |           |         | (cfs)   | (ft)      | (ft)      | (ft)      | (ft)      | (ft/ft)    | (ft/s)   | (sq ft)   | (ft)      |              | (ft)         | (ft/ft)     |
| c-1   | -3087.7*  | PF 1    | 131.00  | 1757.06   | 1758.41   | 1758.62   | 1759.26   | 0.018674   | 7.40     | 17.70     | 17.51     | 1.30         | 1.35         | 0.017504    |
| c-1   | -3187.7*  | PF 1    | 131.00  | 1755.27   | 1756.65   | 1756.83   | 1757.45   | 0.017258   | 7.17     | 18.27     | 17.70     | 1.24         | 1.38         | 0.017945    |
| c-1   | -3287.7*  | PF 1    | 131.00  | 1753.48   | 1754.84   | 1755.04   | 1755.67   | 0.018132   | 7.31     | 17.91     | 17.58     | 1.28         | 1.36         | 0.017687    |
| c-1   | -3387.7*  | PF 1    | 131.00  | 1751.70   | 1753.07   | 1753.26   | 1753.89   | 0.017639   | 7.23     | 18.11     | 17.65     | 1.26         | 1.37         | 0.017883    |
| c-1   | -3487.7*  | PF 1    | 131.00  | 1749.91   | 1751.27   | 1751.47   | 1752.10   | 0.018164   | 7.32     | 17.90     | 17.57     | 1.28         | 1.36         | 0.017899    |
| c-1   | -3587.7*  | PF 1    | 131.00  | 1748.12   | 1749.49   | 1749.68   | 1750.31   | 0.017788   | 7.26     | 18.05     | 17.62     | 1.26         | 1.37         | 0.017975    |
| c-1   | -3687.7*  | PF 1    | 131.00  | 1746.33   | 1747.70   | 1747.89   | 1748.52   | 0.018000   | 7.29     | 17.97     | 17.60     | 1.27         | 1.37         | 0.017894    |
| c-1   | -3787.7*  | PF 1    | 131.00  | 1744.54   | 1745.91   | 1746.10   | 1746.73   | 0.017975   | 7.29     | 17.98     | 17.60     | 1.27         | 1.37         | 0.017988    |
| c-1   | -3874.10  | PF 1    | 131.00  | 1743.00   | 1744.37   | 1744.56   | 1745.19   | 0.017762   | 7.25     | 18.06     | 17.63     | 1.26         | 1.37         | 0.017868    |

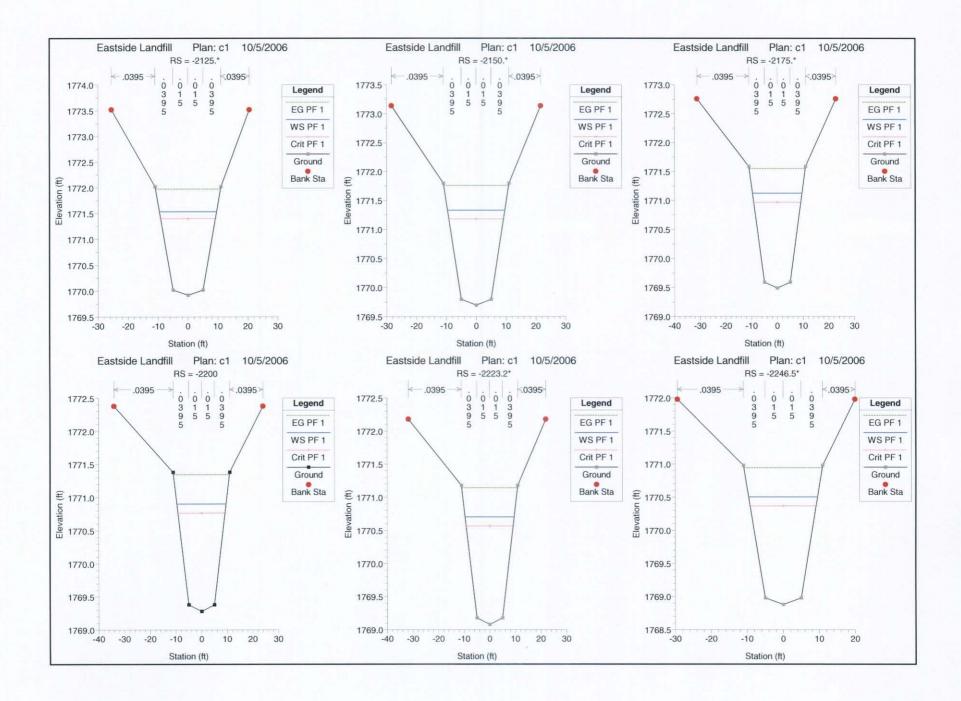


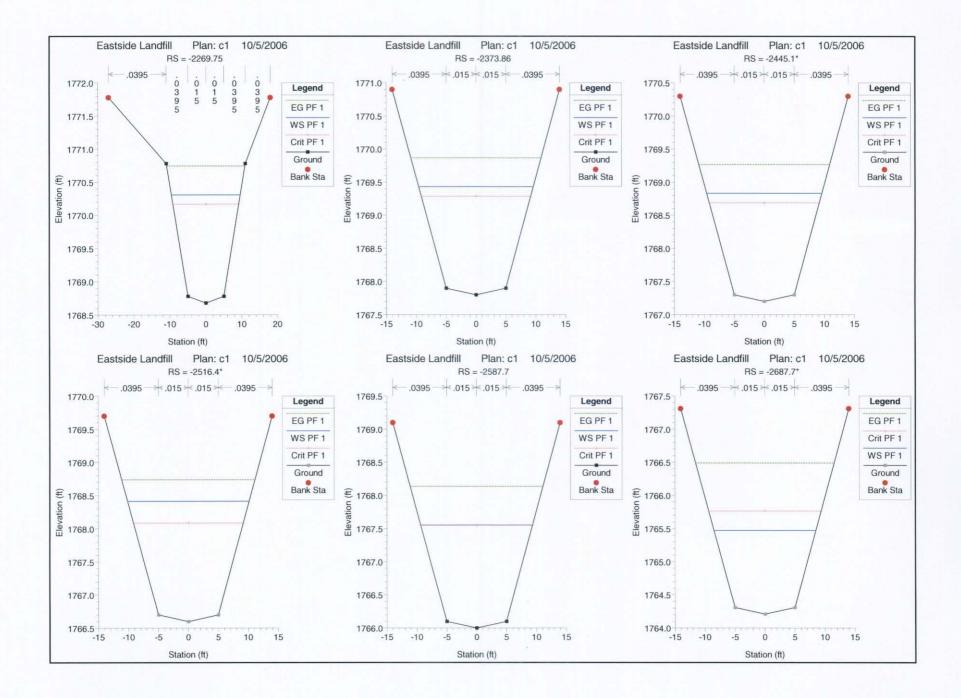


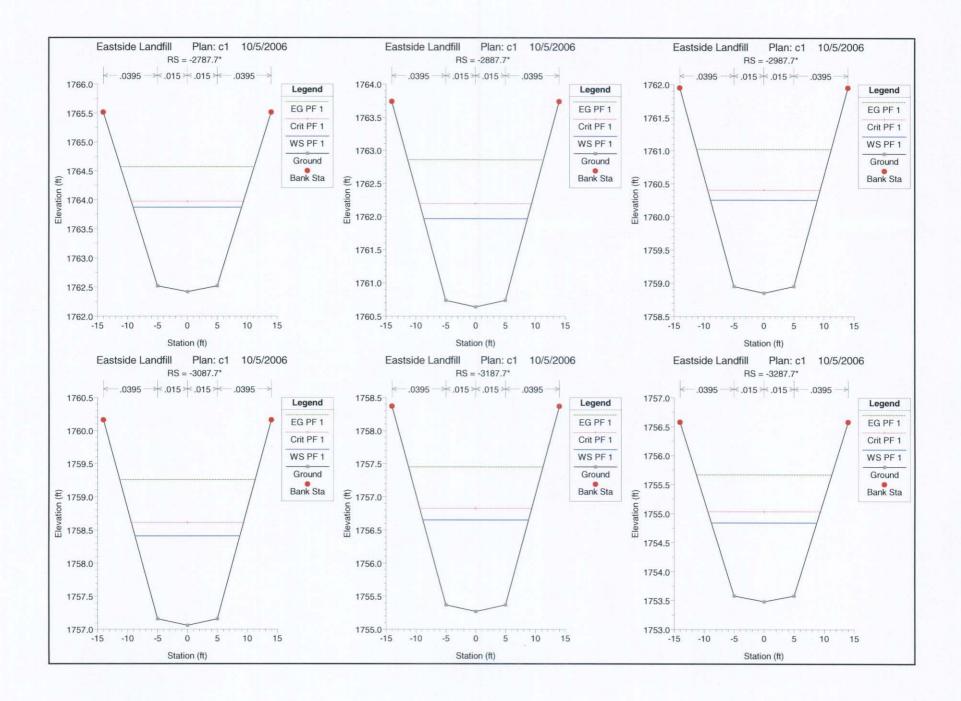


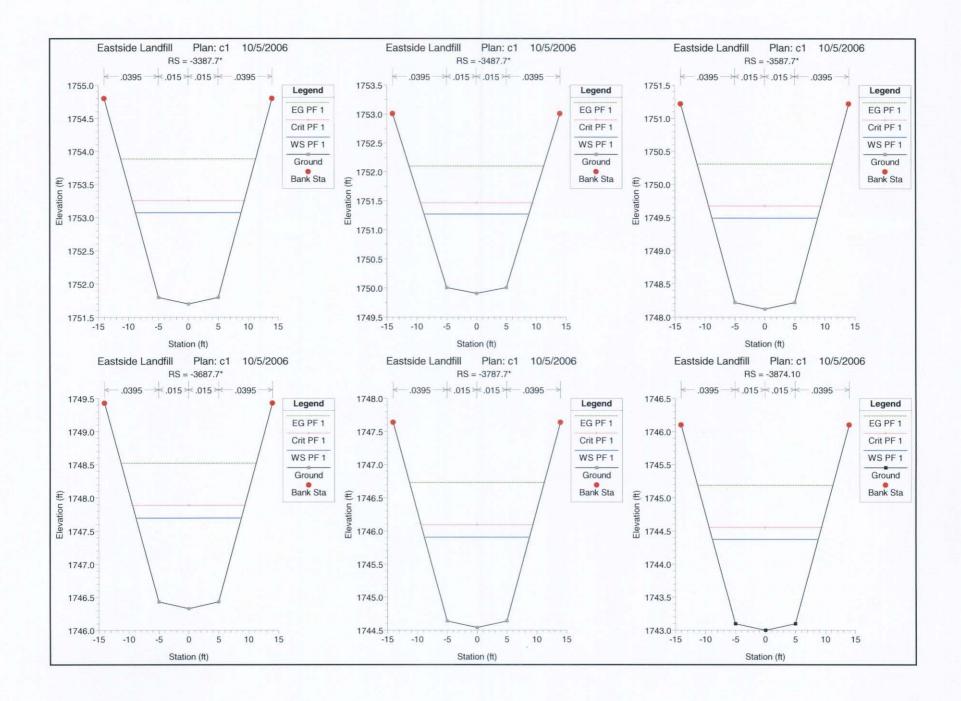






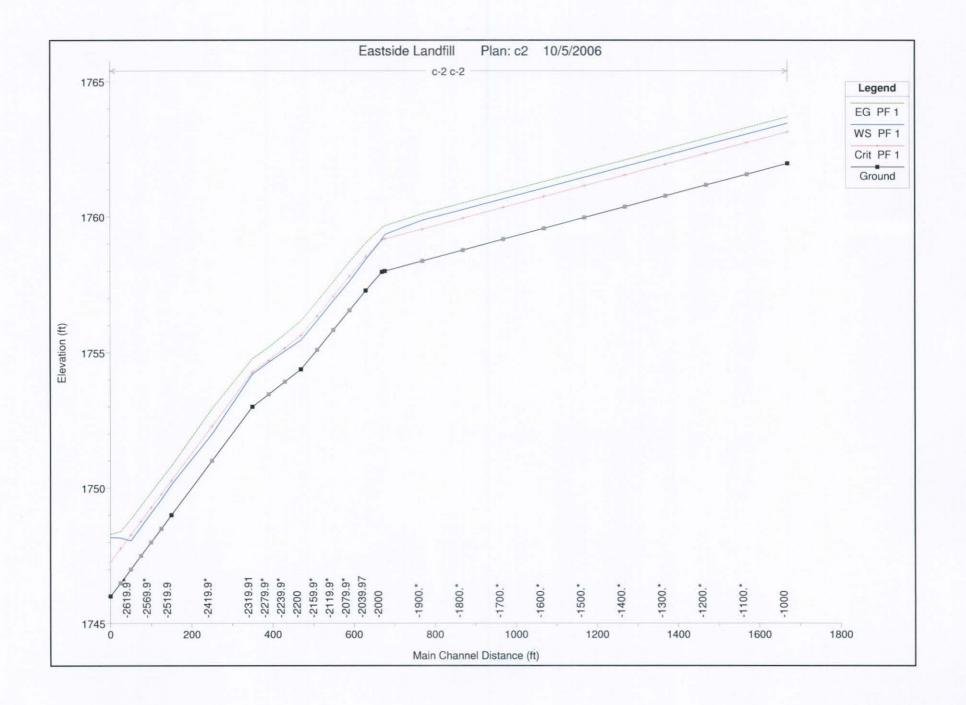






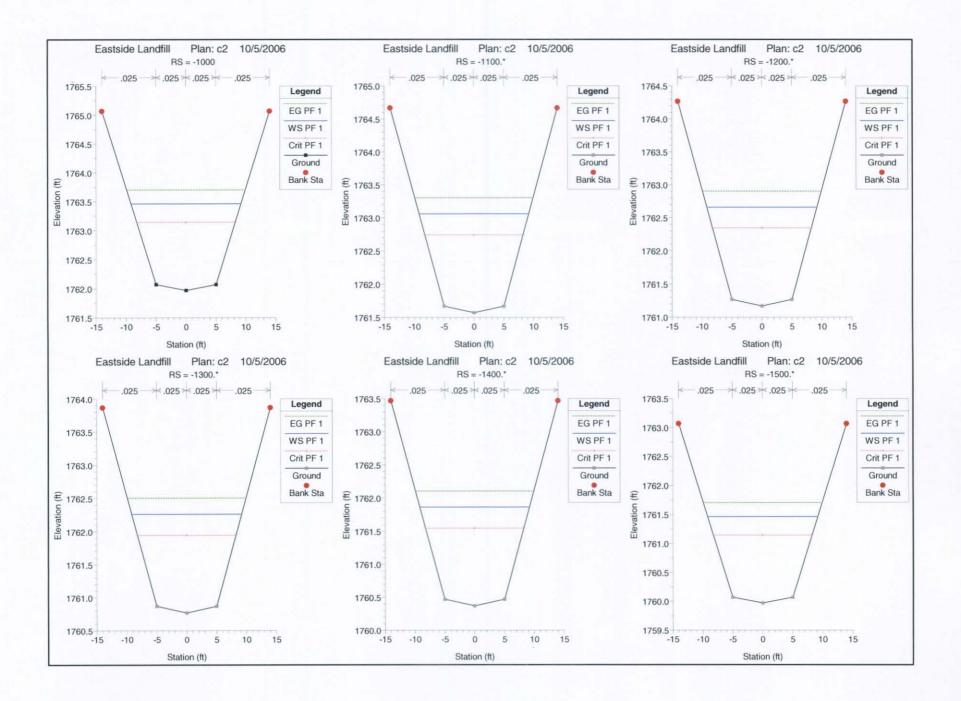
An electronic copy of the HEC-RAS Report is provided in Appendix F.

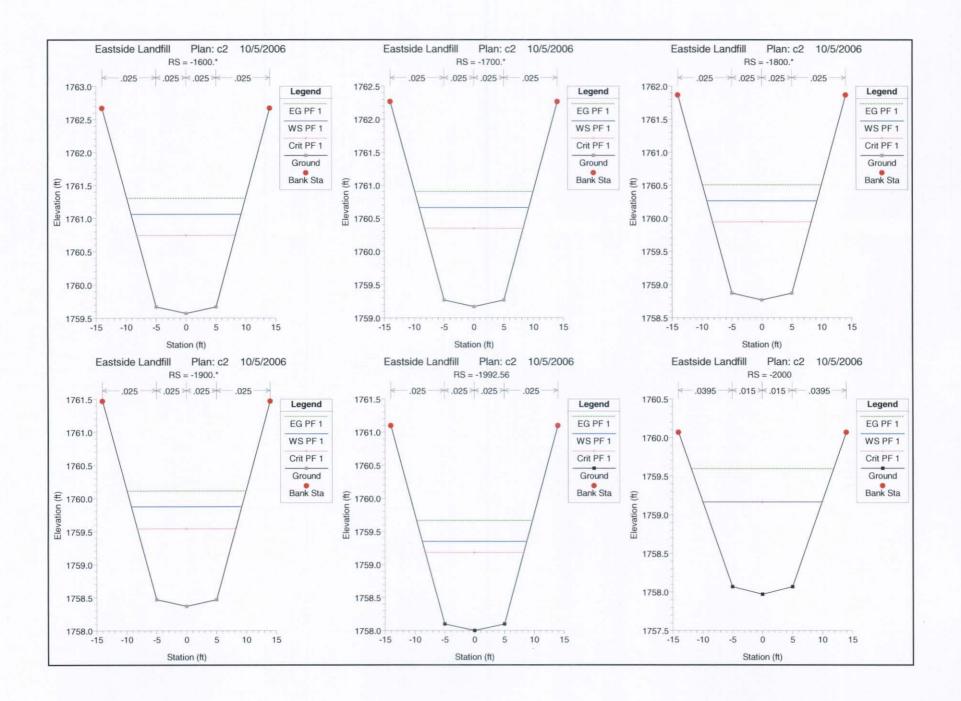


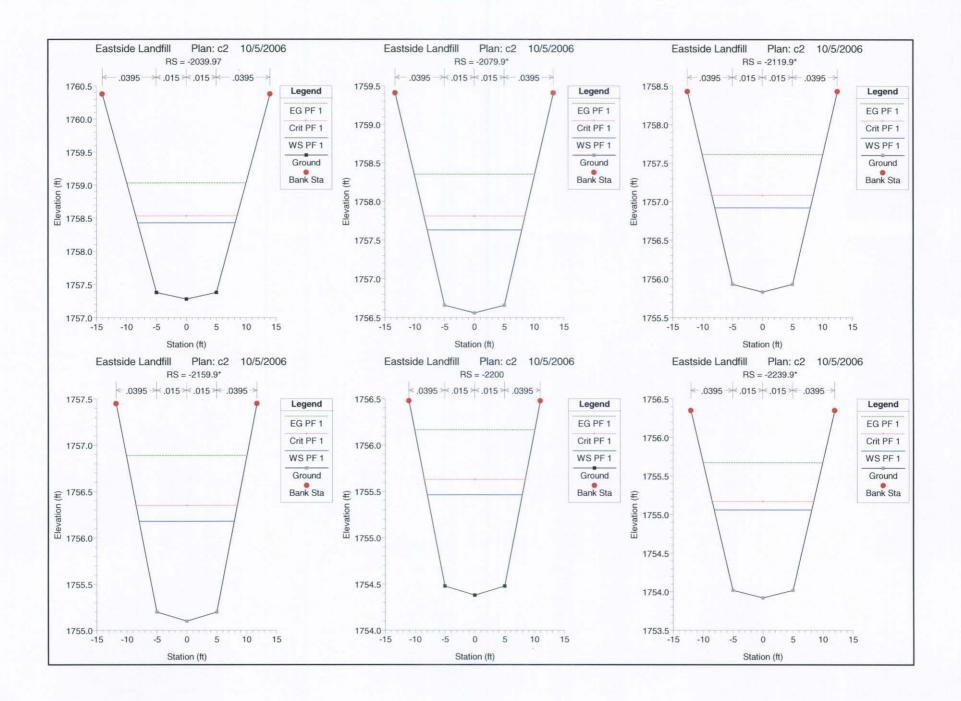


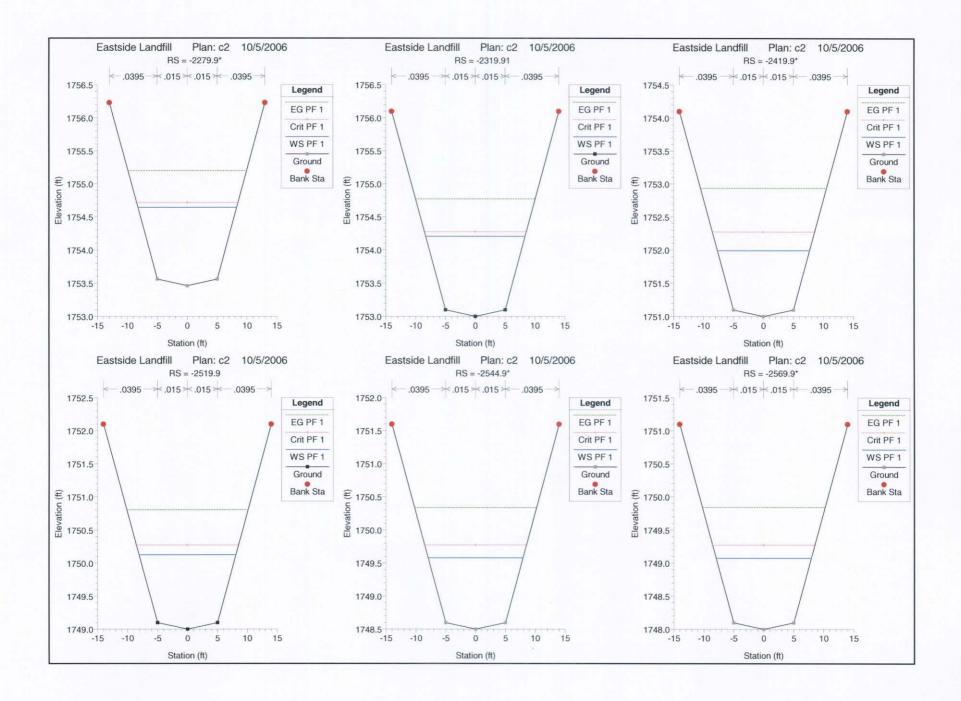
HEC-RAS Plan: c2 River: c-2 Reach: c-2 Profile: PF 1

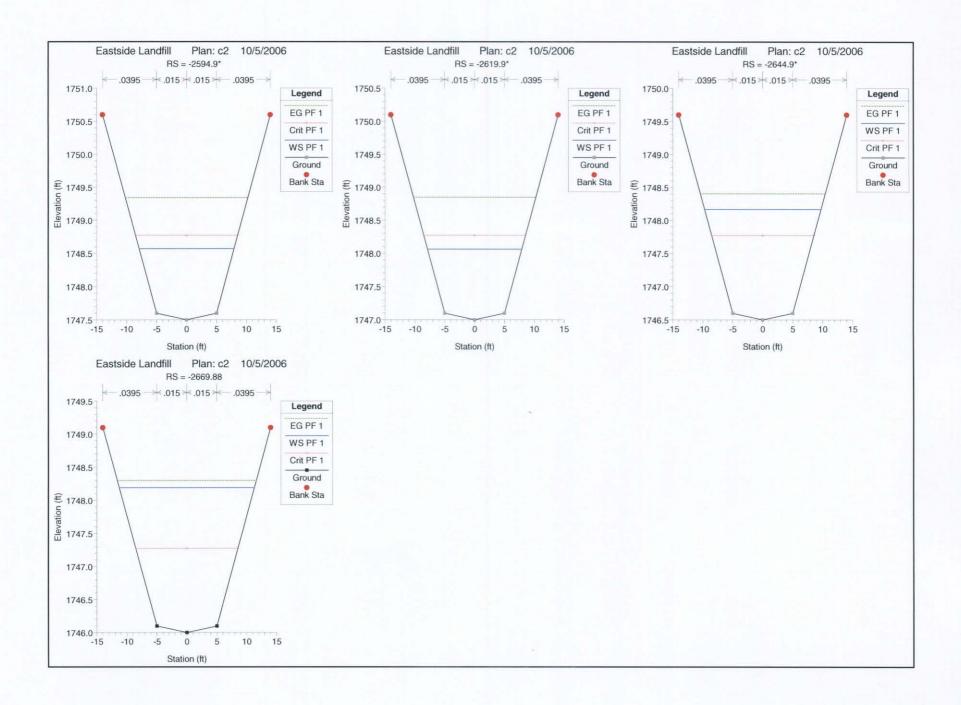
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl | Max Chl Dpth | Frctn Slope |
|-------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|--------------|-------------|
|       |           |         | (cfs)   | (ft)      | (ft)      | (ft)      | (ft)      | (ft/ft)    | (ft/s)   | (sq ft)   | (ft)      |              | (ft)         | (ft/ft)     |
| -2    | -1000     | PF 1    | 80.00   | 1761.97   | 1763.46   | 1763.15   | 1763.71   | 0.003999   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.004000    |
| 0-2   | -1100.*   | PF 1    | 80.00   | 1761.57   | 1763.06   | 1762.75   | 1763.31   | 0.004000   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.004000    |
| 0-2   | -1200.*   | PF 1    | 80.00   | 1761.17   | 1762.66   | 1762.35   | 1762.91   | 0.004001   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.004001    |
| :-2   | -1300.*   | PF 1    | 80.00   | 1760.77   | 1762.26   | 1761.95   | 1762.51   | 0.004001   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.004001    |
| 0-2   | -1400.*   | PF 1    | 80.00   | 1760.37   | 1761.86   | 1761.55   | 1762.11   | 0.004001   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.004000    |
| 0-2   | -1500.*   | PF1     | 80.00   | 1759.97   | 1761.46   | 1761.15   | 1761.71   | 0.003999   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.004000    |
| 0-2   | -1600.*   | PF 1    | 80.00   | 1759.57   | 1761.06   | 1760.75   | 1761.31   | 0.004000   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.004000    |
| 0-2   | -1700.*   | PF 1    | 80.00   | 1759.17   | 1760.66   | 1760.35   | 1760.91   | 0.004001   | 3.95     | 20.26     | 18.36     | 0.66         | 1.49         | 0.003989    |
| 0-2   | -1800.*   | PF 1    | 80.00   | 1758.77   | 1760.27   | 1759.95   | 1760.51   | 0.003977   | 3.94     | 20.30     | 18.37     | 0.66         | 1.50         | 0.003925    |
| 0-2   | -1900.*   | PF 1    | 80.00   | 1758.37   | 1759.88   | 1759.55   | 1760.11   | 0.003874   | 3.90     | 20.49     | 18.44     | 0.65         | 1.51         | 0.004716    |
| 0-2   | -1992.56  | PF 1    | 80.00   | 1758.00   | 1759.35   | 1759.18   | 1759.67   | 0.005867   | 4.52     | 17.71     | 17.51     | 0.79         | 1.35         | 0.008603    |
| -2    | -2000     | PF 1    | 89.00   | 1757.97   | 1759.17   | 1759.17   | 1759.60   | 0.013101   | 5.27     | 16.88     | 19.87     | 1.01         | 1.20         | 0.012058    |
| 0-2   | -2039.97  | PF 1    | 89.00   | 1757.28   | 1758.43   | 1758.53   | 1759.03   | 0.014778   | 6.23     | 14.28     | 16.29     | 1.17         | 1.15         | 0.013814    |
| 0-2   | -2079.9*  | PF 1    | 89.00   | 1756.56   | 1757.63   | 1757.81   | 1758.36   | 0.018603   | 6.83     | 13.03     | 15.82     | 1.33         | 1.07         | 0.016526    |
| 0-2   | -2119.9*  | PF 1    | 89.00   | 1755.83   | 1756.92   | 1757.08   | 1757.61   | 0.017629   | 6.69     | 13.31     | 15.93     | 1.29         | 1.09         | 0.018106    |
| 0-2   | -2159.9*  | PF 1    | 89.00   | 1755.10   | 1756.18   | 1756.35   | 1756.89   | 0.018146   | 6.77     | 13.16     | 15.87     | 1.31         | 1.08         | 0.017885    |
| 0-2   | -2200     | PF 1    | 89.00   | 1754.38   | 1755.46   | 1755.63   | 1756.17   | 0.017906   | 6.73     | 13.23     | 15.90     | 1.30         | 1.08         | 0.018026    |
| 0-2   | -2239.9*  | PF 1    | 89.00   | 1753.92   | 1755.06   | 1755.17   | 1755.67   | 0.015100   | 6.29     | 14.16     | 16.25     | 1.19         | 1.14         | 0.013937    |
| 0-2   | -2279.9*  | PF 1    | 89.00   | 1753.46   | 1754.64   | 1754.72   | 1755.20   | 0.013337   | 5.99     | 14.87     | 16.50     | 1.11         | 1.18         | 0.012804    |
| 0-2   | -2319.91  | PF 1    | 92.00   | 1753.00   | 1754.21   | 1754.28   | 1754.77   | 0.013470   | 6.05     | 15.21     | 16.63     | 1.11         | 1.20         | 0.012170    |
| 0-2   | -2419.9*  | PF 1    | 92.00   | 1751.00   | 1751.99   | 1752.28   | 1752.93   | 0.025420   | 7.79     | 11.81     | 15.35     | 1.56         | 0.99         | 0.018045    |
| 0-2   | -2519.9   | PF 1    | 92.00   | 1749.00   | 1750.13   | 1750.28   | 1750.81   | 0.016885   | 6.62     | 13.90     | 16.15     | 1.26         | 1.12         | 0.020503    |
| 0-2   | -2544.9*  | PF 1    | 92.00   | 1748.50   | 1749.58   | 1749.78   | 1750.34   | 0.019368   | 6.99     | 13.16     | 15.87     | 1.35         | 1.08         | 0.018063    |
| 0-2   | -2569.9*  | PF 1    | 92.00   | 1748.00   | 1749.07   | 1749.28   | 1749.84   | 0.019636   | 7.03     | 13.09     | 15.85     | 1.36         | 1.07         | 0.019502    |
| 0-2   | -2594.9*  | PF 1    | 92.00   | 1747.50   | 1748.57   | 1748.78   | 1749.34   | 0.019761   | 7.05     | 13.06     | 15.83     | 1.37         | 1.07         | 0.019698    |
| -2    | -2619.9*  | PF 1    | 92.00   | 1747.00   | 1748.06   | 1748.28   | 1748.85   | 0.020254   | 7.12     | 12.93     | 15.78     | 1.39         | 1.06         | 0.020005    |
| 0-2   | -2644.9*  | PF 1    | 92.00   | 1746.50   | 1748.17   | 1747.78   | 1748.41   | 0.004515   | 3.91     | 23.55     | 19.41     | 0.63         | 1.67         | 0.002647    |
| 0-2   | -2669.88  | PF 1    | 92.00   | 1746.00   | 1748.19   | 1747.28   | 1748.30   | 0.001737   | 2.67     | 34.50     | 22.54     | 0.38         | 2.19         |             |



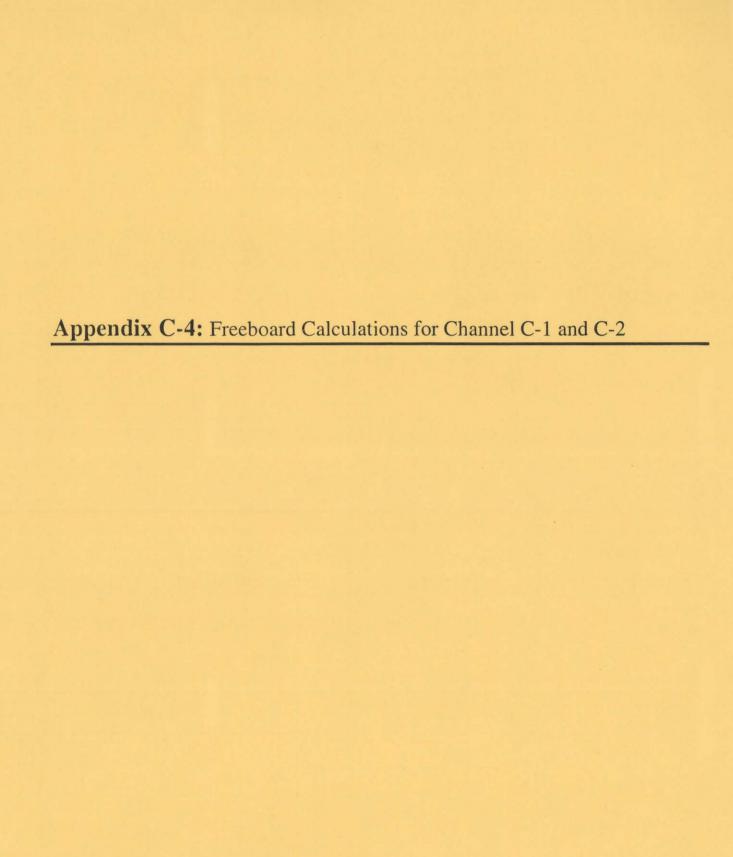








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Channel 1 - (HEC-RAS Channel - C1)

| Station      | Depth of Weterift)                     | Velocity (file) | Charmel Top Welth (ft) | Fromba No. | Бызжен/Бырмесей               | Freetopant (ft) | (kuper Elevation (ft) | Required Depth (ft) | Minimum Channel Depth (ft) |
|--------------|--|-----------------|------------------------|------------|-------------------------------|-----------------|-----------------------|---------------------|----------------------------|
| -1100        | 0.70                                   | 0.39            | 13.62                  | 6.00       | 10,000,750,00                 | 1.0             | G 000                 | 1,70                | 3.00                       |
| -111G."      | 0.74                                   | 0.37            | 13.88                  | 0.08       | <b>有效的</b>                    | 10              | 0.00                  | 1.24                | 3.00                       |
| 4912O        | 0.78                                   | 12.24           | 14 (3)                 | 200        | #ACCES.                       | 1.0             | 0.00                  | \$.2%               | 3(2)                       |
| -1130°       | 0.82                                   | 0.32            | 14.33                  | 2//        | \$4.5×.958.86                 | 1.0             | \$ 00                 | 1.52                | 3.00                       |
| 481#CL*      | 0.36                                   | 0.30            | 14 54                  | 0.07       | NACCOTICNI                    | 1.0             | 0.00                  | 1.86                | 3.00                       |
| 41120        | 0.90                                   | 0.29            | 14.80                  | 0.04       | W-Exc#90046                   | 10              | 0.00                  | 1.60                | 3.00                       |
| -116Q        | ************************************** | 0.27            | 15.04                  | 0.00       | 35/27/85¢i                    | 18              | 0.00                  | 154                 | 3 30                       |
| -1170        | £2 \$48                                | 0.26            | 15.28                  | 0.00       | 10.2009 (E.O.)                | 1.02            | 0.00                  | 1.38                | 330                        |
| *3180°       | 1.02                                   | 0.25            | 15.52                  | 0.04       | SANTO FEBRUAR                 | 1.0             | 0.00                  | 2.52                | 3.00                       |
| :1190        | 1.06                                   | 0.23            | 18.78                  | 0.00       | SLEW OBK SK                   | 1.0             | 0.50                  | 2.06                | 3.80                       |
| ~ \$2500     | # \$4                                  | 301             | 1 & LG2                | 0.62       | %,22:555(3)                   | 1 ()            | 540                   | 134                 | 3 (2)                      |
| : 2.2502     | £0.94                                  | 3.61            | 15.03                  | 0.62       | ndorensi                      | 1.0             | 0.00                  | \$ <b>24</b>        | 3.23                       |
| ×1.36361.1   | 0.94                                   | 301             | 15.01                  | 0.63       | autorateral                   | 1:0             | 0.00                  | 1.94                | 3.520                      |
| ×1.35G       | Ø.94                                   | 3 61            | 18.01                  | 5.62       | <b>第4章的</b> 关系的               | 1.0             | 0.00                  | 1.94                | 3.40                       |
| -14CS)."     | ************************************** | 3.61            | 15.22                  | 2.62       | %-24/18E2i                    | 10              | 0.00                  | 1.54                | 333                        |
| -1450        | © 34                                   | 3.01            | 18.03                  | 0.80       | ALEXTRES!                     | 1.0             | 0.00                  | 3.34                | 330                        |
| ~150G        | 0.94                                   | 301             | 15.00                  | B #Q       | \$4.50(798).64                | 1.0             | 0.60                  | 1.94                | 3.00                       |
| *1880        | S P4                                   | 3.65            | 16.63                  | 0.62       | \$0.600 (\$100) (\$0.00)      | 10              | 0.00                  | 1.94                | 3.00                       |
| ×15(2)       | 98                                     | 2.36            | 15.29                  | SAT        | 31,2073836                    | 1.0             | 5.00                  | * <b>*</b>          | 100                        |
| 1860         | 0.98                                   | 2 85            | 15.26                  | 9.58       | %.EXC2780/6                   | 10              | 0.00                  | 1.98                | 3.00                       |
| = \$.7(3E).* | 1.534                                  | 2 £4            | 15.61                  | 0.82       | 84,600,000,001                | 1.6             | 0.00                  | 2 04                | 2.80                       |
| -1750.       | 1.14                                   | 2.23            | 18,23                  | 0.44       | Solder PRESS                  | 3.0             | 0.00                  | 2.54                | 3.(4)                      |
| -1800        | 24                                     | 2.50            | 5 <i>7 17</i> 4        | 0.26       | #.Ex.758.#i                   | 1.0             | 0.00                  | 2.28                | 330                        |
| -1850        | ************************************** | 1.70            | 1807                   | 0.29       | make reason                   | 1.0             | 0.00                  | 2.44                | 3 (8)                      |
| -1900        | 1.52                                   | 3.46            | 19.14                  | 0.24       | audocemical                   | 1 (3            | 0.00                  | 2 42                | 3.20                       |
| -138Q        | 1 8 1                                  | 1.25            | 23.74                  | 8.19       | WARE PROB                     | 10              | 600                   | 2.61                | 3(2)                       |
| -0020        | 200                                    | * 39            | 21.34                  | 0.16       | 39.43/128/W                   | 1.0             | 0.00                  | 320                 | 3.32                       |
| -27.000      | 1.62                                   | 2.24            | 19 15                  | 2.85       | 80.80(1980)86                 | 1 %             | 0.13                  | 3.12                | 4.(2)                      |
| 2015         | 167                                    | 5.24            | 19.14                  | 0.86       | #PERCHANCES                   | 10              | 0.13                  | 3.12                | 4.50                       |
| -218G        | 1 52                                   | 9.36            | 19.12                  | 0.86       | \$4.500 A                     | 1.0             | 6.13                  | 2.12                | 4 00                       |
| -2125        | 1.62                                   | 3.32            | 1979                   | 0.86       | \$0.60K;10K;46                | 1.0             | 0.13                  | 3.12                | <b>*</b> (30)              |
| -2150        | 1.63                                   | 8.25            | 19.19                  | 8.85       | 84.837.590.84                 | 1.0             | 0.13                  | 2.13                | <b>4</b> .333              |
| -\$1.7\$.    | 1,64                                   | 6.23            | 19.21                  | D 84       | \$00.8007/FB\$().88           | 1.0             | 0.13                  | 2.14                | 4.00                       |
| 4200         | 1 🔯                                    | 8.33            | 19.14                  | G-86       | 36,630,000,000                | 1.0             | 0.13                  | 3.12                | * 35                       |
| -32232.      | 1.62                                   | 5.33            | 12.14                  | 0.86       | 44.45C.1708;36                | 1.8             | 0.13                  | 3.17                | * (11)                     |
| -2245A       | 1.63                                   | 5.22            | 19 15                  | G.86       | \$1.000 PBC/ski               | 1.0             | G 13                  | 3.13                | 4.00                       |
| -2284 FB     | 163                                    | 5.31            | 19.17                  | Q 86       | \$6.素30.37等6.303              | 140             | 0.13                  | 3.13                | 4 (%)                      |
| 4373.86      | 163                                    | \$.30           | 19.19                  | 0.86       | 91.84(778134                  | 1.0             | G 13                  | 3.13                | +30                        |
| -2445 1°     | 1.63                                   | 5.29            | 1970                   | 0.8%       | 56.Ex.(56.06)                 | 1.0             | 0.00                  | 3.63                | 3.53                       |
| 42.18.47     | 1.82                                   | 4.67            | 29.29                  | 6.7        | quint of the last             | 10              | 0.00                  | ※ 翻                 | 3.00                       |
| -2587.7      | 1.56                                   | £ 13            | 1873                   | 1.01       | \$4.5 NOTE TO SEE             | 1.3             | 3.00                  | 2.74                | 3.00                       |
| -2687.7*     | 1.26                                   | 8.29            | 18.99                  | 1.46       | 94(00)7575476                 | 1.3             | a é                   | 2.48                | 355                        |
| -2787.Y      | 1.45                                   | 6.71            | 18.12                  | 1,14       | negatoritesi                  | 1.2             | 6.00                  | 7.64                | 3 (8)                      |
| -2887.T      | 1.33                                   | 7.58            | 17.26                  | 1.34       | support (Real                 | 1.2             | 9.00                  | 2.54                | 3.00                       |
| ·2087.7      | \$ AG                                  | 7.03            | 17.82                  | 1,31       | 30.40年代7年2月                   | 1.2             | 0.00                  | 2.69                | 3.55                       |
| -3688 2.3°   | 1.35                                   | 7.40            | 178)                   | 3.3        | supercrisia:                  | 12              | 0.0                   | 2.34                | 30                         |
| -3182.7"     | 138                                    | 7.17            | 17.70                  | 1.24       | supercritical                 | 12              | 876                   | 2.58                | 3.99                       |
| -3267.7"     | 1.36                                   | 7.31            | 17.58                  | 1.28       | manererenal                   | 1.2             | 9.00                  | 2.50                | 3.00                       |
| 43387.7°     | 1.37                                   | 7.23            | 17.65                  | 1.28       | 10.504F1/F18/36               | 1.2             | 9.0                   | 2.57                | 3, (8)                     |
| -3487.Y°     | 1.36                                   | 7.32            | 13.83                  | 1,23       | 30,000079838                  | 1.2             | 0.00                  | 3.86                | 13                         |
| -38/87 T*    | 137                                    | 7.26            | 17.60                  | 1.76       | 84,0485548.20                 | 1.2             | 0.03                  | 2.4                 | 3.93                       |
| +36/37.7*    | 1.37                                   | 7.29            | 17.60                  | 1.27       | and an expension and a second | 1.2             | 0.00                  | 2.87                | 3.60                       |
| 3787.71      | 1.37                                   | 7.29            | 17 443                 | 1.97       | napovernikai                  | 1.2             | 0.00                  | 2.57                | 3.60                       |
| -3874.3      | 1.37                                   | 7.25            | 1743                   | 1.26       | \$4,000 celesai               | 1.2             | 0.00                  | 2.5/                | 3 (4)                      |

Notes: Super Elevation dispits were applied from station -2000.00 through -2011.86 around the channel bend. Concrete Riprap material starts at station -2000.00 and confinent through station -3074.10.

Subscribinal Provincent: Fix = 0.5 × V/Gg
Supercribinal Previncent: Fix = 1 × 0.035\*V\*g\*\*
Super Elevation: Six = CV\*Lygr (C = 1.0, t = 1271)
Required Depth = Depth of Pixe + Freeboard + Super Elevation

Notes: A minimum of 19 was added for automical headsound if bredsound was loss that 19, 19 automical super elevation was less that 0.5%, 0.5% was to the total channel depth around strained brests.

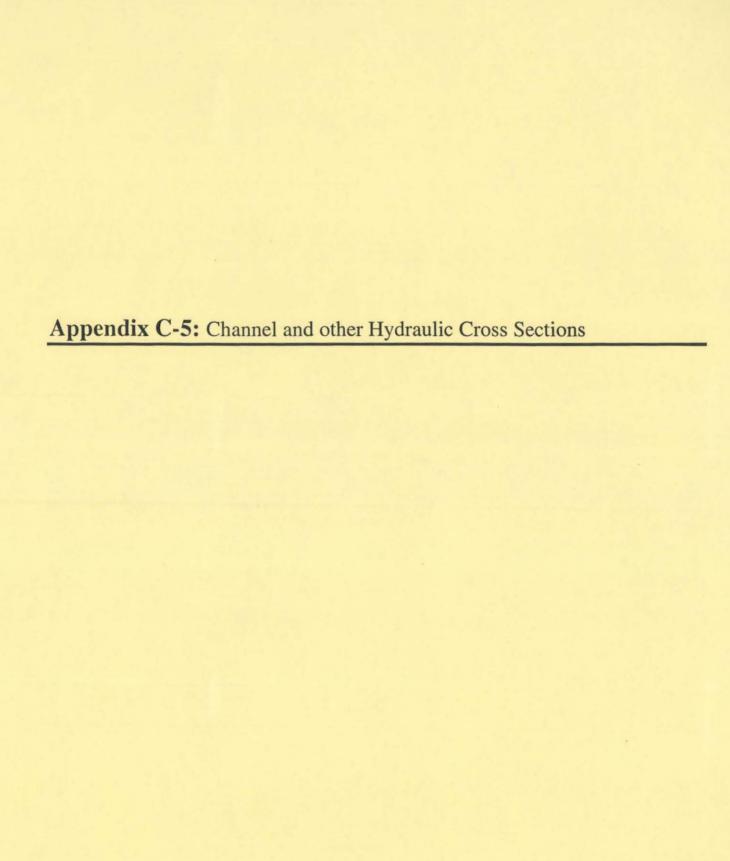
Channel 2 - (HEC-RAS Channel - C2)

| Station.     | Depth of Water(ft) | Velocity (fi/s) | Channel Top Welth (ft) | Francis No. | balantil/bapererit     | Freetwoord (11) | Super Elevation (ft) | Required Depth (ft) | Minimum Channel Depth (ft) |
|--------------|--------------------|-----------------|------------------------|-------------|------------------------|-----------------|----------------------|---------------------|----------------------------|
| +1000        | 1.43               | 3.66            | 18.36                  | 0.60        | 46.此次7例638             | 1.(X)           | 900                  | 2.49                | 3,00                       |
| +1100        | 1.43               | 3.86            | 18.36                  | 0.66        | \$4,655.75K.36         | 1.00            | 840                  | 2.49                | 355                        |
| -120X3.*     | 1.49               | 3.86            | 18.36                  | 0.66        | \$6,\$00,998036        | 1.00            | Q (X)                | \$. <b>4</b> 9      | 3 06                       |
| +1300        | 1.49               | 3 86            | 18.36                  | 9 68        | 06,8307,980,000        | 1.00            | 9 (10)               | 2.43                | 3.00                       |
| 11400        | 1.49               | 3.96            | 16.36                  | 自 前命        | \$1.000 \$100 \$1      | 1 (3)           | 9.00                 | 2.49                | 3.50                       |
| ×1500.*      | 1.49               | 3.98            | 18.36                  | 0.84        | nacenters:             | 1 (3)           | 0.00                 | 2.43                | 3.0c                       |
| *1632        | 1.#3               | 3.9%            | 18.38                  | O 柳花        | \$1.60(F9E)88          | 100             | 9.00                 | 2.49                | 3.00                       |
| +17001       | 1.49               | 3:95            | 18.36                  | 0.66        | and continues.         | t.00            | 0.00                 | 37.433              | 388                        |
| (1800)       | 1.50               | 3.94            | 10.37                  | G 464       | 84.南风干部638             | 1.00            | 0.00                 | # 940               | 3.56                       |
| 4190G."      | 1.51               | 336             | 195 香春                 | 0.4/6       | 91.810(180)(9)         | 1 (2)           | 600                  | 251                 | 3.00                       |
| 2 t 3092 5/4 | 1.35               | 4.83            | 1731                   | 0.79        | pade Pinesi            | 1.00            | 0.00                 | 238                 | 349                        |
| -20X00       | 1.20               | 5.27            | 19.87                  | 1.01        | \$1,000/05/00/05       | 1.14            | 9.00                 | 234                 | 3.50                       |
| ·\$5339.97   | 1.15               | 6.23            | 16.29                  | 1.17        | \$0.45°#(\$1.75%).\$6  | 1.18            | 613                  | S .0:4              | 3.00                       |
| 40799        | 197                | 6.83            | 19.82                  | 1,33        | \$2,000,000,000        | 1,37            | <b>21</b> \$         | 2.40                | 3.33                       |
| 3119.2       | 1.00               |                 | 18.93                  | 1.29        | \$44,0400,058,36       | 1.17            | G.15                 | 2.41                | 3.28                       |
| ·21883       | 1 (30)             | 6.77            | <b>48.87</b>           | 3.31        | SUD-STOPEUM            | 1.17            | 0.15                 | 2.40                | 3.30                       |
| -2200        | 1.08               | 6.73            | 14.(8)                 | 1.3         | to govern Pilitaria    | 1.17            | Ø:18                 | 2.40                | 3,00                       |
| 2229.9       | 3,54               | 6.73            | 16,35                  | 1.19        | NACHTE PRINT           | 1.18            | 0.13                 | 2.44                | 3.00                       |
| -2279.9"     | 3.18               | 5.399           | 16.50                  | 1.11        | SALD STATE OF THE SALE | 1,18            | 0.12                 | .49                 | 349                        |
| ·高斯1多黎1      | 9.20               | 6.05            | 18.63                  | 1,11        | go grapes e tiles avi  | 3.16            | 0.13                 | £.43                | 3.00                       |
| -2041年201    | 0.99               | 7.79            | 15.38                  | 5.A6        | <b>第5項300年代平開股(統</b> 計 | 1,13            | 0.00                 | 2.18                | 3 (90)                     |
| -25199       | 1.13               | 0.02            | 16.15                  | 1.28        | 91.57 ST (\$1.00)      | 1,17            | 0.00                 | 2.29                | 256                        |
| :2544.9"     | 1.08               | 京 排除            | 15.57                  | 1.3%        | \$1,0,0000,000,000     | 1.18            | 0.00                 | 2.26                | 369                        |
| -2569.9"     | 1.97               | 7.00            | 18,86                  | 1.26        | \$1.600FCFEC44         | 1.1施            | 0.00                 | 2.23                | 4.00                       |
| -250A.S      | 167                | 7.06            | 16.83                  | 1.37        | 36.67477788.00         | 1.38            | 0.00                 | 2.20                | 4.00                       |
| -2619.91     | 108                | 7.12            | 18.79                  | 1.3\$       | 91.8 (497.798.66)      | 1.18            | 0.00                 | 3.34                | 4:8                        |
| -2544.0      | 1.67               | 3.91            | 1941                   | G & S       | te doc PROM            | 1.00            | 0.00                 | 3.87                | 4/22                       |
| 心物的体验        | 2.19               | 2.67            | 22.54                  | 0.36        | macor ocai             | 1:20)           | 0.00                 | 3.19                | 4.00                       |

Hotes: Super Elevation depths were applied from station 2009.07 through -2019.01 around the channel bend. Concrete/Riprop material starts at station -2000.00 and continues through station -2009.86.

Subcritical Previousist: Pb = 0.5 × V<sup>2</sup>Cg Supercritical Previousist: Pb = 1 + 0.005 V<sup>2</sup>G<sup>20</sup> Super Blowatters: Se = CV<sup>2</sup>T<sub>e</sub>/gr : (C = 1.0, r = 1500) Required Depth = Depth of Plow + Previousist + Super Steveton

Hotes: A recommenced of the was added for advertical freelectory if translations was long that 19. If autophical super elevation was long that 0.5%, 0.5% was to the total character depth around character founds.



## **Worksheet for Cross Section A**

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Channel Slope
 2.85000 %

 Discharge
 40.00 ft%

Section Definitions

| Station (ft) | Elevation (fl) |      |
|--------------|----------------|------|
| 0+           | 00             | 2.50 |
| 0+           | 43             | 0.00 |
| 0+           | 97             | 2.50 |

#### Roughness Segment Definitions

| Start Station    | Er              | iding Station |                 | Roughness | Coefficient |
|------------------|-----------------|---------------|-----------------|-----------|-------------|
|                  | (0+00, 2.50)    | <b>(0</b> *   | 87, 2.50)       |           | 0,025       |
| Results          |                 |               |                 |           |             |
| Normal Depth     |                 | 0.68          | ft              |           |             |
| Elevation Range  | 0.00 to 2.50 ft |               |                 |           |             |
| Flow Area        |                 | 8.15          | ft <sup>a</sup> |           |             |
| Wetted Perimeter |                 | 23,85         | **              |           |             |
| Top Width        |                 | 23.82         | ft              |           |             |
| Normal Depth     |                 | 0.68          | ft              |           |             |
| Critical Depth   |                 | 0.80          | ft              |           |             |
| Critical Slope   |                 | 0.01239       | fvft            |           |             |
| Velocity         |                 | 4,91          | ft/s            |           |             |
| Velocity Head    |                 | 0.37          | ft              |           |             |
| Specific Energy  |                 | 1.06          | ft.             |           |             |
| Froude Number    |                 | 1,48          |                 |           |             |
| Flow Type        | Supercritical   |               |                 |           |             |
|                  |                 |               |                 |           |             |

| Workshee            | et for Cross S | ec    |
|---------------------|----------------|-------|
| GVF Input Data      |                |       |
| Downstream Depth    | 0.00           | ft    |
| Length              | 0.00           | ft    |
| Number Of Steps     | 0              |       |
| GVF Output Data     |                |       |
| Upstream Depth      | 0.00           | ħ     |
| Profile Description |                |       |
| Profile Headloss    | 0.00           | ft    |
| Downstream Velocity | Infinity       | Ns    |
| Upstream Velocity   | Infinity       | ft/s  |
| Normal Depth        | 0.68           | Ħ     |
| Critical Depth      | 0.80           | ft    |
| Channel Slope       | 0.02850        | ft/ft |

0.01239 n/n

Critical Slope

## **Cross Section A**

## Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

#### Input Data

Channel Slope

2.85000 %

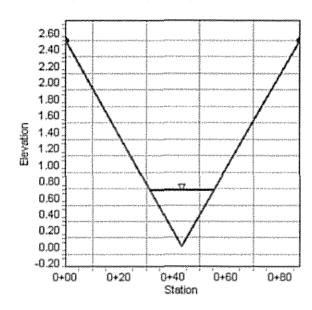
Normal Depth

0.68 ft

Discharge

40.00 ft³/s

#### Cross Section Image



Q = 40 cfs = CP-5

# **Worksheet for Cross Section B**

# Project Description

Friction Method Manning Formula
Solve For Normal Depth

### Input Data

 Channel Slope
 2.85000 %

 Discharge
 13.50 ft³/s

Section Definitions

| Station (ft) | Elevation (ft) |
|--------------|----------------|
| 0+00         | 2.40           |
| 0+74         | 0.00           |
| 1+74         | 2,40           |

| Start Station    |                 | Ending Station |           | Roughness Coefficient |   |
|------------------|-----------------|----------------|-----------|-----------------------|---|
|                  | (0+00, 2.40)    | <b>€</b>       | 74, 2.40) | 0.02                  | 5 |
| Results          |                 |                |           |                       |   |
| Normal Depth     |                 | 0.35           | ř.        |                       |   |
| Elevation Range  | 0.00 to 2.40 ft |                |           |                       |   |
| Flow Area        |                 | 4.33           | ft#       |                       |   |
| Wetted Perimeter |                 | 25.08          | ft        |                       |   |
| Top Width        |                 | 25.07          | ft        |                       |   |
| Normal Depth     |                 | 0,35           | ft        |                       |   |
| Critical Depth   |                 | 0.39           | ft        |                       |   |
| Critical Slope   |                 | 0.01576        | ft/ft     |                       |   |
| Velocity         |                 | 3,11           | fVs       |                       |   |
| Velocity Head    |                 | 0.15           | ft        |                       |   |
| Specific Energy  |                 | 0.50           | ħ         |                       |   |
| Froude Number    |                 | 1,33           |           |                       |   |
| Flow Type        | Supercritical   |                |           |                       |   |
|                  |                 |                |           |                       |   |
|                  |                 |                |           |                       |   |

# **Worksheet for Cross Section B**

| GVF Input Data      |          |       |
|---------------------|----------|-------|
| Downstream Depth    | 0.00     | ft    |
| Length              | 0.00     | ft    |
| Number Of Steps     | 0        |       |
| GVF Output Data     |          |       |
| Upstream Depth      | 0.00     | n     |
| Profile Description |          |       |
| Profile Headloss    | 0.00     | Ħ     |
| Downstream Velocity | Infinity | ft/s  |
| Upstream Velocity   | Infinity | ft/s  |
| Normal Depth        | 0.35     | ft    |
| Critical Depth      | 0.39     | #     |
| Channel Slope       | 0.02850  | ti/tt |
| Critical Slope      | 0,01576  | fvt   |

# **Cross Section B**

# **Project Description**

**Friction Method** 

Manning Formula

Solve For

Normal Depth

### Input Data

Channel Slope

2,85000 %

-755

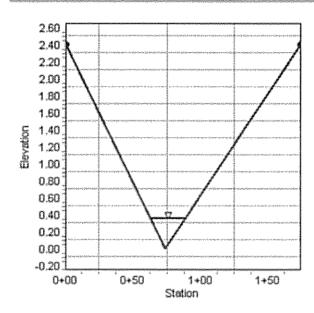
Normal Depth

0,35 n

Discharge

13.50 ft³/s

# Cross Section Image



Q = 13.50 cfs = 12 OND 4

# **Worksheet for Cross Section C**

# **Project Description**

Friction Method Manning Formula Solve For Normal Depth

# Input Data

 Channel Slope
 2.85000
 %

 Discharge
 13.50
 ft/s

Section Definitions

| Station (ft) | Elevation (ft) |  |
|--------------|----------------|--|
| 0+00         | 2.60           |  |
| 1+10         | 0.00           |  |
| 1+93         | 2.60           |  |

| Normal Depth 0.34 ft  Elevation Range 0.00 to 2.60 ft  Flow Area 4.36 ft²  Wetted Perimeter 25.46 ft  Top Width 25.45 ft  Normal Depth 0.34 ft  Critical Depth 0.38 ft  Critical Slope 0.01581 ft/ft  Velocity 3.10 ft/s  Velocity Head 0.15 ft  Specific Energy 0.49 ft  Froude Number 1.32  | Start Stati      | on En           | ding Station |                 | Roughness C | cefficient |
|---|------------------|-----------------|--------------|-----------------|-------------|------------|
| Normal Depth 0.34 ft  Elevation Range 0.00 to 2.60 ft  Flow Area 4.36 ft²  Wetted Perimeter 25.46 ft  Top Width 25.45 ft  Normal Depth 0.34 ft  Critical Depth 0.38 ft  Critical Slope 0.01581 ft/ft  Velocity 3.10 ft/s  Velocity Head 0.15 ft  Specific Energy 0.49 ft  Froude Number 1.32  |                  | (0+00, 2.60)    | (1+          | 93, 2.60)       |             | 0.025      |
| Elevation Range       0.00 to 2.60 ft         Flow Area       4,36 ft         Wetted Perimeter       25.46 ft         Top Width       25.45 ft         Normal Depth       0.34 ft         Critical Depth       0.38 ft         Critical Slope       0.01581 ft/ft         Velocity       3.10 ft/s         Velocity Head       0.15 ft         Specific Energy       0.49 ft         Froude Number       1.32   | Results          |                 |              |                 |             |            |
| Flow Area       4,36       ft²         Wetted Perimeter       25.46       ft         Top Width       25.45       ft         Normal Depth       0.34       ft         Critical Depth       0.38       ft         Critical Slope       0.01581       ft/ft         Velocity       3.10       ft/s         Velocity Head       0.15       ft         Specific Energy       0.49       ft         Froude Number       1.32       From the second sec | Normal Depth     |                 | 0.34         | A               |             |            |
| Wetted Perimeter         25.46         ft           Top Width         25.45         ft           Normal Depth         0.34         ft           Critical Depth         0.38         ft           Critical Slope         0.01581         ft/ft           Velocity         3.10         ft/s           Velocity Head         0.15         ft           Specific Energy         0.49         ft           Froude Number         1.32         Froude Number   | Elevation Range  | 0.00 to 2.60 ft |              |                 |             |            |
| Top Width         25.45         ft           Normal Depth         0.34         ft           Critical Depth         0.38         ft           Critical Slope         0.01581         ft/ft           Velocity         3.10         ft/s           Velocity Head         0.15         ft           Specific Energy         0.49         ft           Froude Number         1.32         Froude Number   | Flow Area        |                 | 4,36         | ft <sup>3</sup> |             |            |
| Normal Depth         0.34         ft           Critical Depth         0.38         ft           Critical Slope         0.01581         ft/ft           Velocity         3.10         ft/s           Velocity Head         0.15         ft           Specific Energy         0.49         ft           Froude Number         1.32  | Wetted Perimeter |                 | 25.46        | ħ               |             |            |
| Critical Depth         0.38 ft           Critical Slope         0.01581 ft/ft           Velocity         3.10 ft/s           Velocity Head         0.15 ft           Specific Energy         0.49 ft           Froude Number         1.32   | Top Width        |                 | 25.45        | #               |             |            |
| Critical Slope         0.01581         n/t           Velocity         3.10         ft/s           Velocity Head         0.15         ft           Specific Energy         0.49         ft           Froude Number         1.32  | Normal Depth     |                 | 0.34         | ħ               |             |            |
| Velocity 3.10 ft/s Velocity Head 0.15 ft Specific Energy 0.49 ft Froude Number 1.32   | Critical Depth   |                 | 0.38         | A               |             |            |
| Velocity Head 0.15 ft Specific Energy 0.49 ft Froude Number 1.32  | Critical Slope   |                 | 0.01581      | tin.            |             |            |
| Specific Energy 0.49 h Froude Number 1.32   | Velocity         |                 | 3.10         | ft/s            |             |            |
| Froude Number 1.32  | Velocity Head    |                 | 0.15         | ft              |             |            |
|   | Specific Energy  |                 | 0.49         | ħ               |             |            |
| Flow Type Supercritical   | Froude Number    |                 | 1.32         |                 |             |            |
|   | Flow Type        | Supercritical   |              |                 |             |            |
|   |                  |                 |              |                 |             |            |

| Wor                 | ksheet for Cross S | ection C |  |
|---------------------|--------------------|----------|--|
| GVF Input Data      |                    |          |  |
| Downstream Depth    | 0.00               | ft       |  |
| Length              | 0.00               | ft       |  |
| Number Of Steps     | Q                  |          |  |
| GVF Output Data     |                    |          |  |
| Jpstream Depth      | 0.00               | ħ        |  |
| rofile Description  |                    |          |  |
| rofile Headloss     | 0.00               | ft       |  |
| Downstream Velocity | Infinity           | ft/s     |  |
| Ipstream Velocity   | Infinity           | Na       |  |
| iormai Depth        | 0.34               | ft       |  |
| Critical Depth      | 0,38               | ft       |  |
| hannel Slope        | 0.02850            | ft/ft    |  |
| ritical Slope       | 0.01581            | futt     |  |

# **Cross Section C**

# Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

### Input Data

Channel Slope

2.85000 %

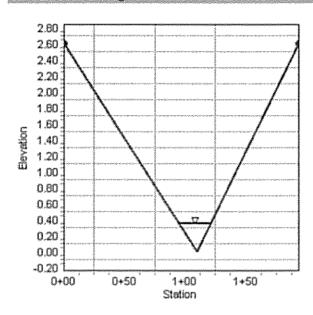
Normal Depth

0.34 ft

Discharge

13.50 n<sup>3</sup>/s

# Cross Section Image



Q= B.50 CF = 1/2 OND4

# **Worksheet for Cross Section D**

# **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

### Input Data

 Channel Slope
 1.00000
 %

 Discharge
 12.00
 ft%

Section Definitions

| Station (ft) | Elevation (ft) |      |
|--------------|----------------|------|
|              | 0+00           | 1.00 |
|              | 0*35           | 0,00 |
|              | 0+57           | 1,00 |

| Start Station    | En              | ding Station |           | Roughness Coefficient |
|------------------|-----------------|--------------|-----------|-----------------------|
|                  | (0+00, 1.00)    | <b>()</b> *  | 57, 1.00) | 0.025                 |
| Results          |                 |              |           |                       |
| Normal Depth     |                 | 0.44         | ft        |                       |
| Elevation Range  | 0.00 to 1.00 ft |              |           |                       |
| Flow Area        |                 | 5.54         | 11*       |                       |
| Wetted Perimeter |                 | 25.15        | ft        |                       |
| Top Width        |                 | 25,13        | Ħ         |                       |
| Normal Depth     |                 | 0.44         | ft        |                       |
| Critical Depth   |                 | 0.41         | ħ         |                       |
| Critical Slope   |                 | 0.01551      | tvn       |                       |
| Velocity         |                 | 2.17         | Ns        |                       |
| Velocity Head    |                 | 0,07         | ft        |                       |
| Specific Energy  |                 | 0.51         | ft        |                       |
| Froude Number    |                 | 0.81         |           |                       |
| Flow Type        | Subcritical     |              |           |                       |
|                  |                 |              |           |                       |

|                     | Worksheet for Cross S | ection D |
|---------------------|-----------------------|----------|
| GVF Input Data      |                       |          |
| Downstream Depth    | 0.00                  | ft       |
| Length              | 0.00                  | ft       |
| Number Of Steps     | O                     |          |
| GVF Output Data     |                       |          |
| Upstream Depth      | 0.00                  | ft       |
| Profile Description |                       |          |
| Profile Headloss    | 0.00                  | A        |
| Downstream Velocity | Infinity              | ft/s     |
| Upstream Velocity   | Infinity              | ft/s     |
| Normal Depth        | 0.44                  | ft       |
| Critical Depth      | 0.41                  | R        |

0.01000 n/n

0.01551 n/n

Channel Slope Critical Slope

# **Cross Section D**

# Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

#### Input Data

Channel Slope

1,00000 %

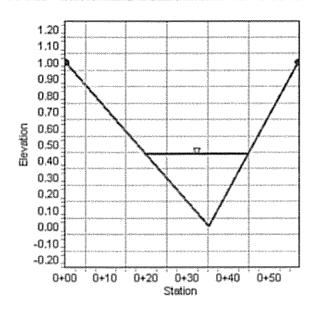
Normal Depth

0.44 ft

Discharge

12.00 111/3

# Cross Section Image



Q= 12 cts = OND5

# **Worksheet for Cross Section E**

### **Project Description**

Friction Method Manning Formula Solve For Normal Depth

# Input Data

 Channel Slope
 1.00000 %

 Discharge
 24.00 ft³/s

Section Definitions

| State Survey and Mark State State Survey   |  |   |
|--|--|---|
| MELLINGER CONTROL TO SUCCIMENTAL METERS OF   |  |   |
| Station (ft)   | en en la companya de | vation (ft)   |
| 19-44 (1444-147) (1446-147) (1446-147) (1446-147) (1446-147) (1446-147) (1446-147) (1446-147) (1446-147) (1466 |  | allered of the transfer of the state of the |
|  | 0+00   | 1,00  |
|  | 0+51   | 0.00  |
|  | 0+89   | 1,00  |

| Start Station    | En              | ding Station |           | Roughness Coeff | icient |
|------------------|-----------------|--------------|-----------|-----------------|--------|
|                  | (0+00, 1.00)    | (0+          | 89, 1.00) |                 | 0.025  |
| Results          |                 |              |           |                 |        |
| Normal Depth     |                 | 0.48         | ħ         |                 |        |
| Elevation Range  | 11,00.1 at 00.0 |              |           |                 |        |
| Flow Area        |                 | 10.40        | ft²       |                 |        |
| Wetted Perimeter |                 | 43.03        | Ħ         |                 |        |
| Top Width        |                 | 43,02        | ft        |                 |        |
| Normal Depth     |                 | 0,48         | ft        |                 |        |
| Critical Depth   |                 | 0.45         | <b>\$</b> |                 |        |
| Critical Slope   |                 | 0.01500      | tun       |                 |        |
| Velocity         |                 | 2.31         | tVs       |                 |        |
| Velocity Head    |                 | 0.08         | ft        |                 |        |
| Specific Energy  |                 | 0.57         | ft        |                 |        |
| Froude Number    |                 | 0.83         |           |                 |        |
| Flow Type        | Subcritical     |              |           |                 |        |
|                  |                 |              |           |                 |        |
|                  |                 |              |           |                 |        |

| Works               | heet for Cross S | ecti  |
|---------------------|------------------|-------|
| GVF Input Data      |                  |       |
| Downstream Depth    | 0.00             | ft    |
| Length              | 0.00             | ft    |
| Number Of Steps     | 0                |       |
| GVF Output Data     |                  |       |
| Jpstream Depth      | 0.00             | ft    |
| Profile Description |                  |       |
| Profile Headloss    | 0.00             | ft    |
| Downstream Velocity | Infinity         | ft/s  |
| Upstream Velocity   | Infinity         | flis  |
| Normal Depth        | 0.48             | ft    |
| Critical Depth      | 0.45             | ft    |
| Channel Slope       | 0,01000          | ft/ft |
| Critical Slope      | 0.01500          | ft/ft |

# **Cross Section E**

# Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

### Input Data

Channel Slope

1.00000 %

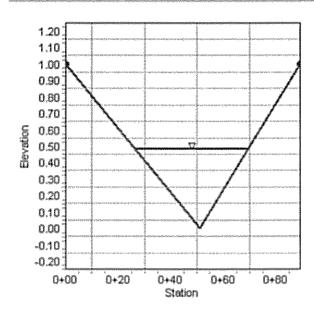
Normal Depth

0.48 ft

Discharge

24.00 ft³/s

### **Cross Section Image**



Q = 24 cfs = ONDII

# **Worksheet for Cross Section F**

# **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

# Input Data

 Channel Slope
 0.40000 %

 Discharge
 12.00 ft³/s

Section Definitions

| Station (ft) Elevi | ation (ft) |
|--------------------|------------|
| 0+00               | 2.30       |
| 0+25               | 0.49       |
| 0+48               | 0.00       |
| 0+73               | 0.00       |
| 0+80               | 2.30       |
|                    |            |

| Start Station    | Enc             | ling Station |           | Roughness Coefficient |
|------------------|-----------------|--------------|-----------|-----------------------|
|                  | (0+00, 2.30)    | (O+          | 80, 2,30) | 0.025                 |
| Results          |                 |              |           |                       |
| Normal Depth     |                 | 0.27         | ft        |                       |
| Elevation Range  | 0,00 to 2,30 ft |              |           |                       |
| Flow Area        |                 | 8.65         | M³        |                       |
| Welled Perimeter |                 | 38.63        | ħ         |                       |
| Top Width        |                 | 38.58        | t         |                       |
| Normal Depth     |                 | 0.27         | ħ         |                       |
| Critical Depth   |                 | 0.18         | ft        |                       |
| Critical Slope   |                 | 0.01690      | ft/ft     |                       |
| Velocity         |                 | 1.39         | ft/s      |                       |
| Velocity Head    |                 | 0.03         | ħ         |                       |
| Specific Energy  |                 | 0.30         | ft        |                       |
| Froude Number    |                 | 0.52         |           |                       |
| Flow Type        | Subcritical     |              |           |                       |

| Worksheet for Cross Section F |          |       |  |
|-------------------------------|----------|-------|--|
| GVF Input Data                |          |       |  |
| Downstream Depth              | 0.00     | ft    |  |
| Length                        | 0.00     | ft    |  |
| Number Of Steps               | 0        |       |  |
| GVF Output Data               |          |       |  |
| Upstream Depth                | 0.00     | ft    |  |
| Profile Description           |          |       |  |
| Profile Headloss              | 0.00     | 11    |  |
| Downstream Velocity           | Infinity | ti/s  |  |
| Upstream Velocity             | Infinity | ft/s  |  |
| Normal Depth                  | 0.27     | ft    |  |
| Critical Depth                | 0.18     | ft    |  |
| Channel Slope                 | 0.00400  | ft/ft |  |
| Critical Slope                | 0.01690  | ft/ft |  |

### **Cross Section F**

### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

#### Input Data

Channel Slope

0.40000 %

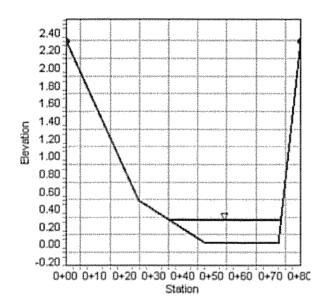
Normal Depth

0.27 n

Discharge

12.00 ft<sup>3</sup>/s

#### **Cross Section Image**



$$F_0 = 0.5 + \frac{V^2}{2g} = 0.5 + \frac{(1.39)^2}{2(31.2)} = 0.53$$
 :  $F_0 = 1.4$ 

# **Worksheet for Cross Section G**

### **Project Description**

Friction Method Manning Formula Solve For Normal Depth

### Input Data

 Channel Slope
 0.40000 %

 Discharge
 23.00 ft³/s

Section Definitions

| Station (ft) Elev | ation (ft) |  |
|-------------------|------------|--|
| 0+00              | 3.00       |  |
| 0+09              | 0.00       |  |
| 0+31              | 0.00       |  |
| 0+40              | 3.00       |  |
|                   |            |  |

| Start Sta        | tion E          | nding Station |              | Roughness Coefficient |       |
|------------------|-----------------|---------------|--------------|-----------------------|-------|
|                  | (0+00, 3.00)    | (0+           | 40, 3.00)    |                       | 0.025 |
| Results          |                 |               |              |                       |       |
| Normal Depth     |                 | 0.46          | ft.          |                       |       |
| Elevation Range  | 0.00 to 3,00 ft | •             |              |                       |       |
| Flow Area        |                 | 10.73         | <b>1</b> 1.2 |                       |       |
| Wetted Perimeter |                 | 24.90         | ft           |                       |       |
| Top Width        |                 | 24.75         | ft           |                       |       |
| Normal Depth     |                 | 0.46          | ft           |                       |       |
| Critical Depth   |                 | 0.32          | ft           |                       |       |
| Critical Slope   |                 | 0.01359       | fVft         |                       |       |
| Velocity         |                 | 2.14          | ft/s         |                       |       |
| Velocity Head    |                 | 0.07          | **           |                       |       |
| Specific Energy  |                 | 0.53          | ft           |                       |       |
| Froude Number    |                 | 0,57          |              |                       |       |
| Flow Type        | Subcritical     |               |              |                       |       |

| Worksheet for Cross S | ection G |
|-----------------------|----------|
|                       |          |
| 0.00                  | ft.      |
| 0.00                  | 我        |
| 0                     |          |
|                       |          |
| 0.00                  | ft       |

| Upstream Depth      | 0.00     | ft    |
|---------------------|----------|-------|
| Profile Description |          |       |
| Profile Headloss    | 0,00     | ft    |
| Downstream Velocity | Infinity | ft/s  |
| Upstream Velocity   | Infinity | ft/s  |
| Normal Depth        | 0.46     | ft    |
| Critical Depth      | 0.32     | ft    |
| Channel Slope       | 0.00400  | ft/ft |
| Critical Slope      | 0.01359  | t/ft  |
|                     |          |       |

**GVF Input Data** 

Downstream Depth

Number Of Steps

**GVF Output Data** 

Length

### **Cross Section G**

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

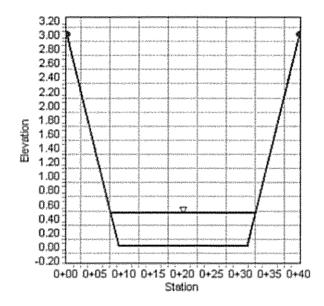
#### Input Data

 Channel Slope
 0.40000
 %

 Normal Depth
 0.46
 ft

 Discharge
 23.00
 ft%s

#### **Cross Section Image**



$$F_0 = 0.5 + \frac{v^2}{20} = 0.5 + \frac{(2.14)^2}{2(32.2)} = 0.57$$
 :  $F_b = 1$ ft

Total Depth = 1+0.4697 = 1.4697.

# **Worksheet for Cross Section H**

### Project Description

Friction Method Solve For Manning Formula Normal Depth

# Input Data

Channel Slope Discharge 0.40000 % 33.00 ft<sup>2</sup>/s

Section Definitions

| 0+00 3.00<br>0+09 0.00<br>0+19 0.00<br>0+94 0.80<br>1+06 1.80<br>1+16 2.80 | Station (ft) Elev | ation (ft) |  |
|--|-------------------|------------|--|
| 0+19 0.00<br>0+94 0.80<br>1+06 1.80  | 0+00              | 3.00       |  |
| 0+94   | 0+09              | 0.00       |  |
| 1+06   | O+19              | 0.00       |  |
|  | 0+94              | 0.80       |  |
| 1+16 2.80  | 1+06              | 1.80       |  |
|  | 1+16              | 2.80       |  |

| Start Station    |  | nding Station |   | Roughness Coefficie                     | The second secon |
|------------------|--|---------------|---|---|--|
|                  | (0+00, 3.00)   | (1*           | 16, 2.80)                               |   | 0,025  |
| Results          |  |               |   |   |  |
| Normal Depth     |  | 0.53          | ft                                      |   |  |
| Elevation Range  | 0.00 to 3,00 ft  |               |   |   |  |
| Flow Area        |  | 19.16         | ft <sup>3</sup>                         |   |  |
| Wetted Perimeter |  | 61.80         | ħ                                       |   |  |
| Top Width        |  | 61,71         | ft                                      |   |  |
| Normal Depth     |  | 0.53          | A                                       |   |  |
| Critical Depth   |  | 0.40          | ft                                      |   |  |
| Critical Slope   |  | 0.01464       | tvn.                                    |   |  |
| Velocity         |  | 1.72          | ft/s                                    |   |  |
| Velocity Head    |  | 0.05          | ħ                                       |   |  |
| Specific Energy  |  | 0.58          | ħ                                       |   |  |
| Froude Number    | kkirin-karis makamulakalistin-vanhimaapaa-karin-aaabistiimismismi misistikansistiisi | 0.54          | *************************************** | *************************************** |  |

|                     | Worksheet   | for Cross S | ec    |
|---------------------|-------------|-------------|-------|
| Results             |             |             |       |
| Flow Type           | Subcritical |             |       |
| GVF Input Data      |             |             |       |
| Downstream Depth    |             | 0.00        | ft    |
| Length              |             | 0.00        | ft    |
| Number Of Steps     |             | 0           |       |
| GVF Output Data     |             |             |       |
| Upstream Depth      |             | 0.00        | ft    |
| Profile Description |             |             |       |
| Profile Headloss    |             | 0.00        | ft    |
| Downstream Velocity |             | Infinity    | Ws    |
| Upstream Velocity   |             | Infinity    | tus.  |
| Normal Depth        |             | 0.53        | ft    |
| Critical Depth      |             | 0.40        | ft    |
| Channel Slope       |             | 0.00400     | fufi  |
| Critical Slope      |             | 0.01464     | fuffi |

# **Cross Section H**

#### **Project Description**

**Friction Method** 

Manning Formula

Solve For

Normal Depth

#### Input Data

Channel Slope

0.40000

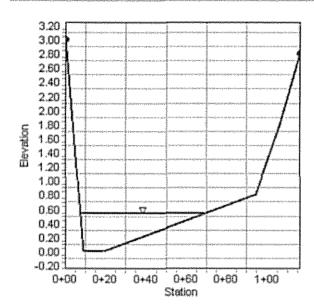
Normal Depth

0.53 ft

Discharge

33.00 ft³/s

#### Cross Section Image



$$F_0 = 0.5 + \frac{V^2}{28} = 0.5 + \frac{(1.72)^2}{2(32.2)} = 0.55$$
 ...  $F_0 = 1.64$ .

$$Se = \frac{CV^2T\omega}{gv} = \frac{1.0(1.72)^2(10.71)}{32.2(100)} = 0.06f$$
 :  $Se = 0.5ft$ .
Subcritical Superelevative

# **Worksheet for Cross Section I**

# **Project Description**

Friction Method Manning Formula Solve For Normal Depth

### Input Data

0.40000 Channel Slope 33.00 ft³/s Discharge

Section Definitions

| Station (ft) Elev | ation (ft) |  |
|-------------------|------------|--|
| 0+00              | 3.00       |  |
| 0+09              | 0.00       |  |
| 0+19              | 0.00       |  |
| 0+25              | 1.52       |  |
| 0+36              | 1.65       |  |
| 0+46              | 3.00       |  |
|                   |            |  |

| Start Station    |                 | Ending Station |           | Roughness Coefficient |
|------------------|-----------------|----------------|-----------|-----------------------|
|                  | (0+00, 3.00)    | (O+            | 46, 3.00) | 0.025                 |
| Results          |                 |                |           |                       |
| Normal Depth     |                 | 0.87           | ft        |                       |
| Elevation Range  | 0.00 to 3.00 ft |                |           |                       |
| Flow Area        |                 | 11.20          | ħ²        |                       |
| Wetted Perimeter |                 | 15.12          | ħ         |                       |
| Top Width        |                 | 15,87          | A         |                       |
| Normal Depth     |                 | 0.87           | ħ         |                       |
| Critical Depth   |                 | 0.65           | ft        |                       |
| Critical Slope   |                 | 0.01133        | ft/ft     |                       |
| Velocity         |                 | 2.95           | ft/s      |                       |
| Velocity Head    |                 | 0.14           | 11        |                       |
| Specific Energy  |                 | 1,00           | ft        |                       |
| Froude Number    |                 | 0.62           |           |                       |

| Worksheet for Cross Section I |             |          |                                |  |  |  |  |  |  |  |  |
|-------------------------------|-------------|----------|--------------------------------|--|--|--|--|--|--|--|--|
| Results 2007                  |             |          |                                |  |  |  |  |  |  |  |  |
| Flow Type                     | Subcritical |          |                                |  |  |  |  |  |  |  |  |
| GVF Input Data                |             |          |                                |  |  |  |  |  |  |  |  |
| Downstream Depth              |             | 0.00     | ħ                              |  |  |  |  |  |  |  |  |
| Length                        |             | 0.00     | ft                             |  |  |  |  |  |  |  |  |
| Number Of Steps               |             | 0        |                                |  |  |  |  |  |  |  |  |
| GVF Output Data               |             |          | ull<br>Sapareshipa (1885-1891) |  |  |  |  |  |  |  |  |
| Upstream Depth                |             | 0,00     | ft                             |  |  |  |  |  |  |  |  |
| Profile Description           |             |          |                                |  |  |  |  |  |  |  |  |
| Profile Headloss              |             | 0,00     | ħ                              |  |  |  |  |  |  |  |  |
| Downstream Velocity           |             | Infinity | ft/s                           |  |  |  |  |  |  |  |  |
| Upstream Velocity             |             | Infinity | ft/s                           |  |  |  |  |  |  |  |  |
| Normal Depth                  |             | 0.87     | ft                             |  |  |  |  |  |  |  |  |
| Critical Depth                |             | 0,65     | ft                             |  |  |  |  |  |  |  |  |
| Channel Slope                 |             | 0.00400  | tt/ft                          |  |  |  |  |  |  |  |  |
| Critical Slope                |             | 0.01133  | tutt                           |  |  |  |  |  |  |  |  |

### **Cross Section I**

### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

#### Input Data

Channel Slope

0.40000 %

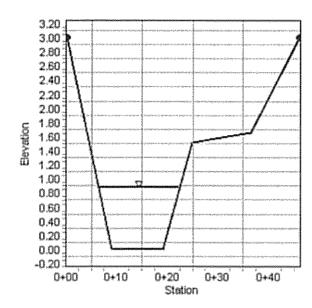
Normal Depth

0.87 n

Discharge

33.00 ft³/s

#### Cross Section Image



$$F_0 = 0.5 + \frac{V^2}{29} = 0.5 + \frac{(2.95)^2}{2(32.2)} = 0.64 \, \text{ft}$$
 :  $F_0 = 14$ .

|                       | Worksheet for Cross | Section J      |
|-----------------------|---------------------|----------------|
| Project Description   |                     |                |
| Friction Method       | Manning Formula     |                |
| Solve For             | Normal Depth        |                |
| Input Data            |                     |                |
| Roughness Coefficient | 0.02                | 5              |
| Channel Slope         | 1.4000              | 0 %            |
| Left Side Slope       | 3.0                 | 0 N/N (H:V)    |
| Right Side Slope      | 3.0                 | 0 N/h (H:V)    |
| Bottom Width          | 24,0                | 0 ft           |
| Discharge             | 33.0                | 0 ft³/s        |
| Results               |                     |                |
| Normal Depth          | 0.3                 | 7 ft           |
| Flow Area             | 9.3                 | 6 A*           |
| Wetted Perimeter      | 26.3                | 6 1            |
| Top Width             | 26.2                | 4 n            |
| Critical Depth        | 0.3                 | 8 ft           |
| Critical Slope        | 0.0128              | 1 NA           |
| Velocity              | 3.5                 | 3 <i>ft/</i> a |
| Velocity Head         | 0.1                 | 9 π            |
| Specific Energy       | 0.5                 | 7 n            |
| Froude Number         | 1.0                 | 4              |
| Flow Type             | Supercritical       |                |
| GVF Input Data        |                     |                |
| Downstream Depth      | 0.0                 | Ο π            |
| Length                | 0.0                 | 0 ft           |
| Number Of Steps       | 1                   | 0              |
| GVF Output Data       |                     |                |
| Upstream Depth        | 0.0                 | Ο π            |
| Profile Description   |                     |                |
| Profile Headloss      | 0.0                 | o n            |
| Downstream Velocity   | Infinit             | y ft/s         |
| Upstream Velocity     | Infinit             | y ft/s         |
| Normal Depth          | 0.3                 | 7 n            |
|                       |                     |                |

ħ/m

0.38 n

0.01281 h/h

0.01400

Critical Depth

Channel Slope

Critical Slope

### **Cross Section J**

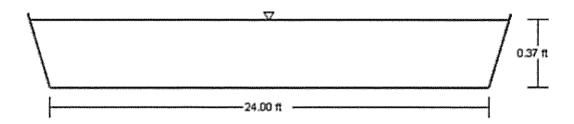
#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

| Roughness Coefficient | 0.025   |             |
|-----------------------|---------|-------------|
| Channel Slope         | 1.40000 | %           |
| Normal Depth          | 0.37    | ft          |
| Left Side Slope       | 3.00    | fuft (H;V)  |
| Right Side Slope      | 3,00    | ft/ft (H:V) |
| Bottom Width          | 24.00   | ft          |
| Discharge             | 33.00   | ft³/s       |

#### Cross Section Image



Q = 33 c/s = OND8  

$$F_{D} = 1.0 + 0.025(V)(d)^{V_{3}}$$
,  $1.0 + 0.025(3.53)(0.37)^{V_{3}}$  v.10  $\stackrel{\triangle}{}_{H1}$   
= 1.06 ft.

$$Se = CV^2T\omega = \frac{1(3.53)^2(26.24)}{(32.2)(55)} = 0.184$$

Total Depth = 1.06+ 0.18 + 0.37 = 1.61 ft.

|                       | Worksheet for  | Cross S  | ection K   |
|-----------------------|--|----------|--|
| Project Description   |  |          |  |
| Friction Method       | Manning Formula  |          |  |
| Solve For             | Normal Depth   |          |  |
| Input Data            |  |          |  |
| Roughness Coefficient |  | 0.025    |  |
| Channel Slope         |  | 33,33000 |  |
| Left Side Slope       |  | 3,00     | tvn (H:V)  |
| Right Side Slope      |  | 3,00     | ft/ft (H:V)  |
| Bottom Width          |  | 10.00    | <b>1</b>   |
| Discharge             |  | 40,00    | ft³/s  |
| Results               | ENGLES GERMANNE GERM<br>ENGLES GERMANNE GERM |          |  |
| Normal Depth          |  | 0.27     | *  |
| Flow Area             |  | 2.93     | M <sup>2</sup>   |
| Wetled Perimeter      |  | 11.72    | 1  |
| Top Width             |  | 11.63    | **   |
| Critical Depth        |  | 0.73     | R  |
| Critical Slope        |  | 0.01091  | M  |
| Velocity              |  | 13.63    | ti/s   |
| Velocity Head         |  | 2.89     | at the state of th |
| Specific Energy       |  | 3.16     | <b>13</b>  |
| Froude Number         |  | 4.78     |  |
| Flow Type             | Supercritical  |          |  |
| GVF Input Data        |  |          |  |
| Downstream Depth      |  | 0.00     | A  |
| Length                |  | 0.00     | \$ 1 m   |
| Number Of Steps       |  | 0        |  |
| GVF Output Data       |  |          |  |
| Upstream Depth        |  | 0.00     | ft .   |
| Profile Description   |  |          |  |
| Profile Headloss      |  | 0.00     | The state of the s |
| Downstream Velocity   |  | Infinity | 1Vs  |
| Upstream Velocity     |  | Infinity | Ws   |
| Normal Depth          |  | 0.27     | <b>1</b>   |
| Critical Depth        |  | 0.73     | ħ  |
| Channel Slope         |  | 0.33330  | 柳  |
| Critical Slope        |  | 0.01091  | tv/tt  |

# **Cross Section K**

### Project Description

Friction Method

Manning Formula

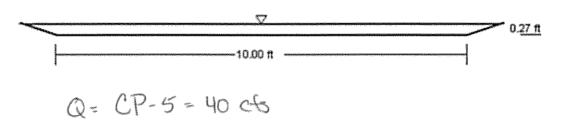
Solve For

Normal Depth

#### Input Data

| Roughness Coefficient | 0.025    |            |
|-----------------------|----------|------------|
| Channel Slope         | 33,33000 | %          |
| Normal Depth          | 0.27     | ħ          |
| Left Side Slope       | 3.00     | t/ft (H:V) |
| Right Side Slope      | 3.00     | tutt (H:V) |
| Bottom Width          | 10.00    | ħ          |
| Discharge             | 40.00    | ft'/a      |

### Cross Section Image



Page 1 of 1

| Worksheet for Cross Section L     | *************************************** |
|-----------------------------------|---|
| Project Description               |   |
| Friction Method Manning Formula   |   |
| Solve For Normal Depth            |   |
| Input Data                        |   |
| Roughness Coefficient 0.025       |   |
| Channel Slope 33.33000 %          |   |
| Left Side Slope 3.00 ft/ft (H:V)  |   |
| Right Side Slope 3.00 ft/ft (H:V) |   |
| Boltom Width 10.00 ft             |   |
| Discharge 24.00 ft³/s             |   |
| Results                           |   |
| Normal Depth 0.20 ft              |   |
| Flow Area 2.13 ft <sup>2</sup>    |   |
| Wetted Perimeter 11.27 ft         |   |
| Top Width 11.20 R                 |   |
| Critical Depth 0.53 ft            |   |
| Critical Slope 0.01193 IVIt       |   |
| Velocity 11.29 ft/s               |   |
| Velocity Head 1.98 ft             |   |
| Specific Energy 2.18 ft           |   |
| Froude Number 4.57                |   |
| Flow Type Supercritical           |   |
| GVF Input Data                    |   |
| Downstream Depth 0.00 ft          |   |
| Length 0.00 ft                    |   |
| Number Of Steps 0                 |   |
| GVF Output Data                   |   |
| Upstream Depth 0.00 ft            |   |
| Profile Description               |   |
| Profile Headloss 0.00 ft          |   |
| Downstream Velocity Infinity ft/s |   |
| Upstream Velocity Infinity ft/s   |   |
| Normal Depth 0.20 ft              |   |
| Critical Depth 0.53 ft            |   |
| Channel Slope 0.33330 ft/ft       |   |
| Critical Slope 0.01193 t/n        |   |

# **Cross Section L**

#### **Project Description**

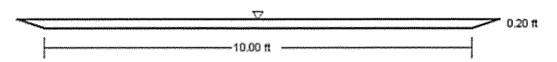
Friction Method Manning Formula
Solve For Normal Depth

### Input Data

| Roughness Coefficient | 0.025    |            |
|-----------------------|----------|------------|
| Channel Slope         | 33.33000 | 1/2        |
| Normal Depth          | 0.20     | ħ          |
| Left Side Slope       | 3.00     | fuft (H:V) |
| Right Side Slope      | 3.00     | fult (H:V) |

Bottom Width 10.00 ft
Discharge 24.00 ft\*/s

### Cross Section Image



Q = OND 11 = 24 c/s

v: 1 <u>L</u>

Appendix C-6: WSPG model for 42" Storm Drain

STORM IRAIN AMALYSIS PLUS

Original version by Los Angeles County Public Morks Portions Copyrighted by CIVILSOFT, 1986, 1987, 1989

Version 1.30 Serial Mondon STOISSIR

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#### IMPUT FILE LISTING

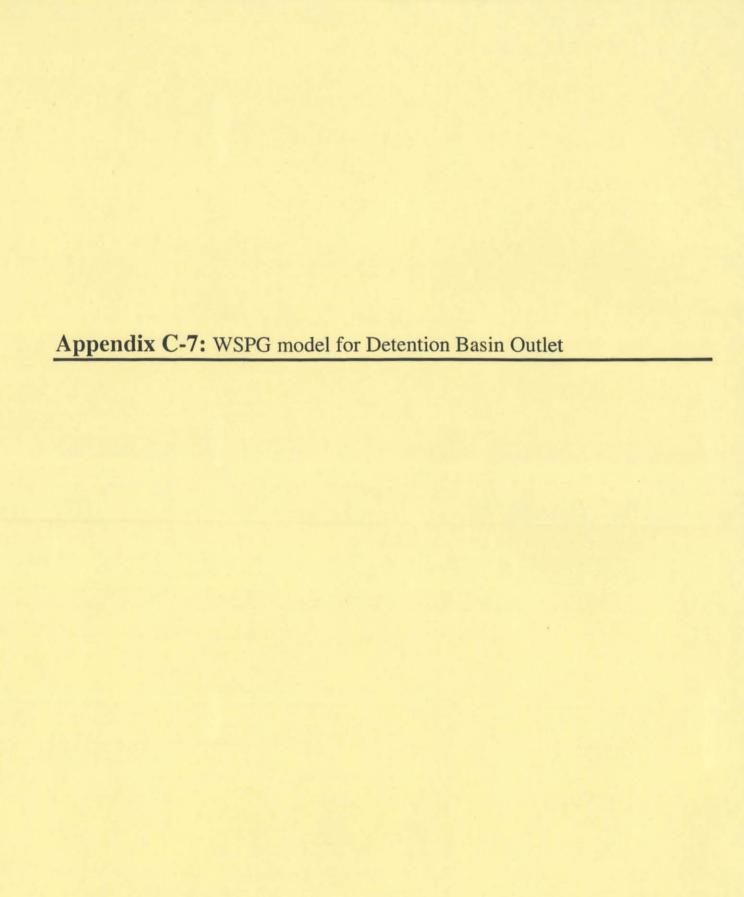
| TI BASTSIIS LAKEVILL   |   |  |   |   |
|--|---|--|---|---|
| T2 41* STORM CRAIN<br>T3 188-YEAR FLAM<br>80 1000_S81714.80 1 .01          | 23 3733.88  |  |   |   |
| ma 1006.0001234.00 1<br>m 1101.001234.00 1                                 | 13  | 4.3  |   |   |
| # 1106.201734.70 1 .01<br># 1104.201734.70 1 .01<br># 1170.261735.03 1 .01 | 1)  | \$ 2<br>\$ 3<br>\$ 4   |   |   |
| * 1175,161735.20 1 .01<br>* 1175,161735.20 1 .01<br>* 1175,161735.20 1 .01 | l)  | 66 97 97 97 97 97 97 97 97 97 97 97 97 97  |   |   |
| 8 1518.391737.00 1 .01<br>8 1940.391737.00 1 .01                           | 13  | 4 11 4   |   |   |
| 8 1849,771718.69 1 .01<br>8 1824,771738.89 1 .01<br>8 2245.811745,79 1 .01 | 3   | 3  |   |   |
| n 3250_311740_99 1 .01<br>n 3250_811740_99 1 .01                           |   | \$ 5   |   |   |
| m 2210.011740.09 1 .01<br>m 2440.021741.02 1 .01<br>m 2440.121742.12 1 .01 | ()  | \$ & \$  |   |   |
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| COOK NO TYPE PIEZE WILM  |   | SMOR.  |   |   |
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| O KLAMBYT BO 1 18 A SYSTEM CATE<br>1/0 CATA                                | TLET * * * * * * * * * * * * * * * * * * *        |  | * \$ \$2.87<br>}333.86  |   |
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| O ELECTET NO 11 12 A REACH<br>U/A DATA                                     | 1323.33 1737.28 1                                 | .613   | . FÖ.<br>Enle eniger  | 00 ,00 0<br>LE AMIPT MARIN                |
| O SLEWSSIT NO. 12 18 A REACH   | 1949.39 1717.38 1<br>812712W 187787 SECT          | , & ; 3<br>**  |   | 2 .00 1                                   |
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| 060.00 1714.00<br>ALL KNIT   |  | £.57 £7.  | 9.44  | 1.24   | 1737.79  | .38   | 2,57   |  | 3.50   | .95   | .09  | 3  | , 40   |
| 000.00 1714.00   |  | £,\$7 £7.   | 9.86  | 2 % %<br>2 × 8 d<br>6 × 8 d  | 1737.79  | .00   | 3.57   | 75 W.G   | 3.50   | .00   | .00  | \$   | ,90  |
| 25,27 .05494<br>22,27 1734.12  | 3.69 173   | 8,41 67,  | 8,45  | ,00534<br>1.11<br>20884  | .13<br>:737.92   | -1 05 50<br>-1 05 50  | 2,37   | 3.71   | 3.50   | .60   | .59  | -  | ,50  |
| 17,58 .02494<br>042.85 1734.23   |  | £.\$\$ £7.  | 9,44  | .60064<br>1.11   | .07<br>1738.51   | .00   | 2,57   | 2.71   | 3.30   | ,49   | .00  | 3  | ,90  |
| #AULIC JUKF<br>541.85 1734.21  |  | 6,44 67.  | 9.31  | 1.35   | 1730.51  | .00   | 2 - 37   | -200 105.00  | 3,80   | .90   | .00  | 8  | , 20   |
| 17,53 .00494<br>(040,44 17)4.30  | 3,34 179   | 6.64 47.  | 9.78  | 1.49   | 1739.13  | .09   | 2.37   | 3,71   | 3.50   | ,08   | - \$\$<br>\$\$<br>\$\$   | 8  | .00  |
| 30.04 .00494<br>1000.48 1714.40  | 2.25 173   | 6,64 67.  | 0 10.24   | .00757   | 1718.28  | .89   | 0.57   | 3,71   | 3,50   | .00   | .00  | 麥  | , be   |
| 10,71 .00494   | 3.16 173   | 6.64 67.  | 10.76   | ,50851<br>1,82   | 17)9.46  | .22   | 3.57   | 2,71   | 3.50   | .40   | .40  | \$   | , 29   |
| 21 .01999<br>22.8573 14.5813   | 3.34 173   | £.£7 £7.  | 10.73   | ,00901   | 1738.46  | ,24   | 3.27   | 1.39   | 2.50   | , 94  | .00  | Ş  | .00  |
| 2,10 .61999<br>68,8071 17.6311   | 3,35 173   | 6.85 KT.  | 10.23   | .50246<br>1.63   | .03<br>1738.50   | . 44  | 3,47   | 1.39   | 3,50   | ,00   | .00<br>00,   | \$   | ,\$0   |
| 1.36 .01791<br>1185.17 1734.61   | 3.15 17)   | 7,01 67.  | 9.75  | 99751<br>1,48  | 1738,49  | -20   | 2,57   | 1.39   | 3.50   | . 84  | .00  | 8  | . 20   |
| .93 .63995   |  |   |   | .09848   | .48  |   |  | 3.39   |  |   | . 22   | 7.663A   | 2  |
|  |  | LANSFILL  | WATE:   | SINFACE  | PROFILE L  |   |  |  |  |   |  |  |  |
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|  | *****  |   |   |  |  |   | *****  | (2001 (30.0°T))<br>********  | 女母母子准备分百   |   |  |  | ****   |
| 06.30 1734.78<br>19.93 .00116  |  | 7,1% %7.:   |   | \$ . 34<br>. 88887   | 1738.80  | .00   | 2.57   | 1.44   | 3,50   | , 88  | , 20<br>, 20   | 32   | .89  |
| 136,13 1734,88<br>22.09 .00116   | 2.33 173   | 7.16 67.  | 9,74  | \$.47<br>\$6749  | 1730.63  | , \$00<br>0.00  | 3,37   | 3,64   | 1,98   | . \$\$  | 30.<br>30.   | 劳  | . 94   |
| 149.22 1714.92<br>21.20 17.12  |  | 7,17 87,:   |   | 1,43   | 1729,79  | •₩  | 2.87   | 2,64   | 3.50   | ,00   | , 35   | 22   | .90  |
| (70,16 1715.0)<br>(80,00)  |  | 7,30 67,  | \$4.73  | 1.70   | 1730.90<br>.86   | ,00   | 3.27   | 3,48   | 3.50   | ,20   | , \$6<br>, \$5   | 8  | .99  |
| 170.16 1735.03<br>2.19 03799   |  | 7.30 67,  | 9 30.71   | 1.78   | 1720.90  | .20   | 2.57   | 1.39   | 3.58   | .00   | .00  | 2  | .90  |
|  |  | 7.37 67.:   |   | 1 52   | 17,30,00   | .00   | 8,37   | 1.39   | 3.,50  | , A&  | . 52<br>. 66   | 8  | . \$0  |
| 1,67 ,01991  |  |   | 3.75  | 3.48   |  | .40   |  |  | 3,3%   | .60   |  |  | 49.76  |
| 1.67 .01999<br>81.677  | 2.35 373   |   | y 20/2  | 00643  | 1739.41<br>.01   |   | \$.57  | 1,39   |  | 50.5  | , 00<br>, 00   | Ş  | .99  |
| 00000. 70.1<br>81.207  | 2.35 373<br>2.45 173   | 7.53 %Y.<br>7.67 67,  |   | ,008£9<br>1,74   |  | .88   | 2.57   |  | 3.50   | .08   |  | 400  | ,50  |
| 7,677 (0)<br>81,5173 (20,511)<br>80,6183 44.<br>11,5174 48.4711<br>80,888 (0)  | 2.35 373<br>3.45 173<br>3.27 173   | 7.67 67.<br>7.80 67.  | 9,38  | , \$3,523  | .01<br>.02. (171<br>.03. (171)   |   | 2.97   | 1.39   | 3.58<br>3.50   | .00   | ,00<br>,00   |  |  |
| 1,87 .2999<br>27,22 27,5.18<br>24 .2999<br>1174 24 .715.12<br>21,24 .25 .25<br>21,24 .25 .25   | 2.35 373<br>3.45 173<br>2.27 173<br>2.69 173   | 7.67 67.<br>7.60 67.<br>8.03 67.  | 9,38<br>9,86<br>8,45  | .00849<br>1.74<br>.00587<br>1.27   | 10.<br>12.4671<br>20.<br>17.10171  | .00   | 2.37   | 1.3%   |  | .00   | .00<br>.00<br>.00<br>.00   | Š  | , <del>2</del> 3   |
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| 1  | 2.35 373<br>3.45 173<br>2.27 173<br>2.69 173   | 7.67 67.<br>7.60 67.<br>8.03 67.  | 9.30<br>9.86<br>9.45<br>9.32  |  |  | . \$4<br>. \$4<br>. \$5<br>. \$5  | 2.37<br>2.37<br>2.37   | 1.39<br>2.73<br>2.73   | 3,50<br>3,52   | .00   | .00  | \$3<br>\$3<br>\$9  | .00  |
| 1,57   | 2.35 373<br>3.45 173<br>3.27 173<br>2.69 173<br>3.73 373   | 7.67 67.<br>7.80 67.<br>8.03 67.<br>8.39 67.  | 9.30<br>9.86<br>9.45<br>9.32  |  | # 1  | . \$4<br>. \$4<br>. \$5<br>. \$5  | 2.37<br>2.37<br>2.37   | 1.39<br>2.73<br>2.73   | 3,50<br>3,52   | .00   | .00  | \$ \$ \$   | .00  |
| 1.87 .01299  | 2.35 373  2.45 173  2.27 173  2.69 173  2.73 173  EASTTIES  42 5755  EESTW 8.  | 7.87 67.<br>7.80 67.<br>8.83 67.<br>8.59 67.  | 9.30<br>9.86<br>9.45<br>9.32  | \$28.63<br>2.33<br>2.33<br>2.33<br>2.33<br>3.33<br>3.33<br>3.33<br>3   | # 1  | . \$5<br>. \$5<br>. \$5<br>. \$5  | 2.37<br>2.37<br>2.37<br>2.37   | 1.39<br>2.73<br>2.73   | 3.50<br>3.50<br>3.50   | . 98<br>. 98<br>. 98<br>. 98  | .00  | \$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$ | .50  |
| 1.07 .03999 273.92 1735.38 24 .24 .735.32 10 .23792 10 .23792 110  | 2.35 373 2.45 173 2.27 173 2.45 173 3.73 373 42 273 42 273 42 273 47 7244 42   | 7.67 67.7, 67.7, 7.60 67. 67. 67. 67. 67. 67. 67. 67. 67. 67.   | 9.38<br>9.85<br>9.45<br>9.21<br>MATES   | . 028.63<br>1.33<br>. 025.83<br>. 025.83<br>. 026.85<br>1.07.487<br>. 026.87<br>. 026.8  | # 1  | .00<br>.00<br>.00<br>.00<br>.00<br>.00                                    | 2.57<br>2.57<br>2.57<br>2.57   | 1.39<br>2.73<br>2.73<br>2.73   | 3.50<br>3.50<br>3.50   | . 98<br>. 05<br>. 35  | .00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00  | \$<br>\$<br>\$   | .50  |
| 1  | 2.35 373 2.45 173 2.27 173 2.69 173 2.73 373 42° 570 42° 570 12273 41  | 7.67 67.7, 67.7, 7.60 67. 67. 67. 67. 67. 67. 67. 67. 67. 67.   | 9.39<br>9.49<br>9.42<br>9.21<br>MATES   | \$28.62<br>2.32<br>2.22<br>2.23<br>2.23<br>2.23<br>2.23<br>2.25<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27  | # 1  | . \$5<br>. \$5<br>. \$5<br>. \$5  | 2.57<br>2.57<br>2.57<br>2.57   | 2.78<br>2.78<br>2.78<br>3.78   | 3.50<br>3.50<br>3.50   | . 98<br>. 98<br>. 98<br>. 98  | .00  | \$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$ | .50  |
| 1.67 .012092 17.392 17.38.3 17.392 17.38.3 12.74 .02 .012093 12.74 .02 .012093 12.74 .02 .02047 12.74 .02047 | 2.35 373 2.45 173 2.27 173 2.63 173 2.73 373 42° STREETH ST. GEFTEN ST. GEFTEN ST. GEFTEN ST. 2.73 373 2.41 173  | 7.87 67.7.88 87.38 87.88  | 9.30<br>9.30<br>9.45<br>8.45<br>9.21<br>WATES   | ,00849<br>1,397<br>2,397<br>3,25<br>3,41<br>3,02849<br>1,03<br>4,03<br>4,03<br>4,03<br>4,03<br>4,03<br>4,03<br>4,03<br>4   | ## 2 ## 2 ## 2 ## 2 ## 2 ## 2 ## 2 ##  | .05<br>.05<br>.05<br>.05<br>.05<br>.05                                    | 2.97<br>2.97<br>2.97<br>2.97<br>Emirent                              | 2.75<br>2.73<br>2.73<br>2.73   | 3.50<br>3.50<br>3.50<br>3.50   | . 00<br>. 00<br>. 00<br>. 00<br>. 00<br>. 00<br>. 00<br>. 00  |  | 0<br>0<br>0<br>0<br>0<br>74633   | .50  |
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| 1 07 .01909 173.131 173.21 1735.131 173.21 1735.131 174.181 1735.131 175.181 1735.131 175.181 1735.131 175.181 1735.131 175.181 1735.131 175.181 1735.131 175.181 1735.131 175.181 175 | 2.35 173 2.45 173 2.47 173 2.47 173 2.47 173 4.2° 5734 4.2° 5734 4.2° 5734 4.3° 5734 4 | 7.87 67. 7.80 67. 2.80 67. 8.02 67. 8.02 67. 8.02 67. 8.02 67. 8.02 67. 9.24 67. 9.24 67. 9.24 67. 9.25 67. 9.26 67. 9.27 67. 9.28 67. 9.28 67.   | 9 9,30 8.46 8 8.41 40787 1782 1782 1782 1782 1782 1782 1782 1   | 。 200 年 2 日 2 日 2 日 2 日 2 日 2 日 2 日 2 日 2 日 2  | ### ##################################   | .05 .05 .05 .05 .05 .05 .05 .05 .05 .05                                   | 2.37 2.57 2.57 2.57 2.57 2.57 2.57 2.57 2.5                          | 2.33 2.73 2.73 2.73 2.73 2.73 2.73 1.33 1.33 1.33 2.73 2.73                          | 3,50<br>3,50<br>3,50<br>3,50<br>3,50<br>3,50<br>3,50<br>3,50   | . 000 | <ul> <li>(2) (2) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4</li></ul>  |  | .00 .00 .00 .00 .00 .00 .00 .00 .00 .00                                    |
| 1 67 .03999 173.33 273.92 1735.33 274.96 1735.32 175.16 175.27 175.16 175.27 175.16 175.27 175.16 175.27 175.16 175.27 175.16 175.27 175.16 175.27 175.16 175.27 17 | 2.35 173 2.45 173 2.47 173 2.47 173 2.47 173 2.47 273 2.41 173 2.41 173 2.41 173 2.42 173 2.43 173 2.45 173 2.47 174 2.47 174 2.4 | 7.87 67. 7.80 67. 2.80 67. 8.02 67. 8.02 67. 8.02 67. 8.02 67. 8.02 67. 9.24 67. 9.24 67. 9.24 67. 9.25 67. 9.26 67. 9.27 67. 9.28 67. 9.28 67.   | 9 9,30 8.46 8 8.41 40787 1782 1782 1782 1782 1782 1782 1782 1   | 。 200 年 2 日 2 日 2 日 2 日 2 日 2 日 2 日 2 日 2 日 2  | ### ##################################   | .05 .05 .05 .05 .05 .05 .05 .05 .05 .05                                   | 2.37 2.57 2.57 2.57 2.57 2.57 2.57 2.57 2.5                          | 2.33 2.73 2.73 2.73 2.73 2.73 2.73 1.33 1.33 1.33 2.73 2.73                          | 3,50<br>3,50<br>3,50<br>3,50<br>3,50<br>3,50<br>3,50<br>3,50   | . 000 | <ul> <li>(2) (2) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4</li></ul>  |  | .00 .00 .00 .00 .00 .00 .00 .00 .00 .00                                    |

| \$   | 1799.00  | 1779,45  | 3.73  | 1741.18   | \$7.5  | 0,31   | 1,07   | 1742.23   | ,00   | 2,37   |   | 3.50   | , 22  | . \$4  | 8                                       | .00   |
|--|--|--|---|---|--|--|--|---|---|--|---|--|---|--|---|---|
|  | DAAULIC .<br>1779.80   | 21343<br>1739.41   | 2.41  | 1740.00   | 67.0   | 9.30   | 1.40   | 1742.25   | , \$4   | 3,67   |   | 3.30   | .04   | .00  | 49                                      | . 20  |
| <b>%</b>   | 19.17  | .00487   |   | 1742.95   | 47.2   | 9.74   | .00684   | ·27   | ,00   |  | 2,73  | 3.50   | ,00   | .03<br>90  | -                                       | .00   |
| \$   | 1805,97  | -95487   | 2,3%  |   |  |  | ,00749   | 1742.12   |   | 3,57   | 3,73  |  |   | , 85   |   |   |
| \$ :<br>\$   | 1829.61<br>70.16   | 1738.59  | 2,3%  | 274岁,25   | 67.£   | 18.21  | 00843  | 1743.47   | . \$6   | 3,57   | 2,73  | 3,50   | .99   | .00  | *                                       | -99   |
|  | 1249.77  | 1738.69<br>.04003  | 2.17  | 1749.86   | \$7.5  | 18,71  | 4.78   | 1742.64<br>.02  | ,42   | 3.69   | 1.39  | 3.30   | .39   | , \$5<br>, \$6   | \$                                      | -84   |
| 8  | 1251.96  | 1732,78  | 2:35  | 1741,03   | \$7.8  | 10.23  | 1.63   | \$742.64  | , \$\$  | 2,87   |   | 1.59   | , (A)                                       | . 44   | 4                                       | , 99  |
| 2 :  | 1.56   | .64562<br>1718.84  | 3.35  | 1741,19   | 47,0   | 9.72   | .00792<br>1,48   | .01<br>1743.47  | , 20  | 2,87   | 1,39  | 3.50   | .00   | 26,<br>66,   | 43                                      | ,00   |
| 8  | .94<br>1934.47   | .04202<br>1738.00  | 2.45  | 17#1,33   | 47.0   | 9.30   | .00669<br>1,34   | .0;<br>1743,60  | .90   | 3,57   | 3.39  | 3,50   | 88  | .00  | 9                                       | .90   |
| \$   | .30  | .04502   |   |   |  |  | 100597   | .02   |   |  | 1,39  |  |   | 1 Se 2   | å.                                      |   |
| -\$5   | 20,77  | 1718.99  | 2.57  | 1741.48   | \$7.5  | 8.54   | .00534   | 1743.40   | .02   | 2.%  | 2.74  | 3,50   | , <u>20</u> 0                               | .02  | -                                       | ,80   |
| - \$<br>- \$<br>- \$   | 1879.74  | 1718.99  | 3.69  | 1741.80   | \$7.8  | 8,45   | .00496   | 1743,70   | . 22  | \$.67  | 2.74  | 3,50   | , \$4                                       | , 20<br>60   | 2                                       | .00   |
|  | 1984.19  | 1739.53  | 2,74  | 1742,27   | \$1.5  | \$.30  | 4,47   | 1743,34   | \$5   | 3,37   | 2.74  | 3.50   | ,\$\$                                       | . 65   | 9                                       | * \$5 W   |
| \$   | 210.47   | .00486   |   |   |  |  | _20488   | 1,02  |   |  | <b>老女子等</b>   |  |   | .95  | PAGE                                    | 5   |
|  |  |  | EAS   | TVIDE LAMETI  | L.L.   | MATER  | NUMBER OF  | Profile Li  | : N.E.3.1862  |  |   |  |   |  |   |   |
|  |  |  | 100   | STORM IRAIS<br>-YEAR FLOW   | Ī  |  |  |   |   |  |   |  |   |  |   |   |
| 0 2  | TATION   | INVEST   | DEFTH   | ¥,\$.   | Q  | V. Kan   | 786×   | SXXXX   | SUVER   | CRITICAL   |   | HUT!   | SASU/                                       | 44   |   | AYBYR   |
|  | / 801.834  | 82.8V<br>80  | of flow   | e.ey  |  |  | eead<br>By ave   | ord, el.,<br>W  | T. 17.4   | IMPTH<br>  | rand Exert  | 373.A.   | 466 383.                                    | I,B  | 7133                                    |   |
|  | ********<br>21%#   | 1740.55  | :********<br>2.74   | ***********<br>243.29   | ********<br>****   | 0.38<br>35.8   | *********<br>1.87  | **********<br>1744.35   | , 694, 644<br>182   | 2,57   | ******  | 1,38   | ,29   | *******<br>., 88   | ******                                  | .55   |
| 2877   | CHAULIC<br>1196.66   |  | 2,48  | 1742.99   | 67.0   | 9.51   | 2.41   | 1744.36   | . 20  | 2.57   |   | 1.50   | .00   | . 99<br>99   | - 6                                     | . 24  |
| .89  | 9.82   | _354#A   |   |   |  |  | ,命令主要为   | .07   |   | •  | 2.74  |  |   | ,09  |   |   |
| \$ :   | 19.55  | \$749.50<br>.00486   | 2.35  | 1743.93   | \$7,8  | 9.74   | 1.47   | 1744.42   | ., 88   | 3,87   | 2,74  | 2,30   | .00   | ,02<br>,03   | ð.                                      | -94   |
| 8 3  | 2219,7)<br>20.00   | 1740,69  | 10 × 20   | 1742,95   | 47.0   | 30.23  | 1.43   | 1744.57   | , <u>\$\$</u>   | 2,83   | 2.74  | 3.30   | ., 24                                       | .09  | *                                       | .52   |
| . A  | 2345.91  | 1740,79  | 2,47  | 1743.94   | £7.8   | 10,71  | 1.78   | 1744,74   | , \$1.00<br>1.00<br>1.00<br>1.00<br>1.00<br>1.00<br>1.00<br>1.00            | 2,67   |   | 2.50   | .00   | ,02  | \$                                      | .09   |
| *  | 2248,00  | ,03799<br>1740,88  | 2.35  | 1749,12   | 67.0   | 10.23  | .00845<br>1.61   | .S2<br>1744.76  | .00   | 2.57   | 1.29  | 3.30   | .90   | .00  | £                                       | .00   |
| - 6  | 1.07   | .53999<br>1745.44  | 2.39  | 1743,29   | 87.0   | 9.75   | .00752   | 1744.77   | . \$4   | 2.57   | 1,29  | 3.50   | . 参考  | , 60<br>, 60   | *                                       | _00   |
| 25   | . 94   | .03999   |   |   |  |  | _00669   | * \$ \$   |   |  | 2、清黄  |  | . 20  | ,05  | 2                                       | +84   |
| -53  | 16.005E  | 1740.28  | 2,49  | 1743.4)   | 67.2   | 9.38   | \$4.5<br>Yedda   | 1744,19<br>.90  | .00   | 3,87   | 1,39  | 3.30   |   | ,59  |   |   |
| \$ ;   | 2340.81  | 1740,99  | 2.57  | 1743,56   | 67,4   | 8.88   | .02534   | 1744.78   | , 84  | 2.97   | 2.72  | 1.50   | . 79  | , \$3<br>, \$9   | 4                                       | -09   |
| \$ .   | 102.88   | 1741.11  | \$,49   | 1743.79   | \$7.9  | 8.43   | 1.11   | 1744.90   | , 66  | 2,67   | 2.72  | 3,30   | .30   | , 29<br>, 59   | \$                                      | .00   |
| 3 (  | 2277,30  | 1741.81  | 2,72  | 2744.33   | 有个,容   | 0.15   | 1.08   | 1745,43   | .88   | 2,47   |   | 1.26   | .00   | , @8   | \$                                      | .\$9  |
| 8  | 30.49  | .00491   |   |   |  |  | .00493   | .53   |   |  | 3.73  |  |   | .88  | 李林存取                                    | -8,   |
|  |  |  | ZA.S  | tiles lageri  | Lž.  | <b>36</b> 17.25  | eletace  | PROFILE LI  | arims   |  |   |  |   |  |   |   |
|  |  |  | 43"   | STORM DRAID   |  |  |  |   |   |  |   |  |   |  |   |   |
|  |  |  | 4306  | × 100 m 2 m 2 m 2 m 2 m 2 m 2 m 2 m 2 m 2 m   |  |  |  |   |   |  |   |  |   |  |   |   |
| 8 8  | <b>************************************</b>  | THENTHE  | ご家界で終   | ₩.#.  | Q  | WEG.   | 3/202  | ######################################  | 2517 TER  | CRITICAL   |   | HCTT/  | <b>新热宗队》</b>                                | Til.   |   | AVSVE   |
| 8 %  | /21,224  | 10.17V<br>20)  | of Flow   | alier   |  |  | ezad<br>Syave  | encest<br>GFG . EL .<br>KF  | et ea<br>Stable   | DEPTH  | ejska daliyi  | 202A   | masij<br>ID MO.                             |  | eq<br>Fire                              | AVBPR   |
| 0 %<br>***   | /\$1.834<br>*******  | ELEV<br>ED<br>*******  | 07 Y1538  | %.E9<br>**********  | *****  | *******  | ezad<br>Sf avz<br>*******  | (76), E.,<br>KF<br>*********  | SLS7<br>******  | (SF15  |   | \$2A<br> <br>  | 10 M.                                       | \$漢<br>★◆H*★3  | 9188<br>*****                           | ****  |
| 0 L<br>***<br>0 L  | /ELEM<br>********<br>2387.80<br>DBAULIC  | 12.57<br>20<br>1741.44<br>2007   | 02 YLDH<br>************************************   | 33.67<br>************************************   | *******  | ********<br>8.38   | XZAS<br>SF AVZ<br>*******  | KF  | 51.8V<br>*******<br>.98   | (SETT)<br>***********************************                        |   | 324<br>(********<br>3.35   | 10 m.<br>*******                            | \$38<br>**!***<br>. 26<br>, 26   | #100<br>*****                           | .00   |
| 0 L<br>***<br>0 L  | /ELEM<br>********<br>2187.80<br>CBAULIC<br>2187.80   | NLEV<br>20<br>***********************************  | 07 Y1538  | %.E9<br>**********  | *****  | ********   | ezad<br>Sf avz<br>*******  | (76), E.,<br>KF<br>*********  | SLS7<br>******  | (SF15  |   | \$2A<br> <br>  | 10 M.                                       | *****<br>*****<br>***<br>***<br>***<br>***   | 9188<br>******                          | ****  |
| 0 1.<br>0 10<br>0 10<br>0 10   | /81.894<br>2187.80<br>CMAULIC<br>2187.88<br>11.97<br>2173.77   | 20.37<br>*********<br>1741.84<br>2049<br>1741.86<br>.00491<br>1741.72  | 02 YLDH<br>************************************   | 33.67<br>************************************   | *******  | ********<br>8.38   | #245<br>57 AV2<br>********<br>1.58<br>1.19<br>20580  | (96), 82.<br>MF<br>**********************************   | 51.8V<br>*******<br>.98   | (SETT)<br>***********************************                        | : 6 7 3 3 4 2 5 1<br>2 . 7 2  | 324<br>(********<br>3.35   | 10 m.<br>*******                            | *****<br>****<br>***<br>***<br>***<br>***  | #100<br>*****                           | .00   |
|  | /81.894<br>************************************  | 227<br>*********<br>1741.86<br>1741.86<br>1741.82  | 07 Y128<br>*********<br>2.72<br>2.42  | 33.63<br>**********************************   | ********<br>\$7.0<br>\$7.2   | ********   | # # # # # # # # # # # # # # # # # # #  | MF  **********  *********  *********  ****  | 33.87<br>*******<br>. 88<br>. 69  | 10278<br>10077<br>2,27<br>2,27                                       | 3.73<br>3.73  | 3:30   | 10 W.                                       | *****<br>*****<br>***<br>***<br>***<br>***<br>***  | 9188<br>******                          | ****<br>200<br>,00  |
|  | /  | **************************************   | 3 71200<br>2 72<br>3 42<br>3 33   | #3.27<br>************************************   | *******<br>\$7.0<br>\$2.2<br>\$7.5   | *******<br>8.35<br>9.46<br>9.74  | **************************************   | \$\$\partial \partial \par  | *******<br>. \$0<br>. \$0   | 2.27<br>2.27<br>2.27   | 2.72<br>2.72  | 3.50<br>3.50<br>3.50   | 10 %.<br>*******<br>.%<br>.%                | ****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>****<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>***<br>*** | 9188<br>******<br>\$                    | ****<br>200<br>300  |
| 2 * 2 * 2 * 4 * 4 * 4 * 4 * 4 * 4 * 4 *  |  | 12.47<br>************************************  | 2.72  | ######################################  | *******<br>\$7.5<br>\$7.5  | *********<br>\$ . 3 \$<br>\$ . 4 \$<br>\$ . 7 \$<br>\$ . 7 \$  | **************************************   | MF ********  *********  *********  ******   |   | 2.27<br>2.27<br>2.27<br>2.37   | 3.73<br>3.73  | 32x<br>1.50<br>2.50<br>3.50<br>1.50                                  | 70 W.                                       | *****  | #100<br>******<br>#                     | .00   |
| 0 * * * * * * * * * * * * * * * * * * *  |  | 12.47<br>************************************  | 2 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | \$7.64.37<br>\$7.64.37<br>\$7.64.37<br>\$7.64.39<br>\$7.64.39   | \$7.5<br>\$7.5<br>\$7.5<br>\$7.5   | **************************************   | **************************************   | \$745, AL,<br>************************************  | .00   | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27                         | 2.72<br>2.72  | 1  | 70 W:                                       | **************************************   |   | .00   |
| 0 * 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  |  |  | 2 72 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3  | \$784.39<br>\$784.09<br>\$784.09<br>\$784.09<br>\$744.09<br>\$744.28<br>\$744.28  | 87.8<br>87.8<br>87.8<br>87.8<br>87.8   | **************************************   | 22 A V | \$\$\$\text{\$\exititt{\$\text{\$\exititt{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\   | **************************************                                      | **************************************                               | 2 . 7 2   | 1.25<br>1.25<br>1.26<br>1.26<br>1.20<br>1.20                         | 10 Mi                                       | **************************************   |   | .00   |
| 多。 多。  | ######################################   | **************************************   | 2.13<br>2.33<br>2.35<br>2.35<br>2.35<br>2.35  | \$784.39<br>\$784.07<br>\$784.09<br>\$784.09<br>\$784.28<br>\$784.28  | **************************************   | **********<br>\$ .35<br>\$ .45<br>\$ .74<br>\$ .75<br>\$ .75<br>\$ .75<br>\$ .75<br>\$ .75   | ######################################   | \$\$\text{\$2}\$, \$\text{\$2}\$, \$\text{\$2}\$, \$\text{\$2}\$, \$\text{\$4}\$, \$\text{\$5}\$, \$\text{\$6}\$, \$\text{\$2}\$, \$\text{\$4}\$, \$\text{\$5}\$, \$\text{\$6}\$, \$\text{\$2}\$, \$\text{\$4}\$, \$\text{\$5}\$, \$\text{\$6}\$, \$\text{\$2}\$, \$\text{\$2}\$, \$\text{\$6}\$, \$\text{\$2}\$, \$\text{\$6}\$, \$\text{\$2}\$, \$\text{\$6}\$, \$\te | 25. 25. 25. 25. 25. 25. 25. 25. 25. 25.                                     | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27         |   | 22.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.2         | 10 MG.                                      | # * * * * * * * * * * * * * * * * * * *  |   | .20   |
| 多年多年中华安全安全安全安全安全安全安全安全安全安全安全安全安全安全安全安全安全安全安全   |  | ######################################   | 2 72 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3  | \$784.39<br>\$784.09<br>\$784.09<br>\$784.09<br>\$744.09<br>\$744.28<br>\$744.28  | 87.8<br>87.8<br>87.8<br>87.8<br>87.8   | **************************************   | 22. A V 22. A  | \$\$\text{\$2.}\$\text{\$2.}\$\text{\$2.}\$\text{\$2.}\$\text{\$3.}\$\text{\$4.}\$\text{\$5.}\$\text{\$5.}\$\text{\$4.}\$\text{\$5.}\$\$5.   | **************************************                                      | **************************************                               |   | 1.25<br>1.25<br>1.26<br>1.26<br>1.20<br>1.20                         | 10 Mi                                       | **************************************   |   | .00   |
| 安全会会会会会会会会会会会会会会会会会会会会会会会会会会会会会会会会会会会会   | **************************************   | 200  | 2.13<br>2.33<br>2.35<br>2.35<br>2.35<br>2.35  | \$784.39<br>\$784.07<br>\$784.09<br>\$784.09<br>\$784.28<br>\$784.28  | **************************************   | **********<br>\$ .35<br>\$ .45<br>\$ .74<br>\$ .75<br>\$ .75<br>\$ .75<br>\$ .75<br>\$ .75   | **************************************   | 3985, 87<br>1745, 47<br>1745, 57<br>1745, 53<br>1745, 53<br>1745, 73<br>1745,   | 25. 25. 25. 25. 25. 25. 25. 25. 25. 25.                                     | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27         | 2.73<br>2.73<br>2.22<br>3.33<br>1.39<br>1.39  | 22.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.2         | 10 MG.                                      | **************************************   |   | .20   |
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| 多,我们的是是我们的是我们的我们的我们的,我们们们们们们们们们们们们们们们们们们们  | **************************************   | 200 8 6 6 8 7 2 1 7 8 8 7 8 8 7 2 1 7 8 8 7 8 8 7 8 1 8 1 8 1 8 1 8 1 8 1  | 2-72<br>2-82<br>2-35<br>2-35<br>2-35<br>2-35<br>2-35<br>2-35<br>2-35<br>2-3   | \$184.39<br>2744.09<br>2744.09<br>2744.09<br>2744.29<br>2744.25<br>2744.35<br>2744.35<br>2744.35  | 67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0   | # 35<br># 48<br># 74<br># 74<br># 75<br># 75 | 22.42 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  | \$250, 82- \$4745.47 \$745.47 \$745.47 \$745.87 \$745.87 \$745.87 \$745.87 \$745.87 \$745.87 \$745.87 \$745.87 \$745.87 \$745.87  | **************************************                                      | 2.27<br>2.27<br>2.37<br>2.37<br>2.37<br>2.57<br>2.57<br>2.57<br>2.57 | 2.73<br>2.72<br>2.72<br>3.13<br>1.39<br>1.39<br>2.73  | 2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20         | .00 WG00 .00 .00 .00 .00 .00 .00 .00 .00 .0 | ***************************************  |   | . 22<br>. 23<br>. 20<br>. 20<br>. 25<br>. 25<br>. 25<br>. 25<br>. 26<br>. 26<br>. 26  |
| 安全年龄的特殊的特殊的特殊的特殊的特殊的特殊的特殊的特殊的特殊的特殊的特殊的特殊的特殊的   | **************************************   | **************************************   | 2.72<br>2.42<br>2.35<br>2.37<br>2.39<br>2.45<br>2.45<br>2.45<br>2.72<br>2.49<br>2.72  | 27.89 .39 17.84 .39 17.84 .39 17.84 .39 17.84 .39 17.84 .39 17.84 .39 17.84 .39 17.85 .40 17.85 .40 17.85   | 67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0   | # 35<br># 48<br># 74<br># 74<br># 75<br># 75 | 22.A2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  | 2745,47<br>1745,47<br>1745,47<br>1745,52<br>1745,52<br>1745,57<br>1745,67<br>1745,67<br>1745,97<br>1745,97<br>1745,97<br>1745,97<br>1745,97<br>1745,97<br>1745,97<br>1745,97  | 22.27<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50        | 2.27<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37         | 2.73<br>2.72<br>2.72<br>3.13<br>1.39<br>1.39<br>2.73  | 2.24<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20         | 70 MG.                                      | 是一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个  |   | . 22<br>. 23<br>. 20<br>. 20<br>. 25<br>. 25<br>. 25<br>. 25<br>. 26<br>. 26<br>. 26  |
| \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$   | **************************************   | 22.20  | 2.72<br>2.42<br>2.35<br>2.47<br>2.39<br>2.46<br>2.57<br>2.48<br>2.72<br>2.49<br>2.72  | \$124.39<br>\$744.39<br>\$744.39<br>\$744.39<br>\$744.39<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$744.35<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745<br>\$745  | 57.0<br>57.0<br>57.0<br>57.0<br>67.0<br>67.0<br>67.0<br>67.0   | \$ .35<br>9 .45<br>4 .74<br>30 .23<br>9 .75<br>9 .84<br>8 .45<br>8 .65<br>8 .65<br>8 .65<br>8 .65  | 22 AC 2  | 2745.47 2745.4  | 20 .00 .00 .00 .00 .00 .00 .00 .00 .00 .                                    | 2.27<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37         | 2.72<br>2.72<br>3.38<br>1.39<br>1.39<br>2.73<br>2.73  | 2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30         | 10 Mg.                                      | *************************************  | **************************************  | . 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20  |
| 多。全部是是是是是是是是是是是是是是是是是是是是是是是是是是一个,我们就是一个,我们就是一个,我们就是一个,我们就是一个,我们就是一个,我们就是一个,我们就是一个,我们就是一个,我们就是一个,我们就是 | / Sales  | 22.20  | 2.72<br>2.42<br>2.35<br>2.76<br>2.37<br>2.38<br>2.45<br>2.45<br>2.45<br>2.47<br>2.48<br>2.72  | \$2.29<br>\$7.86.00<br>\$7.86.00<br>\$7.86.00<br>\$7.86.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00<br>\$7.88.00  | 67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0   | 7.35<br>7.46<br>7.76<br>37.71<br>30.22<br>7.25<br>7.30<br>8.45<br>8.64   | 22. A2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | 2005, EL.  1745, 37  1745, 37  1745, 35  1745, 37  1745,  | 21.TV   | 2.27<br>2.27<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37         | 2.72<br>2.72<br>3.23<br>1.29<br>1.29<br>2.29<br>2.29<br>2.72  | 2.24<br>2.20<br>2.20<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30 | 10 MG.                                      | 本************************************  | ######################################  | .00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00  |
| · · · · · · · · · · · · · · · · · · ·  | / Sale   | 1741, 8 49 1741, 1742, 8 49 1742,   | 2.72<br>2.42<br>2.35<br>2.36<br>2.27<br>2.46<br>2.32<br>2.46<br>2.72<br>4.72<br>4.72<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73  | \$2,200<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44 | 67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0   | 7.35<br>7.46<br>7.76<br>7.76<br>7.75<br>7.37<br>7.37<br>7.37<br>7.37<br>8.88<br>8.84<br>8.85<br>8.85<br>8.85<br>8.85<br>8.85<br>8.85   | 22.A2 27.A2 27.A2 2.32 20.42 2.42 2.42 2.42 2.42 2.42 2.42 2.  | 2005, EL.  1745, 37  1745, 37  1745, 35  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1745, 37  1746, 37  1747, 37  1747, 37   | 22.4V<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50 | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.37<br>2.3  | 2.72<br>2.72<br>3.38<br>1.39<br>1.39<br>2.73<br>2.73  | 2.24<br>2.20<br>2.20<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30 | 10 MG00 .00 .00 .00 .00 .00 .00 .00 .00 .   | *************************************  |   | . 186<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20   |
| 《《《《《《》《《《》《《》《》《《》《》《《》《》《》《》《》《》《》《》   | /*************************************   | ######################################   | 2.72<br>2.42<br>2.35<br>2.36<br>2.27<br>2.48<br>2.48<br>2.72<br>2.48<br>2.72<br>4.89<br>4.89<br>4.89<br>4.89<br>4.89<br>4.89<br>4.89<br>4.89  | \$2,200<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000<br>\$7,84,000   | 57.0<br>57.0<br>57.0<br>57.0<br>57.0<br>57.0<br>57.0<br>57.0   | 7.35<br>7.48<br>7.78<br>7.73<br>7.75<br>7.37<br>7.37<br>7.37<br>7.37<br>8.88<br>8.88<br>8.88<br>8.88   | 22.42 27.42 2.32 2.32 2.32 2.32 2.32 2.32 2.32 2   | 2785,82- 1745,47 1745,47 1745,53 1745,53 1745,70 1745,53 1745,70 1745,  | 22.4V .00 .00 .00 .00 .00 .00 .00 .00 .00 .0                                | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.37<br>2.3  | 2.72<br>2.72<br>3.38<br>1.39<br>1.39<br>2.73<br>2.73  | 2.24<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26         | 10 MG00 .00 .00 .00 .00 .00 .00 .00         | · 《 · · · · · · · · · · · · · · · · · ·  |   | . 100<br>. 50<br>. 50<br>. 50<br>. 50<br>. 50<br>. 50<br>. 50   |
| · · · · · · · · · · · · · · · · · · ·  | ######################################   | 1242   | 2.72<br>2.42<br>2.35<br>2.36<br>2.27<br>2.46<br>2.32<br>2.46<br>2.72<br>4.72<br>4.72<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73<br>4.73  | \$2,200<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44,00<br>\$7,44 | 67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0   | 7.35<br>7.46<br>7.76<br>7.76<br>7.75<br>7.37<br>7.37<br>7.37<br>7.37<br>8.88<br>8.84<br>8.85<br>8.85<br>8.85<br>8.85<br>8.85<br>8.85   | 22.42 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  | 3385, 82.   | 22.4V<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50 | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.37<br>2.3  | 2.73<br>2.73<br>2.73<br>3.13<br>1.39<br>1.39<br>2.73<br>2.73  | 2.24<br>2.20<br>2.20<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30 | 10 MG00 .00 .00 .00 .00 .00 .00 .00 .00 .   | 本,我们就是一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个   | ######################################  | . 186<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20   |
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| 《《《《《《》《《《《《》《《》《《》《《》《《》《《》《《》《《》《《》《《  | ######################################   | 1242   | 2.72<br>2.42<br>2.35<br>2.36<br>2.37<br>2.38<br>2.48<br>2.72<br>2.48<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72  | \$7.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.44.39<br>27.45.39<br>27.45.39<br>27.45.39<br>27.46.37<br>27.46.37<br>27.46.37<br>27.46.37   | 57.0<br>57.0<br>57.0<br>57.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0   | #  | 22.A2 22 22 22 22 22 22 22 22 22 22 22 22 2  | 2745, 82, 1745, 82, 1745, 835, 835, 835, 835, 835, 835, 835, 83   | 22.29<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.0  | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27         | 2.79<br>2.79<br>2.29<br>1.39<br>1.39<br>2.73<br>2.73<br>2.73  | 2.24<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26         | 10 MG00 .00 .00 .00 .00 .00 .00 .00 .00 .   | *************************************  | ######################################  | . 200<br>. 200 |
| 李子在在在在在在在在在在上,一个是是在一个,他们就是一个一个,我们就是一个一个,我们就是一个一个,我们就是一个一个,我们就是一个一个,我们就是一个一个,我们就是一个一个一个一个一个一个一个一个一个一个 | ######################################   | ######################################   | 2.72<br>2.42<br>2.35<br>2.35<br>2.35<br>2.35<br>2.45<br>2.35<br>2.45<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.89<br>2.72<br>2.72<br>2.72<br>2.72<br>2.72<br>2.72<br>2.72<br>2.7 | \$7.44.39 27.48.39 27.49.39 27.49.39 27.49.39 27.49.39 27.49.39 27.49.39  | 57.0<br>57.0<br>57.0<br>57.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0   | # 35   | 22. A. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.  | 2745, 87<br>1745, 87<br>1745, 87<br>1745, 87<br>1745, 87<br>1745, 87<br>1745, 87<br>1745, 89<br>1745, 89<br>1745, 91<br>1745, 91<br>1745, 91<br>1745, 91<br>1745, 91<br>1745, 91<br>1745, 91<br>1747, 91<br>1747, 95<br>1747, 81<br>1747, 81  | 22.4V .00 .00 .00 .00 .00 .00 .00 .00 .00 .0                                | 2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.27<br>2.37<br>2.3  | 2.72<br>2.72<br>3.32<br>1.39<br>1.39<br>2.72<br>2.73<br>2.73<br>2.73  | 2.24<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26<br>2.26         | **************************************      | **************************************   | ######################################  | . 200<br>. 200 |
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| 《《《《《《《《《《》》,  | ######################################   | **************************************   | 2.72<br>2.42<br>2.35<br>2.37<br>2.35<br>2.35<br>2.35<br>2.35<br>2.45<br>2.72<br>2.40<br>2.72<br>2.40<br>2.72<br>2.72<br>2.73<br>2.73<br>2.73<br>2.73<br>2.73<br>2.73  | \$129<br>\$784.00<br>\$784.00<br>\$784.00<br>\$744.00<br>\$744.00<br>\$744.00<br>\$744.00<br>\$744.00<br>\$744.00<br>\$744.00<br>\$744.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.00<br>\$745.0  | 57.0<br>57.0<br>57.0<br>57.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>67.0<br>6  | # 35   | 22. A. 2 . 2 . 2 . 2 . 2 . 2 . 2 . 2 . 2   | 2745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1745,47 1747,41 1747,47 1747,4  | ######################################                                      | 2.27<br>2.27<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37<br>2.37         | 2.72<br>2.72<br>3.02<br>1.03<br>1.03<br>1.03<br>1.03<br>2.72<br>2.73<br>2.73<br>2.73<br>2.73<br>2.73<br>2.73<br>2.7 | 2.24<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30<br>2.30 | **************************************      | **************************************   |   | . 200<br>. 200 |
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| C STEAMENT AS IN 19 WERECO.  | ATTR SCREACE S  | *                                      | 3                                      | ut card L                                | i pri pri                              |            |  |                             |  |  | PASK M   | . )                       |
| dis data<br>o slegget no 14 15 a sisce   | STATION<br>1318.96 1  |  |  |  | #<br>.01)                              |            |  |                             | 8010AN<br>00.                          |  | ANG FT<br>15,00  | PRAME<br>C                |
| u/# Data   | otatica<br>1110. je 1   |  |  |  | #<br>.013                              |            |  |                             | KADI ISB<br>. \$4                      |  | AMG PT<br>15.05  | man n<br>g                |
| 9 SLEWSKY NO 15 18 A REACH<br>U/S DATA   | 1929.96 1   |  | 4                                      |  | .911                                   |            |  |                             | AADIUS<br>00                           | AMSLA<br>.00                                   | AMG PT<br>13.00  | 753.25 JH<br>1            |
| S CLEMENT NO 16 18 A REACH<br>S/S DATA   | *<br>************************************                         | 107221<br>1751.41                      | 835.7                                  |  | .013                                   |            |  |                             | 842104<br>00.                          | AMSLA<br>00                                    | A363 PT  | 752.51 N                  |
| S ELEMENY NO 17 10 A SIACH<br>9/0 CATA   | *   | 1mvent                                 | 320.T                                  |  | 8                                      |            |  |                             | 2.451135<br>\$4.                       | 4001.H   | ANG PT   | Mam n<br>e                |
| S KLAMENT NO 18 18 A JUNETICA<br>USE DATA  | etation .   | INVENT                                 |  | AT-1 LAT-                                | j 16                                   | Q)<br>la.o | Q4                                     | invent-l:                   |  | .9   | F941 4   | -                         |
| C PLEMENT NO 19 13 A REACH<br>U/S DATA   |   | infert                                 | *<br>SBC.7                             | * *                                      | 舞                                      | * 62 = 60  | +44                                    | 8199133                     | NADIUS                                 | A3X31.56                                       | ANG PT   | 262428 N                  |
| O ELEMENT NO 20 IS A REACH<br>3/8 IATA   | ijes.ņi i<br>Varion   | ::V::<br>:ev:xx:                       | -8                                     |  | .013                                   |            |  |                             | .00<br>Madius                          | .00.<br>AMELE                                  | 15.00<br>ANG PT  | PAN N                     |
| S ELEXENT NO 31 12 A REACH<br>0/S DATA   | 1395.95 1<br>*<br>**********************************              | 1703.)0<br>*<br>!#Y##T                 | 1 *                                    |  | .51)                                   |            |  |                             | ee.<br>Buidas                          | OC.<br>SLEWEA                                  | 15.00<br>ANG PT  | e<br>Bab u                |
| e maneet en 12 la a erace<br>Vie data  | \$39£,75 \$   |  | 1 +                                    |  | .617                                   |            |  |                             | oo.<br>Retiches                        | +86  | 15.00<br>ANG PT  | \$ \$52.01 N              |
| e element no 13 is a reach   | 1391.95 1   | 1703,45                                | \$                                     |  | ,81)                                   |            |  |                             | , % S                                  | .79  | 488  | **                        |
| U/S DATA<br>S SIEMENT NO 24 IS A JUNCTICE  | 1752.06 }   | +                                      | 1 *                                    | *  | .013                                   | я          |  | ъ                           | autua<br>95.                           | .99<br>*                                       | AMS PT<br>.90  | Masi di<br>T              |
| TATA   | 7787158<br>1757.06 1  | 1969,74                                | art W                                  | AT-1 1AT-<br>2 A                         |  | Q)<br>10,0 | ş#<br>3.0                              | 197587-3 1<br>1708.70       |  |  | 7917 4<br>90.00<br>7422 90                                       | · 4                       |
| O ELEMENT NO IN TH A MEACH   | ATEX SUBFACE :  | 30                                     | *                                      | et cald L                                |  |            |  |                             | 50 a 40 A                              | \$ 9.44° W                                     |  |                           |
| 9/2 DATA<br>S ELEMENT BO 14 IS A SUSSETION   | 2277,83 }   | *                                      | 3. +                                   | *  | ,913                                   | æ          |  | *                           | 55                                     | \$3035.Z<br>.50                                | 17 DAM<br>00,  | NAS N                     |
| GIZ DATA<br>O KLIMENT NO 17 18 A RIACH   | STATICS<br>1001.00 1  |  | SECT L                                 | AT-1 LAT-<br>7 9                         |  | ()<br>44.0 |  | 1710.54                     |  | P#1 ]<br>90,60                                 | 90,00  |                           |
| CVS DATA   | STATION<br>STRINGS  | invert<br>ITIS.18                      |  |  | 朝<br>, 古言诗                             |            |  |                             | radius<br>20.                          | alena<br>Pē.                                   | AMG PT<br>15.00  | Man n<br>O                |
| tis tata   | WYATIOM<br>2731.78 1  | invent<br>(Tip.is                      | 3                                      |  | #<br>.013                              |            |  |                             | radius<br>S9                           | ANGLE<br>60.                                   | ANG PT<br>15.00  | 1982.19 TH<br>1           |
| i planami mi in in a maach<br>iin iais   | #*************************************                            | :00/5007<br>1719.40                    | 72.T                                   |  | #<br>.013                              |            |  |                             | AADIUS<br>00                           | AVELE<br>.00                                   | AMG PT<br>,00  | 252.33 El<br>D            |
| S SLIMENT NO 16 IN A REACH<br>S/S CATA   | #<br>####################################                         | 1975WT<br>1731.33                      | SECT                                   |  | #<br>,013                              |            |  |                             | ###2112E                               | A2822.S  | ANS 97   | 363,51 H                  |
| CHEMINA II IS A TURNILE C<br>UNI DATA  | etation   | INVENT                                 | sect L                                 | AT-1 LAT-                                | 3 M                                    | Q)<br>18.4 |  | invent-1 :                  | nvent-1                                | PWI)   | \$361 4  |                           |
| STARREST NO. 12 TH A BRACES S<br>ATAC STU  |   | 134/2007                               |  | 3 8                                      | #                                      | 8 40 4 76  | * 4                                    | 1721,40                     | ealine                                 |  | .00<br>AMS PT  | 1882A 31                  |
| SCITARIO SI EE CH THURLIS S  |   | *                                      | SET L                                  | e<br>At-1 Lat-                           | .913                                   | ş.i        | ĝė.                                    | INVENT-I I                  | 60.<br>4-132374                        | .90<br>*<br>********************************** | .00<br>FRI 4   | 3                         |
| S ELEMENT MED 34 IN A REACH<br>USE DATA  | 2009.20 1   |  | 3 .                                    |  |  | #1.0       | .\$                                    | ,00                         | SS.<br>BIICAN                          | -90  | .00<br>AND PT  | 369.53 34                 |
| \$   | 2913.09 1   | 1708.91                                | 2                                      |  | .01.9                                  |            |  |                             | .00                                    | .50  | .00<br>18421 82  | ä                         |
| o slament de la 12 12 a braca<br>U/s rata  |   | INVENT                                 | *                                      | MT CARD L                                | .34                                    |            |  |                             | KADIUS                                 | ASEGLE   | ASES 977   | 10(A,3) 34                |
| E KLIMENT BO IN IN A ARACH   | INID.CP 1   | ifib.ll<br>*<br>impert                 | a a section                            |  | .919                                   |            |  |                             | eorax                                  | .00<br>Amile                                   | 19.60<br>TH 1884   | S MAN II                  |
| S ELEMENT NO 37 IS A MEACH   | 2919.09 I   | 1719.11                                | 3                                      |  | .813                                   |            |  |                             | . 25                                   | .60  | 12,00  | **                        |
| 0 Elemet 20 20 10 a elach  | 2015,09 1   |  | 1 *                                    |  | ,513                                   |            |  |                             | MADINE<br>00.                          | .00  | ANG PT<br>15.80  | \$                        |
| 11/S IATA<br>O ELEMENT NO 12 IS A SEACH  | 2717.09 1   | 100000<br>1725.11                      | SET                                    |  | .01)                                   |            |  |                             | RACIUS<br>.00                          | 18651.E<br>.00                                 | ANG PT<br>15.00  | Marie de<br>Ĉ             |
| u/s data   |   | SHIFTHY                                | ä                                      |  | .013                                   |            |  |                             | ########<br>.90                        | ANGLE<br>.00                                   | AMG PT<br>15.00  | 36436 31<br>0             |
| SELECTION AS IS A REACH USE DATA   | STATION<br>1919.09 1  | invert<br>1722.11                      | ************************************** |  | #<br>(10,                              |            |  |                             | edicam<br>co,                          |  | ANG PT   | HAN N                     |
| S ELEMENT NO 41 IS A REACH<br>HAS DATA   | STATION<br>ESSELLA L  | INVERT                                 | *                                      |  | M<br>.013                              |            |  |                             | radius<br>00.                          | ARALA.   | ANG PT   | Man n<br>S                |
| d flament m: al la a system m<br>E/S Cala  | CALDED NO.  | SHVERT                                 | SET.                                   |  |  | 4          |  | ₩ 5 XLEV<br>1713.80         | ,                                      |  | ,,,,   | •                         |
| NO KOTT BROOM ENCOMERAGE-CO  |   |  |  |  |  |            |  | 無下各名 12 學家                  |  |  |  |                           |
| ę,   | SIDA LAMIYILL   |  |  |  | MOTILA LI                              | 271K)      |  |                             |  |  | ¥4.0   | z i                       |
| 並みでき   |   |  | D MITH                                 | eg. Mess:                                |  | er e hare  | CRITICAL                               |                             | MOT!                                   | <b>製工室供</b> =                                  | 62 v   | \$ 3,1000 0van            |
| CX314  | ET FROM DETENT<br>TR FLOW   |  | 2,9991                                 | 3,70511                                  | icrost opropuestones                   |            | 70.99 4 4 4 5 4 5 May 10               |                             |  | NA 163   | 24 390<br>313  | AVERE                     |
| OCTI.  S STATION INVENT DEPTH  KINY OF FICE  S LIELAN SC   | TA FLOW<br>W.S.<br>ELEV   | Q                                      | V30.                                   | sy ave                                   | ENINGY<br>FRISER<br>FRISER             |            | ereta<br>F                             | edn depth                   |  | 19 %C.   | 2,20   |                           |
| CTIAL STATION SHARET SEPTH SERVER FROM CLIEBE SCIENCES SERVER FROM CLIEBE SERVER SERVE | 73.2%<br>M.S.<br>ELEV<br>Brancheniesy                             | ·<br>••••••                            |  | erat<br>er ave                           | 1983) - \$3.<br>1987                   |            | 3                                      |                             |  | 10 30.<br>*******<br>10.00                     | 2A<br>********<br>.00 0  | ****                      |
| STATION INVEST DEPTH 120 1 1.0 | 73.28<br>M.B.<br>83.27<br>Whater the same of the same<br>\$700.30 | 0<br>*********<br>}6}.0<br>}           | *******<br>17.68<br>15.09              | ######################################   | 1908.15<br>1908.15                     | *****      | ************************************** | edn depth                   | 01A<br>******<br>5.20<br>5.00          | 12,23  | 2%<br>********<br>.60<br>.60<br>.05                              | *****<br>- 59<br>- 259    |
| 0754 0 974108 197407 10778 0 1/8109 107707 0 1/8109 07 0 144.50 1679.87 1.69 0 164.50 1679.87 1.69 0 16.20 17.00 1 | ** FLEW M.S. **********************************                   | ************************************** | ********<br>17.68                      | 27 8 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 | ************************************** | .00        | *********<br>2,59                      | EDN JEFTH                   | DIA<br>******<br>3.20                  | r*******<br>\$2.09                             | 2A<br>********<br>****<br>***<br>***<br>***<br>***<br>***<br>*** | ******<br>- 95<br>- 26    |
| ######################################   | ** F.C.**  *****  *****  *****  *****  *****  ****                | ************************************** | ********<br>\$7.88<br>\$3.08           | ######################################   | ************************************** | .00        | ************************************** | 200 1270<br>2242222<br>3.51 | Dia<br>*******<br>*.20<br>*.00<br>*.00 | **************************************         | 2.00<br>***********************************                      | ***** - 58 - 58 - 58 - 58 |

| 0 1198.20                              |  | 6.36  | 1706,75                               |                      | 11,00            | 1.49                     | 1708.43<br>1708.73                            | ,00                     | 4.15                          |                           | 3.50<br>3.50 | ,00              | , 99<br>20,          | #                  | .00            |
|--|--|---|---------------------------------------|----------------------|------------------|--------------------------|---|-------------------------|-------------------------------|---------------------------|--------------|------------------|----------------------|--------------------|----------------|
| 0 1199.70<br>0 1199.70<br>0 5.00       | 1700.45                                  | 8.19  | 1706.84                               | 214.0                | 11.00            | 1.88<br>1.88<br>,00483   | 1708.91                                       | , 20                    | 4,18                          | 3,09                      | 5.00         | *88              | , 66<br>, 66<br>, 66 | -9                 | .50            |
| 0 1201.20                              | 1700.71                                  | 6.34  | 1707,24                               | 314.0                | 11.00            | .00428                   | 1708.94                                       | , 2-2                   | 4.12                          | 3.49                      | 9.20         | .00              | . 56                 | 0                  | ,44            |
| 0 1320.06                              | 1702.94                                  | 5.48<br>6.57                                  | 1708.01<br>1708.11                    | 214.0                | 11.00<br>11.00   | 1.88                     | 1709.90<br>1709.99                            | ,49<br>48.              | 4.38<br>4.38                  |                           | 5.00<br>5.00 | .00              | 22<br>22             | <b>\$</b>          | . \$9<br>. \$0 |
| 0 1318,96<br>0 5.00                    | 1701.34<br>.01199                        | 3,76  | 1700.36                               | \$4.6 × 5            | 11,50            | .004<br>004<br>004       | 1718.18<br>.0)                                | . 24                    | 4,19                          | 3,09                      | 9.50         | .90              | , \$5<br>, \$5       | **                 | . 22           |
| ž.                                     |  |   |                                       |                      | MATER            |                          | PROFILE LI                                    | etim:                   |                               |                           |              |                  |                      | ****               | **             |
|  |  | QI/T  | TOIDE LANDY<br>LET THOU DE            |                      | es elin          | 88° WARS                 | CH SD   |                         |                               |                           |              |                  |                      |                    |                |
| 0 STATION                              | INVEST                                   | SEPTH   | YR FLOW<br>N.S.                       | Q                    | \$2902<br>\$204  | VIII.                    | (36F267)                                      |                         |                               |                           | MIT!         | <b>多本高奖</b> 了    |                      |                    | AVSPA          |
| 0 1,/ELEM                              | 21.5V<br>50                              | SE FLOM                                       | \$1.27                                |                      |                  | WZAD<br>SV AVX           | SED.EL.,<br>KF                                | K3.K3                   |                               | 9088 DEFIN                |              | 19 10.           | ##<br>*******        | FIER<br>Sees       |                |
| 0 1333.9%                              |  | 5.7)  | 1708.34                               |                      | 11,00            | 1,49                     | 1710.13                                       | ,00                     | 4,18                          | 3.04                      | 5.50         | .00              | . 00<br>.00          | 2                  | . 48           |
| 0 1071.40<br>0 1071.40<br>CAUSET STR   | 1701.19                                  | 5.42  | 1700.41                               | 214.0                | 11,00            | .00688<br>1.89<br>.00637 | 1710.49                                       | . \$5                   | 4,18                          | \$300                     | 9.00         | .60              | , 85<br>, 85<br>, 44 | 9                  | .90            |
| S 1375,45<br>S 11.58                   | 1703.21                                  | 5,75  | \$798.94                              | 295.0                | 10,49            | ,50636                   | 1710.47                                       | .00                     | 4,29                          | 3.94                      | 8.00         | .05              | . 25<br>26.          | \$                 | , \$2 d        |
| 0 1386.35                              | 1701.10                                  | 5,74<br>5,83                                  | 1709.12<br>1709.10                    | \$04.\$<br>\$0.8\$\$ | 10,49            | 1.71                     | 1710.83<br>1710.81                            | .60                     | 4,09                          |                           | 5,00<br>5,00 | .03              | .00                  | 9                  | .00            |
| 0 1396.75                              | 1701.38<br>,01399                        | 5.33  | 1709.17                               | 328.0                | 10.49            | 1.71                     | 1211.00                                       | .49                     | 4.09                          | 2.99                      | 3.20         | , 98             | 20.<br>20.           | 8                  | - 88           |
| 0 1391.95                              | 1703.45                                  | 5.25  | 1709,46                               | 104.0                | 10,49            | 1.71                     | 1711.11                                       | 189                     | 4.07                          | 3,96                      | 5.50         | .59              | , 64<br>00           | ₽                  | .00            |
| 0 1478.61<br>Dericalizaci              | 1704.70<br>Jime                          | 5.26  | 1709.74                               | 208.0                | 表點。看學            | 1.71                     | 1711.87                                       | .00                     | 4,29                          |                           | 3,22         | .00              | , 0.5<br>0.0         | 0                  | .00            |
| 0 1478,43<br>0 94.47                   | 1704.70<br>.81447                        | 3.54  | 1707,74                               | 264.0                | 14.14            | 4.1%                     | 1711.92                                       | .09                     | 4,69                          | 2.94                      | 5.00         | .00              | .02                  | \$                 | . 90           |
| 0 1571.10<br>0 78.14                   | 1706.07                                  | 3,33  | 1709.20                               | 201.2                | 19.38            | .01155                   | 3713.3  | .89                     | 4.07                          | 3,96                      | 5,90         | .00              | .05                  | *                  | .9\$           |
| 0 1401.34                              | 1787.30                                  | 3.36  | 2715.46                               | 308.0                | 10.31            | 2.59<br>81010.           | 1714.00                                       | .00                     | 4,09                          | 3,24                      | 5.50         | ,66<br>68        | .00<br>.00           | \$                 | ,98<br>an      |
| 0 1675.33                              | 1767,84                                  | 3.40  | 3733,24                               | 255.0                | 14.50            | 3,27                     | 1714,50<br>.2%                                | .02                     | 4,49                          | 3.94                      | 5.00         | , AAB            | ,00<br>00            | \$<br>7422         | .95            |
| 3                                      |  | 20.0  | THIDE LANDS                           | 443.                 | matem            | MANACY.                  | PROFILE LI                                    | 27103                   |                               |                           |              |                  |                      | a-91511 fi         | A              |
|  |  | CATT  | INTO LAMOR<br>LET PROM DE<br>TR PLOM  |                      | SED WITH         | 40° MARE                 | CH BD   |                         |                               |                           |              |                  |                      |                    |                |
| O STATION                              | invent                                   | DAVIN<br>OF FLOX                              | ¥.2.                                  | ē                    | ve.              | VII.<br>HIAD             | energy<br>(SC: SL:                            | super<br>CLV            | CATTICAL<br>DEPTH             |                           | mit/<br>Dia  | 845E/<br>10 80.  | 84                   | \$16()<br>\$13.836 | AVEFR          |
| 9 1.521.69                             | 98/2                                     |   |                                       | ******               |                  | 27 AV#<br>********       | 988°  |                         | ********                      | MC998 [CKPT9<br>********* | ******       | *******          | 22<br>14748<br>14748 | ****               |                |
| 9 1722.88                              | ~#\$447                                  | 3.86  | 1711.79                               | 794.0                | 13.82            | 7.97<br>31802.           | 1714.76<br>.14                                | ,44                     | 4.29                          | 2,94                      | 李、秦帝         | , 65             | , 44<br>44,          | 8                  | .00            |
| 0 1739.82                              | \$700.48<br>.01447                       | 7.73  | 1712.19                               | 354.8                | 13,28            | of.c<br>Lergo.           | 1714.09<br>.07                                | ,99                     | 4,09                          | 2,92                      | 3,34         | .25              | .00<br>90,           | 0                  | .99            |
| 0 1749,31                              | 1708.41<br>.01447                        | 3,48  | 1717,31                               | \$58.0               | 32,27            | 2.45                     | 1734.96<br>.93                                | , 23                    | 4.03                          | 3.94                      | 3,86         | , 33             | .00<br>.00           | <b>&amp;</b>       | -\$5           |
| 0 1702.06<br>SJUWET STR                | 1708,66<br>.01190                        | 4.09  | 1713,75                               | 794,0                | \$2.99           | .00141                   | 1714,78                                       | . 60                    | 4.09                          |                           | 5,00         | , \$4            | , 88<br>. 88         | *                  | -26            |
| 0 1707.04                              | 1708,74                                  | 3-13  | 1714,07                               | 183.5                | 7.32             | 1.77                     | 1715,43                                       | .00                     | 1,27                          | 3,84                      | 5.50         | .80              | .00                  | į.                 | .00            |
| O 1789.11<br>OMYDDAUS.IC               |  | 9,19  | 1714,31                               | 182.5                | 9.31             | 1.38                     | 1715.56                                       | . 57                    | 3,87                          |                           | 5.50         | ,20              | .00                  | 9                  | .00            |
| 0 1785.11                              | 1709,11                                  | 2,85  | 1711.96                               | 183.5                | 10:83            | 2.284                    | 1715.04<br>3,01<br>1757.48                    | .43                     | 3,#7<br>3.#7                  | 显。带着                      | 9.90         | .99              | .00<br>.00<br>.00    | <b>9</b>           | ,00<br>,00     |
| 0 1919,20<br>0 182,47<br>0 2113,72     | 1710.99<br>.01203<br>1711.17             | J.99  | 1710.87                               | 193.0                | 18.88            | 1.81<br>2112<br>24,5     | 1.14  | , 474<br>, 484          | 3,87                          | 2.94                      | 2,20         | .00              | ,89                  | 8                  | ,20            |
| 0 73,39                                | .01301<br>1714,33                        | 3.11  | 1717,43                               | 193.5                | 34.3)            | -81548<br>3.11           | 1710.50                                       | . 444                   | 3.87                          | 3,84                      | 5.80         | .00              | .00                  | 83                 | ,80            |
| 8 41.15<br>0 2214.94                   | .01321                                   | 3.34  | 1718.10                               | 181.0                | 13.87            | .00912                   | .38<br>1730.96                                | ,98                     | 3.83                          | 3,84                      | 3.00         | .00              | . 00<br>00           | â                  | .90            |
| S 25.19                                | .01303                                   | ,   | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |                      |                  | .00059                   | .31   |                         |                               | 2.84                      |              |                  | , \$3                | *****              | 4              |
|  |  |   | TOIDE LABOR                           |                      |                  |                          | PROFILE LI                                    | 071W)                   |                               |                           |              |                  |                      |                    |                |
|  | W 10 10 11 11 11 11 11 11 11 11 11 11 11 | 198   | LET FROM DE                           |                      |                  |                          |   |                         | observation of the control of |                           |              |                  |                      |                    |                |
| O STATION                              | invert<br>ELEY                           | CRPTH<br>CF FLOW                              | 11.27<br>11.27                        | Q                    | 724              | vel<br>Head              | CAS. EL.                                      | super<br>ELEV           | CRITICAL<br>CEPTH             |                           | rest/<br>DIA | nase/<br>15 mg.  |                      | PO<br>Fire         | avere          |
| 0 1/22/29                              |  |   | **********                            | ********             |                  |                          | \$150<br>************************************ |                         | ******                        | ese serii                 | *****        | *****            | ##<br>*******<br>*** | * @ @ # #.<br>//·  | # <b>*</b> **  |
| 0 1311.96 0 15.11                      | .01102                                   | 3.30  | 1718.S7<br>1718.91                    | 183.0                | 13.94            | .00729                   | 1721.17<br>.33<br>1721.30                     | . 848<br>. 848<br>. 848 | 1.87                          | 2,84                      | 1.00<br>1.00 | .00              | .00                  | 0                  | ,00            |
| 0 8.35                                 | .01902                                   | 9.53<br>3.47                                  | 1719.10                               | 143.5                | 13.74            | .00451<br>.00451         | 1721,33                                       | , 65<br>, 65            | 3.47                          | 2.84                      | 2,00         | , 64<br>, 64     | .00                  | *                  | .00            |
| 9 2.43                                 | .01303<br>1715-23                        | 3.97  | 1719.19                               | 181.8                | 34.23            | .00383                   | 1731.35                                       | ,00                     | 3.83                          | 2.84                      | 5.00         | . 66             | .00                  | 8                  | .00            |
| SJUNCT STR<br>0 JINJ.0)                | .00398                                   | 5.74  | 1721.33                               | 136.5                | 6.93             | .00412<br>.75            | .01<br>1721.08                                | .00                     | 3.34                          |                           | 1.00         | .00              | .00                  | 6                  | ,00            |
| S 138.85<br>S 2421.68                  | ,00949<br>1716.75                        | 1.00  | 1731.75                               | 134.0                | 4.93             | ,20271<br>27,            | .38<br>1729,48                                | ,68                     | 2.34                          | 2.89                      | 5.00         | . \$40           | .99                  | ğ                  | .98            |
| 0 65.30<br>0 3486,27                   | .0444<br>1717_35                         | 4.54  | 1721.84                               | 138.0                | 7.34             | ,00254<br>.82            | 1722.66                                       | . \$4                   | 3.34                          | 3,49                      | 5.00         | .80              | . 94<br>44.          | ě                  | 200            |
| 0 16.99<br>0 1503.87                   |  | 4.39  | 1721.04                               | 13%,≙                | 7,44             | 182342<br>36_            | .94<br>1723.70                                | ,00                     | 3.34                          | 2,49                      | 5.69         | , 35             | .00                  | 0                  | .99            |
| CHITELULIC<br>0 3501.97                | 1717.45                                  | 2,30  | 1717.75                               | 136.0                | 33,84            | 3.98                     | 1722.0)                                       | ,00                     | 3,34                          |                           | 1,00         | ,00              | . 20                 | ø                  | .89            |
|  | .20949<br>1717,45                        | 2.30  | 1319,45                               | 134.0                | 2.多二的名           | ,61691<br>1,98           | 1722.90                                       | ,25                     | 2,34                          | 2.69                      | 1.00         | . 60             | 20                   | 0                  | .89            |
|  | 1718.00                                  | 2.41  | 1725,41                               | 196.9                | 14.93            | 3.20                     |   | .00                     | 3.34                          | 2,49                      | 9.50         | .00              | .88                  | 8                  | ,08            |
| 9 30.71<br>1                           | 。當當華希達                                   |   |                                       |                      | Name and a Com-  | *5118.                   | ,£7   | 1 00/000-01 (A-41111    |                               | 3,49                      |              |                  | . 69                 | PAGE               | . \$           |
|  |  | \$4.8<br>************************************ | TOTER LANGE                           | Marina Marina Marina |                  |                          | fROFILE LI                                    | 18472864                |                               |                           |              |                  |                      |                    |                |
| .fa gang.ne==an                        | 5 300 000000                             |   | Let from Di<br>Th flow                |                      | und mite<br>Wel  | vel<br>Vel               |   | 694 7 40 Miles          | CATTICAL                      |                           | WST /        | BASE;            | Ž.\$.                | -899/1             | &\/%39&        |
| 0 STATION                              |  | COF FLICH                                     | n.s.<br>Zlev                          | 4                    | to Side          | MEAD<br>ST AVE           | GRO.EL.                                       | ELXY                    | DESTR                         | scen dept                 | 2284         | MARKET<br>ID MO. | ZA<br>ZR             | F ( 4/8            |                |
| 8 44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | *****                                    | **************************************        | ***********<br>1730.75                | ********<br>\$,846   | *******<br> %.34 | ******                   |   | , 200<br>, 200<br>, 200 |                               |                           |              | , 60             | , 60<br>, 60<br>, 60 |                    | ****<br>.00    |
| 9 42,30<br>9 1841,34                   | . \$5949                                 | 2,26  | 1721.03                               | 138.5                | \$ 25 a 25 T     | -01564<br>76.6           | 1725.00                                       | . 24                    | 3,34                          | 3.49                      | 8.00         | "@@<br>****      | .00                  |                    | , ##           |
| 6 38,88                                | .50845                                   |   | 1721.26                               |                      | 14,77            | .81714<br>4.33           | 1725,43                                       |                         | 3,34                          | 2,69                      | 5.80         | .63              | 88                   |                    | .00            |
| \$ 33.76                               | .00\$49<br>1719.38                       |   | 1721.46                               |                      | 37.59            | .01991<br>4.81           | .44<br>1726,57                                |                         | 3,34                          | 2,69                      | 5.20         | . 22             | .00                  | ð                  | .00            |
|  |  | \$0.00 A                                      | * - 4-4-2-22                          | 2 N N 1 N            | 2 - 1 - 1        | .02019                   | ,15   | 4.46-48                 | -344                          | \$,10                     | 2-2-8        | n garan          | ,66                  | -0*                | 2.00.00        |
|  |  |   |                                       |                      |                  |                          |   |                         |                               |                           |              |                  |                      |                    |                |

| S 1736.78<br>S 15.64   | 1719.48  | 2.00                          | 1731,3€  | 134.8                   | 17,60   | 4,81  | 1726.37                | , 00   | 3.34                                    | 1.84                             | 2.00   | ,29   | , 89<br>. 89                           | \$          | .98      |
|--|--|-------------------------------|--|-------------------------|---|---|------------------------|--|---|----------------------------------|--|---|--|-------------|----------|
| 9 2742.42  | 1720.11  | 2.15                          | 1722.47  | 136.8                   | 18.83   | 4.40  | 1734.07                | ., 99  | 3,34                                    | 1.84                             | \$.09  | , \$\pi\$   | .00                                    | ø           | ,89      |
| 9 2783,04  | 1791-00  | 2,23                          | 1771.33  | 134.0                   | 16.04   | 4,00  | 1727,23                | .00  | 3.34                                    |                                  | \$,00  | .00   | 0.0                                    | 9           | . \$\$\$ |
| 0 15.83  | .01200<br>1771.02  | 3.22                          | 1773,43  | 138.0                   | 15.36   | .61529<br>3.44  | .24<br>1727.47         | .25  | 3,34                                    | 1.84                             | 3.00   | .55   | .00                                    | \$          | .00      |
| GJANCT STR<br>S 2803.98  | .01701<br>88.4271  | 2,04                          | 1723.73  | 126.0                   | 15.42   | -101 564 A  | .00<br>1718.05         | ,88  | 3.23                                    |                                  | \$.00  | .90   | , \$\$<br>, \$\$                       | ş           | .24      |
| 03/39CT STR<br>0 2803.98   | .01701<br>1721.48  | 2.94                          | 1713,72  | 124.0                   | 16.49   | .01905<br>4.33  | .00<br>1719.61         | ,00  | 3.33                                    |                                  | 3,50   | , \$\$  | . 44<br>44                             | \$          | .88      |
| 0 19.64<br>0 2923.42   | .01301   | 2.34                          | 1714.64  | 134,8                   | 15.98   | 3671G.  | 1718,45                | .00  | 1.21                                    | 1.76                             | 1.00   | . 22  | , \$45<br>. \$45                       | 2           | .89      |
| 9 16.79  | .01181   |                               |  |                         |   | .01588  | .33                    |  |   | 2,76                             |  |   | . 19                                   | 9400        | *        |
| ~  |  | 20 N 200                      | more investigation in a summore  | a s .h                  | 粉集了克斯   | MATALE.   | popile Li              | 871384   |   |                                  |  |   |  |             |          |
|  |  | exten                         | tribe laket<br>Let tech be   |                         | and bitts   | 60° MARS  | CVA SID                |  |   |                                  |  |   |  |             |          |
| S DINTIES  | ;wvext   | 100<br>IMPTH<br>IF FLIM       | VR FLOW<br>W.S.<br>KLEY  | ÷                       | VII.  | vel<br>Esad   | EMERGY<br>OND RI.      | SUPER  | CRITICAL<br>CEPTS                       |                                  | wet/<br>Cia  | 3426/<br>10 30.   | ZL,                                    | 080<br>8338 | aver     |
|  |  |                               |  |                         |   |   |                        |  |   |                                  |  |   |  |             |          |
| 9 1,/23,234  | #G   |                               |  |                         |   | er ave  | 16P                    |  |   | ecen captn                       |  | *****   | 艾麻                                     |             |          |
| 0 1040.32  | **************************************   | 2.19                          | **********<br>1725.06  | *********<br>126.0      | ********<br>78.2\$  | .),8ž   | **********<br>\$738.87 | 244899 <b>8</b><br>,09                               |   | ******                           |  | · * * * * * * * * * * * * * * * * * * *                                       | ******<br>,69                          | *****       | .00      |
| *******  | ******   |                               |  |                         |   | 28484898  | 1738.87<br>1738.87     |  | *******                                 | 1.76                             | *****  |   | 224.800                                |             |          |
| 0 1040.)1  | 1722.07<br>.03282  | 2,19                          | 1725.06  | 138.0                   | 15.24   | <br>  | 1738.87                | ,89  | 3.72                                    | ******                           | *******<br>3.00  | .66<br>.66  | ,09<br>,09                             | \$          | .00      |
|  | **************************************   | 2.15                          | 1725.06<br>1725.57<br>1726.00  | 128.8                   | 15.28   | 3,43<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3,123<br>3 |                        | .65  |   | 1.76                             | ******<br>3.00<br>5.00<br>5.00   | . \$5<br>. \$5<br>. \$5   | ,00<br>,00<br>,00<br>,00<br>,00<br>,00 | 0 0         | .00      |
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| **************************************   |  |                               | 1725.06<br>1725.00<br>1726.00<br>1726.36   |                         | 10.28<br>12.33<br>13.21<br>12.39  |   |                        | .00  |   |                                  | 3.00<br>5.00<br>5.00<br>5.00<br>5.00   | .00<br>.00<br>.00<br>.00  |  | 0 0         | .00      |
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Appendix C-8: Riprap Calculations for C-1 and C-2

Critical Shear Stress Calculations for Channel 1 (HEC-RAS Channel - C1)

| *************************************** | e<br>B                | A                   | <b>\$0.2</b>              |
|---|-----------------------|---------------------|---------------------------|
| 1                                       | Angle of Repose (121) |                     | Arrolle of Pheposes (24") |
| ÿ                                       | (25%)                 |                     | (2442)                    |
|   | £25.4                 | W<br>Di             | 140.70                    |
|   | Serselly Cil Water    | Specific Gravity of | Asmany of Paperage        |

| HEC-TAS 18W4 St.                        | ,                                       | 5 8      | WS. Elw                                 | å ŝ      | Vel Cryd  | 1                   | i i      |               | Street Street  | Calical Shear Street<br>on banks & side<br>(Nopes | Factor of Salary<br>(Barta & Side<br>Slopes) |
|---|---|----------|---|----------|---|---------------------|----------|---------------|--|---|--|
| 882                                     | 3                                       | 17573    | 1772.73                                 | 1000     | 1.23  | 8.0                 | 10000    | 7             | 20   | 3.28  | 77.77  |
|   | 921                                     | 1770.55  | 1 w.to. 18                              | 0.000    |   | 0.85                | 110000   | 8146.<br>\$10 | *90  | 2.5   | N  |
| ******                                  | (2)                                     | Warri    | \$2174                                  | 03331    |   | 0.50                | 0.00845  | 1             | 190  | 3.2   | \$ \$ \$                                     |
|   | 83                                      | 1770.13  | 1771,75                                 | 878000   |   | 800                 | 0.000    | **            |  | 2.7%  | 88   |
| -\$125°.                                | 130                                     | 1769.92  | \$772.54                                | 0.0000   |   | 0.00                | 0,00043  | 2,5           | *80  | 3.75  | 5.87   |
| ~2150.*                                 | (33)                                    | 1789.70  | 1771.23                                 | 60000    | **************************************  | 0.00                | 0.00025  | <b>12</b>     | 0,00   | 3.75  | \$ (\$)                                      |
| -2378.*                                 | (22)                                    | 1789.49  | \$7/1,13                                | 0.00021  | 223   | 284                 | 0.00.29  | **            | 0.84   | 275   | 5.82   |
| 00000                                   | 121                                     | 1769.28  | 1770.00                                 | 0.000888 | 233   | 800                 | 0.00057  | 23            | 0.65   | 3.75  | 5.77   |
|   | ***                                     | 1769.08  | 1770.70                                 | 0.00055  |   | 0.05                | O.CAZESS | 1.2           | 0.65   | 3.73  | 6.73   |
| -2246.5*                                | 121                                     | 1756.88  | 1770.51                                 | 0.00063  | 223   | 0.00                | 0.00831  | 1.2           | 0.65   | 3.7%  | 5.78   |
| 2002                                    | # ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( | 1768 68  | 1770.31                                 | 0.00348  | i i i i i i i i i i i i i i i i i i i   | 0.86                | 0.00845  | Z             | 0.04   | 3.75  | 2,000  |
| 2373 (8)                                | 127                                     | 08.737.1 | 1779.43                                 | 24000    | \$20  | 980                 | 0.00641  | 12            | 160  | 3.75  | 5.84   |
| 1 976                                   | 121                                     | 178720   | 1788.83                                 | 0,000,40 | \$23  | 540                 | 0.00000  | 12            | 0.83   | 3,7%  | 7.09   |
| -\$40°                                  | 121                                     | 09 994   | 1768.42                                 | 0.000    |   | aro l               | 0.000.00 | ę.            | 0%0  | 3.7%  | 2.44   |
| 2.0902                                  | 121                                     | (700.00  | 1767.48                                 | 0.01160  |   | 101                 | 001159   | ę.            | 0.25   | 37%   | 4 23   |
| .2.28.2.                                | * C.                                    | 175421   | 1745.47                                 | 953,550  | # CO  | 1,46                | 001594   | 12            | 0.84   | 2.5   | 360  |
| *                                       | \$ P                                    | 1752.42  |   | 221100   | 23  | ***<br>****<br>**** | 0.01823  | 7%<br>20%     | Ž  | Z.  | Br   |
| *************************************** | 3.6                                     | 176264   | 28182                                   | 0.01987  |   | *****               | 2000     | f*4           | 1,05   | 3.73  | 220  |
|   | 900<br>(19)<br>(20)                     | 20.00    | 70 CM.                                  | 179100   |   | en<br>Cili          | 0.010.0  | (V)           | in the second se | 27.0  | ri<br>ri                                     |
| *                                       | <i>i</i>                                | 8220     | *************************************** | 0.01667  | 2.4%  | 2                   | 2000     | 74<br>***     | 111  | 0   | R  |
| 1.760                                   | ***                                     | 175527   | 27.8.73                                 | 27.00    | 1.2.2   | **                  | 0.01785  | eų.           | 3,18   | e   |  |
|   | \$25                                    | 1753.48  | 1754.304                                | Cocata   | ***   | 83                  | 0.01789  | PN<br>300     | 1,13   |   | N  |
| *****                                   | ***                                     | 1731.773 | 175,207                                 | 001764   | S   | \$2.5               | 0.01788  | 12            | 27.3   | 312   | 327  |
| 1,1970                                  | 'n                                      | 1749.91  | 1751.27                                 | aonate   |   | 87                  | 001700   | 22            | ***  | 200   |  |
| た./原治・                                  |   | 174%.12  | 1749.43                                 | 001773   |   | \$2.5               | 0.01738  | £2            | 1,35   | 22  |  |
| - 12 TANK                               | 10x                                     | 1746.33  | 87.47.73                                | 0.01800  |   | 1.27                | 0.01789  | Ŋ             | 100  | 373   | \$27   |
| 17.60%                                  | 131                                     | 1744.54  | 1745.91                                 | 0.017968 | 7.28  | 1.27                | 0.0173/0 | 814<br>***    | 1.15   | 27%   | 223  |
| -3874.1                                 | 122                                     | 1743.00  | 1744.37                                 | 0.01778  | n in the state of | 1.28                | 0.01767  | enj<br>1      | 100 m  | 3.73  | 3.27   |

Notes: Riprap design applies to stations -2000 through -3874.10.

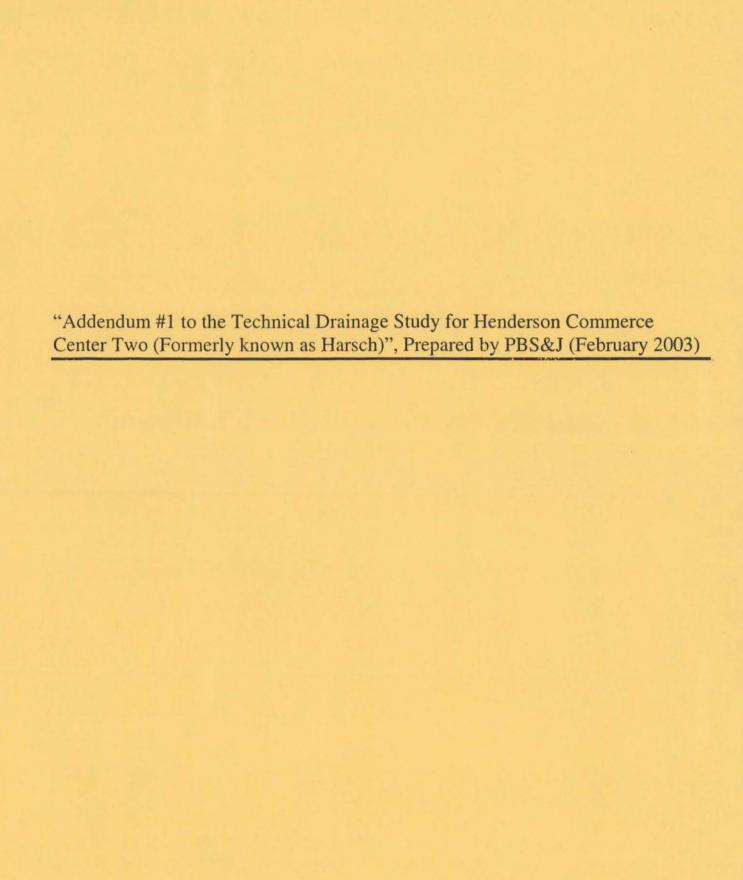
Critical Shear Stress Calculations for Channel 2 (HEC-RAS Channel - C2)

|  | Angle of Personal 127 Cats Count Colo State (217) | Angle of Repose (18") 20 8 Days Side Sign (depress) 18.43 |                    |
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| And the second s | 62.4 (20th)                                       |   |                    |
| A CONTRACTOR OF THE PROPERTY O | Dennity of Water                                  | Specific Gravity of<br>Pipras                             | Certific Districts |

| L        | _          |          |  |        |  |            |   |       | 1.00                   | 3 4  |
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| <u> </u> |            |          | 10 00 00 00 00 00 00 00 00 00 00 00 00 0 | No.    | 13.05<br>4 Q   | Frem Shape | R.> Pag Sur                               |       | Original Street Street | Factor of Switch<br>(Barrier & Side<br>Singer) |
| 3        |            | 8        | (44)                                     | (17,3) |  | 8.8        | (Jan)                                     | (444) | Chai                   |  |
| 1757 97  |            | 1759.17  | 001310                                   | 527    | .01  | 004500     |   | 0.58  | 22.5                   | *  |
| 1757.29  |            | 17.43    | 001478                                   |        | 1,17   | 1600       | 24  | *4.0  | 3.75                   | 3,   |
| 1755.55  |            | 1757.83  | 0.010.0                                  | £.     | SE*  | 0.01653    | 12  | 265   |                        | **   |
| 1755 83  |            | 17.00    | 001100                                   |        | Ç.   | 0.01813    | **  | X O   |                        | 90*  |
| 1755.10  | _          | 1724.18  | 0.01815                                  | 2.0    | 131  | 0.01789    | 2   | 0.83  | 3.23                   | * 10   |
| 154 38   | -          | \$755.48 | 001791                                   | £3     | 8.   | 00000      | ***                                       | 180   | S. P.                  | <b>*1</b>                                      |
| 1753.02  | _          | 1755,00  | 001210                                   | 823    | Ø. 1.  | 148.100    | 21  | ****  | 7.25                   | *0*  |
| 1753.48  | -          | 1754.54  | 1/21,00                                  | 8%     | igen<br>Time<br>Time<br>Time<br>Time<br>Time<br>Time<br>Time<br>Time | 001580     | **  | 0.71  | 2.2                    | 8  |
| 1753.00  | - minning  | 12,421   | 001347                                   | 88     | ***  | 001217     | €.<br>•                                   | 80    | 372                    | 3*6  |
| 1751.00  | ranena e   | 1751.90  | 00342                                    | 7.73   | 1.56   | 0.0100     | 1. T. | 0.84  | S S                    | 4,4%   |
| 00.810   | -imino-    | 1723.13  | 0.010.03                                 | 88     | 87   | 03030      | 1   | 100   | 3.75                   | 3,48   |
| 1748.50  | 0          | 1740.58  | 0.01927                                  |        | 8,   | 0.01828    | 4   | 0.91  | 372                    | 4.13   |
| 1748.00  | 0          | 1749.07  | 100100                                   | 7.03   | 37.3   | 02100      | 12  | 0.06  | 3.75                   | 3.84   |
| 174750   | _          | 1748.57  | 0.01976                                  | 7.85   | 1.37   | 0.01970    | 1 m                                       | 0.99  | 3.75                   | 3,80   |
| 1747.00  | _          | 1748.00  | 0.000.5                                  | 2,12   | (A)  | 0.00001    | 2.00<br>***                               | 0.83  | 3.75                   | 3.73   |
| 1748.50  | , C. C. C. | 1748.17  | 0.00452                                  | 3.91   | 0.63   | 0.00,065   | 12  | 0.21  | 3.75                   | 18.12  |
| 1748.00  |            | 1740.19  | 0.00174                                  | 2.87   | 0.30   |            |   |       |                        |  |

Notes: Piprap design applies to stations -2000.00 through -2669.88.

Appendix D: Reference Material



# ADDENDUM #1 TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMMERCE CENTER TWO (FORMERLY KNOWN AS HARSCH)

Prepared for:

Harsch Investment Properties LLC 1121 SW Salmon Street Portland, Oregon 97205

Prepared by:

PBS&J 2770 Corporate Circle, Suite 100 Henderson, Nevada 89074

PBS&J Reference Number: 511434 February 18, 2003



FLOOD STDROGRAFH PACEAGE (SEC-1)
JUN 1998
VERSION 4.1
RUN DATE GTJANG3 TIME 16:37:43

U.S. ARMY CORPS OF EMPINEERS
HYDROLOGIC EMPINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 755-1104

| X   | ×    | XXXXXXX | XX | XXX |       | X.  |
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1GS, AND HEC1EM,

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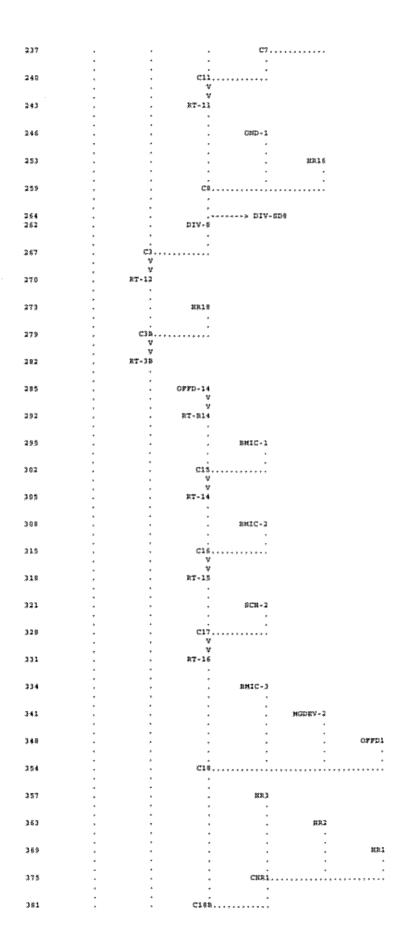
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MARSCH OMSITE BASIN

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|            | *   | ,       |  |  |             |
| 196        |     | *       | 8                                      | ~~~~~» DIV   | - SD\$      |
| 294        | *   | н<br>2  | A<br>PIA-8                             |  |             |
| 199        | *   | ٠       | ¥T+7                                   |  |             |
| 499        | -8  | *       | ****                                   |  |             |
| 202        | . * | *       | 4                                      | na?  |             |
| ***        | *   | *       |  | *  |             |
| 200        | *   | *       | CEA                                    |  |             |
|            | *   | *       |  |  |             |
| 211        | *   | *       | 4                                      | HE13   |             |
|            | ,   |         | ¥                                      |  |             |
| 217        | *   | .9      | Csn                                    | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,   |             |
|            | 16  | *       | *                                      |  |             |
| 230        | *   | *       | *                                      | offd-Kl  |             |
|            | *   | •       | ,                                      | ¥  |             |
| 227        | *   | •       | ,                                      | KT-10  |             |
|            | *   | *       | *                                      | 7  |             |
| 230        | *   |         |  | ,  | OFFD-4      |
|            | •   | *       | a<br>4                                 | . ,  | 7 11        |
|            |     |         |  |  |             |



|              |                 | *  | *       | *     |                         |                     |                                       |      |
|--------------|-----------------|----|---------|-------|-------------------------|---------------------|---------------------------------------|------|
| 31           | 85              | *  | *       | *     | 製業系                     |                     |                                       |      |
|              |                 | *  | 4       | 2     |                         |                     |                                       |      |
| 31           | 81              | *  | *       | *     | *                       | an i                |                                       |      |
| -97          | <del>7. 5</del> | *  | ,       | *     | *                       | 9                   |                                       |      |
| 20.0         | no 70s          | 0  | ,       | *     |                         | ٠                   | Yers A                                |      |
| 3 9          | 8.3             | *  | 4       | *     | ,                       |                     | 3R-46/18                              |      |
|              |                 | .8 | ,       |       |                         | -8                  | *                                     |      |
| 48           | ))              |    | .8      | 4     | CHAI                    | 264004333434        | *******                               |      |
|              |                 | 4  | *       | ,     |                         |                     |                                       |      |
| 44           | 29              | *  | *       |       | * * * * * * * * * * * * |                     |                                       |      |
|              |                 | *  | ,       |       |                         |                     |                                       |      |
| 43           | 1.3             | *  | •       |       | <b>彩製 1.0</b>           |                     |                                       |      |
|              |                 | *  | 9       | ,     | ,                       |                     |                                       |      |
| 41           | L9              | ,  | и       | *     | *                       | MA.9                |                                       |      |
|              |                 | *  | *       | *     |                         | *                   |                                       |      |
| 42           | 15              | ,  | e<br>it | *     | cara i                  | ,<br>,,,,,,,,,,,,,, |                                       |      |
|              |                 | *  |         | ,     | *                       |                     |                                       |      |
| 43           | 11              | *  | ir      | 4     | 4                       | 推測者                 |                                       |      |
| শুক <i>য</i> | **              |    | ,       | *     | *                       | 99-80 (8            |                                       |      |
| 43           | .~              | ¢  | *       | ,     | 4                       | 9                   |                                       |      |
| 40,7         | 1.9             | *  | ,       | £180, | *********               |                     |                                       |      |
|              |                 |    | *       | -0    |                         |                     |                                       |      |
| 44           | i               | k  | a<br>н  | 4     | BNIC-4                  |                     |                                       |      |
|              |                 | *  |         | a     | ,                       |                     |                                       |      |
| 4 4          | 18              | *  |         | Clas, | = + + * + + * * + + +   |                     |                                       |      |
|              |                 | ,  | ,       |       |                         |                     |                                       |      |
| 难想           | 12              | *  | *       | *     | e Lan                   |                     |                                       |      |
|              |                 | *  | *       | *     | *                       |                     |                                       |      |
| 4.5          | 10              | ٠  | 9       |       | *                       |                     |                                       |      |
|              |                 | «  | ,       | *     | ,                       | *                   |                                       |      |
| 4.0          | 4               | k  |         | *     |                         |                     |                                       |      |
|              |                 | *  | *       | 9     | 9                       |                     |                                       |      |
| 47           | 6               | *  | *       |       | *                       | ER13                |                                       |      |
|              |                 | •  | 7       | ,     | *                       |                     |                                       |      |
| 47           | 16              | ,  | 4       | *     |                         | **                  | NA17                                  |      |
|              |                 | *  | *       |       |                         | 4                   | ,                                     |      |
| 看着           | 12              | *  |         | *     | 4                       | *                   | *                                     | MR15 |
|              |                 | *  | ٠       | ,     | 2                       | *                   |                                       |      |
| 4.8          | 18              | *  | *       | ,     | curs.                   | *                   | · · · · · · · · · · · · · · · · · · · |      |
|              | -               |    | *       | ,     | *                       |                     |                                       |      |
| 43           | 1.4             | à  | *       |       | * * * * * * * * * *     |                     |                                       |      |
| · ***        | •               | .2 | 9       | 9     | ********                |                     |                                       |      |
| 45           | v 40            | y  | *       | *     | 0770-13                 |                     |                                       |      |
| **3          | ₹ ₹             | *  | *       | *     | *******                 |                     |                                       |      |
| 40.0         | s -s            | 4  | *       | *     |                         |                     |                                       |      |
| \$8          | 49              |    | *       | ٠     |                         | SCH-1               |                                       |      |
|              |                 |    | *       | *     | ,                       |                     |                                       |      |
| \$3          | IJ              | •  | ,       | •     |                         | *                   | CULCH-1                               |      |
|              |                 | *  | -8      | •     | *                       |                     | *                                     |      |
| \$3          | 16              | 9  | *       | я     | *                       | C13                 |                                       |      |
|              |                 |    |         |       |                         |                     |                                       |      |

(\*\*\*) RUMOFF ALSO COMPUTED AT TRIS LOCATION

| * | FLOOD   | HTDROGRAPH | PACKAGE | (MEC-1)  |     |
|---|---------|------------|---------|----------|-----|
| * |         | 3131       | 1990    |          | 4   |
| * |         | version    | 4.1     |          | •   |
| * |         |            |         |          | •   |
| * | RUN DAT | TE 07JANO: | TIME    | 16:37:43 | -18 |
| * |         |            |         |          |     |
|   |         |            |         |          |     |

U.S. ARMY CORPS OF ENGINEERS HYDROLOGIC EMPLIMENTING CENTER 699 SECOND STREET DAVIS, CALIFORNIA 95616 (916) 758-1194

TECHNICAL DRAINAGE STUDY FOR HARSCE FILE - BADEY RI.DAT HEC-1 FOR HARSCH PROJECT NUMBER: 511434

OFFSITE BASINS REFERENCED FROM THE UPDATE TO THE TECHNICAL DRAINAGE STUDY FOR EASTGATE BOAD (EGS2)

### PREPARED BY PREAJ, MAY 1002

| 2.3 | 10      | OUTPUT CONTROL  | VARIABLES |                                 |
|-----|---------|-----------------|-----------|---------------------------------|
|     |         | IPENT           | \$        | PRINT CONTROL                   |
|     |         | TPLOT           |           | FLOT CONTROL                    |
|     |         | COCAL           | 0.        | HYDROGRAPH PLOT SCALE           |
|     | **      | eydrogrape Ties | I DATA    |                                 |
|     |         | 10173           | 3         | MINUTES IN COMPUTATION INTERVAL |
|     |         | IDATE           | 1 9       | STARTING DATE                   |
|     |         | ITIME           | 0000      | STARTING TIME                   |
|     |         | #Q              | 300       | NUMBER OF HYDROGRAPH CADINATES  |
|     |         | MINDATE         | 1 0       | ENDING DATE                     |
|     |         | MUTIME          | 2.457     | ENDING TIME                     |
|     |         | ICENT           | 2.排       | CENTURY HARK                    |
|     |         | COMPUTATION I   | mterval.  | .05 BCCRS                       |
|     |         | TOTAL TI        | ME BASE   | 14,95 NOURS                     |
|     | exclisa | UNITS           |           |                                 |

ING UDATE
DRAINAGE AREA
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET

CUBIC FRET PER SECOND

YLON STORAGE YOUNE SURFACE AREA ACRE-FEET

TEMPERATURE DEGREES PARREMEET

MULTI-PLAN OPTION HTLAN

3

1 NUMBER OF FLAMS

MULTI-RATIO OPTION
BATIOS OF PERCIPITATION
.58 1.00 JE

\*\*\* FIRRUT HABBIEG TIME STEP CALCULATION FAILED TO CONVERGE. STABILITY PROBLEMS MAY RESULT

PRAE FLOW AND STAGE (SMC-OF-PERIOD) SUMMART FOR MULTIPLE FLAW-RATIO ECONOMIC COMPUTATIONS FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES TIME TO PEAK IN SOURS

| operation       | STATION       | AREA        | FLAN |               | EATIO 1     | to precipitation |
|-----------------|---------------|-------------|------|---------------|-------------|------------------|
| HTD*CODAPH AT   | offd-1a       |             | 3    | FL/JH<br>TIME | 19.<br>2.88 |                  |
| NTDROJEANN AT   | OFFD-1B       | .03         | 1    | PLOM<br>TIME  | 33.<br>3.55 |                  |
| * HTDROGRAPH AT | OFFD-H1       | .01         | 1    | Pl/M<br>Timb  | 4,<br>3,55  |                  |
| ROUTED TO       | # <b>T</b> -1 | .01         | 3.   | FLON<br>TINE  | 4.<br>3.55  |                  |
| HTDRIXIRAPH AT  | Cf73-bhi      | .01         | 1    | 71.7%<br>Tins | 3.<br>3.55  |                  |
| 3 COMMINED AT   | C1            | , <b>84</b> | 1    | Plon<br>Tine  | 31.<br>3.55 |                  |
| BOUTED TO       | ¥2×3          |             | 1    | FLAM<br>TIKE  | 27,<br>3.60 |                  |
| STEROGRAPH AT   | OFFD-1        | . © 1       | 1    | linz<br>Liva  | 4.<br>9.50  |                  |
| 2 COGINED AT    |               | 405         | 1    | PL/M<br>Tine  | 33.<br>3.53 |                  |
| *               | x7-3          | ±0\$        | *    | Fi.CH         | 32.<br>3.40 |                  |
| HYDROGRAPH AT   | offd-1        | .01         | 1    | P1/34<br>Tike | 5.<br>3.50  |                  |

| 2 COMBINED AT                          | CNS           | ,04           | 3         | flow<br>Tine  | 34.<br>3.55    | 84.<br>3,55        |
|--|---------------|---------------|-----------|---------------|----------------|--------------------|
| DIVERSION TO                           | DIA-2DA2      | , \$€         | 3 .8.     | Plow<br>Time  | 38.<br>3.33    | 75.<br>2.55        |
| HIDEGRAPH AT                           | DIA-HB        | .06           | 2         | PLON<br>TINE  | \$ a<br>a \$ 4 | 9.<br>3.35         |
| ETDROGRAFE AT                          | 0770-13       | ,81           | 1         | FLAN<br>Tine  | 34.<br>3.85    | 26,                |
| NTDROGRAPH AT                          | ONT) S        | . 80          | 1         | FLOW<br>TIME  | 3.50           | 3.                 |
| 2 COMBINED AT                          | CX.           | .61           | 1         | flom<br>Tikk  | 14.<br>3.39    | 24.<br>3.55        |
| Diamsion to                            | DIV-EDE       | . \$1         | 3         | FLOW<br>TIME  | 15.            | *1.<br>3.33        |
| NYDROGRAPH AT                          | DIA-E         | , \$ <u>1</u> | 3         | FLOM<br>Time  | 3.             | 7.                 |
| ROMITED TO                             | # <b>*</b> ** | .01           | :4<br>.a. | PLON          | 3.53           | 7.                 |
| NTDROGRAPH AT                          | OND-4         | . 43          | 1         | Tins<br>Fiam  | \$.\$\$        | 3,                 |
| HTDROGRAPH AT                          | OSD-11        | .03           | **        | Time          | .2.58<br>24.   | 43,                |
| ) COMMINED AT                          | C4            | ₃ Ñ <b>ા</b>  | 1         | Time          | 2.55           | 54.                |
| HIDROGRAFH AT                          | (240×)        | , 8 \$        | 3.        | Time<br>Flor  | 3.55<br>3.     | <b>\$</b> ,        |
| HTDROUBAPH AT                          | CULCH«3       | .00           | **        | TIMS<br>FLOW  | 3,55<br>8.     | 7.83<br>1.         |
| 3 COMBINED AT                          | C\$           | .85           | 7         | Tims<br>FL/34 | 7.55<br>30.    | 3.50<br>\$4.       |
| piversion to                           | DIV-SDS       | * 尊多          | 1         | Tine          | 3.25           | 3.55<br>84.        |
| NTDROGRAPH AT                          | piy.š         | *\$5          | 1         | Time          | 2.55<br>8.     | <b>å</b> ,         |
| HTDROUBAPH AT                          | OMD+18        | , 俊惠          | 1         | Time<br>Flow  | ,00<br>24.     | .00<br>40.<br>3.55 |
| 2 COMBINED AT                          |               | . 87          | ž         | Tine<br>Flan  |                |                    |
| ************************************** | 27.4          | .07           | 1         | Tins          |                | 3.55               |
| NTDEOGRAPH AT                          |               | .01           |           |               | 3.55           |                    |
| HTDROGRAPH AT                          |               | . 85          |           | TIME          | 3.88           |                    |
| 1 COMBINED AT                          |               | .00           |           | TIME          | 3.50           |                    |
| NTDROGRAPH AT                          |               |               |           | TIME          |                | \$3.<br>3.85       |
| *                                      | 23.1.12×04    | .0)           | 1         | FL CH         | 23.            | \$7.               |

|   |              |         |      | TIME                     | 3,50            | 3,50         |
|---|--------------|---------|------|--------------------------|-----------------|--------------|
| 2 COMBINED AT                           | C.S          | ,33     | 3.   | TLON<br>TIME             | 63.<br>3.50     | 120.<br>3.50 |
| piarrica 10                             | niv-sps      | , 1.1   | .3.  | FLOM<br>TIME             | 51.<br>3.50     | 99.<br>3.50  |
| #71280733A#8 AT                         | \$17×4       | .33     | .\$. | FLOW<br>TIME             | 1.<br>3.50      | 32.<br>3.58  |
| *************************************** | <b>聚</b> 省»等 | ÷ \$.\$ | 1    | flom<br>Time             | 1,<br>3,55      | 30.<br>2.55  |
| NIDROGRAPH AT                           | 製洗7          | .00     | 1    | FLCM<br>TIME             | 2.<br>3.55      | 5.<br>3.55   |
| 2 COMBINED AT                           | CSA          | .11     | 3.   | FLON<br>TIME             | 夢?<br>漢   ※ ※ ※ | 35.<br>3.55  |
| exproduate at                           | ur13         | .00     | 1    | PLON<br>TIME             | \$.<br>3.50     | 9.<br>3.50   |
| * COMBINED AT                           | CER          | . 11    | 1    | PLON<br>TIME             | 0.<br>3.50      | 4).<br>3.55  |
| NYDROGRAFE AT                           | OFFD-HG      | ,91     | *    | PLOM<br>TIME             | 10.<br>3.59     |              |
| * ************************************* | *T-10        | .81     | 3.   | TLOM<br>TIME             | 10.<br>1.50     |              |
| HYDROGRAFE AT                           | 0770-4       | .81     | 3.   | PL/M<br>TIME             | 43.<br>3,55     | 27.<br>3.50  |
| 1 COMBINED AT                           | C7           | . 92    | 1    | PLOM<br>TIME             | 23.<br>3.50     | 4%.<br>3.50  |
| 1 COMBINED AT                           | £23          | .14     | 1    | FLAM<br>TIME             | 31.<br>3.50     | 98.<br>3.50  |
| NOUTED TO                               | ***11        | .14     | 1    | TIME                     | 30.<br>2,55     | 87.<br>3.55  |
| HYDROGRAPH AT                           | cso-1        | .00     | 1    | FLOM<br>TIME             | 4.<br>3.50      | #.<br>3.50   |
| NYDROGRAPH AT                           | HALL         | .00     | 1    | PL/M<br>Tinz             | ).<br>3,50      | 7,<br>1,50   |
| ) COMBINED AT                           | Ca           | .14     | 3    | FLCM<br>TIME             | 38.<br>3.50     | 100.         |
| pivaraion to                            | \$\$**\$\$\$ | .14     | 1    | FLOM<br>TIME             | 11.<br>1.50     | 18.<br>3.55  |
| HYDROGRAPH AT                           | DIV-8        | .14     | 1    | PLOM<br>TIME             | 漢字·<br>漢·黎朝     | 82,<br>2,55  |
| 1 COGINED AT                            | СЭ           | .30     | 1    | ric <del>u</del><br>Tiks | 27.<br>3.30     | 91.<br>3.85  |
| * *                                     | XT-13        | .70     | 1    | FLOW<br>TIME             | 27.<br>3.55     | 91,<br>3,35  |
| NYDROGRAPH AT                           | HR.13        | * 99    | 3.   | F1.CM<br>TIME            | 4.<br>3.58      | 9.<br>3.85   |
| 2 COMMINED AT                           | C)B          | .20     | 3.   | FLCH<br>TIME             | 31,<br>3,5\$    |              |
| ROUTED TO                               |              |         |      |                          |                 |              |

| *                                      | ET-3D                   | .20          | 1     | FLOW          | 39.                | 95.           |
|--|-------------------------|--------------|-------|---------------|--------------------|---------------|
| RTDROGRAPH AT                          |                         |              |       | TIKE          | 1,60               | 3,55          |
| *                                      | OFFD-14                 | .00          | 1     | flon<br>Time  | 1.<br>3.65         | 3,40          |
| * TO CATED TO                          | RT=#14                  | .60          | 1     | PLON<br>Tins  | 1.                 | 3.<br>3.65    |
| HYDROGRAPH AT                          | BNIC-1                  | , S & &      | 3.    | YLON<br>TIME  | 27.<br>2,55        | 24.<br>3.50   |
| * COMPIESD AT                          | C15                     | <b>此</b> 泰元  | 1     | FLOW<br>TIME  | %4.<br>2.53        | 28.<br>3.35   |
| * SCALED 10                            | <b>独学。3.4</b>           | × 0 3        | 2     | FLCM<br>TIME  | 24.<br>3.56        | 28.<br>3.55   |
| ************************************** | BMIC-2                  | .01          | 3.    | FLOM<br>TIME  | 11.<br>3.50        | 22.<br>3.50   |
| 2 COMBINED AT                          | Clé                     | . 83         | 1     | FLOW<br>TIME  | 24.<br>3.55        | 59.<br>3.50   |
| NOTED TO                               | RT+15                   | . 93         | 1     | Time<br>Time  | 24.<br>3.55        | \$\$.<br>3.85 |
| NTINGGRAPH AT                          | \$C# - 1                | »& <b>3</b>  | 1     | FLOW<br>TIME  | š.<br>3.30         | 13.<br>3.50   |
| 2 (3981) AT                            | , গুণ কু বা<br>বৈশ্ব কু | .94          | 1     | FLOW<br>Time  | 29.<br>1.54        | \$2.<br>3.50  |
| * ************************************ | NT-16                   | 4 <b>0 4</b> | 3.    | line          | 39.<br>3,55        | 61.<br>3.53   |
| Sydenmate at                           | nmic-j                  | 桌臀和          | *     | FLOW<br>TIES  | \$ 0 ,<br>\$ . 5 0 | 31.<br>3.50   |
| HTDROGRAPH AT                          | MCCEV-1                 | ·, \$2       | 1     | 71.cm<br>Tine | 9,<br>1,52         | 18.<br>3.50   |
| eturcurate at<br>*                     | offd1                   | +基基          | 3.    | Tine<br>Tine  | 14.<br>3.95        | 56.<br>3.90   |
| . COMPLIED AT                          | <b>花</b> 茅              | ×26          | 1     | flox<br>Tirk  | 50.<br>3.53        | 120.<br>3.55  |
| HYDROGRAPH AT                          | uri                     | ,00          | 1     | flox<br>Tiks  | 1.<br>1.50         | 3.<br>3.50    |
| BYDROGRAPH AT                          | XR2                     | <b>小春</b> 台  | , Age | VLCH<br>Tine  | 2.<br>2.50         | 4,<br>3,50    |
| HYDROGRAPH AT                          | HRI                     | , 99<br>,    | 1     | PLON<br>TIRE  | 2.<br>3.50         | 3.<br>3.50    |
| 3 COMBINED AT                          | сия:                    | ,00          | 1     | PLON<br>TIES  | 5.<br>3.50         | 10.<br>3.50   |
| 2 COMMINED AT                          | <b>C.18</b> 8           | 4.3.7        | 1     | Flow<br>Tinz  | 34.<br>3.5\$       | 127.          |
| HYDROGRAPH AT                          | 解測多                     | . 98         | 1     | Plon<br>Tiez  | J.<br>3,50         | 4.<br>1.50    |
| HYDROGRAPH AT                          | <b>新真新</b>              | n 🔮 🛣        | *     | PLOM<br>Tinz  | 11.<br>2.50        | 19.<br>3.50   |
| HTDROGRAPH AT                          | 2234                    | .01          | 3,    | Plan<br>Tiks  | 11.<br>3.38        | 19.<br>3.50   |

| . COMBINE                              | ID AT        | CMRI                      | .02            | 1  | FLOW<br>TIME         | 24.<br>3.56                               | 44.<br>3.50  |       |          |  |              |
|--|--------------|---------------------------|----------------|----|----------------------|---|--------------|-------|----------|--|--------------|
| 2 COMBINE<br>*                         | ID AT        | 238Z                      | *19            | 3  | FLAM<br>Tana         | **.<br>3.50                               | 169.<br>2,58 |       |          |  |              |
| htdrograph<br>*                        | l at         | 製料達容                      | .00            | *  | TL/M<br>Tinz         | <b>5</b> • <b>2</b> • <b>2</b> • <b>2</b> | 10.<br>3.50  |       |          |  |              |
| HYDROIRAFE<br>*                        | at at        | <b>以取</b> 多               | .00            | 1. | plon<br>Tinz         | \$ .<br>3 . 30                            | 10.<br>3.30  |       |          |  |              |
| . COMPINE                              | d at         | CEL                       | .91            | 1  | FLOM<br>TIME         | 10.<br>3.50                               | 30.<br>3,79  |       |          |  |              |
| HYDROGRAPH<br>*                        | i at         | nna                       | <b>,</b> \$\$  | 3. | PLON<br>TIME         | 3.50                                      | *.<br>1.50   |       |          |  |              |
| . COMBINE                              | D AT         | C180                      | .20            | 1  | fiom<br>Time         | #1.<br>I.AP                               | 195.<br>3.30 |       |          |  |              |
| NYDROGRAPH<br>*                        | 1 <b>a</b> t | <b>新棋工作。</b> *            | .01            | 1  | TLOM<br>TIME         | 10.                                       | 30.<br>3,30  |       |          |  |              |
| 2 COMBINE<br>*                         | D AT         | Cler                      | .21            | 1  | Pian<br>Tine         | 109.                                      | 215.<br>3.50 |       |          |  |              |
| NTUROGRAPE<br>*                        |              | 類然是者                      | , 00           | 1  | Plon<br>Tirk         | 3.29                                      | 5.<br>3.50   |       |          |  |              |
| ntdrografe<br>*                        |              | 超级录法                      | ,00            | 3. | TIME<br>TIME         | 4,<br>3.50                                | 11.<br>3.50  |       |          |  |              |
| 2 COMBINE                              |              | CERI                      | .01            | 1  | flox<br>Time         | 3,50                                      | 16.<br>3.50  |       |          |  |              |
| ************************************** |              | E212                      | . 88           | 1  | Tinz<br>Tinz         | *.<br>3,59                                | 7.<br>3.50   |       |          |  |              |
| RYDROGRAFE                             |              | MA17                      | ,00            | 1  | Time<br>Time         | 3.59                                      | 9.<br>3.84   |       |          |  |              |
| * COMBINE                              |              | MR15                      | .00            | 1  | FLON<br>TINE         | 3.39                                      | 3.50         |       |          |  |              |
| · COMBINE                              | D AT         | CMRS                      | ,51            | 3. | TIKE<br>TIKE         | 20.<br>3.50                               | 35.          |       |          |  |              |
| HYDROGRAFI                             | i at         | CFFD-13                   | .22            | 1  | FLOH<br>TIME<br>FLOH | 3 - 5 A                                   | 250,<br>3.50 |       |          |  |              |
| ###################################### | i at         | *CH-1                     | , ###<br>  ### | *  | TIME                 | 3.50<br>7.                                | 3.50         |       |          |  |              |
| NYTHOGRAPH                             | i at         | CULON-1                   | .88            | 1  | TIME                 |   | 3.80         |       |          |  |              |
| 1 commina                              | ED AT        | (2)                       | . 8 %          | 1  | Time<br>Plon         | 3,50                                      | 3.50         |       |          |  |              |
| 3                                      |              |                           |                |    |                      | 3.50<br>T OF KINEMAT:<br>LOW IS DIREC     |              |       | sk plon) |  |              |
|  | 1STA         | o element                 | DT.            |    | Peak                 | TIME TO<br>PEAK                           | AUTRWE       | et    |          | LATED TO<br>LAVELTHIE N<br>OT SHIT<br>LASE | ACTURE       |
|  |              |                           | (MIM)          | )  | (CFS)                | (16.214)                                  | (IM)         | (MIN) | (CFS)    | (MIH)                                      | (IN)         |
|  |              | LAN • 1 RATI:<br>T-1 NAME | )• .58<br>.6.  | *  | 4.44                 | 214,19                                    | . 47         | 3,09  | *.3%     | 21).00                                     | <u>, \$7</u> |

17

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CONTINUIT SUMMARY (AC-FI) - INFLORM. ,23818-88 EXCESS. .88980-00 COTFLOR. ,23818-88 ENGRAGE. .48980-98 PERCENT ERROR. -.1
                FOR PLAN - 1 RATIO- 1.00
                                                     .61
                                                                                               1.43
                      my - 1 MANE
                                                               10.28 311.12
                                                                                                                3.60
                                                                                                                                 10.19
                                                                                                                                               213.00
                                                                                                                                                                        1.63
CONTINUITY SUBMART (AC-FT) - INFIGN. .5573E.00 EXCESS. .0000E.00 OUTPLOW. .5578E.00 BASIN STORAGE. .4890E.08 PERCENT ERROR. -.1
                FOR PLAN - 1 RATIO- .58
                                                     . $7
                      RT-2 MANE
                                                                  30.66 214.70
                                                                                                   .71
                                                                                                               3.00
                                                                                                                               19.18 216.00
COMPANY TOTALE STATEMENT S
               FOR PLAN = 1 RATIO: 1,05
                      RT-3 MANE
                                                     。拼节
                                                                  49.07 211.95
                                                                                                   1.69
                                                                                                                    3.00
                                                                                                                                   67.93
CONTINUITY SUMMARY (AC-FT) - INFLOW- .1945E-01 EXCESS- .8800E-05 OUTFLOW- .1945E-01 BASIN STORAGE- .1092E-05 PERCENT REPOR- -.1
                FOR PLAN + 1 FATTO- . SE
                                                      .61
                                                              33.92 214.50
                                                                                                    .70
                                                                                                                    3.00
                                                                                                                                   22.39
                                                                                                                                               216,00
CONTINUITY COMMANY (AC-FT) - INFLOW- .18588-01 EXCESS- .80000-00 COUTFLOW- .18588-01 RABIN STORAGE- .18758-05 PERCENT ERROR- -.1
                FOR FLAN - 1 RATIO- 1.00
                                                              77.01 211.87
                                                    ****
                      BT-1 MANE
                                                                                                3.49
                                                                                                                    3.00
                                                                                                                                 75.58
                                                                                                                                               213.00
                                                                                                                                                                         1.68
CONTINUITY SUMMARY (AC-FT) - INFLOW- .44678-01 EXCESS- .00008-00 OUTFLOW- .44698-01 BASIN STORAGE- .30598-06 PERCENT ERROR- .0
                YOR PLAN - 1 BATTO- ,58
BT-X MANE 1.
                                                    1.35
                                                                      .98 215.44
                                                                                                                                               216,00
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CONTINUITY SUMMANY (AC-FT) - INFLOW- .8142E-01 EXCERS- .8200E-5.00 COLTUMITY SUMMANY (AC-FT) - 1340E-07 PERCENT ERROR- .1340E-07 PERCENT ERROR- .1340E-07
                POR PLAN - 1 BATIO- 1.00
                                                     . 23
                                                                    7.02 314.44
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                                                                                                                                     4.20
                                                                                                                                                 213.00
                      ST-I MANE
CONTINUITY SUMMARY (AC-FT) - INFLOW- .2048E-90 EXCESS- .0000E-00 OUTFLOW- .2057E-00 BASIN STORAGE- .1172E-07 PERCENT ERBOR- -.4
                FOR PLAN + 1 PATIO+ .SE
ETAN 3-TH
                                                      . 18 £
                                                              23.42 213.70
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CONTINUITY SUMMART (AC-FT) - INFIGM. ,1374E-01 EXCESS. ,900SE-00 OUTFLOW. .1376E-01 BASIN STORAGE. .420SE-07 PERCENT ERBOR. ..1
                FOR PLAN - 1 PATIO- 1.00
BT-6 MANE .0
                                                     . 63
                                                              48,13 213.75
                                                                                                     .72
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                                                                                                                                               213.00
CONTINUITY SUMMARY (AC-FT) - INFLOW- .2775E-01 EXCESS. .6090E-00 CUTFLOW- .2775E-01 BASH STORAGE- .3012E-07 PERCENT ERROR- -.1
                FOR PLAN - 1 RATIO- .58
BI-7 MANE 1.
                                                    1.49
                                                                       .98 212,00
                                                                                                      .01
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                                                                                                                                     .98 213.00
CONTINUITY SUMMARY (AC-FT) - INFLOM- .58128-01 EXCESS- .00008-00 OUTFLOM- .5858-01 BASIN STORAGE- .2055E-07 PERCENT ERROR- -.4
                FOR PLAN + 1 BATTO- 1.00
                                                               31.47 311.36
                                                                                                      .11
                                                                                                                     3.00
                                                                                                                                              213.00
                                                                                                                                   29.95
CONTINUITY SUMMARY (AC-FT) - INFLOR- .60028-00 EXCESS. .00028-00 LOTYLON- .5058-00 BASH STORAGE- .22608-07 PERCENT ERROR- .5
                FOR PLAN - 1 RATIO- ,58
ET-10 MANE .57 10.32 210.92
                                                                                                     1.40
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CONTINUITY SUMMARY (AC-FT) - INFLOM- ,61818-00 EXCESS- ,0000E-00 OUTFLOM- ,5190E-00 BASIN STORAGE- .5110E-00 PERCENT REPOR- -.1
                FOR FLAN + 1 RATIO+ 1.00
                                                               10,20 210.94
                                                                                                                                17.73 210.00
                     RT-10 MANE
                                                     . 35
                                                                                                     3.55
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                                                                                                                                                                         2 44
COMPUNITY SUMMARY (AC-FT) - INFLOW- .11318-81 EX-ESSA .0000000 001710-01.11348-81 BASHN STORAGE- .33550-00 FRECENT ERROR- -.1
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|            | FOR FLAN           | * 1 RATIO*         | .38         | 30,70     | 211                                    | .60                                     | ,24        | 3,49        | 38.47    | 213,00    | , <del>2</del>     | •        |            |        |
|------------|--------------------|--------------------|-------------|-----------|--|---|------------|-------------|----------|-----------|--------------------|----------|------------|--------|
| CONTINUIT  | r summant          | (AC-YT) - II       | TLON-       | ,1740E+01 | KICESS =                               | .00005*40                               | CESTIFICAL | 17408+6     | )l BASIN | STORAGE.  | .37378*67          | PERCENT  | EXROX.     | .0     |
|            | FOR PLAN<br>RT-11  | · i RATIO·<br>MANE | 1.00        | #7.72     | 210                                    | × <b>5</b> 5                            | .56        | 3.50        | 87.13    | 213.00    | ÷ \$ \$            | ļ        |            |        |
| CONTINUIT  | i shayaa           | (AC-77) - D        | YL/34+      | .40318+01 | ###################################### | .99902.09                               | GUTPLON.   | ,4952E+6    | I BASIN  | #TORAGE.  | .30008-07          | PERCENT  | ERROR.     | .0     |
|            | YOR PLAN<br>RT-12  | - 1 MATIO*<br>MASE | .38<br>1.33 | 26.66     | 213                                    | .92                                     | , 15       | 1.00        | 24.61    | 217.00    | » <b>3</b> .5      | <b>,</b> |            |        |
| CONTINUIT  | f Summart          | (AC-FT) - IN       | IVLON=      | .1540#*01 | Kacasa.                                | .00002.00                               | OUTFLOH.   | 15452+0     | l basin  | STORAGE-  | .72798-05          | PERCENT  | ERECR.     | 4      |
|            | FOR PLAN<br>RT-12  | - 1 NATIO-<br>NAME | 1,00        | 90.95     | 214                                    | . · · · · · · · · · · · · · · · · · · · | . 37       | 3.00        | 90.61    | 213.00    | .38                | i        |            |        |
| CONTINUIT  | T SUMMARY          | (AC-FT) - IB       | iylom*      | .38632.01 | excess.                                | ,000 <b>01</b> *00                      | OUTFLOW.   | · .3878E*\$ | l Basin  | STORAGE.  | .10042-04          | PERCENT  | ERROR-     | * - 4  |
|            | POR FLAN<br>RT-JB  | • 1 PATID•<br>MARK | ,59<br>1.01 | 19,12     | 225                                    | . \$2                                   | . 46       | 3.00        | 20.01    | 216.00    | ,3,8               | }        |            | ·<br>· |
| CONTINUIT  | f Summary          | (AC-FT) - IN       | orlow.      | .17718+01 | excess.                                | .0000**00                               | CUTFLOW.   | · .2774#+6  | l basin  | STORAGE.  | .1797E+04          | PRACEST  | ENNOR-     | * . 3  |
|            | rce vlan<br>rt-je  | * 1 BATIO*<br>Kane | 1.00        | 98,33     | 214                                    | .07                                     | , 40       | 3.00        | 34.93    | 213.00    | . <b>4</b> \$      | ı        |            | •      |
| CONTINUES. | COMMANY            | (AC-FT) - IN       | iylam*      | .43668-01 | ricess.                                | .coasm+00                               | CHTTLON.   | . ,4374E+8  | l Basin  | STONAGE*  | .15472-04          | Percent  | \$\$\$O#.* | *.1    |
|            | POR PLAN<br>PT-B14 | * 1 NATIO*<br>NAME | .58<br>1.01 | 1.48      | 221                                    | .29                                     | . \$7      | 3.00        | 1.47     | 222,00    | .a. \$ 6           | ,        |            |        |
| CONTINUET  | f Summart          | (AC-FT) - IN       | men.        | .9979%-01 | ercess-                                | .0050#*00                               | CCTTF1/28+ | 399)% «0    | i basin  | STORAGE*  | .41252-07          | PERCENT  | ERROR-     | پ      |
|            | ror Plan<br>RT-314 | * 1 RATID*<br>MANK | 1.00        | 1,52      | 219                                    | . %4 1                                  | . 43       | 1.00        | 1.30     | 219.00    | 1.4                | <b>;</b> |            |        |
| CONTINUIT  | SUMMARY            | (AC-PT) - IN       | ¥1,674 =    | .24388+00 | XXC232.*                               | .0000 <b>x</b> +53                      | COTFLON.   | · ,24418+6  | HIBAS C  | STORAGE.  | ,6533 <b>x</b> -97 | PERCENT  | ERROR-     | 1      |
|            | FOR FLAH<br>RT-14  | - 1 MATIO-<br>MANU | .5#<br>.51  | 11,53     | 223                                    | , <b>2</b> &                            | * # # #    | 3,98        | 13,52    | 213,80    | ., \$ 8            | į.       |            |        |
| CONTINUIT  | SUMMARY            | (AC-FT) - IN       | TLON-       | .7779E.00 | eacess.                                | .0000#.00                               | OUTFLAN.   | . ,7781#+C  | O BASIN  | STORAGE.  | .5333%-07          | PERCENT  | ERROR.     | . Đ    |
|            |                    | * 1 HATTO*         | 1.05        | 28.49     | 212                                    | .76 1                                   | . 91       | 1.00        | 38.49    | 213,88    | 1,9                | <b>L</b> |            |        |
| CONTINUET  | f SUMMARY          | (AC-PT) - IN       | flon-       | .17218+01 | eicess.                                | .0000x+00                               | OUTFLOW.   | · .1721E+6  | 11 BASIN | STORAGE.  | .571 <b>4</b> E-07 | PERCENT  | eregr.     | . 0    |
|            |                    | * 1 RATIO*<br>RANX |             | 23 ×91    | 213                                    | * <b>*</b>                              | » 鞍霉       | 3.00        | 23,99    | 21),00    | . 86               | 3        |            |        |
| CONTINUIT  | C SUMMARY          | (AC-FT) - IN       | ifizm=      | .13462-01 | EXCESS.                                | .00005.00                               | QUITION:   | · .1346E+   | )l Basin | STORAGE - | .6782E-07          | PERCENT  | erece-     | . 9    |
|            |                    | * 1 RATIO*<br>MANN |             | 49.80     | 231                                    | .09 1                                   | .93        | 1.00        | 49.86    | 213.80    | 1.9                | )        |            |        |
| CONTINUIT  | TRANSCOR Y         | (AC-FT) - 1)       | ivi.cm=     | .29585+91 | excess.                                | .0000 <b>E+</b> 00                      | OUTFLOW:   | 29588*(     | li basin | STORAGE   | .7275E-07          | PENCENT  | ERROR.     | * \$   |
|            |                    | * 1 NATIO*         |             | 29.34     | 213                                    | , 15                                    | . 88       | 3.00        | 29.34    | 213.00    | , 8 :              | )        |            |        |
| *** MCRHAL | END OF HE          | C-1 ***            |             |           |  |   |            |             |          |           |                    |          |            |        |

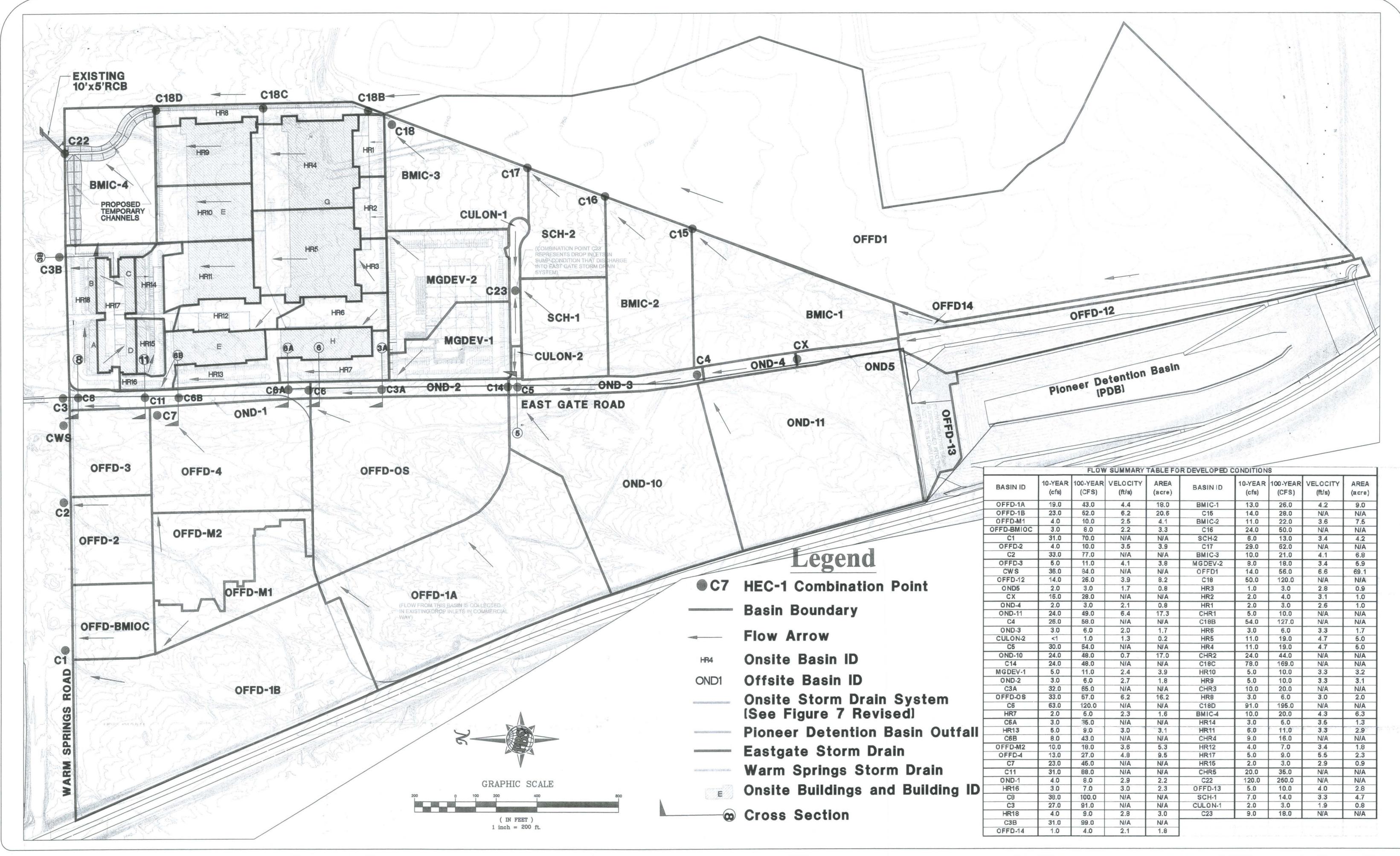


FIGURE 6 REVISED DRAINAGE BASIN MAP FOR DEVELOPED CONDITION

Harsch Addendum #1 - 511434



901 N. Green Valley Pkwy Suite 100 Henderson, Nevada 89014 Telephone: 702/263-7275 Fax: 702/263-7200

"Update to the Technical Drainage Study for Henderson Commerce Center (Formerly known as Harsch)", Prepared by PBS&J (February 2005)

# UPDATE TO THE TECHNICAL DRAINAGE STUDY FOR HENDERSON COMMERCE CENTER (FORMERLY KNOWN AS HARSCH) Permit Number: 2002740088

## Prepared for:

Harsch Investment Properties, LLC 1121 SW Salmon Street Portland, Oregon 97205

Prepared by: PBS&J

2270 Corporate Circle, Suite 100 Henderson, Nevada 89074

Reference Number 511434.00 February 22, 2005



TUO. CFC-VAC

STORM DRAIN ANALYSIS PLUS

Original version by Los Angeles County Public Works Portions Copyrighted by CIVILSOFT, 1886, 1887, 1889

Version Serial Busher

SATTUTE SPENSORS

Feb 22, 3005 11:13:52

Input file : DEV-272.DAT Cutput file: DEV-272.COT

### IMPUT FILE LISTING

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CHEADING LINE NO 3 IS -
                                 60° STORM DRAIN - PUTURE CONDITION STORM DRAIN
CHEADING LINE NO 3 IS -
                                 0100×165 CFS
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O ELEMENT NO 8 IS A SEACH
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Page 1

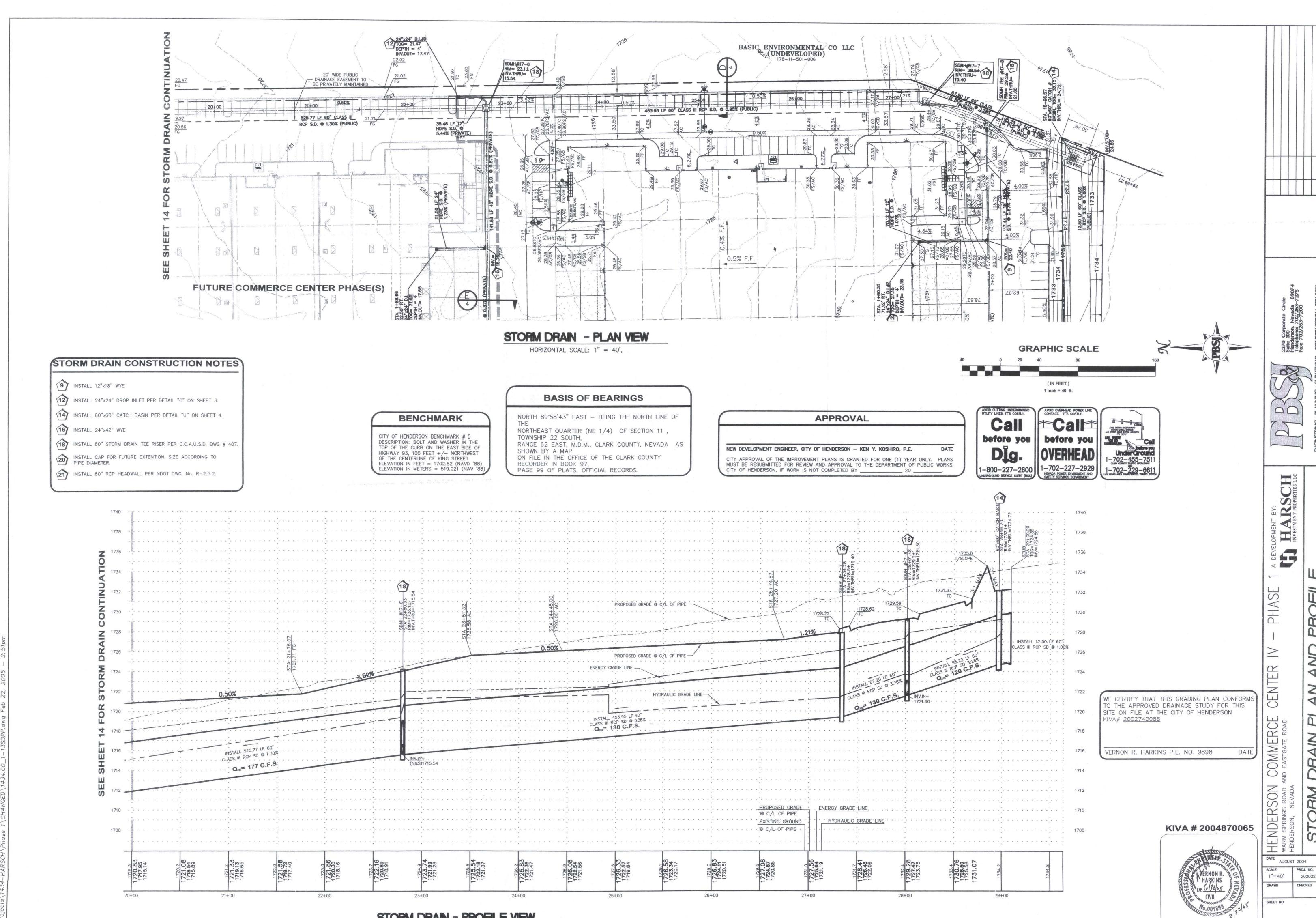
|  |           | JA Ser Section       |  | At hell survivour me | VI 00 0000     | 5/3ii            | જે " જો તે માં રચને" હોં |                  |                   |   |                 |                 |                    |              |
|--|-----------|----------------------|--|----------------------|----------------|------------------|--------------------------|------------------|-------------------|---|-----------------|-----------------|--------------------|--------------|
| O ELEMENT NO   | 9 18 A    | V/S DATI<br>REACH    | A STATION<br>1194.70                       | INVERT<br>1700.50    | 2607           | ,                | #<br>.013                |                  |                   |   | RADIUS<br>.00   | ANGLE<br>.00    | AKI PT<br>.00      | Man n<br>O   |
| O ELEMENT NO   | 10 IS A   | U/S DATA             | A STATICM<br>1198.20                       | INVERT               | SECT<br>1      |                  | .013                     |                  |                   |   | AADIUS<br>.SO   | akcle<br>.co    | AMG PT<br>15.00    | MAN N<br>O   |
| O ELEMENT NO   | 11 : A    | U/S DATA             | 1198.20                                    | INVERT<br>1700.6%    | SECT           |                  | .013                     |                  |                   |   | RADIUS<br>00.   | AMILE<br>.00    | ANG PT<br>15.00    | MAN H<br>O   |
|  | 12 IS A   | U/S DAT              | N STATION<br>1198.20                       | INVERT<br>1700.65    | SECT<br>1      |                  | ,013                     |                  |                   |   | RADIUS<br>. CO  | ANGLE<br>.00    | ANG PT<br>15.00    | man n<br>1   |
| •  |           | U/S DATA             | N STATICM<br>1203.20                       | INVERT<br>2700.72    | SECT<br>1      |                  | #<br>.513                |                  |                   |   | RADIUS<br>.00   | AMCLE<br>00.    | ANG FT<br>.00      | D<br>MYN H   |
| 0  | ** ** *   |                      | sater surface                              |                      |                | ENT CARD I       | .18TING                  |                  |                   |   |                 |                 | de lacertaine Navo | , *          |
| THE STATE OF THE S | 13 IS A   | U/S DATI             | A STATION<br>1321.96                       | :NYEXT<br>1761.54    | SECT<br>1      | •                | ))<br>.013               |                  |                   |   | RADIUS<br>00.   | AWGLE<br>,00    | ANG PT<br>15.00    | MAN N        |
|  | 14 12 A   | U/S DATA             | *  | 187887<br>1702.54    | 28CT           |                  | #<br>.013                |                  |                   |   | RADIUS<br>,00   | AMGLE<br>.00    | AMG PT<br>15.00    | man n<br>c   |
|  | _         | U/S DATE             | N STATION                                  | INVERT<br>1702.54    | SECT           |                  | #<br>.913                |                  |                   |   | EUIUAN<br>00.   | ANGLE<br>.00    | ANG PT<br>15.00    | man n<br>1   |
|  | 16 18 A   | U/S DATA             | V STATICS<br>1333.96                       |                      | 1              | •                | N<br>.913                |                  |                   |   | RADIUS<br>00.   | ANGLE           | TY DWA             | Man H        |
|  | 17 IS A   | U/S DAT              | 1373.45                                    | 1701.19              | SECT<br>1      | ,                | N<br>-913                |                  |                   |   | evidas<br>00.   | AMGLE<br>.00    | ANG PT             | man n<br>o   |
| O ELEMENT HO   |           | JUNCTICA<br>U/S DATA |  | 18VERT<br>1703.21    | WECT           | LAT-1 LAT-       |                          | Q3<br>10.0       | Q4<br>. S         | :HVERT:1<br>1706.26                                 | INVERT-4        | * PMI 3 90.00   | PH: 4              |              |
|  | 19 IN A   | U/S DATI             | NOITATES A                                 | 1HVERT<br>1701.30    | SECT<br>1      | •                | .613                     |                  |                   |   | RADIUS<br>CO.   | AMILE           | AM) PT             | Man H<br>O   |
| O ELLMENT NO   | 20 18 A   | U/S DATE             | * STATION 1386.95                          | * INVERT 1703.30     | SECT           | •                | .013                     |                  |                   |   | RADIUS<br>.00   | AWGLE           | ANG PT             | MAN N        |
| 0 ELEMENT NO   | 21 IS A   | U/S DATA             | ATATION<br>1386.95                         | 187287<br>1703.38    | escr<br>1      | •                | #<br>.013                |                  |                   |   | RADIUS<br>00    | AWGLE<br>00     | ANG PT             | man n<br>1   |
| i saeMs. si  | 23 IX A   | U/S DATI             | * ************************************     | INVERT<br>1701.45    | ercr<br>1      | •                | N<br>.913                |                  |                   |   | RADIUS<br>.00   | AMGLE<br>.00    | ANU PT             | MAN N        |
| y Klement del  | 2) IZ A   | U/S DATE             | 1752.06                                    | INVERT               | SECT<br>1      | ·                | N<br>.013                |                  |                   |   | RADIUS          | AMGLE<br>00.    | ANG PT             | man n        |
| 0 <b>ELEMENT</b> NO  | 24 18 A   | JUNCTICS<br>U/S CATI |  | #VERT<br>1708.74     | SECT           | IAT-1 LAT        |                          | \$<br>Q3<br>20.0 | Q4<br>3.9         | 187887-3<br>1708.70                                 |                 | PHI 3<br>90.00  | PHI +              |              |
| 1  |           |                      | ater surface                               | 0200112              | 30'9 50'94     | rivero maleira e | 3 (2000 - 3 A)(27)       |                  |                   |   |                 |                 | PAGE MO            | 4            |
| O ELEMENT NO   | 25 IS A   | REACH<br>U/S DATE    | · STATION                                  | invert               |                | Angels America i | 83                       |                  |                   |   | RADIUS          | ANGLE           | ANG PT             | MAN H        |
| OR THEMSAIR C  | 26 IS A   | JUKTIC               | 3277.13                                    | 1715.53              | 1.             |                  | .013                     | *                |                   | *   | -00             | .00             | .00                | 3            |
| O ELEMENT NO   | 27 18 A   | U/S DATI             | 2382.83<br>•                               | INVERT               | SECT           | LAT-1 LAT-       |                          | 93<br>44.9       | 04<br>3.0         | 187227-3<br>1715.54                                 | 1715,54         | PHI 3<br>90.00  | PW: 4              |              |
| O ELEMENT NO   | 28 IS A   | U/S DATA             | V STATION<br>2731.78                       | INVERT<br>1719.38    | SECT<br>1      |                  | #<br>.013                |                  |                   |   | RADIUS<br>00.   | ancia<br>Co.    | 74 CMA<br>20.01    | Man n<br>o   |
| O ELEMENT NO   | 29 IS A   | U/S DATE             | TATION 2731.78                             | 1#VERT<br>1719.38    | SECT<br>1      | ı                | , 07.3                   |                  |                   |   | RADIUS<br>. SO  | AWILE<br>.00    | A363 PT<br>15.00   | man n<br>1   |
| o element no   | 30 18 A   | U/S DATA             | 2736.78                                    | INVERT               | ARCT<br>1      |                  | #<br>.013                |                  |                   |   | RADIUS<br>.00   | amile<br>.gg    | AMS PT             | MAN H<br>C   |
| o element no   |           | U/S DATA             | 2798.98                                    | INVERT<br>1721.53    | SECT           |                  | , 013                    | *                |                   |   | RADIUS<br>CO.   | AMGLE<br>00.    | ANG PT             | man n<br>1   |
|  | )2 IS A   | u/a data             |  |                      | 3              | LAT-1 LAT-<br>3  |                          | Q)<br>10.0       | Q4<br>, p         | INVERT-1<br>1721.60                                 | INVERT-4<br>.00 | PHI 3<br>60.00  | P%I 4              |              |
|  |           | U/G DATA             | STATION<br>1894.10                         |                      | Bener<br>1     | i                | #<br>,01.3               |                  |                   |   | RADIUS<br>00.   | ANGLE<br>.00    | AMG PT<br>.00      | Man ii<br>1  |
| O ELDEST NO  |           | U/S DATA             | 2#99.20                                    | :NYERT<br>1734.75    |                | :                | n<br>.013                |                  |                   |   | NADIUS<br>.00   | ANGLE<br>.co    | AM) PT             | MAN H        |
|  |           | U/S DATA             | 2899.20                                    |                      | SECT<br>1      | •                |                          | •                |                   | * S ELEV  |                 |                 |                    |              |
| io dit erroi   |           |                      |  |                      |                |                  |                          |                  |                   |   |                 |                 |                    |              |
| ** WARNING MC  | ). 2 ** : | · WATER S            | WRFACE ELEVA:                              | rion give            |                |                  |                          |                  | ELEVATION         | IN HOMEDS   | , W.S.SLJ       | rv » inv        | • DC<br>PAG        | E 1          |
|  |           | 40*                  | M DRAIN ANAL)<br>STORM DRAIN -<br>-155 CP5 |                      | HARRO          |                  |                          | e:IM)            |                   |   |                 |                 |                    |              |
|  | ELEV (    | DEPTH<br>OF FLOW     | *.5.                                       | Q                    | vel            | nead<br>Nead     | energy<br>Grd.el.<br>Ny  | Super<br>Elev    | CRITICAL<br>DEPTH | 200 14 To 20 10 10 10 10 10 10 10 10 10 10 10 10 10 | DIA             | iast/<br>Id No. | FIE                | ) avepa<br>R |
| *********  | ******    |                      | ****                                       | *******              | *****          | ********         | *******                  | *****            | ********          | orm depth<br>********                               | ******          | ******          | 33<br>*******      | ****         |
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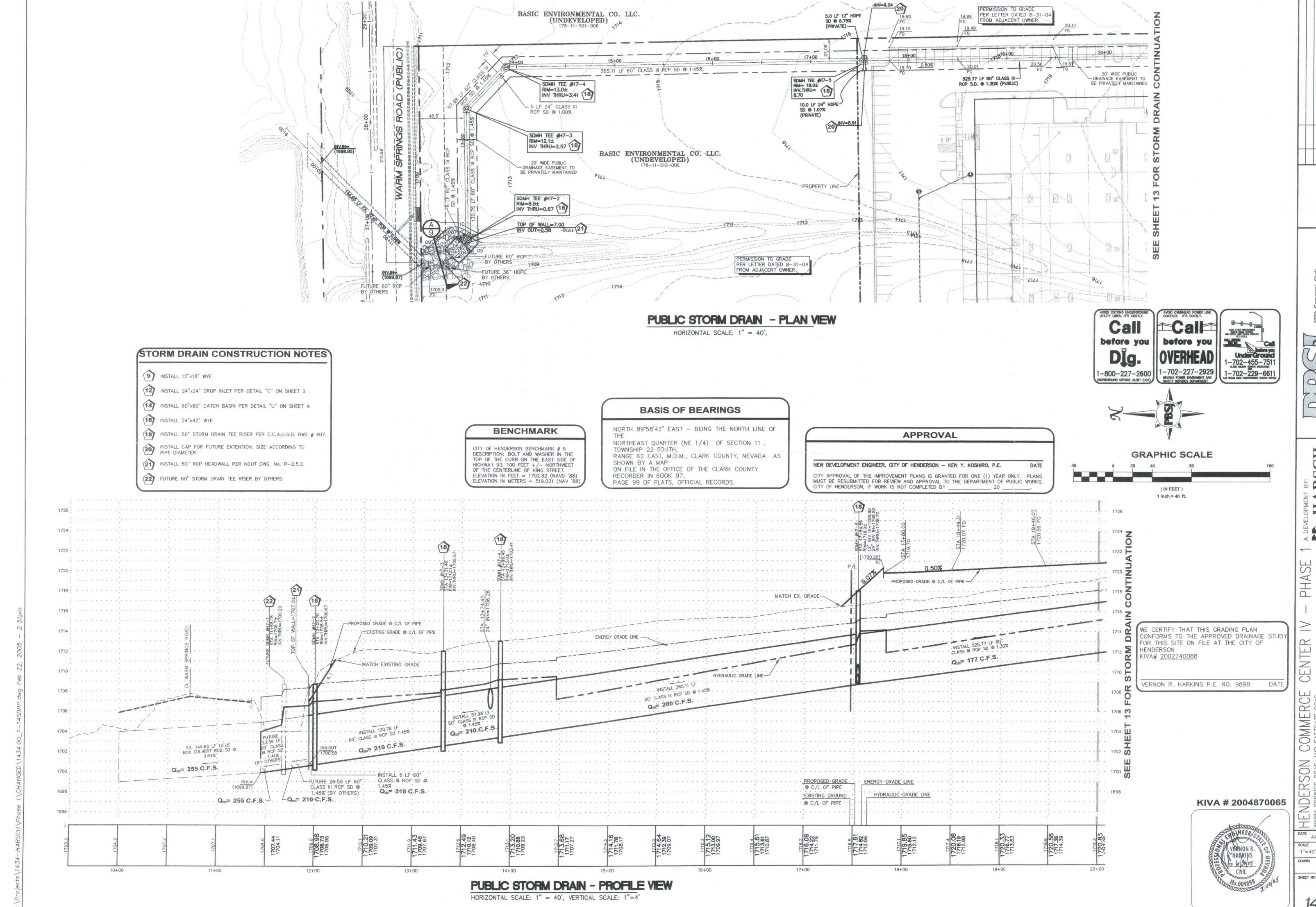
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| 0                       |  | 1700.04  | 4,20   | 1704.26  | 355.0  | 3.4、4前   | 3.26<br>,00448   | 1707.51<br>70.   | . 09   | 4.45   | 3.44   | 3.00  | .00  | .00  | Q  | .00  |
| ŧ,                      |  | 1700.17<br>.01196  | 4.45   | 1704.62  | 255.9  | 11.40  | 2.96   | 1707.59  | .00  | 4.45   | * 1 4 4  | 5.00  | .00  | ,00  | \$   | .00  |
| 0 43                    | 1168.18  | 1700.10  | 8,19   | 1706.19  | 210.0  | 10.70  | 1.78   | 1708.17  | .00  | 4 + 4.2  | 2.38   | 5.00  | .00  | .00  | \$   | . 99   |
| 0                       | 1194.70  | 1700.59  | 5.97   | 1706.54  | 210.0  | 10.70  | 1.7a<br>.cossu   | 1708.34  | .69  | 4.13   | 2.84   | 5.00  | .80  | .00  | 0  | , QQ   |
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| 0                       | 1196.20  | 1700.65<br>.01399  | 6.39   | 1706.94  | 210.0  | 10.70  | 1.78   | 1708.72  | .00  | 4.13   | 3.03   | 5.00  | .00  | .00  | Ø  | .00  |
| 0.00                    | 1203.20  | 1700.73  | 6.25   | 1706,97  | 210.0  | 10.70  | 1.78   | 1708.75<br>.83   | .96  | 4.23   | 2.99   | \$,05   | .68  | 20,  | •  | .00  |
| Q                       | 1320.96  | 1702.54  | 5.14   | 1707.88  | 210.0  | 10.70  | 1.78   | 1709.65  | .50  | 4.13   | ****   | 5.00  | .00  | .00  | 0  | .00  |
| 0                       | 1328.96  | 1702.54<br>1702.54<br>.01399   | 5.42<br>5.60   | 1707.96<br>1708.14   | 210.0  | 10.70  | 1.78<br>1.78<br>.00650   | 1709.74<br>1709.93<br>.03  | .00  | 4.13   | 3.03   | 5.00<br>5.00  | .90  | .00  | 0  | .00  |
| 1                       |  | 2 M # 2 2 2  |  |  |  |  |  |  |  |  | 米の部門   |   |  |  | PAGE   | 2  |
|                         |  |  |  | ua kiaro me<br>Haro medita   |  | HARSCH   | N.T  | PROFILE LI   | STIME  |  |  |   |  |  |  |  |
|                         |  |  | 010  | 0-255 CFS  |  |  |  |  |  |  |  |   |  |  |  |  |
|                         | STATION  | invert<br>Elev.  | DEPTH<br>OF FLOW   | W.S.   | Ç  | yel  | vel<br>Head  | CKD.KL.  | elev   | CRITICAL<br>DEVTH  | hillindran av an avanni V                                    | NGT/<br>DIA   | BASE/<br>ID MO,  | #1,  | MO<br>Pira   | aybyr  |
|                         |  | SQ<br>********   | *******  | ******   | ******   | ******   | SF AVE   |  | ****   |  | Cem Depth  | ****  | ******   | 28<br>****   | ****   | ***  |
| 0                       |  | 1702.61<br>.01469  | 5.56   | 1708.17  | 210.0  | 10.70  | 1.78   | 1709.95  | .00  | 4.13   | 9 94   | 5.00  | .00  | .00  | 0  | . 95   |
| 4                       | 1373.45  | 1703.19  | 5.24   | 1708.43  | 210.9  | 19,70  | .00650<br>1.78   | 1710.21  | .00  | 4.13   | 2.98   | 5,00  | .00  | .00  | \$   | .00  |
| 43                      | - Marchinister and March   | .01001<br>1703.21  | 5.54   | 1708.77  | 200.0  | 10.19  | .00620<br>1.61   | .01<br>1710.39   | .00  | 4.04   |  | 5.00  | -00  | .00  | ø  | \$9  |
| 0                       |  | .01479<br>at.101.  | 3.54   | 1701.93  | 200.0  | 10.19  | .00590<br>1.61   | .07<br>1710.5)   | .00  | 4.04   | 2.88   | 5,00  | .00  | .00  | 9  | .00  |
| 8                       |  | 1703.38<br>1703.38   | 5.42   | 1709.00<br>1709.16   | 300.0<br>300.0   | 10.19  | 1.61   | 1710.61<br>1710.77   | .06<br>.00   | 4.04   |  | 5.00<br>5.00  | .00<br>.50   | .00  | 0  | . 00<br>00                                   |
| ĝ                       | 5.00   | .01399   |  |  |  |  | .00590   | .0)  |  |  | 2.93   |   |  | .00  | -  |  |
| 2                       | \$5.71   | 1703.45  | 5.74   | 1709.19  | 200.0  | 10.19  | 1.61   | 1710.80<br>.3)   | .00  | 4,04   | 2.90   | 5.00  | .00  | ,04<br>,09   | 9  | .00  |
| 50                      | ) 1447.66<br>HYDRAULIC   | 1704,26<br>JUMP  | 5,27   | 1709.53  | 280.0  | 10.19  | 1,61   | 1711.14  | ,90  | 4.04   |  | 5.00  | .00  | .00  | 0  | - 50   |
| 8                       |  | 1704.26<br>.01447  | 2.97   | 1707.23  | 200,0  | · 新 · 辛芬   | 4.21<br>.01346   | 1711.4)  | .60  | 4,04   | 2.90   | 5.00  | .00  | .00  | 0  | .00  |
| £9<br>43                |  | 1704.28  | 2.97   | 1707.25  | 200.0  | 16,44  | 4.20<br>.01267   | 1711.45  | .90  | 4.04   | 2.90   | 5.00  | .00  | .50  | Q  | .00  |
| 8                       | 1593.97  | 1706.37  | 3,69   | 1769.47  | 206.0  | 15,68  | ).12<br>.01121   | 1711.70  | .00  | 4,04   | 2.90   | 5,55  | .90  | .00  | -0   | .00  |
| á                       |  |  |  |  |  |  |  |  |  |  | 4136   |   |  |  |  |  |
|                         |  | 1707.34  | 3,22   | 1710.57  | 200.0  | 14.93  | 3,47   | 1714.04  | .00  | 有、存者   | * **   | 5.00  | .00  | .00  | Q  | , 00   |
| 9<br>9                  | 39.68  | 1707.34  | 3.32   | 1710.57  | 200.0  | 14,93  | 3,47<br>,00997   | 1714.04<br>,40   | .00  | 4.04   | 2.20   | 5.00  | , 90   | .00  | PAGE   | .00  |
| S                       | 39.68  |  | \$#\$  | em Crain an  | ALYSIS FO  | VATER<br>I VATER   | .00997<br>EURFACE<br>N.7   | .46<br>PROPILE LI  |  | 4.04   | ¥ - 29   | 5.00  | , 20   |  |  |  |
| 1                       | 39,6\$   | . \$1447   | 60°<br>60°   | nm drain am<br>Storm draii<br>0-185 cf8  | Alisis Poi<br>H - Poitosi  | MATER<br>HARSON<br>COMBIT  | .00997<br>ERIBYACE<br>N-7<br>ICH STORM   | PROFILE LI<br>CEAIN  | 771163   |  | ¥.26   |   |  | .00  | PAGE   | 3  |
| 1                       | 39.68  | 177847   | \$7C   | n chair an<br>Store chai:  | ALYSIS FO  | VATER<br>I VATER   | .00997<br>EURYATE<br>N-7<br>ICH STORM<br>VEL<br>HEAD   | PROFILE LI<br>DEATH<br>DEATH<br>DED.EL.  |  | CRITICAL<br>DEPTH  |  | BIT/<br>DIA   | nase/  | .00  | PAGE   |  |
| 1                       | 39,6\$   | .01447   | 010:<br>60*<br>610:<br>610:  | nm Crain am<br>Storm Crain<br>O-11: Cri<br>W.S.<br>RLEY  | Alisis foi<br>D - futuri<br>C  | MATER<br>HARSON<br>COMBIT  | .00997<br>EURFACE<br>N-7<br>ION STOWN<br>YEL   | PROPILE LI<br>DEAIN<br>DEESTY  | erea<br>erea<br>erino  | CRITICAL<br>DEFIN  | 2.20<br>XXM DEFTH  | MIT/<br>DIA   | BASE/  | .00  | PAGE   | 3  |
| \$ \$ \$ \$ \$ \$ \$ \$ | 39.68<br>3787108<br>3787108<br>3787108<br>3787.64  | . 51447  197527  2227  *********   | OF FLOW<br>OF THE<br>STO   | nm Crain am<br>Storm Crain<br>O-11: Cri<br>W.S.<br>RLEY  | Alisis foi<br>D - futuri<br>C  | WATER<br>HARSCH<br>E CONDIT<br>YEL   | .00997<br>EUBYACE<br>H:7<br>108 STORM<br>VEL<br>HEAD<br>SF AVE   | PROFILE LI<br>DEAIR<br>EMERCY<br>CRD-EL-<br>HP   | erea<br>erea<br>erino  | CRITICAL<br>DEFIN  | orm depth  | MIT/<br>DIA   | BASE/  | .00<br>.24<br>.****  | PAGE   | 3  |
| \$ 6 4 4 6 6 6          | 39.68<br>37ATION<br>21/ELEM<br>************************************  | 177577<br>31447<br>3127<br>3027<br>1707,447<br>1708,38   | DEVINOR TO STORY   | em Drain am<br>Stoom Drain<br>D-125 CPS<br>W.S.<br>KLEY  | Alibis foi<br>d - futusi<br>C  | WATER MARCH CONDIT   | ,00997<br>ENRYACE<br>H-7<br>IOS STREM<br>VEL<br>HEAD<br>SF AVE<br>1.16<br>.00867<br>2.87   | PROFILE 1.1<br>DEATH<br>EMERGY<br>DRD-EL.<br>HP<br>***********************************   | STIMS<br>STIMS<br>STAN<br>STAN<br>STAN<br>STAN<br>STAN<br>STAN<br>STAN<br>STA  | CRITICAL<br>DEPTH  | CORM DEPTH   | 897/<br>DIA   | BASE/<br>20 MO.  | . 20<br>. 24<br>. 24<br>. 20<br>. 20<br>. 20<br>. 20<br>. 20   | #0<br>#1   | J<br>Avren                                   |
| 8 0 0 0 0 0 0 0         | 39.68<br>37ATION<br>0 L/ELEM<br>   | **************************************   | STO<br>60°<br>DEPTH<br>OF FLOW   | em Crain am<br>Storm Crain<br>D-Sis Cri<br>W.S.<br>Riev  | ALESIS POS<br>Q  | MATERIAL VIII  | ,00997<br>ENEFACE<br>H-7<br>IOS STOWN<br>VEL<br>HEAD<br>SF AVE<br>   | PROFILE LI DRAIN EMERCY TREESL. HF  1714.43 .1714.65 .1714.77  | STIME<br>SUPER<br>ELZY   | CRITICAL<br>DEFIR<br>1   | CORM DEFIN<br>************************************           | BUT/<br>DIA<br>******   | BASE/<br>ID WO.  |  | #ACE #C  | AVREN  |
|                         | 0 17ATION<br>0 1/11AN<br>0 1/11AN<br>0 1765.64<br>0 1765.64<br>15.82<br>0 1745.82<br>0 1745.83<br>0 1745.83  | 1872<br>1872<br>1872<br>1872<br>1872<br>1873<br>1873<br>1873<br>1873<br>1873<br>1873<br>1873<br>1873 | 870<br>60°<br>08°71<br>08°710<br>3.36  | AM DRAIN AN<br>STORM DRAIN<br>D-JES CES<br>W.S.<br>RLEV<br>1711.78   | Alisis For<br>O<br>-*********<br>200.0   | WATER<br>HARRING<br>CONDIT-<br>VEL<br>14.25  | ,00997<br>EURFACE<br>N-7<br>ION STORM<br>VEL<br>HEAD<br>SF AVE<br>1.16<br>.00187<br>7.87<br>.00791<br>2.61<br>.00792<br>2.61   | .40 PROFILE LI DEAIN EMERCY UNIL LI 1714.43 1714.43 1714.77 .06 1714.83  | CALITE SUPER ELS VALUE V | CRITICAL<br>DEFIN<br>4.04  | 3.99<br>2.99<br>2.90   | NGT/<br>DIA<br>******<br>5.00   | BASE/<br>ID NO.<br>************************************          | **************************************   | PAGE<br>PIER   | AVRFR<br>.co                                 |
|                         | ### 1  | **************************************   | 070<br>60°<br>02773<br>07 7108   | RM GRAIN AN<br>STORM DRAID<br>0-255 CFS<br>W.S.<br>ELEV<br>1711.78<br>1711.78  | ALISTS FOR   | WATER<br>HARROW<br>CONDITY<br>VIL<br>14.25<br>13.59<br>12.99   | ,00997 EXECT STORM WELL HEAD SF AVE  | 980FILE LI<br>DRAIN<br>ENRINGY<br>ENDI-RI-<br>HF<br>   | SALLE<br>SALLE<br>VALLE<br>CO.   | CRITICAL<br>DEFIN<br>4.04<br>4.04<br>4.04  | CORM DEFIN<br>************************************           | #777/<br>DIA<br>*******<br>5.00   | BASE/<br>2D MO.<br>-00<br>-00                                    |  | PAGE<br>PIER   | AVEFR<br>.co<br>.co                          |
|                         | ######################################   | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$   | 010<br>010<br>0171<br>01710<br>3.36<br>3.36<br>3.51  | RM CRAIN AN<br>STORM DRAID<br>0-255 CFS<br>W.S.,<br>ELEV<br>1711.78<br>1712.17<br>1712.46  | ALTESS FOR  | WATER HARRON COMDIT.  VEL.  14.25  13.59  12.35  | .00997<br>EURFACE N-7<br>ION STORM<br>VEL<br>HEAD<br>SF AVE<br>1.16<br>.00587<br>2.00792<br>2.15<br>.00792<br>2.15<br>.00792<br>1.15<br>.00792   | .40<br>PROFILE LI<br>DRAIN<br>SHERRY<br>CREASL.<br>LY<br>LYLA.43<br>LYLA.65<br>LYLA.65<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67<br>LYLA.67 | SUPER ELEV   | CRITICAL<br>DEPTH<br>3<br>4.04<br>4.04<br>4.04   | 2.20<br>2.20<br>2.20<br>2.20                                 | NOT/<br>DIA<br>5.00<br>5.00<br>5.00   | BASE/<br>2D NO.<br>-00<br>-00                                    |  | PAGE PIER 0 0 0  | AVEFR .co .oo                                |
|                         | 27.68 27.41.09 21.71.09 21.71.09 21.71.09 21.71.0.04 21.5.3.3 21.71.0.06 21.71.0.06 21.71.0.06 21.71.0.06 21.71.0.06 21.71.0.06 21.71.0.06 21.71.0.06  | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$   | 070<br>60°<br>0771<br>07720<br>3.36<br>3.51<br>3.57  | RM CRAIN AN<br>STORM DRAIN<br>0-25 CF<br>H.S.<br>ELSV<br>1711.78<br>1711.17<br>1712.17<br>1712.70  | ALYSIS FOR PURISH - P | MATER HARSCH CONDIT.  VEL  14.25 13.59 12.35 13.77   | ,00997<br>EURFACE N-7<br>ION STORM<br>VEL<br>HEAD<br>SF AVE<br>1.00887<br>1.87<br>.00709<br>1.37<br>.00519<br>1.37   | ## PROFILE LI DEATH EMERGY EMERGY EMERGY 1714.43 1714.65 1214.77 1714.83 192 1714.83   | SUPER<br>ELEV<br>.00<br>.00  | CRITICAL. DEPIH  4.04  4.04  4.04  4.04  | 3.99<br>2.99<br>2.90   | HOT/<br>DIA<br>******<br>5.00<br>5.00<br>5.00                               | BASE/<br>ID MO.<br>-00<br>-00<br>-00<br>-00                      |  | PAGE NO PIER O O O O O   |  |
|                         | 39.68  8 TATION  1 / ELEM  1 24.80  1 25.82  1 25.83  1 27.8.83  1 27.8.83  1 27.8.83  1 27.8.83  1 27.8.83  1 27.8.83  1 27.8.83  1 27.8.83   | **************************************   | 9700<br>60*<br>07FTH<br>0F FLOW<br>3.26<br>3.53<br>3.57<br>3.87<br>4.04  | ## DRAIN AN<br>STORM DRAIN<br>0-255 CFS<br>W.S.<br>ELEV<br>1711.78<br>1711.78<br>1712.17<br>1712.46<br>1712.70<br>1714.91  | ALYSIS POS<br>************************************   | MATER HARRCH E CONDIT.  VEL  14.25 13.59 12.35 13.77 9.61  | .00997 EURFACE N-7 IOS STORM VEL .00887 2.16 .00787 2.27 .00534 1.26 .00452 1.26 1.26 1.26   | ## PROFILE LI DRAIN  EMERTY  EMEL 1714.43  1714.67  1714.87  1714.87  1714.87  1714.87  1714.87  1715.40   | SUPER<br>ELEV<br>.90<br>.90<br>.90   | CRITICAL,<br>DEPIH J<br>4.04<br>4.04<br>4.04<br>4.04<br>4.04                               | 2.90<br>2.90<br>2.90<br>2.90                                 | BOT/<br>DIA<br>5.00<br>8.00<br>8.00<br>8.00                                 | BASE/<br>ID NO.<br>-00<br>-00<br>-00<br>-00                      |  | PAGE  MO PIES  G G G G G G G G G G G G G G G G G G   |  |
|                         | ######################################   | **************************************   | 573<br>60*<br>010*<br>07 710*<br>3 . 53<br>3 . 57<br>3 . 57<br>3 . 57<br>3 . 57<br>3 . 57  | RM DRAIN AN<br>STORM DRAIN<br>0-255 CFS<br>W.S.<br>ELEV<br>1711.78<br>1712.17<br>1712.46<br>1712.70<br>1714.01   | ALYSIS FOR CO. 100.0 200 | MATER HARRCH E CONDIT.  VEL.  14.15  13.59  12.35  11.77  9.61  9.01   | .00997 EURFACE N-7 ION STORM VEL .00887 2.161 .00792 2.761 .00792 1.126 .00534 1.26 1.26 2.612 2.62  | ### ##################################   | SUPER<br>SLEY<br>.00<br>.00<br>.00   | CRITICAL. DEPTH 4.04 4.04 4.04 4.04 4.04 3.83  | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.90                 | BOT/<br>D1A<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00                         | BASE/<br>2D BO.<br>-00<br>-00<br>-00<br>-00                      |  | PAGE PIER O O O O O  |  |
|                         | 39.68  37.50.64  1.750.64  24.80  1.750.65  1. | **************************************   | 3.36<br>3.51<br>3.57<br>3.67<br>3.67<br>3.67<br>3.67<br>3.67<br>3.67   | RM GRAIN AND STORM BRAID CP255 CF5 W.S. ELEV 1711.78 1712.17 1712.46 1712.70 1714.01 1714.23 1714.23   | ALYSIS FOR CO. 10 10 10 10 10 10 10 10 10 10 10 10 10  | WATER HARRCH E COMDIT.  YEL,  14.25  13.59  12.95  11.77  9.61  9.01   | .00997 EURFAGE 8:-7 ION STORM WEL 1.16 1.02897 2.161 1.02799 2.17 1.02534 1.16 1.16 1.16 1.16 1.16 1.16 1.16 1.1   | 1980 FILE 11 DEATH ENGINE ENGINE ENGINE 1714.43 1714.65 1714.63 1714.63 1714.63 1714.63 1714.63 1714.63 1714.63 1714.63 1714.63 1714.63 1714.63 1714.63 1716.63  | SUPER SLEY   | CRITICAL DEFINITION A. 04 4.04 4.04 4.04 3.81 3.81   | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.78                 | MAT/<br>22A<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00                         | ######################################                           |  | PAGE PAGE PAGE PAGE PAGE PAGE PAGE PAGE  |  |
|                         | ######################################   | **************************************   | 3.36<br>3.51<br>3.57<br>3.67<br>3.67<br>3.67<br>2.64   | RM DRAIN AM<br>0-25 CP<br>W.S.<br>ELSY<br>1711.78<br>1712.17<br>1712.46<br>1712.70<br>1714.91<br>1714.60   | **************************************   | MATER HARGCH CONDIT.  VEL.  14.25 13.59 12.35 13.77 9.01 9.01 13.69  | .00997 SURVACE N-7 ION STORM VEL 1.16 .00897 2.687 2.697 2.697 2.75 .00534 .00462 1.16 2.68 3.14 3.164 3.164 3.164 3.164 3.164 3.164 3.164 3.164 3.164 3.164 3.164 3.164   | 1714.43<br>1714.43<br>1714.63<br>1714.63<br>1714.63<br>1714.63<br>1714.63<br>1714.63<br>1715.28<br>1715.29<br>1715.30  | SUPER ELECT  | CRITICAL DEPTH 4.04 4.04 4.04 4.04 3.81 3.81 3.83  | 2.99<br>2.99<br>2.99<br>2.90<br>2.90<br>2.78                 | HOT/<br>DIA<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00                 | #ARE/<br>ID WO.<br>  |  | PAGE NO. PIER.   | .00<br>.00<br>.00<br>.00<br>.00              |
|                         | 29.68  27.100  1.7100  1.7100  24.00  24.00  17.00  | **************************************   | 2000 000 000 000 000 000 000 000 000 00  | ## DRAIN AN STORM DRAIN OF THE STORM DRAIN DRA | ALYSIS FOR PORT OF THE PORT OF | MATER HARRCH E CONDIT.  VEL.  14.25 13.59 12.35 11.77 9.01 9.01 15.59 15.39 14.67                                    | .00997 EURFACE N-7 ION STORM TEAD SF AVE 1.00887 2.87 2.87 2.75 2.00534 1.26 1.26 1.26 1.21 2.248 2.146 3.34 2.0098  | ### 12   | SUPER ELEV   | CRITICAL, DEFIN J 4.04 4.04 4.04 4.04 3.81 3.81 3.81                                       | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.78                 | 1077/<br>Dia<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00                | BARR/<br>2D NO.<br>-00<br>-00<br>-00<br>-00<br>-00<br>-00<br>-00 |  | PAGE NO. PIER.   |  |
|                         | ######################################   | **************************************   | 3.36<br>3.53<br>3.53<br>3.67<br>3.67<br>2.67<br>2.84<br>4.04<br>5.27<br>2.06<br>2.79<br>2.84<br>3.95   | ## DRAIN AN STORM DRAIN OF THE STORM DRAIN DRA | ALYSIS POI<br>0  | WATER HARRCH E COMDIT.  VEL.  14.25 13.59 12.95 12.95 13.69 14.67 13.99 14.67  | .00997 EURFACE 8:-7 ION STORM VEL 1.16 .00897 2.161 .00799 2.125 .00462 1.26 .01462 1.268 .01462 .01464 .01 | 1714.43<br>1714.43<br>1714.63<br>1714.63<br>1714.63<br>1714.63<br>1714.63<br>1714.63<br>1715.28<br>1715.29<br>1715.30  | SUPER ELEV   | CRITICAL, DEFIN J 4.04 4.04 4.04 4.04 3.81 3.81 3.81                                       | 2.99<br>2.99<br>2.99<br>2.90<br>2.90<br>2.78                 | 1077/<br>Dia<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00                | BARR/<br>2D NO.<br>-00<br>-00<br>-00<br>-00<br>-00<br>-00<br>-00 |  | PAGE NO.   |  |
|                         | 39.68  21/KLDM  1750.64  1750.64  1750.65  1750.38  1750. | **************************************   | 3.36<br>3.52<br>3.52<br>3.52<br>2.67<br>2.79<br>2.84<br>4.04<br>5.27<br>2.79<br>2.84   | RM GRAIN AN<br>STORM DRAID<br>0-255 CFS<br>W.S.,<br>ELSY<br>1711.78<br>1712.17<br>1712.17<br>1712.46<br>1712.70<br>1714.03<br>1714.13<br>1714.60<br>1716.56<br>1717.01   | ALYSIS FOR ALLYSIS FOR ALLYS | MATER HARECH E CONDIT.  VEL,  14.25 13.59 12.35 11.77 9.01 9.01 15.69 15.39 14.67 13.99 HATER HARECH                 | .00997 BURFACE N-7 COM NT COMM READ SF AVE   | ## ## ## ## ## ## ## ## ## ## ## ## ##   | SUPER ELEV   | CRITICAL, DEFIN J 4.04 4.04 4.04 4.04 3.81 3.81 3.81                                       | 2.99<br>2.99<br>2.99<br>2.90<br>2.90<br>2.78                 | 1077/<br>Dia<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00                | BARR/<br>2D NO.<br>-00<br>-00<br>-00<br>-00<br>-00<br>-00<br>-00 |  | PAGE NO.   |  |
|                         | ######################################   | **************************************   | 2. 84<br>2. 79<br>2. 84<br>2. 85<br>2. 87<br>2. 84<br>2. 88<br>2. 89<br>2. 89  | ## DRAIN AM<br>## DRAIN DRAIN<br>## DRAIN<br>1711.78<br>1711.78<br>1711.17<br>1712.46<br>1712.46<br>1714.01<br>1714.01<br>1714.01<br>1714.01<br>1714.01<br>1714.00<br>1716.56<br>1717.51<br>## DRAIN AM<br>#* BYORN DRAIN<br>## BYORN DRAIN<br>## BYORN DRAIN<br>## BYORN DRAIN<br>## BYORN DRAIN  | ALYSIS FOR ALLYSIS FOR ALLYS | MATER HARECH E CONDIT.  VEL,  14.25 13.59 12.35 11.77 9.01 9.01 15.69 15.39 14.67 13.99 HATER HARECH                 | .00997 SURFACE N-7 108 STORM VEL .00887 2.161 .00792 2.70792 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839 2.717 .00839   | ## ###################################   | SUPER ELEV   | CRITICAL, DEFIN J 4.04 4.04 4.04 4.04 3.81 3.81 3.81 3.81 3.82                             | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.78<br>2.78         | ######################################                                      | **************************************                           |  | PAGE PAGE PAGE   | AVEFR  |
|                         | 39.68  STATION  1./ELEM  1.750.64  1.750.64  1.750.63  1.740.55  1 | **************************************   | 500<br>500<br>500<br>500<br>500<br>500<br>500<br>500   | RM DRAIN AN STORM DRAIN OF 255 CFS W.S. ELEV 1711.78 1711.79 1712.46 1712.70 1714.60 1714.60 1716.56 1716.56 1716.56 1716.56 1716.56 1716.56 1717.51 RM DRAIN AN STORM DRAIN AND | ALYSIS FOR PUTTERS OF THE PUTTERS OF | MATER HARECH E CONDIT.  VEL.  14.15  13.19  12.95  12.35  11.77  9.01  13.69  14.67  13.99  MATER HARECH E CONDIT    | .00997 EURFACE N-7 IOS STORM VEL .00887 .00887 .261 .00792 .27 .00534 .126 .283 .248 .2146 | ## PROFILE 1.1  PRAIN  EMERGY  TREE NI.  1714.43  1714.65  1714.83  1714.83  1715.40  1715.61  1715.63  1715.64  1715.63  1715.64  1715.63  PROFILE 1.1  PROFILE 1.1  EMERGY  GROUND  HE   | SUPER ELEV   | CRITICAL<br>DEFINE<br>4.04<br>4.04<br>4.04<br>4.04<br>4.04<br>3.81<br>3.81<br>3.81<br>3.81 | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.78<br>2.78 | 1077/<br>101A<br>100<br>100<br>100<br>100<br>100<br>100<br>100<br>100<br>10 | **************************************                           | * Office of the control of the contr | PAGE NO D D D D PAGE NO PIER   | AVEFR  |
|                         | ######################################   | \$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\  | 200<br>000<br>000<br>000<br>1.00<br>1.00<br>1.00<br>2.00<br>2.00   | RM GRAIN AN<br>STORM DRAIN<br>0-255 CPS<br>N.S.<br>2LSY<br>1711.78<br>1712.17<br>1712.46<br>1712.70<br>1714.81<br>1714.87<br>1714.60<br>1714.50<br>1714.50<br>1714.50<br>1715.56   | ALYSIS FOR ALLYSIS FOR ALL | WATER HARRCH E COMDIT.  VEL.  14.25 13.59 12.35 13.77 9.01 15.69 15.18 14.67 13.89 HARRCH HARRCH E COMDIT.           | .00997 SURVACE N-7 ION STORM VEL 18AD SF AVE 1.16 .00487 2.61 .00709 1.37 .00462 1.126 .01248 2.68 3.14 .010898 SURFACE N-7 ION STORM VEL MEAD SF AVE  | PROFILE 1:1  DRAIN  DRAIN  DRAIN  DRAIN  DRAIN  DRAIN  DRAIN  DRAIN  DRAIN  ENERGY  GRD.EL.  1714.83  1714.83  1714.83  1714.83  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28   | SUPER ELEV   | CRITICAL<br>DEFINE<br>4.04<br>4.04<br>4.04<br>3.81<br>3.81<br>3.81<br>3.81<br>3.81         | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.78<br>2.78 | #WTT/<br>DIA<br>\$.00<br>\$.00<br>\$.00<br>\$.00<br>\$.00<br>\$.00          | **************************************                           |  | PAGE PIER COCCUPIER PAGE PAGE  | AVEFE  |
|                         | 39.68  STATION  1./ELEM  24.80  1.725.44  1.725.44  1.725.43  1.749.38  1.749.38  1.749.38  1.759.43  1.75 | **************************************   | 27 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | RM DRAIN AN STORM DRAIN OF 255 CFS W.S. ELEV 1711.78 1711.79 1712.46 1712.70 1714.60 1714.60 1716.56 1716.56 1716.56 1716.56 1717.51 RM DRAIN AN STURM DRAIN AND STURM DR | ALYSIS FOR 177.0 1 | MATER HARRCH E CONDIT.  VEL.  14.15  13.19  12.35  11.77  9.01  15.69  15.39  14.67  13.99  WATER HARRCH E CONDIT    | .00997 EURFACE N-7 ION STORM VEL .00487 .00487 .261 .00792 .270 .20534 .212 .20534 .2124 . | ## PROFILE 1.1  PRAIN  | SUPER  | CRITICAL<br>DEPTH<br>4.04<br>4.04<br>4.04<br>4.04<br>3.81<br>3.81<br>3.81<br>3.81<br>3.81  | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.78<br>2.78 | 1077/<br>101A<br>1000<br>1000<br>1000<br>1000<br>1000<br>1000<br>100        | #AARE/<br>2D #O  | \$   | PAGE NO PIER PAGE NO PIER NO P | AVEFE  |
|                         | 39.68  37.68  1.71.00 | **************************************   | 573<br>60°<br>010°<br>07 7100°<br>3.36<br>3.51<br>3.57<br>3.87<br>3.98<br>2.79<br>2.88<br>3.97<br>2.88<br>3.97   | RM DRAIN AN<br>STORM DRAIN<br>0-255 CFS<br>W.S.<br>ELEV<br>1711.78<br>1712.17<br>1712.46<br>1712.70<br>1714.01<br>1714.01<br>1714.01<br>1714.01<br>1714.55<br>1717.51<br>RM DRAIN AN<br>BYORM DRAIN<br>18.55 ELEV<br>1718.11   | ALYSIS FOR ALLYSIS FOR ALLYS | WATER 8 HARSCH CONDIT.  VEL.  14.25  13.59  12.95  12.35  11.77  9.01  13.69  14.67  13.99  WATER HARSCH CONDIT VEL. | .00997 EURFACE 8:-7 IOH ETORM VEL .00897 .00897 .37 .00834 .37 .00834 .3124 .3134 .3 | PROFILE 1.1  DEATH  EMERGY  GREAT  1714.43  .22  1714.85  1714.83  1715.33  PROFILE 1.1  | SUPER ELEV   | CRITICAL DEPTH 4.04 4.04 4.04 4.04 3.81 3.81 3.81 3.81 3.81 3.81 3.81 3.81                 | 2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.78<br>2.78<br>2.78 | ######################################                                      | **************************************                           | \$ 1. 4. *05050505050505050505050505050505050505   | PAGE NO D D D D D D D D D D D D D D D D D D D  | AVEFR .00 .00 .00 .00 .00 .00 .00 .00 .00 .0 |
|                         | 39.68  OTATION  1/500.64  124.80  124.80  15.38  15.38  1752.06  1 | **************************************   | 2000<br>0000<br>0000<br>0000<br>3.36<br>3.53<br>3.53<br>3.53<br>3.53<br>2.67<br>2.79<br>2.84<br>3.05<br>2.79<br>2.84<br>3.05<br>2.79<br>2.84<br>3.05<br>3.37 | RM GRAIN AN<br>STORM DRAIN<br>6-255 CFS<br>W.S.<br>1711.78<br>1712.17<br>1712.17<br>1712.17<br>1714.01<br>1714.01<br>1714.01<br>1714.60<br>1716.55<br>1717.51<br>RM DRAIN AN<br>STORM DRAIN<br>M.S.<br>ELEV<br>1718.11<br>1718.55  | ALYSIS FOR 177.0 1 | WATER HARRCH E CONDIT.  VEL.  14.25  13.59  12.95  12.95  13.59  14.67  13.99  WATER HARRCH E CONDIT.  VEL.  13.14   | .00997 SURFACE N-7 ION STORM VEL 1.16 .00897 .00792 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834 .1.26 .00834   | ## PROFILE 1.1    DRAIN     DRAIN     DRAIN     1714.43     1714.65     1714.67     1714.67     1714.67     1714.67     1715.77     1715.70     1715.70     1715.70     1717.71     1717.7   | SUPER ELEV   | CRITICAL DEFINE 4.04 4.04 4.04 4.04 3.81 3.81 3.81 3.81 3.81 3.81 3.81 3.81                | 2.90<br>2.90<br>2.90<br>2.90<br>2.78<br>2.78<br>2.78<br>2.78 | ######################################                                      | **************************************                           | \$ 1. 14. * 0000 00 00 00 00 00 00 00 00 00 00 00  | PAGE PIER PIER PIER PIER PIER PIER   | AVEFE  |
|                         | ######################################   | **************************************   | 573<br>60°<br>010°<br>07 7100°<br>3.36<br>3.51<br>3.57<br>3.87<br>3.98<br>2.79<br>2.88<br>3.97<br>2.88<br>3.97   | RM DRAIN AN<br>STORM DRAIN<br>0-255 CFS<br>W.S.<br>ELEV<br>1711.78<br>1712.17<br>1712.46<br>1712.70<br>1714.01<br>1714.01<br>1714.01<br>1714.01<br>1714.55<br>1717.51<br>RM DRAIN AN<br>BYORM DRAIN<br>18.55 ELEV<br>1718.11   | ALYSIS FOR ALLYSIS FOR ALLYS | WATER 8 HARSCH CONDIT.  VEL.  14.25  13.59  12.95  12.35  11.77  9.01  13.69  14.67  13.99  WATER HARSCH CONDIT VEL. | .00997 BURFACE 88-7 IOM ST CAM SE AVE  | PROFILE 1:  DRAIN  DRAIN  DRAIN  1714.43  1714.63  1714.63  1714.63  1714.63  1714.63  1714.63  1714.63  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28  1715.28   | SUPER ELEV   | CRITICAL DEPTH 4.04 4.04 4.04 4.04 3.81 3.81 3.81 3.81 3.81 3.81 3.81 3.81                 | 2.90 2.90 2.90 2.90 2.78 2.78 2.78 2.78 2.78 2.78            | ######################################                                      | ######################################                           |  | PAGE PAGE PAGE PAGE PAGE   | AVEFR .00 .00 .00 .00 .00 .00 .00 .00 .00 .0 |

Page 3

|          |   |   |  |   |   |   |   | v-172.Cut  |  |   |  |  |   |   |   |  |
|----------|---|---|--|---|---|---|---|--|--|---|--|--|---|---|---|--|
|          | OJAMCT STR  | .00998  | 5.41   | 1721.28   | 130.0   | 6.62  | .0019J<br>.88   | .02<br>1721.2)   | , 29   | 3.24  |  | 5.00   | .00   | .00   | 0   | . 0.5  |
| 4        | 0 118.92<br>0 2401.76   | .00849<br>1716.58   | 5.00   | 1721.58   | 130.0   | 6.41  | .00148  | .29<br>1722.26   | .00  | 3.26  | 2.62   | 5.00   | .00   | .00   | 0   | .00  |
|          | 0 64.01<br>0 2465.78  | .00049<br>1717.12   | 4.34   | 1721.46   | 130.6   | 4,94  | .00112  | .15<br>1722.41   | .00  | 1.26  | 2,52   | 5.00   | .00   | .00   | ٥   | .00  |
|          | 0 28.51<br>0 2494.29  | .00849  | 4.29   | 1731.66   | 130.0   | 7.25  | .00225<br>.82   | .06<br>1723.47   | .00  | 1.76  | 2,63   | 9.00   | .00   | .00   | Ü   | .00  |
|          | CHYGRAULIC<br>0 2494.29   | JUMP<br>1717.36   | 2.44   | 1719.80   | 130.0   | 13.68   | 2.91  | 1722.71  | .00  | 3.36  |  | 5.00   | .00   | .00   | 0   | , GS   |
|          | 0 17.96<br>0 2513.25  | .00849  |  | 1719.74   | 130.0   | 13.75   | .01094<br>2.94  | .20  | .00  | 3.26  | 2,62   | 5.05   | .00   | .00   | ů.  | .00  |
|          | 0 62.67   | .00849  | 2,43   | *   | *3M * M   | *3 * 1 #  | .01177  | ******   | * 24.94  | ஃ <b></b>   | 2.62   | क्षे ७ वेट श   | 4 197 99  | .00   |   |  |
|          | 1   |   |  |   |   |   |   | PROFILE LI   | STING  |   |  |  |   |   | PAGE  | 5  |
| •        |   |   | 6g*  | em crain an<br>Etcan drat<br>G-155 CVS  |   |   |   | DRAIN  |  |   |  |  |   |   |   |  |
|          | O STATION   | inver.  | CEPTI<br>OF YEAR   | W.S.  | Ç   | YEL   | vel<br>Dead   | ENERGY<br>CRO.EL   | Super<br>Elev  | CRITICAL<br>CEPTH   |  | HUT/<br>DIA  | BASE/<br>ID NO.                                     | ****  | no<br>Pier                                    | aver   |
| ì        | 0 L/ELEM  | 80  |  | EL.EV   |   |   | SY AVE  | HF   | Strapito F   | 2   | KAN DEPTH  |  | sia amas  | 主義  | F + 3/3%                                      |  |
|          | 0 2074.92   | 1718.05   | **************************************   | **********<br>2720.39   | 130,0   | 34.43   | *********<br>3.73   | *********<br>1733,62   | ,00  | *********<br>3.26   | ******   | ******<br>\$.00  | ********<br>,00                                     | *****<br>88.                                  | ·****   | .00  |
|          | 0 48.85   | .00949<br>1718.46   | 3.36   | 1720.72   | 130.0   | 10,12   | .01338<br>3.55  | .65<br>1714.17   | .00  | 3.26  | 2.62   | 5.00   | .00   | .00   | ō   | .00  |
|          | 0 40.75<br>0 2664.51  | .00849  |  |   |   |   | .01522  | , 42   | ,00  |   | 7.62   |  |   | -00   |   |  |
|          | 0 35.53   | 1718.81   | 1.17   | 1720.90   | 130.0   | 25.86   | 3.91  | 1714.89  |  | 3.26  | 2.6%   | 5.00   | .00   | .00   | \$  | .00  |
|          | 0 2700.05   | 1719.11   | 2.10   | 3773.72   | 130.0   | 16.64   | 4.30<br>.01973  | 1715.51<br>.6)   | .00  | 3.34  | 2.42   | \$ . 05  | ,00   | .09   | ٥   | .00  |
|          | 0 1731.78<br>0 5.00   | 1719.30<br>.02000   | 2.02   | 1721,40   | 135.0   | 17,45   | 4.73  | 1726.13  | .00  | 3.26  | 2.65   | 5.00   | -09   | .00   | Ģ   | .00  |
| ĺ        | 0 2716.78   | 1719.48<br>.03200   | 2.02   | 1731.50   | 130,0   | 17.46   | 4.74  | 1736,34  | .00  | 3,36  | 1.79   | 5.00   | .00   | .00   | ø   | .00  |
| 1        | 0 2763.34   | 1720.32   | 2.09   | 1722.41   | 130.0   | 16,71   | 4.34  | 1726.74  | .00  | 3.24  |  | 3.60   | .88   | .00   | 0   | .00  |
| <b>*</b> | 0 20.78<br>0 2783.02  | .01180<br>1721.00   | 2.37   | 1721.16   | 130.0   | 18.93   | .01753<br>3.94  | .36<br>1727.11   | ,00  | 3.26  | 1.78   | 5.00   | .00   | .00   | 0   | ,00  |
|          | 0 15.96<br>0 2798.98  | .01200  | 2.25   | 1723-77   | 130.0   | 15.19   | .01540<br>3.58  | .25<br>1737.38   | .00  | 3,26  | 1.79   | 5.00   | ,00   | .00   | Q   | .00  |
|          | GJUNCT STR<br>G 2803.98   | .03201<br>1721.68   | 1,98   | 1723-44   | 120.0   | 16.63   | .01498<br>4.20  | .09<br>1727.96   | .00  | 3.23  |  | 5.00   | .00   | .00   | Q   | . 00   |
|          | 0 8.78<br>0 2813.76   | .03201  | 2.00   |   | 129.0   |   | .01909  | .37  |  | 2.13  | 3.72   | 5.00   | .00   | .00   |   | .00  |
| ŝ        | 8 13.96   | 1721.97<br>.03201   | * 1,44.2   | 1711.97   | 李林湖。到   | 14.34   | 4.15<br>.01749  | 1738.12  | , 60   | 2123  | 1.72   | .D = V V   | 9 W W   | .00   | 0   |  |
| ĝ.       | *   |   |  |   |   | Warren  | Elmora, me  | PROFILE LI   | 871160   |   |  |  |   |   | FACE  | 45   |
|          | *   |   | When   |   |   |   |   |  | and the second   |   |  |  |   |   |   |  |
|          | - q   |   | 65*  | em death ax<br>Stoem deat   |   | HARRON  | 制 ~ "Y  |  | W. A. II. y  |   |  |  |   |   |   |  |
|          | o station   | inver;  | 65*  |   |   | HARRON  | 制 ~ "Y  |  | Siper  | CRITICAL  |  | mat/   | rase/   | in q<br>indir                                 | WO  | AVEPE  |
|          |   | elev  | 65*<br>Q19   | STORM DEAT<br>0-155 CFS   | n - Putini  | HARRON<br>COMDIT  | N-7<br>TON STORM<br>VEL<br>NEAD   | DMAIN<br>EBERGY<br>CAD.EL.   |  | DEPTH   | ern tert   | DIA  | BASE/<br>ID MO.                                     |   | NO<br>FIRR                                    | Avere  |
|          | 0 1/ELEM  | ELEV<br>50  | 65°<br>OLO<br>DEFTN<br>OF FLCW   | 2:027 DAA:<br>0-135 C75<br>4.3.<br>11.27  | 0<br>   | HARDON<br>COMDIT<br>VEL   | N-7<br>100 27033<br>VEL<br>25AD<br>57 AYE   | DNAIN<br>EMERGY<br>GRO.EL.<br>HF   | S:/PER<br>E1.ZV  | UKP78   | ************   | DIA<br> <br> ******  | 123 MO.   | ZZ<br>*****                                   | F122  | ***  |
|          | 0 1/ELEM<br>**********<br>8 20)1.63<br>0 15.29  | #1.EV<br>50<br>********<br>1722.62<br>.01281  | 65*<br>CID<br>DEPTH<br>CF FLC*   | 5:08/ 18A:<br>0-71: CFS<br>W.S.<br>ELEY   | e polices   | KARJON<br>COMUIT<br>VEL   | N-7<br>10M STORM<br>VEL<br>HEAD<br>SF AVE   | EMAIN<br>EMERGY<br>GRO.EL.<br>MF   | SIJPER<br>ELZV<br>******                               | DEPTH 1   |  | DIA  | m m.  | ZR.   | FIRA  |  |
|          | 0 1./21.24<br>***********<br>0 10.29<br>0 15.39   | 1327<br>1327<br>1327<br>1327<br>1327<br>1327  | 65°<br>OLO<br>DEFTN<br>OF FLCW   | 2:027 DAA:<br>0-135 C75<br>4.3.<br>11.27  | 0<br>   | HARDON<br>COMDIT<br>VEL   | **************************************  | EMERGY<br>GAD.EL.<br>MF<br>1728.47<br>1728.47<br>1718.78   | S:/PER<br>E1.ZV  | UKP78   | **************************************                       | DIA<br> <br> ******  | 123 MO.   | ##<br>****<br>20.<br>20.                      | F122  | ***  |
|          | 0 1./81.8M<br>************<br>0 18.39<br>0 18.39<br>0 2847.90<br>0 2809.91                              | 22.27<br>20<br>27.22.22<br>27.22.22<br>27.22.22   | SS*<br>Q10:<br>DEFTA<br>CF FLC*  | FICEN DAAI<br>9-145 CYS<br>4-3-<br>ELEY<br>**********************************   | 0<br>   | YEL   | VEL<br>HEAD<br>SF AVE<br>************************************   | ######################################   | SIJPER<br>ELZV<br>******                               | ********  | **************************************                       | DIA<br>!<br>!******<br>S-00                                  | 10 MO.  | *****<br>.00<br>.00<br>.00                    | FIER<br>*****                                 | ****   |
|          | 0 1./ELEM<br>   |   | 50+<br>019<br>DEFTH<br>OF FLOW<br>1.07   | #: #: #: #: #: #: #: #: #: #: #: #: #: #  | 9 . YUTURI<br>Q<br>   | VEL   | VEL HEAD STORM 3.77 .01315 .3.43 .01349 .3.22 .01185  | 204428<br>2042924<br>20224<br>2024<br>2024<br>2024<br>2024<br>2024   | 217ER<br>ELZV  | 1.11  | **************************************                       | DIA<br>!<br>   | #######<br>#############################            | *****<br>.000<br>.000<br>.000<br>.000         | *****<br>*****                                | ****<br>.89<br>.89   |
|          | 0 1./ELEM<br>************************************   | 1722 62<br>1722 62<br>1722 62<br>1722 62<br>1722 62<br>1722 62<br>1722 62<br>1723 62<br>1724 62 | 50*<br>019:<br>02:FIN<br>02:FLOW<br>1.07:<br>1.15:   | FIGH 1841<br>9-155 CPS<br>W.S.<br>FLEY<br>1724.65<br>1725.75  | 9 ************************************  | VEL   | 18-7<br>100 ETCH<br>VEL<br>HEAL<br>S. P.  | DHAIH  EMERGY ORD. SL.  UF ******** 1728.43 1728.30 1728.32 1728.32 1728.30 1728.30  | #127<br>#127<br>.00                                    | DAPTH 1   |  | DIA<br>!<br>!******<br>5.00<br>8.00                          | 30 MQ.  | ***************                               | *****<br>0<br>0                               | ****<br>.00<br>.00   |
|          | 0 1/818M<br>1812 39<br>0 18 29<br>0 2047 91<br>0 12 00<br>0 2089 81<br>0 2089 81<br>0 2089 81<br>0 7 61 |   | 50* 010<br>DEPTA<br>OF FLOW<br>1.07<br>1.15<br>2.23<br>2.31  | 2708M ISBAT<br>8-135 CPS<br>M.S.<br>ELEV<br>1724.69<br>1725.27<br>1725.75   | % YUTURE Q  | YEL  *******  13.30  14.36  14.36   | ##-7 100 ETCHM  VEL.  HEAD BY AVE  ******* 3,77 0,134 3,43 0,143 0,143 0,143 1,143 0,143 1,143 0,143 1,143  | SMAIN<br>SMERGY<br>GRO.EL.<br>MF<br>***********************************  | 2172X<br>21.2V<br>************************************ | 3.33<br>3.33<br>3.33<br>3.33                                      | **************************************                       | DIA<br>1<br>5.00<br>5.00<br>5.00                             | 33 MQ.  | *****<br>.000<br>.000<br>.000<br>.000<br>.000 | *****   | ****<br>. 29<br>. 29<br>. 20                                       |
|          | 0 1./81.88 **********************************   | #129<br>************************************  | 50*<br>DEPTH<br>OF FLOW<br>************************************  | 2708M DRAI<br>9-355 CPS<br>W.S.<br>1724.69<br>1729.75<br>1725.75<br>1726.48<br>1726.48<br>1726.48                                 | 2   |   | ##-7 ***********************************  | ######################################   | SUPER<br>ELEV - 00<br>.00<br>.00                       | 0.23<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13                      |  | 5.00<br>5.00<br>5.00<br>5.00<br>5.00                         | **************************************              | ***   | **************************************        | .00  |
|          | 0 1./2  | #127<br>************************************  | 60*<br>DEFTH<br>OF FLOW<br>***********<br>2.07<br>2.15<br>2.23<br>2.21<br>2.40<br>2.40   | 2708M DBA1<br>8-35 CPS<br>4-8-<br>1724-69<br>1725-75<br>1725-75<br>1726-14<br>1726-88<br>1726-73                                  | 2<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0                       | HARRON   CORDIT   VEL   13.58   14.36   13.50   12.28   12.28   12.71   | : N-7 : ON ETCHE  VEL.  HEAD  SF AVE  ********  3.25 3.449 3.22 0.1283 0.1283 0.1283 0.1283 0.1283 0.1283 0.1283  | THATH  EMERGY GRO.EL.  HF  ********* 172.5.5.1  172.6.6.1  172.6.6.1  172.6.6.1  172.6.6.1  172.6.6.1  | SIPER<br>ELEV<br>.00<br>.00<br>.00                     | DEFER 1   | 1.72<br>1.72<br>1.72<br>1.72                                 | 51A<br>5.60<br>8.00<br>8.00<br>8.00<br>8.00                  | .00<br>.00<br>.00<br>.00<br>.00                     | # * * * * * * * * * * * * * * * * * * *       | 7288<br>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | .00  |
|          | 1/21-22-23-23-23-23-23-23-23-23-23-23-23-23-  | #127<br>************************************  | 50*<br>DAFFI<br>OF FLOW<br>2.07<br>2.15<br>2.23<br>2.31<br>2.40<br>2.40<br>2.59  | 2709M DRAI<br>9-35 CPS<br>W.S.<br>ELRY<br>1724.65<br>1725.75<br>1726.44<br>1726.40<br>1727.02<br>1727.02                          | 130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0                   | HARSCH<br>  CORDIT<br>  VEL<br>  13.38<br>  14.16<br>  12.30<br>  12.30<br>  12.30<br>  12.30<br>  12.30  | # # * * * * * * * * * * * * * * * * * *   | THATH  ENERGY  ORD. EL.  1728 2738  1728 3738  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  1728 68  | SIPER ELEV   | DRVIN 3.33 3.13 3.13 3.13 3.13 3.13 3.13 3.1                      | 2.72<br>2.72<br>2.72<br>2.72<br>2.72<br>2.72                 | 51A<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00          | 30 M3.  .82 .83 .83 .00 .00 .00                     |   | 712A<br>0<br>0<br>0<br>0                      | **** .09 .00 .00 .00 .00 .00 .00 .00                               |
|          | 1/21-22-23-23-23-23-23-23-23-23-23-23-23-23-  | #127<br>##***********************************   | 60*<br>DEFTH<br>OF FLOW<br>***********<br>2.07<br>2.15<br>2.23<br>2.21<br>2.40<br>2.40   | 2709M 18842<br>8-35 CPS<br>W.S.<br>1724.69<br>1725.27<br>1725.75<br>1726.34<br>1726.48<br>1726.77<br>1727.02<br>1727.24           | 2<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0                       | HARRON   CORDIT   VEL   13.58   14.36   13.50   12.28   12.28   12.71   | : #-7 *********** ******* ****** ****** *****   | THATH  EMERGY GRO.EL.  HF  ********* 172.5.5.1  172.6.6.1  172.6.6.1  172.6.6.1  172.6.6.1  172.6.6.1  | ######################################                 | DEFER 1   | 2.72<br>2.72<br>2.72<br>2.72<br>2.72<br>2.72                 | 51A<br>5.60<br>8.00<br>8.00<br>8.00<br>8.00                  | .00<br>.00<br>.00<br>.00<br>.00                     |   | **************************************        | .00  |
|          | 0 1.7 ** 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  | #1.27<br>************************************   | 50*<br>DAFFI<br>OF FLOW<br>2.07<br>2.15<br>2.23<br>2.31<br>2.40<br>2.40<br>2.59  | 2709M DRAI<br>9-35 CPS<br>W.S.<br>ELRY<br>1724.65<br>1725.75<br>1726.44<br>1726.40<br>1727.02<br>1727.02                          | 130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0                   | HARSCH<br>  CORDIT<br>  VEL<br>  13.38<br>  14.16<br>  12.30<br>  12.30<br>  12.30<br>  12.30<br>  12.30  | : H-7 ************ ********* ******* *******  | ### ### ### ### ### ### ### ### ### ##   | SIPER ELEV   | DRVIN 3.33 3.13 3.13 3.13 3.13 3.13 3.13 3.1                      | 1.72<br>1.72<br>1.72<br>2.72<br>2.72<br>2.72<br>2.72         | 51A<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00          | .00 .00 .00 .00 .00 .00 .00 .00 .00                 |   | 7 2 X A                                       | **** .09 .00 .00 .00 .00 .00 .00 .00                               |
|          | 0 ** 2910017830480777830480777783088088888888888888   | ######################################  | 50* DAPTA DA | 2709M 18842<br>8-35 CPS<br>W.S.<br>1724.69<br>1725.27<br>1725.75<br>1726.34<br>1726.48<br>1726.77<br>1727.02<br>1727.24           | 130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>120.0<br>120.0                   | HARPCH   CORDIT   VEL   13.38   14.86   13.38   12.28   11.71   11.16   10.64   | : # - 7   | THATH  EMMANNY  ORDER  THAT  T | ######################################                 | 0.23<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1 | 1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72 | 31A<br>3.00<br>3.00<br>3.00<br>3.00<br>3.00<br>3.00          | .00<br>.00<br>.00<br>.00<br>.00<br>.00              |   |   | .00<br>.00<br>.00<br>.00<br>.00<br>.00                             |
|          | 0 *** *** *** *** *** *** *** *** *** *   | ######################################  | 50* DAPTA DA | 2709M ISBAT 9-38 CPS 1738.69 1728.27 1728.75 1726.44 1726.48 1726.77 1727.42 1727.43  | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | MARRON<br>CONTIT<br>VEL<br>14.35<br>14.35<br>14.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35<br>12.35 | : # - 7   | **************************************   | ######################################                 | 1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13      | 1.72<br>1.72<br>1.72<br>2.72<br>2.72<br>2.72<br>2.72         | 5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00         | .00<br>.00<br>.00<br>.00<br>.00<br>.00              |   |   | .23<br>.80<br>.80<br>.80<br>.80<br>.80<br>.80                      |
|          | 0 *** ** ** ** ** ** ** ** ** ** ** ** *  | ######################################  | 50* DASTA  | 2708M IMAE<br>8-35 CPS<br>W.S.<br>1724.69<br>1725.27<br>1725.75<br>1726.14<br>1725.48<br>1726.27<br>1727.02<br>1727.24<br>1727.02 | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | HARSCH<br>CORNIT<br>VEL<br>14.35<br>14.36<br>12.38<br>12.38<br>12.71<br>11.16<br>10.64<br>10.64<br>10.71<br>11.46<br>10.71  | ## 7 **********************************   | ######################################   | ######################################                 | 1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13      | 1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72 | 5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00         | .00<br>.00<br>.00<br>.00<br>.00<br>.00              |   | 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2       | .as<br>.as<br>.as<br>.as<br>.as<br>.as<br>.as                      |
|          | 0 *** *** *** *** *** *** *** *** *** *   | ######################################  | 60* DRFTM OF FLOW  2.07 2.15 2.23 2.31 2.40 2.59 2.59 2.59 2.69 2.69 2.69 2.69   | TOOM DRAY 0-355 CPS 18.8. 1724.65 1725.75 1725.75 1726.44 1726.46 1727.74 1727.74 1727.74   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | HARSCH<br>CONDIT<br>VEL<br>13.38<br>14.86<br>14.36<br>12.38<br>12.78<br>11.71<br>11.46<br>10.64<br>10.64<br>10.71<br>HARSCH<br>CONDIT   | ### 7 104 STURM  ********  \$\$ \$\text{AVE}\$  *******  \$\$ \$\text{AVE}\$  *******  \$\$ \$\text{AVE}\$  *******  \$\$ \$\text{AVE}\$  *******  \$\$ \$\text{AVE}\$  \$\$\text{AVE}\$  \$\$\text{AVE}\$  \$\$ \$\text{AVE}\$  \$\$\text{AVE}\$ | ######################################   | SIPER ELEV   | DRYTH 3.33 3.13 3.13 3.13 3.13 3.13 3.13 3.1                      | 1.72<br>1.72<br>1.72<br>2.72<br>2.72<br>2.72<br>2.72<br>2.72 | 3. 00  | .00<br>.00<br>.00<br>.00<br>.00<br>.00              |   | PERRORS OF STREET                             |  |
|          | 0 *** ** ** ** ** ** ** ** ** ** ** ** *  | ######################################  | 50* DIDING TO  | TTORM ISBAT  STATE CPS  W.S.  1728.69  1728.79  1728.48  1728.48  1728.48  1727.49  1727.74  2727.74  2727.74                     | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | HARSCH<br>CORNIT<br>VEL<br>14.35<br>14.36<br>12.38<br>12.38<br>12.71<br>11.16<br>10.64<br>10.64<br>10.71<br>11.46<br>10.71  | ## 7 **********************************   | ######################################   | SIPER ELEV   | 1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13<br>1.13      | 1.72<br>1.72<br>1.72<br>2.72<br>2.72<br>2.72<br>2.72<br>2.72 | 5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00         | .00<br>.00<br>.00<br>.00<br>.00<br>.00              |   | PERR CO   | .00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00 |
|          | 0 *** *** *** *** *** *** *** *** *** *   | ######################################  | 50* DAPTA DAPTA 1.07 1.15 1.23 2.31 2.40 2.49 2.59 2.69 2.79 2.09 3.01   | # 200 CPS   | 130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0 | HARRON CONTIT VEL  13.38 14.36 13.50 13.50 12.71 11.16 10.64 10.71 WATER HARRON VEL   | ##-7 *******  *******  ******  ******  *****  | THATH  ENERGY GROUND, FL.  17 19.70 17 28.86 17 28.66 17 28.06 17  | SUPER LEV  .00 .00 .00 .00 .00 .00 .00 .00 .00 .       | DEFIN 1 1   | 1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72 | 5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00 | 3D MO00 .00 .00 .00 .00 .00 .00 .00 .00             | *** *** *** *** *** *** *** *** *** **        | PIER O O O O O O O O O O O O O O O O O O O    | .00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00<br>.00 |
|          | 0 1.  | ######################################  | 50* DIDING CONTROL OF FLORE CONTROL OT FLORE CONTROL OF F | TOOM DEAT 9-36 CPS 1738.69 1728.75 1728.75 1726.74 1726.74 1727.40 1727.40 1727.74 1727.83  | 130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0<br>130.0 | HARRON CONTIT VEL  13.38 14.36 13.50 13.50 12.71 11.16 10.64 10.71 WATER HARRON VEL   | ## 7 **********************************   | ######################################   | SUPER ELEV   | DRVM 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2                        | 1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72<br>1.72 | 5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00<br>5.00 | 3D MD.  .82 .80 .80 .80 .80 .80 .80 .80 .80 .80 .80 | *** *** *** *** *** *** *** *** *** **        | PERR C C C C C C C C C C C C C C C C C C      | .29<br>.50<br>.50<br>.50<br>.50<br>.50<br>.50<br>.7                |



13 or 16



14 . 16

Please refer to Volume II for Appendix E and Appendix F.

Appendix E: Grading Plans

# Appendix F: Electronic CD